

Paleo Overpressure in the Delaware Basin Determined From DST, Resistivity Logs and Mud Logs

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- Introduction
- Methods used to define overpressure
 - DST, Mudlogs, Resistivity Logs
- Delaware Basin overpressure cell as currently defined
 - where did we have to 'mud up' to drill thru overpressure?
- Overpressure seen on resistivity logs does not match that
- Compare DST data to Resistivity data to Mud Weight data
 - DST derived PG psi/ft, MW derived PG psi/ft, Resistivity N/Resistivity OP derived PG psi/ft
- Conclusions -- OverPressure has been depleted in Western Delaware Basin due to Laramide uplift and erosion







- Seismic velocity increase in overpressure
- **DST/RFT** Drill Stem Test/Repeat Formation Test
- Mud Weights Increase in Mud Weight
- Casing Seat In previously drilled area
- Resistivity Logs Drop in Resistivity
- Sonic Logs Increase in Sonic Velocity
- **ISIP** Initial Shut In Pressure
- **DFIT** Diagnostic Fracture Injection Test
- **BHP** Bottom Hole Pressure Test (producing well)

Methods to Determine Overpressure





Methods to Determine Overpressure Used in This Study

• Seismic

• Drill stem tests RFT

•Mud weights

• Casing Seat

•Resistivity logs

- Sonic Logs
- ISIP
- DFIT



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<u>"Normal Formation Pressure"</u> <u>is slightly higher in the</u> <u>Permian Basin – NOT .45 psi/ft</u>

Salinity	Salinity	Rw B&K	COND	Rw ERC	COND	Rw DK	COND
kppm	Wt%	@75F	@75F	@75F	@75F	@75F	@75F
		ohm-m	Sín	ohm-m	Sim	ohm-m	S/m
0.0	0.0		0.00		0.00	80.739	0.01
10.0	1.0	0.564	1.77	0.575	1.74	0.599	1.67
25.0	2.5	0.242	4.12	0.257	3.89	0.247	4.04
50.0	5.0	0.131	7.63	0.140	7.17	0.130	7.71
75.0	7.5	0.093	10.76	0.098	10.24	0.091	11.01
100.0	10.0	0.074	13.60	0.076	13.19	0.072	13.95
125.0	12.5	0.062	16.19	0.062	16.05	0.061	16.52
150.0	15.0	0.054	18.56	0.053	18.85	0.053	18.72
175.0	17.5	0.048	20.75	0.046	21.58	0.049	20.56
200.0	20.0	0.044	22.79	0.041	24.27	0.045	22.04
225.0	22.5	0.041	24.68	0.037	26.93	0.043	23.14
250.0	25.0	0.038	26.44	0.034	29.54	0.042	23.89

1	Gradient (psi/ft)	Density (g/cc)	TDS (ppm)	TDS (wt %)		
2	4.33	1		0		
3	0.437	1.01	13,500	13.5		
4	0.441	1.02	27,500	27.5		
5	0.444	1.029	37,000	37		
6	0.445	1.03	41,400	41.4		
7	0.451	1.04	55,400	55.4		
8	0.454	1.05	69,400	69.4		
9	0.459	1.06	83,700	83.7		
10	0.463	1.07	98,400	98.4		
11	0.465	1.075	100,000	100		
12	0.467	1.08	113,200	113.2		
13	0.471	1.09	128,300	128.3		
14	0.476	1.1	143,500	143.5		
15	0.48	1.11	159,500	159.5		
16	0.485	1.12	175,800	175.8		
17	0.489	1.13	192,400	192.4		
18	0.491	1.135	200,000	200		
19	0.493	1.137	210,000	210		
20	0.5	1.153	230,000	230		
21	0.51	1.176	260,000	260		



From Engle et al

From AAPG Wiki

<u>"Normal Formation</u> <u>Pressure"</u> <u>is .48 to .49 psi/ft</u> <u>in the Permian Basin</u>







Top of Overpressure from Mudweight, defined as when Pressure Gradient >.5psi/ft, occurs at variable depths in closely spaced wells. Recent horizontal wells are drilled with heavier mud because they are encountering overpressure at a shallower depth than defined by these mudweights.





From: The Role of Shale Pore Structure on the Sensitivity of Wire Line Logs to Over Pressure, by Bowers, G.L., and Katsube T. J., IN Pressure Regimes in Sedimentary Basins and their Prediction, AAPG Memoir 76 *Example from Norway*



Figure 1. Wire-line data from an overpressured well in which sonic velocity and resistivity show a greater response to the onset of overpressure than bulk density data. The curve labeled "R" is the raw resistivity data; the curve labeled "R200" is the resistivity data normalized to a common temperature of 200°F (93°C).







Available database: 55 wells have both Mud logs and Resistivity logs





Calculating Pressure Gradient Using Resistivity Logs





Wells in Blue are AIFE DST Database wells with a Calculated Pressure Gradient from Extrapolated DST Bottom Hole Pressure. NOTE: Many are Lower Quality DST due to low permeability formations (First, Second and Third Bone Spring Sands and Wolfcamp)



Permian Basin Wells in AIFE database which have Pressure Gradient extrapolated from DST data

48 wells contain Wolfcamp or Bone Spring DST data and have AIFE calculated Bottom Hole Pressure Projection (on low quality DST results due to low permeability rocks) and a resulting Pressure Gradient calculated; of these wells, only 18 are located in the overpressured area of highest interest in the Delaware Basin

These Pressure Gradients can be compared to Permian Basin Log Resistivity Data



DELAWARE BASIN SPECIFIC Relationship of Pressure Gradient to Ratio of Normal Resistivity Trend to Observed Resistivity Trend in Overpressure

Why are there so few data points --so few DST's in Delaware Basin Wolfcamp? It is overpressured and difficult to test with the high likelihood of blowout.

"There's gas, sure, but there is nothing in the Wolfcamp, the reservoirs are only as big as this room, it's so impermeable there is no point in running a DST."





- Select LAS file based on depth, location in basin, complete suite (GR, Resistivity, Sonic, Bulk Density)
- Convert LAS file from Text to Excel
- · Delete unneeded curves, merge various GR and Resis Curves to get complete curve over entire well
- Decimate depth from .5 feet to one value every 2 ft because Excel graphs cannot use more than 32,000 pts,
- Histogram on GR to determine what shale breakover is (anything >median API units = Shaley) Median API units per well vary from 40 units to almost 70 units)
- Graph GR for entire well depth in light gray
- Decimate GR values to only shale values per depth
- Graph GR Shale values in Black to highlight shale values
- Use Consistent Depth and GR API Unit scales per graph 0-200 API Units
- Decimate Resistivity curve to use only shale values (GR > median)
- Graph Resistivity shale values
- Use Consistent Depth and Resistivity Ohmm scales per graph .2 to 2000 Ohmm
- Note Resistivity drop at top overpressure map that value = Structure Top Overpressure by Resistivity log.
- Note Resistivity trend at shallow depths on plotted resistivity log pick two or more points manually to define shallow resistivity trend, post trendline equation
- Take trendline equation of shallow resistivity trend to define what deeper resistivities would be if no overpressure this gives Normal Resistivity Trend
- Resistivity curve in overpressure = Observed Resistivity
- Use Pressure Gradient <u>defined by AIFE DST database</u> vs Ratio (Normal/Observed) Resistivity graph and trendline equation Data points to define this graph are 18 wells with both DST and Resistivity LAS data, or well pairs of DST well and nearby Resistivity LAS data.
- Using those two equations compute Pressure Gradient from Observed Resistivity in Excel
- Load Pressure Gradient Curve as an LAS file to Petra Project.
- Resulting database of 55 wells with Pressure Gradient derived from Resistivity Log and Pressure Gradient derived from Mudweight



EXAMPLE From Delaware Basin Drill Stem Tests, Pressure Gradient vs Normal/Observed Resistivity graph Delaware Basin Pressure Gradient= y = 0.0595ln(x) + 0.5421

Shallow Resistivity Trend Line Equation for Gulf Hamon well = y = 2225.8ln(x) + 746.66***

(****different for each well - HAND PICK shallow resistivity trend line for each well)

Depth	Observed Resistivity	In x	x (normal trend resis)	normal/observed	In Normal/Observed Res	Depth	
	Ohmm, From Logs	(A22-746.66)/2225.8	EXP(C22)	D22/B22	LN(E22)	(F22*0.0595)+0.5421	
		y = 2225.8ln(x) + 746.66				Pressure Gradient	
7000	15.8148	2.81	16.60	1.05	0.05	0.54	7000
7002	27.071	2.81	16.62	0.61	-0.49	0.51	7002
7004	38.9433	2.81	16.63	0.43	-0.85	0.49	7004
7006	30.7784	2.81	16.65	0.54	-0.61	0.51	7006
7008	21.9514	2.81	16.66	0.76	-0.28	0.53	7008
7010	17.8265	2.81	16.68	0.94	-0.07	0.54	7010

Calculate Pressure Gradient on 55 wells in Permian Basin



Using Resistivity Logs to





West East Cross Section 1 Datum Top Bone Spring Lime

TX REFVE: 423893042 T75 B56 S SUPERIOR ÖLL EL PASO S	S 2300 540 <i>CO ETAL SHELL I</i> TATE	TX REEVES 42389233100 B13 S34 VESTERN E & P INCORPORATED LP JOHNSON	TX REEVES 423893089200 T7N B57 S17 GULF OIL CORP GOZAR	TX REEVES 423893006300 T7S B54 S20 TEXACO INCORPORATED ARMSTRONG FP	TX REEVES 423893113400 BC9 S15 GETTY OIL COMPANY FARWELL AVA TRUST	TX REFES 423803118800 T85 B51 S13 CHEVRON US ATNCORPORATED NORTHWEST HMON UNIT	TX REEVES 423893129500 T7S B50 S6 OXY USA WTP LP GUTHRIE -6-	TX PECOS 423113319100 T8S E48 S31 POGO PRODUCING COMPANY PAGE ROYALTY	TX PECOS 423713237500 BC3 \$19 CONOCO INCORPORATED TREES J C ESTATE '1	TX WARD 424751074100 B34 589 OCCIDENTAL PERMIAN LIMITED LOCKRIDGE IP
Delaware Basin Project		-14200-	64500-							
Southwest Northeast		4030- 4030- 4030- 4130- 4130- 4130-			AMAGINA STATE		413 413 413 415 415 415 415			

Twn-Rge-Sec © Well Number











- Compared DST Pressure data to Resistivity data to Mud Weight data
 - DST derived PG psi/ft, MW derived PG psi/ft, Resistivity Normal/Resistivity Overpressured derived PG psi/ft
- Conclusions -- Overpressure has been depleted in Western Delaware Basin due to Laramide uplift and erosion, similar to the Anadarko Basin





Thank You! Any Questions?



Thanks to Brian Ayers, VP Geology/ VP Business Development Rosehill Operating, Houston TX

