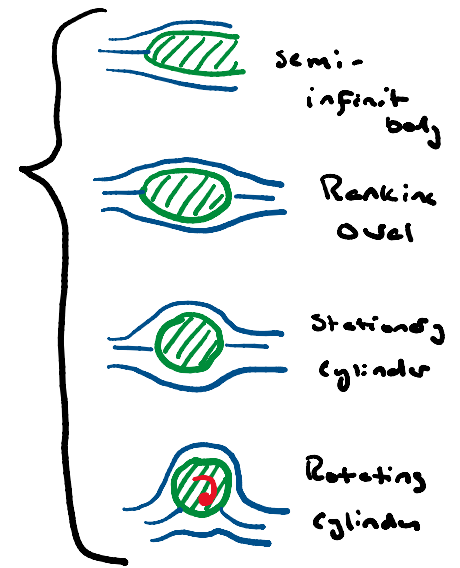
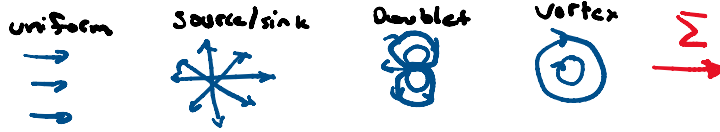
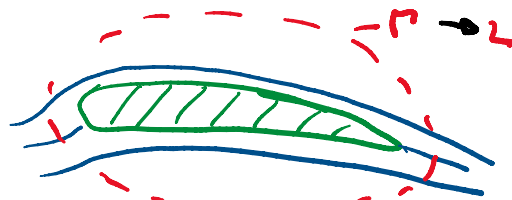


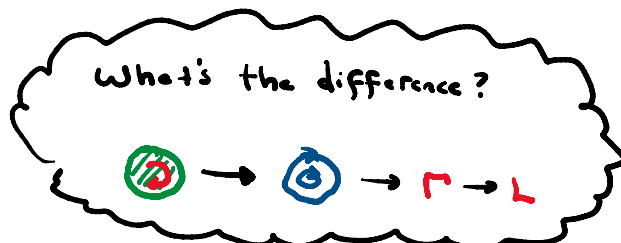
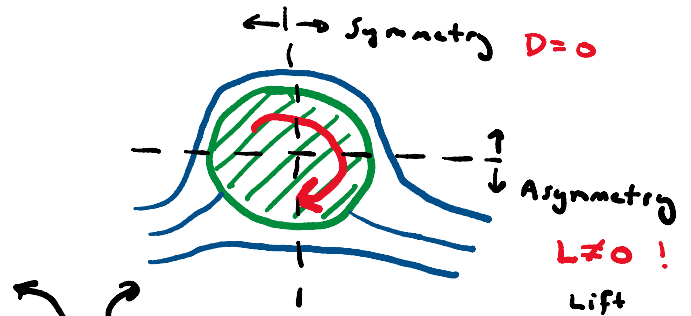
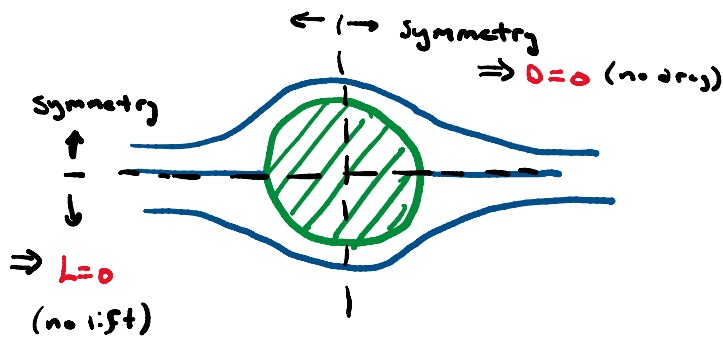
LAST TIME: ELEMENTARY FLOWS



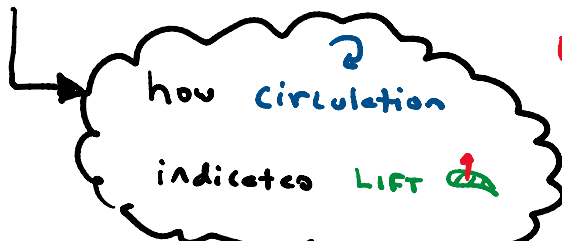
Today: KUTTA-Joukowski theorem $L' = \rho U_{\infty} \Gamma$



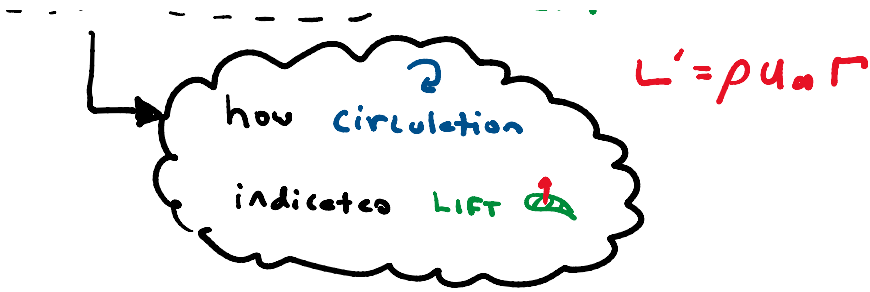
Recall, the STATIONARY & ROTATING CYLINDER from ELEMENTAL FLOWS



(German mathematician) / (Russian physicist) **KUTTA-JOUKOWSKI THEOREM**



$L' = \rho U_{\infty} \Gamma$



Back to the ROTATING CYLINDER



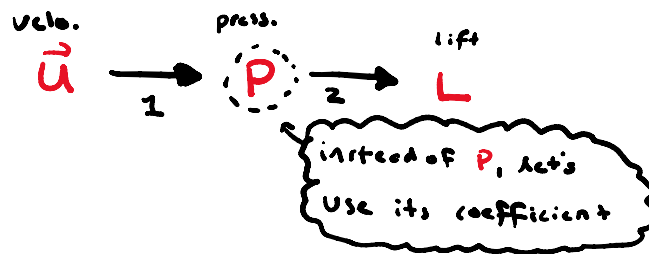
VELOCITY:

$$u_r = \left(1 - \frac{R^2}{r^2}\right) u_{\infty} \cos \theta$$

$$u_{\theta} = -\left(1 + \frac{R^2}{r^2}\right) u_{\infty} \sin \theta - \frac{\Gamma}{2\pi r}$$

(cylindrical coordinates)

Let's try to calculate LIFT



STEP 1: Find PRESSURE from VELOCITY

Pressure coefficient: $C_p = \frac{\Delta P}{\frac{1}{2} \rho u_{\infty}^2}$

~ pressure dif. from atmosphere $(P - P_{\infty}) = \Delta P$

~ dynamic pressure

Let's use BERNULLI to get ΔP in terms of u

$\checkmark \rho = \text{const.}$

$\checkmark \mu = 0$

$$P_1 + \frac{1}{2} \rho u_1^2 = P_2 + \frac{1}{2} \rho u_2^2$$

set $P_1, u_1 \rightarrow P_{\infty}, u_{\infty}$

~ free stream values

$$P_1 + \frac{1}{2} \rho u_1^2 = P_2 + \frac{1}{2} \rho u_2^2 \quad \text{set } P_1, u_1 \rightarrow P_\infty, u_\infty \quad \sim \text{Free stream values}$$

$$P_\infty + \frac{1}{2} \rho u_\infty^2 = P + \frac{1}{2} \rho u^2$$

$$\Delta P \leftarrow P - P_\infty = \frac{1}{2} \rho (u_\infty^2 - u^2)$$

Use this ΔP in above C_p

$$C_p = \frac{\Delta P}{\frac{1}{2} \rho u_\infty^2} = \frac{\frac{1}{2} \rho (u_\infty^2 - u^2)}{\frac{1}{2} \rho u_\infty^2} = \frac{u_\infty^2 - u^2}{u_\infty^2}$$

need this to get LIFT

$$C_p = 1 - \left(\frac{u}{u_\infty} \right)^2$$

we know this

NOTE: Velocity at SURFACE is $u = u_\infty$ at $r=R$

STEP 2: find LIFT from PRESSURE

Recall, we can get FORCES by integrating PRESSURE / SHEAR over surface.

$$N' = - \int_{LE}^{TE} (P_n \cos \theta + \tau_n \sin \theta) ds_1 + \int_{LE}^{TE} (P_n \sin \theta - \tau_n \cos \theta) ds_2$$

trailing edge


inviscid

leading edge

$$A' = \int_{LE}^{TE} (-P_n \sin \theta + \tau_n \cos \theta) ds_1 + \int_{LE}^{TE} (P_n \cos \theta + \tau_n \sin \theta) ds_2$$



lift' normal'

For us  therefore $dx = \cos\theta d\theta$ and $dy = -\sin\theta d\theta$ and $L' = N'$ (Cylinder coords aligned w/ free stream) $D' = A'$ (drag' axial')

$$L' = - \int_{LE}^{TE} P_u dx + \int_{LE}^{TE} P_l dx = \int_{LE}^{TE} (P_l - P_u) dx$$

$$D' = \int_{LE}^{TE} P_u dy - \int_{LE}^{TE} P_l dy = \int_{LE}^{TE} (P_u - P_l) dy$$

We want **NON-DIMENSIONAL** so $L' \rightarrow C_L$

$D' \rightarrow C_D$

$P \rightarrow C_P$

NOTE: our streamwise reference length is D (diameter)

$$C_L = \frac{1}{D} \int_{LE}^{TE} (C_{P_l} - C_{P_u}) dx$$



$$C_L = -\frac{1}{2} \int_{\pi}^{2\pi} C_{P_l} \sin\theta d\theta + \frac{1}{2} \int_{\pi}^0 C_{P_u} \sin\theta d\theta$$

$$C_D = \frac{1}{D} \int_{LE}^{TE} (C_{P_u} - C_{P_l}) dy$$



+ transform

$$\left[\begin{array}{l} y = R \sin\theta \\ dy = R \cos\theta d\theta \\ x = R \cos\theta \\ dx = -R \sin\theta d\theta \end{array} \right]$$

$$C_D = \frac{1}{2} \int_{\pi}^0 C_{P_u} \cos\theta d\theta - \frac{1}{2} \int_{\pi}^{2\pi} C_{P_l} \cos\theta d\theta$$

CARTESIAN

CYLINDRICAL

Note that $C_{P_u} = C_{P_l}$ therefore integrate C_P around whole circle $0: 2\pi$

$$\int_{\pi}^0 C_{P_u}(\dots) + \int_{\pi}^{2\pi} C_{P_l}(\dots) = \int_0^{2\pi} C_P(\dots)$$

Let's get our C_p in full form

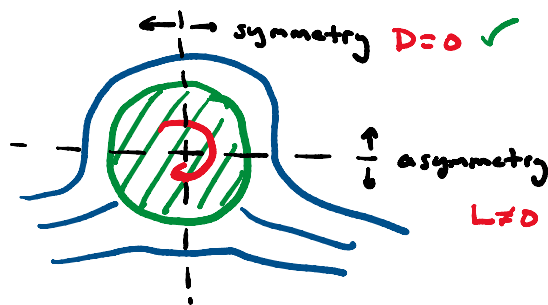
$$C_p = 1 - \left(\frac{u_\theta}{u_\infty} \right)^2 \quad \text{where} \quad u_\theta = -2u_\infty \sin\theta - \frac{\Gamma}{2\pi R} \quad (r=R)$$

← velocity at surf.

$$C_p = 1 - \left(-2\sin\theta - \frac{\Gamma}{2\pi R u_\infty} \right)^2$$

$$= 1 - 4\sin^2\theta - \frac{2\Gamma\sin\theta}{\pi R u_\infty} - \left(\frac{\Gamma}{2\pi R u_\infty} \right)^2 \quad *$$

Ready to solve for **LIFT** & **DRAG** (finally...)



$$C_d = -\frac{1}{2} \int_0^{2\pi} C_p \cos\theta d\theta$$

$$= -\frac{1}{2} \int_0^{2\pi} \left[\cancel{1} - 4\cancel{\sin^2\theta} + \frac{2\Gamma\cancel{\sin\theta}}{\pi R u_\infty} + \left(\frac{\Gamma}{2\pi R u_\infty} \right)^2 \right] \cos\theta d\theta$$

MATH NOTE: $\int_0^{2\pi} \cos\theta d\theta = 0$

$$\int_0^{2\pi} \sin^2\theta \cos\theta d\theta = 0$$

$$\int_0^{2\pi} \sin\theta \cos\theta d\theta = 0$$



$$C_l = -\frac{1}{2} \int_0^{2\pi} C_p \sin\theta d\theta$$

$$= -\frac{1}{2} \int_0^{2\pi} \left[\cancel{1} - 4\cancel{\sin^2\theta} + \frac{2\Gamma\cancel{\sin\theta}}{\pi R u_\infty} + \left(\frac{\Gamma}{2\pi R u_\infty} \right)^2 \right] \sin\theta d\theta$$

~ not zero!

MATH NOTE: $\int_0^{2\pi} \sin\theta d\theta = 0$

$$\int_0^{2\pi} \sin^3\theta d\theta = 0$$

$$\int_0^{2\pi} \dots d\theta = 0$$

$$\int_0^{2\pi} \sin\theta \cos\theta d\theta = 0$$

$$C_d = 0 \quad \checkmark$$

$$\int_0^{2\pi} \sin^2\theta d\theta = \pi$$

$$C_l = \frac{1}{2} \int_0^{2\pi} \frac{2\Gamma}{\pi R U_\infty} \sin^2\theta d\theta$$

(const.)

$$C_l = \frac{\Gamma}{R U_\infty} \quad \checkmark$$

So, the **LIFT** on our **ROTATING CYLINDER** is

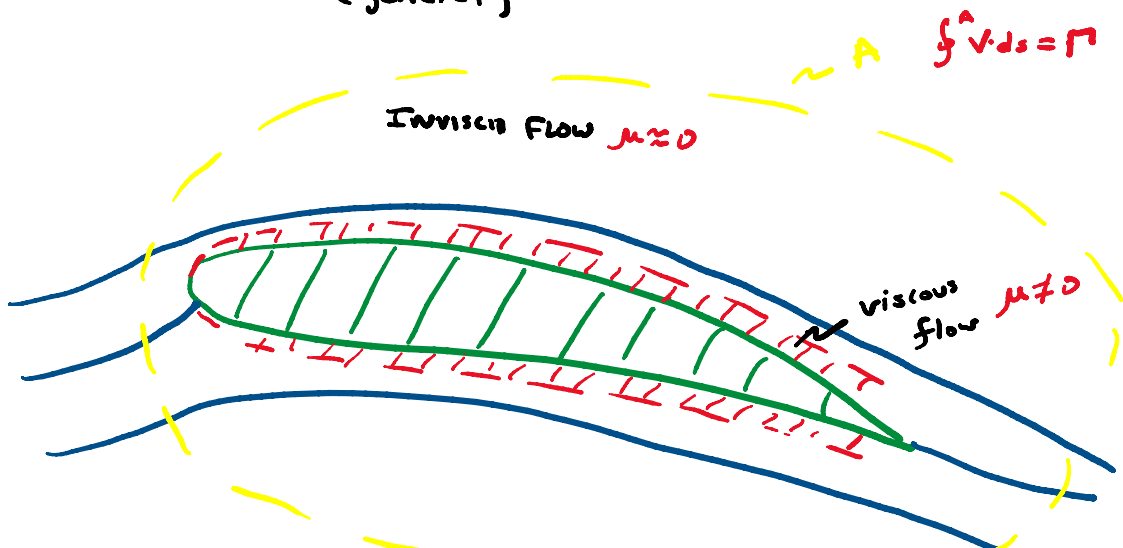
$$L' = \frac{1}{2} \rho U_\infty^2 \overset{\sim \text{our length scale}}{D} C_l = \frac{1}{2} \rho U_\infty^2 (\cancel{2\pi}) \frac{\Gamma}{\cancel{R U_\infty}}$$

$$L' = \rho U_\infty \Gamma$$

\leadsto **KUTTA-JOUKOWSKI THEOREM**

Although it appeared for **ROTATING CYLINDERS** 

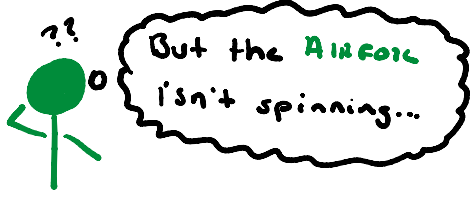
it also works for **AERODYNAMIC BODIES!**
(general)





As long as all the flow Γ is accounted for

$$L = \rho U_{\infty} \Gamma \quad \checkmark$$



But the AIRFOIL isn't spinning...

the CURVATURE (camber) and ANGLE cause FLOW rotation, $\Rightarrow \Gamma \neq 0$

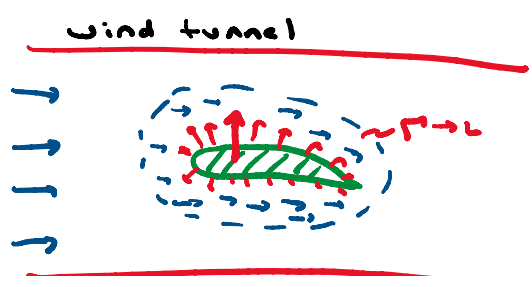
Keep in mind - Γ doesn't make lift, it just indicates it exists

LIFT/DRAG are caused by PRESSURE/SHEAR, CIRCULATION is the footprint

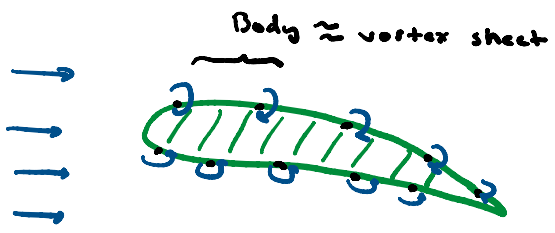


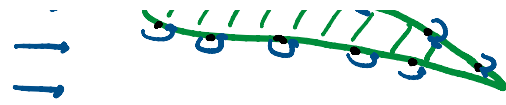
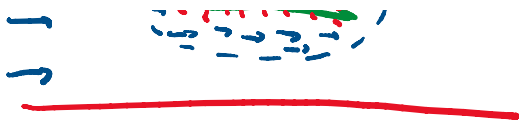
In practice you will see KUTTA-JOUKOWSKI principles often.

EXPERIMENTS



SIMULATIONS





To get **LIFT** you can

- (1) measure directly
- (2) integrate pressure

"VORTEX PANEL METHOD"

$$\Gamma \rightarrow L$$

* (3) Get Γ from \vec{u}

