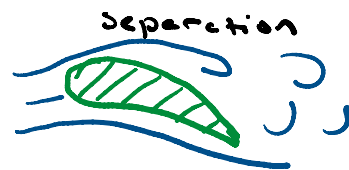
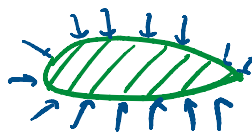


LAST TIME: **DRA**: Pressure & Viscosity

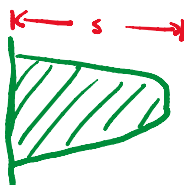


TODAY: **Finite wing effects**



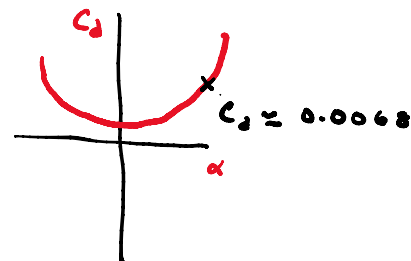
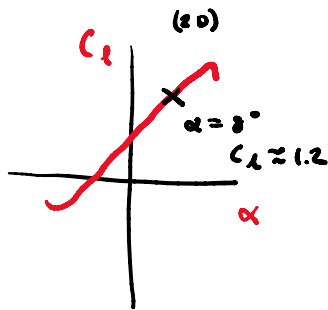
Induced drag / downwash / effective a.o.a.

(N) **FINITE WINGS**
(physical effects)



Beginning to think about
REAL (3D) not **IDEAL** (2D)

Consider a **NACA 4412** foil




So we go from 2D to 3D

Say we go from  2D to  3D

2D $\alpha = 8^\circ$ $C_L = 1.2$
 $C_D = 0.0068$ } these are "per-unit-span"

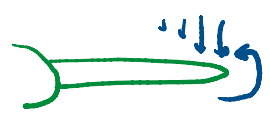
Recall, $C_L = \frac{L}{\frac{1}{2} \rho U_\infty^2 c}$ Lift per unit span
 $C_D = \frac{D}{\frac{1}{2} \rho U_\infty^2 c}$

3D $C_L = C_{L,2D}$? $C_D = C_{D,2D}$?  NO!

"Per unit span" are IDEAL ; assume $s = \infty$

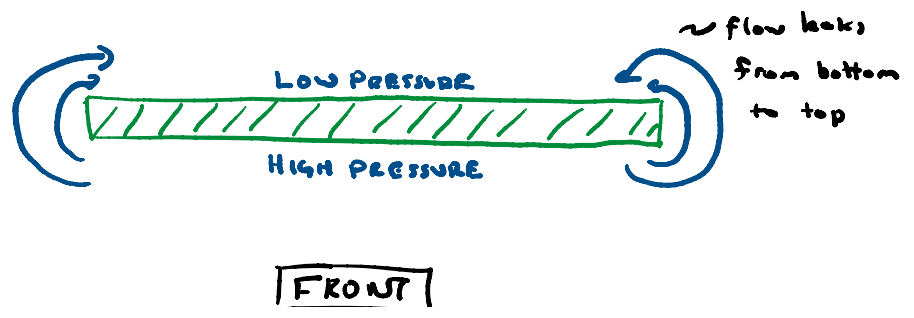
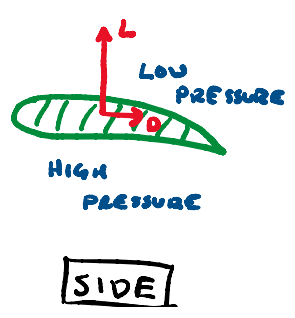
\Rightarrow LIFT & DRAG come from 2D stuff

In REAL cases, $s \neq \infty$, leads to finite-span effects:



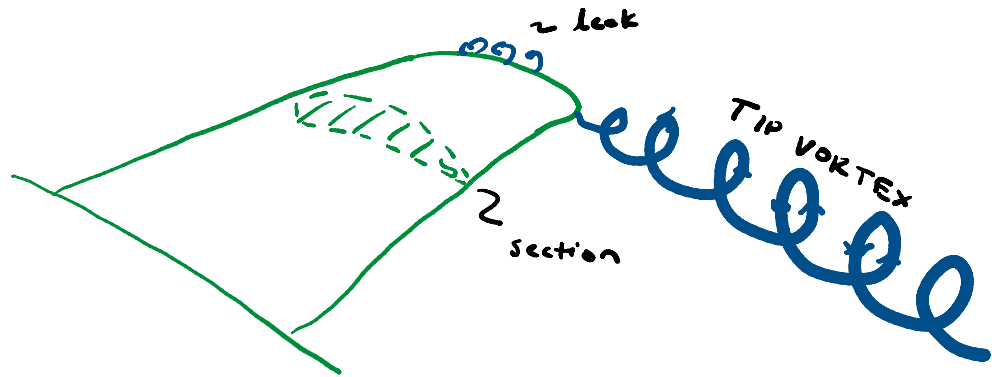
DOWNWASH / EFFECTIVE A.O.A / INDUCED DRAG

Consider a foil

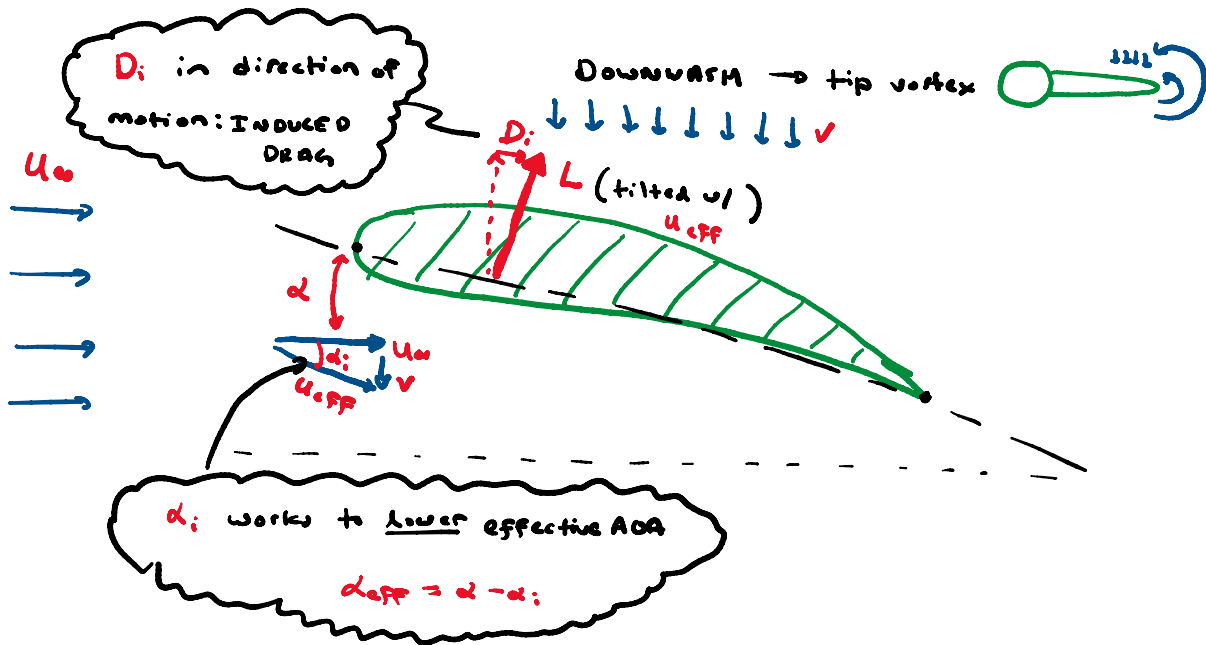


SIDE

FRONT



Consider a **SECTION** near the tip



Downwash leads to:

(1) Change in α locally



(2) Portion of LIFT in direction of motion becomes INDUCED DRAG C_D .

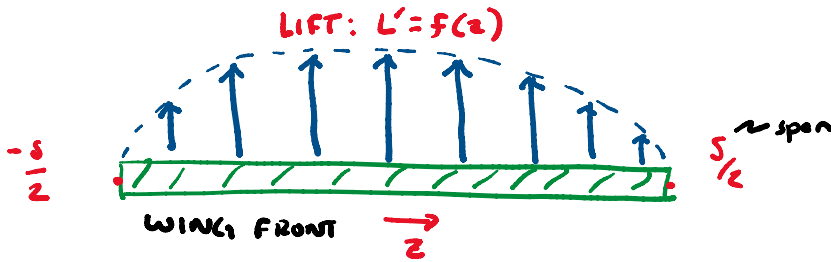
For a finite wing, drag comes from 3 PLACES

SKIN FRICTION
(viscous)

SEPARATION
(pressure)

INDUCED
(pressure)

Downwash also leads to LIFT DISTRIBUTION

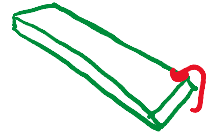


KUTTA - JOUKOWSKI: if $L' = F(z)$
 $(L' = \rho U_\infty \Gamma)$ $\Rightarrow \Gamma = g(z)$

NOTE: other things cause $L' = F(z)$

• chord variation $s(z)$

• geometric twist $\alpha = f(z)$




• aerodynamic twist $f_{aero}(z)$



Since this is all from VORTEX

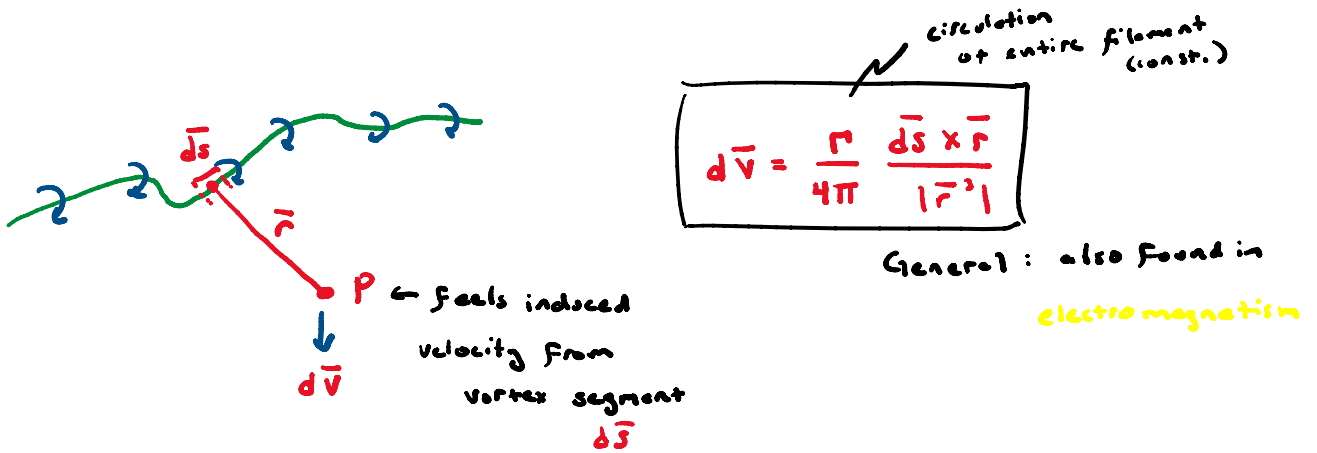


lets ...

Since this is all from **VORTEX** 
 let's explore them

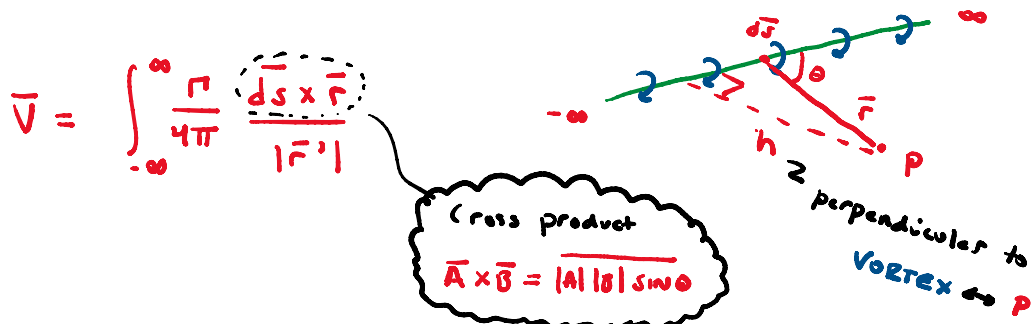
(1) **BIOT-SAVART LAW** : understanding semi-infinite
 vortices (i.e. tip vortex)

Consider a **VORTEX FILAMENT**



What if **VORTEX** is straight from $-\infty \rightarrow +\infty$
 "INFINITE VORTEX"

add up **BIOT-SAVART** along path



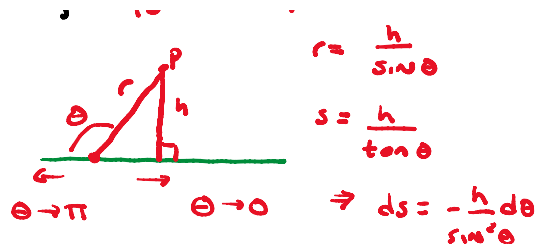
We just want magnitude $v = |\vec{V}|$

$$V = \frac{\Gamma}{4\pi} \int_{-\infty}^{\infty} \frac{\sin\theta}{r^2} ds$$

Change r, s to h, θ
 $r = \frac{h}{\sin\theta}$

$$V = \frac{\Gamma}{4\pi} \int_{-\infty}^{\infty} \frac{\sin \theta}{r^2} ds$$

$$V = -\frac{\Gamma}{4\pi h} \int_{\pi}^0 \sin \theta d\theta$$



$$V = \frac{\Gamma}{2\pi h}$$

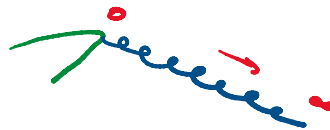
infinite line-vortex

← how you feel standing



What if the VORTEX goes from $0 \rightarrow \infty$

"Semi-infinite vortex"

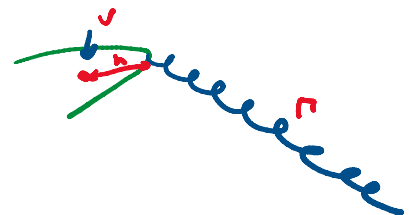


$$V = -\frac{\Gamma}{4\pi} \int_{\pi}^{\pi/2} \sin \theta d\theta$$

$$= \frac{\Gamma}{4\pi} \cos \theta \Big|_{\pi}^{\pi/2}$$

$$V = \frac{\Gamma}{4\pi h}$$

Semi-infinite vortex




There are RULES to VORTEX FILAMENTS


HELMHOLTZ VORTEX THEOREM

(1) The STRENGTH of filament CONSTANT along length.

(2) VORTICES cannot just STOP in fluid

- must terminate @ boundary

- must terminate @ boundary 

- or - loop  (vortex ring)

(3) IF nothing causes ROTATION externally,
IRROTATIONAL stays that way

Goal moving forward: PREDICT / CALCULATE

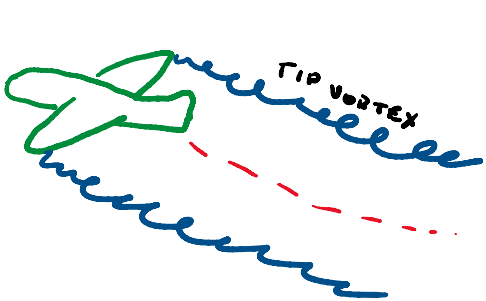
INDUCED DRAG C_D

LIFT L

LIFT DISTRIBUTION $L'(z)$

... for finite wings.

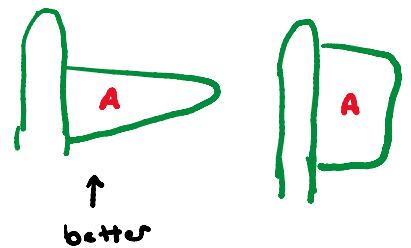
In PRACTICE, tip vortices & induced drag are important



• Dictate TAKEOFF/LANDING schedules at airports



• Avoidance is used (flow control)



• Leads to higher ASPECT RATIOS

