

## GATE 2018 Civil Engineering

(Afternoon Session - 11.02.2018)

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PAGE  
2CATE 2018 [Afternoon Session]  
Civil EngineeringConstrained  
Civil EngineeringConstrained  
Civil EngineeringSol. Given :
$$\frac{a+a+a+a+...+a}{ntimes} = a^2b$$
,  $\frac{b+b+b+...+a}{mtimes} = ab^2$ Constrained  
To find : Value of  $\left(\frac{m+m+m+...+m}{ntimes}\right)\left(\frac{n+n+n+...+n}{mtimes}\right)$ .  
 $\frac{a+a+a+...+a}{ntimes} = a^2b$ In this, number of times a approach = na.  
 $\therefore$  $na = a^2b \Rightarrow n = ab$ In this, number of times a approach = na.  
 $\therefore$  $na = a^2b \Rightarrow n = ab$  $na = a^2b \Rightarrow n = ab$ Sol. Given : $\frac{m+m+m+...+m}{ntimes} = ab^2$  $na = ab^2 \Rightarrow m = ab$ In this, number of times b approach = mb.  
 $\therefore$  $mb = ab^2 \Rightarrow m = ab$ So, $\left(\frac{m+m+m+...+m}{ntimes}\right) = nm$ And $\left(\frac{m+m+m+...+m}{ntimes}\right) = nm$ Then, $\left(\frac{m+m+m+...+m}{ntimes}\right) = nm$ Muting the value of n and m in equation (i), we get  
 $mn \times nm = (a^2b^2) \times (a^2b^2)$   
 $nn \times nm = a^2b^4$ Question 5A three-member committee has to be formed a group of 9 people. How many such distinct committees  
can be formed?  
(A) 27Guestion 5Given : Number of member in a committee = 3  
Number of people in group = 9  
To find : Total number of committees to be formed.  
By using binomial distribution.

$${}^{n}C_{r} = \frac{n!}{(n-r)! \times r!}$$

where, n = Number of people, r = Number of member in a committee.

PAGE 3	GATE 2018 [Afternoon Session Civil Engineering	n] GATE ACADEMY <u>steps to success</u>				
	${}^{9}C_{3} = \frac{9!}{(0-2)!} = \frac{9!}{(1-2)!}$					
	$(9-3):\times 5: 0:\times 5:$					
	${}^{9}C_{3} = \frac{9 \times 8 \times 7 \times 6 \times 5 \times 4 \times 3 \times 2 \times 1}{(6 \times 5 \times 4 \times 3 \times 2 \times 1) \times (3 \times 2 \times 1)}$					
	${}^{9}C_{3} = \frac{9 \times 8 \times 7}{6} = 84$					
	Q.6 to Q.10 Carry t	wo marks each				
Questi	ion 6					
	A faulty wall clock is known to gain 15 minutes even 9 AM on 11 <sup>th</sup> July. What will be the correct time to 15 <sup>th</sup> July of the same year?	ery 24 hours. It is synchronized to the correct time at to the nearest minute when the clock shows 2 PM on				
Ans.	(A) 12:45 PM (B) 12:58 PM (B)	(C) 1:00 PM (D) 2:00 PM				
Sol.	<b>Given :</b> Clock gains 15 minutes in every 24 hours.					
	<b>To find :</b> Correct time to the nearest minute.					
	Clock shows correct time at 9 AM on 11 <sup>th</sup> July up to	o 2 PM on 15 <sup>th</sup> July.				
	Total hours on date 12, 13 and $14 = \frac{24}{3} \times 3 = 72$ hour	rs				
	Total hours on date 11 = 15 hours					
	Total hours on date 15 = 14 hours					
	Total hours from 9 AM on 11 <sup>th</sup> July up to 2 PM on 1	15 <sup>th</sup> July = 72 + 15 + 14 = 101 hours				
	Clock gains 15 minutes in every 24 hours.					
	Gain (per hour) = $\frac{15}{24}$ minutes					
	Gain (Total hours 9 AM on 11 <sup>th</sup> July up to 2 PM on	15 <sup>th</sup> July)				
	$=101 \times \frac{15}{24} = 63.125 \approx 63 \text{ minutes}$					
	Correct time to the nearest minute (63 minutes back from 2 PM) $\approx 12:58$ PM					
Questi	ion 7 SINCE	2004				
	Given that $\frac{\log P}{y-z} = \frac{\log Q}{z-x} = \frac{\log R}{x-y} = 10$ for $x \neq y \neq z$ , what is the value of the product <i>PQR</i> ?					
	(A) 0 (B) 1	(C) $xyz$ (D) $10^{xyz}$				
Ans.	<b>(B)</b>					
Sol.	<b>Given :</b> $\frac{\log P}{y-z} = \frac{\log Q}{z-x} = \frac{\log R}{x-y} = 10$					
	<b>To find :</b> Value of the product <i>POR</i> .					
	$\log P \log Q \log R$					
	$\frac{1}{y-z} = \frac{1}{z-x} = \frac{1}{x-y} = 10$					



GATE A

From the above equation,

 $\log P = 10(y - z)$   $\log Q = 10(z - x)$   $\log R = 10(x - y)$   $\log P + \log Q + \log R = (y - z) + (z - x) + (x - y)$   $\log P + \log Q + \log R = 0$  $\log (PQR) = \log 1$ 

Value of the product PQR = 1

#### **Question 8**

In manufacturing industries, loss is usually taken to be proportional to the square of the deviation from a target. If the loss is Rs. 4900 for a deviation of 7 units, what would be the loss in Rupees for a deviation of 4 units from the target?

(	(A) 400 (	B) 1200	(C) 1600	(D) 2800
U	(A) +00 (	D) 1200	(C) 1000	(D) 2000

#### Ans. (C)

**Sol.** Given :  $(Loss)_1$  : Rs. 4900

Number of units,  $D_1 = 7$ ,  $D_2 = 4$ 

**To find :** Loss for a deviation of 4 units from the target.

It is given that, loss is usually taken to be proportional to the square of the deviation from a target.

$$(Loss)_1 = K \times D_1^2$$

$$4900 = K \times 7^2$$

$$K = 100$$

$$(Loss)_2 = K \times D_2^2$$

Loss for a deviation of 4 units from the target,  $(Loss)_2 = 100 \times 4^2 = 1600$ 

#### **Question 9**

Each of the letters in the figure below represents a unique integer from 1 to 9. The letters are positioned in the figure such that each of (A+B+C), (C+D+E), (E+F+G) and (G+H+K) is equal to 13. Which integers does *E* represent?





**Sol.** Given : Value of (A + B + C), (C + D + E), (E + F + G) and (G + H + K) = 13

**To find :** *E* represent which integer.



*E* represent the integer 4.

#### **Question 10**

The annual average rainfall in a tropical city is 1000 mm. On a particular rainy day (24-hour period), the cumulative rainfall experienced by the city is shown in the graph. Over the 24-hour period, 50% of the rainfall falling on a rooftop, which had an obstruction-free area of  $50 \text{ m}^2$  was harvested into a tank. What is the total volume of water collected in the tank in liters?





The graph of a function f(x) is shown in the figure



GATE AC

teks to

For f(x) to be a valid probability density function, the value of h is

(A) 1/3 (B) 2/3 (C) 1 (D) 3

Ans. (A)

**Sol.** Probability density function : It is defined as a function of continuous random variables whose integral across an interval gives the probability that the value of variable lies within the same interval.

According to the drawn graph (in question), *h* lies between 0 and 1, 2*h* lies between 1 and 2 and 3*h* between 2 and 3.

$$\int_{0}^{1} f(x) dx + \int_{1}^{2} f(x) dx + \int_{2}^{3} f(x) dx = 1$$
  

$$\frac{h}{2} + \frac{2h}{2} + \frac{3h}{2} = 1$$
  

$$0.5h + 1h + 1.5h = 1$$
  

$$3h = 1$$
  

$$h = \frac{1}{3}$$

#### **Question 2**

A culvert is designed for a flood frequency of 100 years and a useful life of 20 years. The risk involved in the design of the culvert (in percentage up to two decimal places) is \_\_\_\_\_.

#### Ans. (18.20)

**Sol.** Given : Flood frequency, T = 100 years, Useful life, n = 20 years

**To find :** Risk involved in the design of culvert.

Risk =  $1 - q^n$ 





where, q =Complementary probability of a flood, q = 1 - P

where, 
$$P = Probability$$
 of a flood,  $P = \frac{1}{T}$ 

$$P = \frac{1}{100}$$

÷.

Then, Risk  $= 1 - q^n = 1 - 0.99^{20} = 0.182093$ 

 $q = 1 - \frac{1}{100} = 0.99$ 

Therefore, risk involved in the design of culvert equal to 18.20%.

(B) Critical depths

#### Note :

**Risk :** It is defined as that probability in which the flood occurs at least once in *n*-successive years.

#### **Question 3**

For a given discharge in an open channel, there are two depths which have the same specific energy. These two depths are known as

(A) Alternate depths

(C) Normal depths (I

(D) Sequent depths

#### Ans. (A)

**Sol.** For the same value of specific energy, discharge is constant and there are two possible values of depth i.e., super critical depth  $(y_1)$  and subcritical depth  $(y_2)$ . These two depths are called alternate depths.



PAGE 8	GATE 2018 [Afternoon Session] Civil Engineering GATE ACADEMY steps to success				
	From IS code 456 : 2000 (Table 28), in the case of structural member subjected to compression has both translation and rotation restrained at one end and only translation is restrained at the other end, the effective				
0	length is equal to 0.80 L.				
Quest	<b>100 5</b> The initial conceptity in the load nonetration curve of a CPD test is NOT due to				
	(A) Uneven top surface $(B)$ High impact at start of loading				
	(C) Inclined penetration plunger (D) Soft top layer of soaked soil				
Ans.	(B) (B)				
Sol.	In a CBR test, when the load-penetration curve is plotted, curve usually gets convex upwards although the				
	initial portion of the curve may be concave due to surface irregularities.				
	The initial concavity is due to the following reasons :				
	• Top surface of soil sample.				
	• Top layer of soaked soil.				
	<ul> <li>Irregular contact between the plunger and soil.</li> <li>Uneven composition</li> </ul>				
	• Uneven compaction. Therefore, high impact at start of loading will not cause any change in the shape of curve				
Questi	ion 6				
~	A reinforced-concrete slab with effective depth of 80 mm is simply supported at two opposite ends on 230				
	thick masonry walls. The centre-to-centre distance between the walls is 3.3 m. As per IS 456 : 2000, the				
	effective span of the slab (in m, up to two decimal plates) is				
Ans.	(3.15)				
Sol.	Given : Effective depth, $d_{eff} = 80 \text{ mm} = 0.08 \text{ m}$				
	Thickness of masonry wall = $230 \text{ mm} = 0.23 \text{ m}$				
	c/c distance between the walls = $3.30 \text{ m}$				
	<b>To find :</b> Effective span of slab $(L_{eff})$				
	Clear span of slab, $L_c = c/c$ distance – Thickness of masonry wall				
	$L_c = 3.30 - 0.23 = 3.07 \text{ m}$				
	From IS code 456 : 2000 (by effective span criteria for simply supported slab), the effective span $(L_{eff})$				
	of a member shall be taken as				
	$L_{e\!f\!f} = L_c + d_{e\!f\!f}$				
	Or, c/c distance between the walls				
	Whichever is less.				
	$L_{e\!f\!f} = L_c + d_{e\!f\!f}$				
	= 3.07 + 0.08 = 3.15  m				
	And c/c distance between the walls = $3.30 \text{ m}$ .				
	$\therefore$ Minimum effective span, $L_{eff} = 3.15 \mathrm{m}$				

PAGE 9	GATE 2018 [Afternoon Session] Civil Engineering GATE ACADEMY steps to success			
Questi	on 7			
-	Peak Hour (PHF) is used to represent the proportion of peak sub-hourly traffic flow within the peak hour. If 15-minute sub-hours are considered, the theoretically possible range of PHF will be			
	(A) 0 to 1.0 (B) 0.25 to 0.75 (C) 0.25 to 1.0 (D) 0.5 to 1.0			
Ans.	(C)			
Sol.	The peak hour factor is defined as the ratio of total hourly traffic volume to the maximum 15-minute traffic			
	volume within an hour. It represents the flow within an hour.			
	If 15-minute period is used, the PHF may be computed as			
	$PHF = \frac{V}{4 \times V_{15}}$			
	where, PHF = Peak hour factor, $V$ = Hourly volume (vph), and $V_{15}$ = Volume during 15 min of the peak			
	hour (vehicle/15 min).			
	The theoretical possible range of PHF will be $0.25 \le PHF_{15} \le 1$ .			
Questi	on 8			
	Probability (up to one decimal place) of consecutively picking 3 red balls without replacement from a box			
	containing 5 red balls and 1 white ball is			
Ans. Sol	(0.5) Civen : Number of red halls in the hoy $= 5$			
<b>301.</b>	<b>Given :</b> Number of red balls in the box = 5 Number of white balls in the box = 1			
	<b>To find :</b> Probability of consecutively picking 3 red balls without replacement.			
	Drehehility of first hell to be red 5			
	Probability of first ball to be red $= \frac{1}{6}$			
	Probability of second ball to be red (out of remaining 5 balls) = $\frac{4}{5}$			
	Probability of third ball to be red (out of remaining 4 balls) = $\frac{3}{4}$			
	Probability of consecutively picking 3 red balls without replacement $=\frac{5}{6} \times \frac{4}{5} \times \frac{3}{4} = \frac{1}{2} = 0.5$			
Questi				
	As per IS 456 : 2000, the minimum percentage of tension reinforcement (up to two decimal places) required in reinforced-concrete beams of rectangular cross-section (considering effective depth in the calculation of area) using Fe 500 grade steel is			
Ans.	(0.17)			
Sol.	<b>Given :</b> Grade of steel = Fe 500 $\Rightarrow f_y = 500 \text{ MPa}$			
	To find : Minimum percentage of steel			
	From IS code 456 : 2000 (by tension reinforcement criteria), the minimum percentage of tension reinforcement shall not be less than given below :			
	Minimum percentage $=\frac{85}{f_y}\% = \frac{85}{500}\% = 0.17\%$			

PAGE 10	GATE 2018 [Afternoon Session] Civil Engineering	GATE ACADEMY steps to success			
Quest	Question 10				
	The solution of the equation $x\frac{dy}{dx} + y = 0$ passing through	the point (1, 1) is			
	(A) $x$ (B) $x^2$ (C)	$x^{-1}$ (D) $x^{-2}$			
Ans.	<b>(C)</b>				
Sol.	<b>Given :</b> $x\frac{dy}{dx} + y = 0$				
	To find : Solution of the above equation passing through	point (1, 1).			
	$x\frac{dy}{dx} = -y$				
	$\frac{dx}{dy}$ $\frac{dx}{dx}$				
	$\frac{dy}{y} = -\frac{dx}{x}$				
	Integrating on both sides, we get				
	$\int \frac{dy}{y} = -\int \frac{dx}{x}$				
	$\ln(y) = -\ln(x) + C \qquad \qquad$	$\left[\ln\left(x\right)\right]$			
	$\ln(y) = \ln\left(\frac{1}{x}\right) + C \qquad \qquad \left[\because \int \frac{1}{x} dx = \right]$	$\ln(x)^{-1} = \ln\left(\frac{1}{x}\right) \qquad \dots (i)$			
	Putting $x = 1$ and $y = 1$ in equation (i)				
	$\ln\left(1\right) = \ln\left(\frac{1}{1}\right) + C$				
	C = 0	T E			
	Putting the value of $C = 0$ in equation (i), we get				
	$\ln(y) = \ln\left(\frac{1}{x}\right) + 0$	004			
	$y = \frac{1}{x}$ [Can	celling (ln) on both sides]			
	$y = x^{-1}$				
Quest	Question 11				
	As per IS 10500 : 2012 for drinking water in the absence of alternate source of water, the permissible				
	limits for chloride and sulphate in mg/L respectively are				

(A) 250 and 200 (B) 1000 and 400 (C) 200 and 250 (D) 500 and 1000

Ans. (B)



steps to success.

**Sol.** From table 2 of IS code 10500 : 2012 (General parameters for substances),

For drinking water in the absence of alternate source of water, the permissible limits for chloride and sulphate in mg/L respectively are

Substances	Permissible limits (mg/L)	
Chloride	1000	
Sulphate	400	

#### **Question 12**

Which one of the following statements is NOT correct?

- (A) When the water content of soil lies between liquid limit and plastic limit the soil is said to be in plastic state.
- (B) Boussinesq's theory is used for the analysis of stratified soil.
- (C) The inclination of stable in cohesive soil can be greater than its angle of internal friction.
- (D) For saturated dense fine sand, after applying overburden correction if the Standard Penetration Test value exceeds 15, dilatancy correction is to be applied.

#### Ans. (B)

**Sol.** For the analysis, Boussinesq assumed that the soil is elastic, isotropic and homogenous for the development of a point load formula. However, the soil is neither isotropic nor homogenous. The most common type of soils are met in the nature are water deposited sedimentary soils.

Therefore, Boussinesq's theory is only applicable for isotropic soil and not for stratified soil.

#### **Question 13**

The intensity of irrigation for the Kharif season is 50% for an irrigation project with culturable command area of 50,000 hectares. The duty for the Kharif season is 1000 hectare/cumec. Assuming transmission loss of 10%, the required discharge (in cumec, up to two decimal places) at the head of the canal is

#### Ans. (27.78)

Sol. Given : Irrigation intensity for Kharif season = 50% Culturable command area (CCA) = 50,000 hectares Duty for Kharif season, D = 1000 hectares/cumec Transmission loss = 10% To find : Discharge at the head of the canal.

Area under Kharif season, A = 50% of CCA

=

$$=\frac{50}{100}\times50,000=25,000$$
 hectares



Discharge (at head of the field),

$$Q = \frac{\text{Area under Kharif season}}{\text{Duty for Kharif season}}$$

$$Q = \frac{A}{D} = \frac{25,000}{1000} = 25$$
 cumec

Transmission loss = 10%

Transmission efficiency,  $\eta_{transmission} = 90\%$ · .

Discharge (at head of the canal) =  $\frac{\text{Discharge at the head of the field}}{-}$ Transmission efficiency

$$=\frac{Q}{\eta_{transmission}}=\frac{25}{0.90}=27.778\approx 27.78$$
 cumec

#### **Question 14**

The quadratic equation  $2x^2 - 3x + 3 = 0$  is to be solved numerically starting with an initial guess as  $x_0 = 2$ . The new estimate of x after the first iteration using Newton-Raphson method is \_\_\_\_\_.

#### Ans. (1)

- Sol. Given :
- $x_0 = 2$

From Newton-Raphson formula,

$$x_1 = x_0 - \frac{f(x_0)}{f'(x_0)}$$

 $f(x) = 2x^2 - 3x + 3$ 

Taking the equation given in question

$$f(x) = 2x^2 - 3x + 3$$

Differentiating on both sides, we get

$$f'(x) = 4x - 3$$

...(ii)

...(i)

teps to

Putting the value of  $x_0 = 2$  in equation (ii), we get

$$f(x_0) = 2(2)^2 - 3(2) + 3$$
$$f(x_0) = 8 - 6 + 3 = 5$$

And

$$f'(x_0) = 4(2) - 3$$
  
 $f'(x_0) = 8 - 3 = 5$ 

Putting the values of  $f(x_0)$  and  $f'(x_0)$  in equation (i)

$$x_{1} = x_{0} - \frac{f(x_{0})}{f'(x_{0})}$$
$$x_{1} = 2 - \frac{5}{5} = 1$$



steps to success

#### **Question 15**

In the figures, Group I represents the atmospheric temperature profiles (P, Q, R and S) and Group II represent dispersion of pollutants from a smoke stack (1, 2, 3 and 4). In the figures of Group I, the dashed line represents the dry adiabatic lapse rate, whereas the horizontal axis represents temperature and the vertical axis represents the altitude.



(A) P-1, Q-2, R-3, S-4 (B) P-1, Q-2, R-4, S-3 (C) P-1, Q-4, R-3, S-2 (D) P-3, Q-1, R-2, S-4

#### Ans. (A)

- Sol. 1. Super adiabatic : Super adiabatic atmosphere is highly unstable. During the high degree of turbulence, the dispersion of plume would be rapid (in a type of loop), yet higher concentrations near the ground may occur due to turbulence, before the dispersion is finally completed.
  - 2. Adiabatic : It is also known as sub-adiabatic condition. Under these conditions, the atmosphere is slightly stable, and there is a limited vertical mixing, thereby increasing the probability of air pollution in the area. The neutral plume tends to get a shape of cone.
  - **3. Inversion :** In this, the emission will spread horizontally, as it cannot lift due to extremely stable atmosphere. In this case, there will be no vertical mixing, and the plume will simply extend horizontally over large distances. Such a plume pattern is known as fanning plume.
  - 4. Inversion over super adiabatic : In such a case, the pollutants cannot escape above the top of the stack because of inversion, and they will be brought down near the ground due to turbulence in the region above the ground and below the inversion, caused by strong lapse rate. This is the case of fumigation.

PAGE 14	GATE 2018 [Afternoon Session] Civil Engineering	<b>GATE ACADEMY</b> steps to success
Orrest	tion 10	
Quest	The clay mineral whose structural units are held together	r by potassium bond is
	(A) Halloysite (B) Illite (C)	Kaolinite (D) Smectite
Ans.	(B)	
Sol.	In the hydrous mica clay minerals such as illite, the 2 : 1 no hydration water in the interlayer space. With loss montmorillonite.	layers are held together by potassium ions with of this structural potassium, illite weathers to
Quest	tion 17	
	A fillet weld is simultaneously subjected to factored norr respectively. As per IS 800 : 2007 the equivalent stress (i	mal and shear stresses of 120 Mpa and 50 MPa, in MPa, up to two decimal place) is
Ans.	(147.99)	
<b>SOI.</b>	<b>Given :</b> Factored normal stress, $f_a = 120$ MPa	
	Factored snear stress, $q = 50$ MPa To find : Equivalent stress of fillet wold	
	From IS code 800 : 2007 (by fillet weld criteria), equivalent	ent stress formula is given by
	$f = \sqrt{f^2 + 3a^2} \le \text{Design strength of fillet}$	t weld $(f_{i})$
	$\int_{e} - \sqrt{f_a + 5q} = Design sublight of find$	
	$f_e = \sqrt{f_a^2 + 3q^2} \le \frac{J_u}{\gamma_{mw}\sqrt{3}}$	
	where, $f_u$ = Ultimate stress ( $f_u$ = 410MPa)	
	$\gamma_{mw}$ = Partial safety factor for welds ( $\gamma_{mw}$ = 1.25	5)
	$f_e = \sqrt{f_a^2 + 3q^2} = \sqrt{120^2 + 3 \times 50^2}$	
	$f_e = \sqrt{21900} = 147.99 \mathrm{MPa}$	
	And $f_e \leq \frac{f_u}{\gamma_{mw}\sqrt{3}}$ 410	T E
	$f_e \le \frac{110}{1.25 \times \sqrt{3}} = 189.37 \mathrm{MPa}$	001
	:. Equivalent stress of fillet weld, $f_e = 147.99 \text{ MPa}$	004
Quest	tion 18	
	A vertical load of 10 kN acts on a hinge located at a dista	ance of $L/4$ from the roller support $Q$ of a beam
	of length $L$ (see figure)	0 kN
	31/4	
	The vertical reaction at support $O$ is	
	(A) $0.0 \text{ kN}$ (B) $2.5 \text{ kN}$ (C)	7.5 kN (D) 10.0 kN
Ans.	(A)	
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**Sol.** Considering all the reaction in the beam due to loads.



Taking from right hand side of the beam,

$$-R_{\varrho} \times \frac{L}{4} = 0$$
 [Taking anticlockwise (-ve)]  
$$R_{\varrho} = 0$$

#### **Question 19**

As per IRC : 37-2012, in order to control subgrade rutting in flexible pavements, the parameter to be considered is

- (A) Horizontal tensile strain at the bottom of bituminous layer
- (B) Vertical compressive strain on to subgrade
- (C) Vertical compressive stress on top of granular layer
- (D) Vertical deflection at the surface of the pavement

#### Ans. (B)

**Sol.** From IRC : 37-2012 (by rutting model criteria), the two equations are :

Allowable number of load repetitions to control permanent distortion

$$N = 4.1656 \times 10^{-8} \left(\frac{1}{\varepsilon_{\nu}}\right)^{4.5337}$$
$$N = 1.41 \times 10^{-8} \left(\frac{1}{\varepsilon_{\nu}}\right)^{4.5337}$$

where, N = Number of cumulative standard axle

 $\varepsilon_v$  = Vertical subgrade strain

The model considers the vertical strain in subgrade as the only variable for rutting, which is a measure of bearing capacity of the subgrade.

Note :

**Rutting :** It is defined as long deep track made by the repeated moving of the wheels of vehicles. Rutting is the permanent deformation in pavement usually occurring longitudinally along the wheel path.

PAGE 16	GATE 2018 [Afternoon Session] Civil Engineering GATE ACADEMY steps to success			
Questi	on 20			
	The contact pressure and settlement distribution for a footing are shown in the figure.			
	$\bot$			
	[↑↑↑↑↑↑↑↑			
	The figure corresponds to a			
	(A) Rigid footing on granular soil (B) Elevible footing on granular soil			
	(C) Flexible footing on saturated clay (D) Rigid footing on cohesive soil			
Ans.	(A)			
Sol.	From the figure (in question), the contact pressure increases from zero at the edges to maximum at the			
	centre and the settlement is uniform. Therefore, it is the case of rigid footing on granular (sandy) soil.			
	Note :			
	In flexible footing, the contact pressure is same throughout in both granular and cohesive soil. And			
Δυσετί	on 21			
Ancon	Dupuit's assumptions are valid for			
	(A) Artesian aquifer (B) Confined aquifer			
	(C) Leaky aquifer (D) Unconfined aquifer			
Ans.	(D)			
Sol.	Dupuit derived a radial flow solution for unconfined aquifers by neglecting the vertical flow component.			
	He estimated the steady-state head difference between two distances from the pumping well for			
	unconfined aquifers as			
	$h^{2}(r_{2}) - h^{2}(r_{1}) = \frac{Q}{-K} \log\left(\frac{r_{2}}{r_{2}}\right)$			
	where, $h =$ Head, $r_1$ and $r_2 =$ Radial distance from the pumping well			
	Q = Volumetric discharge, K = Hydraulic conductivity.			
	Note : Dupuit's assumptions for unconfined agaifors :			
	<ul> <li>The bottom of the aquifer is a horizontal plane.</li> </ul>			
	<ul> <li>Groundwater flow towards the pumping wells is horizontal with no vertical hydraulic gradient</li> </ul>			
	component.			
	• The horizontal component of the hydraulic gradient is constant with depth and equal to the water table			
	slope.			
	• There is no seepage face at the borehole.			
	These assumptions are one of the main approaches to simplify the unconfined flow problems and making them analytically manageable.			
	More questions and solutions of GATE - 2018 are available in the Facebook group			
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PAGE 17	GATE 2018 [Afternoon Session] Civil Engineering	<b>GATE ACADEMY</b> steps to success
Quest	stion 22	
	A flow net below a dam consists of 24 equipotential drops and	17 flow channels. The difference between
	the upstream and downstream water levels is 6 m. The length	of the flow line adjacent to the toe of the
	dam at exit is 1 m. The specific gravity and void ratio of the	ne soil below the dam are 2.70 and 0.70,
	respectively. The factor of safety against piping is	
	(A) 1.67 (B) 2.5 (C) 3.4	(D) 4
Ans.	(D)	
Sol.	<b>Given :</b> Number of equipotential drops, $N_d = 24$	
	Number of flow channels, $N_f = 7$	
	Difference between upstream and downstream water levels, $H$	= 6 m
	Length of flow line, $l = 1$ m	
	Specific gravity of soil, $G_s = 2.7$	
	Void ratio, $e = 0.7$	
	<b>To find :</b> Factor of safety against piping.	
	From the formula,	
	Factor of safety (FOS) = $\frac{\text{Critical hydraulic gradient}}{\text{Exit gradient}} = \frac{i_{\text{critical}}}{i_{\text{exit}}}$	(i)
	Critical hydraulic gradient, $i_{critical} = \frac{G_s - 1}{1 + e}$	
	$i_{critical} = \frac{2.7 - 1}{1 + 0.7} = \frac{1.7}{1.7} = 1$	E
	Exit gradient, $i_{exit} = \frac{\Delta h}{l}$ ince 20	04
	where, $\Delta h$ = Head loss per drop	
	$\Delta h = \frac{h}{N_d} = \frac{6}{24} = \frac{1}{4} \mathrm{m}$	
	$\therefore \qquad \qquad i_{exit} = \frac{1/4}{1} = \frac{1}{4}$	
	Putting the value of $i_{critical}$ and $i_{exit}$ in equation (i), we get	
	$FOS = \frac{i_{critical}}{i_{exit}} = \frac{1}{1/4} = 4$	



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#### **Question 24**

- The setting of cement is determined by using
- (A) Le Chatelier apparatus
- (C) Vicat apparatus

- (B) Briquette testing apparatus
- (D) Casagrande's apparatus

#### Ans. (C)

**Sol.** Vicat apparatus : It is a device used for determining the setting time (initial and final) of cement and consistency that consists of a rod weighing 300 gm, having a needle at each end, and supported in frame with a graduated scale to measure the distance to which the needle penetrates the cement.

#### **Question 25**

All the members of the planar truss (see figure), have the same properties in terms of area of cross-section (A) and modulus of elasticity (E).



For the loads shown on the truss, the statement that correctly represents the nature of forces in the members of the truss is

- (A) There are 3 members in tension and 2 members in compression
- (B) There are 2 members in tension 1 member in compression and 1 zero-force members
- (C) There are 2 members in tension 1 member in compression and 2 zero-force members
- (D) There are 2 members in tension and 3 members

#### Ans. (D)

**Sol.** Considering all the reactions in the planar truss due to loads.



#### **Calculation of tension members :**

From the figure, only members *AB* and *DC* consists of tension force *P*.

Therefore, AB and DC are the two tension members.

#### Calculation of zero force members :

From the figure, member AD consist of only reaction  $V_D$  i.e., zero. Member BC consist of only reaction

 $V_B$ , which is also zero. Member *BD* having no force, and the member neither expand nor contract, which means it is also zero.

Therefore, AD, BC and BD are the three zero force members.



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#### Q.26 to Q.55 Carry two marks each

#### **Question 26**

A prismatic beam *P*-*Q*-*R* of flexural rigidity  $EI = 1 \times 10^4 \text{ kNm}^2$  is subjected to a moment of 180 kNm at *Q* as shown in the figure.



The rotation at Q (in rad, up to two decimal places) is \_\_\_\_\_

#### Ans. (0.01)

**Sol.** Given : Flexural rigidity,  $EI = 1 \times 10^4 \text{ kNm}^2$ , Moment = 180 kNm

**To find :** Rotation at *Q*.

Step 1 : Fixed end moments

$$M_{FQP} = 0$$
$$M_{FQR} = 0$$

**Step 2 : Slope deflection equations** 

#### For span QP :

[Since, slope  $\theta_p = 0$  as it is fixed end and there is no settlement therefore, deflection  $\Delta = 0$ ].

$$M_{QP} = M_{FQP} + \frac{2EI}{L} \left( \theta_P + 2\theta_Q - \frac{3\Delta}{L} \right)$$
$$M_{QP} = 0 + \frac{2 \times 1 \times 10^4}{5} (0 + 2\theta_Q - 0)$$
$$M_{QP} = \frac{2 \times 10^4}{5} \times 2\theta_Q = 8000 \theta_Q$$

#### For span QR :

[Since, slope  $\theta_R = 0$  as it is fixed end and there is no settlement therefore, deflection  $\Delta = 0$ ].

$$M_{QR} = M_{FQR} + \frac{2EI}{L} \left( \theta_R + 2\theta_Q - \frac{3\Delta}{L} \right)$$
$$M_{QR} = 0 + \frac{2 \times 1 \times 10^4}{4} (0 + 2\theta_Q - 0)$$
$$M_{QR} = \frac{2 \times 10^4}{4} \times 2\theta_Q = 10000 \theta_Q$$



Step 3 : Taking moment about Q

$$\sum M_{\varrho} = 0$$
  

$$M_{\varrho P} + M_{\varrho P} - 180 = 0$$
  

$$8000 \theta_{\varrho} + 10000 \theta_{\varrho} - 180 = 0$$
  

$$18000 \theta_{\varrho} = 180$$
  

$$\theta_{\varrho} = \frac{180}{18000} = 0.01 \text{ rad}$$

[Taking anticlockwise (-ve)]

#### **Question 27**

At a small water treatment plant which has 4 filters, the rates of filtration and backwashing are  $200 \text{ m}^3/\text{dm}^2$  and  $1000 \text{ m}^3/\text{dm}^2$ , respectively. Backwashing is done for 15 min per day. The maturation, which occurs initially as the filter is put back into service after cleaning takes 30 min. It is proposed to recover the being wasted during backwashing and maturation. The percentage increase in the filtered water produced (up to two decimal places) would be \_\_\_\_\_\_.

**Sol.** Given : Number of filters = 4

Rate of filtration  $= 200 \,\mathrm{m}^3/\mathrm{dm}^2$ 

Rate of backwashing  $= 1000 \text{ m}^3/\text{dm}^2$ 

Time of backwashing = 15 min per day =  $\frac{15}{24 \times 60}$  days

Time wasted in maturation = 30 min per day =  $\frac{15}{24 \times 60}$  days

**To find :** Percentage increase in the filtered water produced.

Let the area of filter to be unity i.e.,  $1m^2$ .

Time left after backwashing and maturation =  $24 - \frac{15}{60} - \frac{30}{60} = 23.25$  hours

 $\therefore$  Total quantity of water to be produced =  $200 \times \frac{23.25}{24} = 193.75 \,\text{m}^3$ 

Water used for backwashing =  $1000 \times \frac{15}{24 \times 60} = 10.416 \,\mathrm{m}^3$ 

Water used for maturation =  $200 \times \frac{30}{24 \times 60} = 4.167 \text{ m}^3$ 

Total quantity of water =  $193.75 + 10.416 + 4.167 = 208.33 \text{ m}^3$ 

Percentage increase in the filtered water produced 
$$=\frac{208.33-193.75}{193.75} \times 100 = 7.52\%$$



#### **Question 28**

The matrix  $\begin{pmatrix} 2 & -4 \\ 4 & -2 \end{pmatrix}$  has

- (A) Real eigenvalues and eigenvectors
- (C) Complex eigenvalue but real eigenvectors

 $\begin{bmatrix} 2 & -4 \end{bmatrix}$ 

(B) Real eigenvalue but complex eigenvectors

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(D) Complex eigenvalue and eigenvectors

#### Ans. (D)

Sol.

$$P = \begin{bmatrix} 2 & -1 \\ 4 & -2 \end{bmatrix}$$
$$[P - \lambda I] = 0$$
$$\begin{vmatrix} 2 - \lambda & -4 \\ 4 & -2 - \lambda \end{vmatrix} = 0$$
$$(2 - \lambda)(2 - \lambda) - (-4)(4) = 0$$
$$-4 - 2\lambda + 2\lambda + \lambda^{2} + 16 = 0$$
$$\lambda^{2} + 12 = 0$$

On solving the equation, we get

$$\lambda = +2\sqrt{3}i$$
 and  $\lambda = -2\sqrt{3}i$ 

These are the two complex eigenvalues of the matrix.

**First case :** For  $\lambda = 2\sqrt{3}i$ 

Consider the equation  $(P - \lambda I)X = 0$ .

$$\begin{bmatrix} 2-2\sqrt{3}i & -4\\ 4 & -2-2\sqrt{3}i \end{bmatrix} \begin{bmatrix} x_1\\ x_2 \end{bmatrix} = \begin{bmatrix} 0\\ 0 \end{bmatrix}$$

$$2-2\sqrt{3}ix_1 - 4x_2 = 0$$

$$2-2\sqrt{3}ix_1 = 4x_2$$

$$\frac{x_1}{4} = \frac{x_2}{2-2\sqrt{3}i}$$

$$\begin{bmatrix} x_1\\ x_2 \end{bmatrix} = \begin{bmatrix} 4\\ 2-2\sqrt{3}i \end{bmatrix}$$

This is the first complex eigenvector of the matrix.

**Second case :** For  $\lambda = -2\sqrt{3}i$ 





Consider the equation  $(P - \lambda I)X = 0$ .

$$\begin{bmatrix} 2+2\sqrt{3}i & -4\\ 4 & -2+2\sqrt{3}i \end{bmatrix} \begin{bmatrix} x_1\\ x_2 \end{bmatrix} = \begin{bmatrix} 0\\ 0 \end{bmatrix}$$
$$2+2\sqrt{3}ix_1 - 4x_2 = 0$$
$$2+2\sqrt{3}ix_1 = 4x_2$$
$$\frac{x_1}{4} = \frac{x_2}{2+2\sqrt{3}i}$$
$$\begin{bmatrix} x_1\\ x_2 \end{bmatrix} = \begin{bmatrix} 4\\ 2+2\sqrt{3}i \end{bmatrix}$$

This is the second complex eigenvector of the matrix.

 $\therefore \quad \text{The matrix} \begin{pmatrix} 2 & -4 \\ 4 & -2 \end{pmatrix} \text{ has complex eigenvalues and complex eigenvectors.}$ 

#### Note :

**Eigenvalues :** They are the special set of scalars associated with a matrix (linear transformation) equation, which are sometimes also known as characteristic roots or values.

**Eigenvectors :** They are the non-zero vectors of a matrix (linear transformation) that only changes by scalar factors, when that linear transformation is applied to it, which are sometimes also known as characteristic vectors.

#### **Question 29**

Two rigid bodies of mass 5 kg and 4 kg are at rest on a frictional surface until acted upon by a force of 36 N as shown in the figure. The contact force generated between the two bodies is



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 $\blacktriangleright a \text{ m/s}^2$ 

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(D) 144 m

Applying Newton's second law, by considering both the bodies in a system,

36 N



$$F = m \times a$$
$$a = \frac{F}{m} = \frac{36}{9} = 4 \text{ m/s}^2$$

This calculated acceleration causes a force (F') to move the second body as shown in figure.

т

9 kg



Applying Newton's second law,

$$F' = m_2 \times a$$
$$F' = 4 \times 4 = 16 \text{ N}$$

(D) 72 m

#### **Question 30**

A car follows a slow moving truck (travelling at a speed of 10 m/s) on a two-lane two-way highway. The car reduces its speed to 10 m/s and follows the truck maintaining a distance of 16 m from the truck. On finding a clear gap in the opposing traffic stream, the car accelerates at an average rate of  $4 \text{ m/s}^2$ , overtakes the truck and returns to its original lane. When it returns to its original lane, the distance between the car and the truck is 16 m. The total distance covered by the car during this period (from the time it leaves its lane and subsequently returns to its lane after overtaking) is

(C) 120 m

(A) 64 m (B) 72 m (C) 128 m (D) 144 m  
Ans. (B)  
Sol. Given : Speed of car, 
$$u = 10 \text{ m/s}$$
  
Distance (spacing) between car and truck,  $s = 16 \text{ m}$   
Acceleration of car,  $a = 4 \text{ m/s}^2$   
To find : Total distance covered by the car. 2004  
From second equation of motion,  
Total distance covered by the car  $= uT + \frac{1}{2}aT^2$   
where,  $T = Duration$  (time) of overtaking of car,  $T = \sqrt{\frac{4s}{a}}$   
 $T = \sqrt{\frac{4 \times 16}{4}}$   
 $T = \sqrt{16} = 4 \sec$   
 $\therefore$  Total distance covered by the car  $= uT + \frac{1}{2}aT^2 = 10 \times 4 + \frac{1}{2} \times 4 \times 4^2 = 40 + 32 = 72 \text{ m}.$   
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GATE 2018 [Afternoon Session] Civil Engineering GATE A

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...(ii)

**Sol.** Given : Collapse load,

$$=\frac{\alpha M_p}{L} \qquad \dots (i)$$

**To find :** Value of  $\alpha$ .

С

Consider a propped cantilever beam of span L and plastic moment capacity M is subjected to a concentrated load P at its mid-span.



At the collapse load C, B.M.D. is shown in the above figure. Moments at X and A are equal, each having a value  $M_p$ , the plastic moment of resistance of section.

$$\frac{Cl}{4} = M_P + \frac{M_P}{2}$$
$$\frac{Cl}{4} = 1.5M_P$$

∴ Collapse load,

$$C = \frac{6M_P}{L}$$

Equating equation (i) and (ii), we get

$$\frac{\alpha M_p}{L} = \frac{6M_p}{L}$$
 ince 2004

 $\therefore$  Value of  $\alpha = 6$ .

#### **Question 33**

An 8 m long simply supported elastic beam of rectangular cross-section (100 mm  $\times$  200 mm) is subjected to a uniformly distributed load of 10 kN/m over its entire span. The maximum principal stress (in MPa up to two decimal places) at a point located at the extreme compression edge of a cross-section and at 2 m from the support is \_\_\_\_\_.

Ans. (90)



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**Sol.** Given : Length of beam, l = 6 m

Dimension of beam =  $100 \text{ mm} \times 200 \text{ mm}$ 

Uniformly distributed load, w = 10 kN/m

**To find :** Maximum principal stress at a point located at the extreme compression edge of a cross-section and at 2 m from the support.





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#### **Question 34**

PAGE

28

The compression curve (void ratio, e vs. effective stress,  $\sigma_v$ ) for a certain clayey soil is a straight line in semi-logarithmic plot and it passes through the points ( $e = 1.2, \sigma_v = 50$  kPa) and a  $(e = 0.6, \sigma_v' = 800$  kPa). The compression index (up to two decimal places) of the soil is \_\_\_\_\_. Ans. (0.49) **Given :** Void ratio,  $e_1 = 1.2$  and  $e_2 = 0.6$ Sol. Effective stress,  $(\sigma_v')_1 = 50 \text{ kPa}$  and  $(\sigma_v')_2 = 800 \text{ kPa}$ To find : Compression index of soil.  $(e = 1.2, \sigma' = 50 \text{ kPa})$  $(e = 0.6, \sigma')$ Compression index of soil,  $C_c = \frac{\Delta e}{\Delta \log (\sigma_v')} = \frac{e_1 - e_2}{\log (\sigma_v')_2 - \log (\sigma_v')_1}$  $C_{c} = \frac{e_{1} - e_{2}}{\log\left[\frac{(\sigma_{v}')_{2}}{(\sigma')_{2}}\right]} = \frac{1.2 - 0.6}{\log\left[\frac{800}{50}\right]}$  $C_c = \frac{0.6}{1.2041} = 0.4983$  $C_{c} = 0.49$ *.*..

#### Note :

Compression index : It is defined as the ratio of void ratio to the effective stress in a semi-logarithmic scale. It is an important parameter for evaluation of settlement due to primary settlement of clays.

#### **Question 35**

The Laplace transform F(s) of the exponential function,  $f(t) = e^{at}$  when  $t \ge 0$ , where a is a constant and

(D) ∞

$$(s-a) > 0 \text{ is}$$

$$(A) \frac{1}{s+a} \qquad (B) \frac{1}{s-a} \qquad (C) \frac{1}{a-s}$$



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**Sol.** Given :  $f(t) = e^{at}$ 

**To find :** Laplace transform F(s) of the exponential function.

 $L\{f(t)\} = \int_{0}^{\infty} e^{-st} f(t) dt$   $L\{f(t)\} = \int_{0}^{\infty} e^{-st} e^{at} dt \qquad [t \ge 0]$   $L\{f(t)\} = \int_{0}^{\infty} e^{-(s-a)t} dt \qquad [(s-a)>0]$   $L\{f(t)\} = \left[\frac{e^{-(s-a)t}}{-(s-a)}\right]_{0}^{\infty}$   $L\{f(t)\} = \frac{1}{s-a}(-0+1)$   $\therefore \text{ Laplace transform, } F(s) = \frac{1}{-1}$ 

#### **Question 36**

A flocculation tank contains  $1800 \text{ m}^3$  of water, which is mixed using paddles at an average velocity gradient *G* of 100/s. The water temperature and the corresponding dynamic viscosity are  $30^{\circ}$ C and  $0.798 \times 10^{-3} \text{ Ns/m}^2$ , respectively. The theoretical power required to achieve the stated value of *G* (in kW, up to two decimal places) is \_\_\_\_\_.

#### Ans. (14.364)

**Sol.** Given : Volume of water in flocculation tank,  $V = 1800 \text{ m}^3$ 

Average velocity gradient, G = 100/sec

Temperature of water,  $T = 30^{\circ}$ C

Dynamic viscosity,  $\mu = 0.798 \times 10^{-3} \text{ Ns/m}^2$ 

To find : Theoretical power required to achieve the stated value of G.

Theoretical power,  $P = \mu V G^2$ 

 $P = 0.798 \times 10^{-3} \times 1800 \times 100^{2}$ P = 14364 W = 14.364 kW

#### **Question 37**

The total rainfall in a catchment of area  $1000 \text{ km}^2$ , during a 6-hour storm, is 19 cm. The surface runoff due to this storm computed from triangular direct runoff hydrograph is  $1 \times 10^8 \text{ m}^3$ . The  $\phi$ -index for this storm (in cm/h, up to one decimal place) is \_\_\_\_\_.

#### Ans. (1.5)

**Sol.** Given : Area of catchment,  $A = 1000 \text{ km}^2 = 1000 \times 10^{10} \text{ cm}^2$ 

Total duration of storm, t = 6 hours

Total rainfall (precipitation), P = 19 cm

Surface runoff volume  $= 1 \times 10^8 \text{ m}^3 = 1 \times 10^{14} \text{ cm}^3$ 



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**To find :**  $\phi$ -index for the storm.

Formula for  $\phi$ -index is given by

$$\phi$$
-index =  $\frac{P-R}{t}$ 

where, R = Total surface runoff,  $R = \frac{\text{Surface runoff volume}}{\text{Catchment area}(A)}$ 

$$R = \frac{1 \times 10^{14}}{1000 \times 10^{10}} = 10 \,\mathrm{cm}$$
  
\$\phi\$-index =  $\frac{P - R}{1000}$ 

÷.

$$\phi$$
-index =  $\frac{19-10}{6}$  = 1.5 cm/h

Note :

**\$\phi-index :** It is defined as the rate of infiltration above which the rainfall volume equals runoff volume.

*W*-index: It is the average infiltration rate during the time when the rainfall intensity exceeds the infiltration rate.

#### **Question 38**

A 6 m long simply supported beam is prestressed as shown in the figure.



The beam carries a uniformly distributed load of 6 kN/m over its entire span. If the effective flexural rigidity  $EI = 2 \times 10^4$  kNm<sup>2</sup> and the effective prestressing force is 200 kN, the net increase in length of the prestressing cable (in mm, up to two decimal places) is \_\_\_\_\_.

#### Ans. (0.12)

Sol. Given : Length of beam, L = 6 m = 6000 mm Uniformly distributed load, w = 6 kN/m Effective flexural rigidity,  $EI = 2 \times 10^4$  kNm<sup>2</sup> =  $2 \times 10^4 \times 1000$  N  $\times 1000^2$  mm<sup>2</sup> =  $2 \times 10^{13}$  Nmm<sup>2</sup> Effective prestressing force, P = 200 kN =  $200 \times 10^3$  N Eccentricity, e = 50 mm To find : Net increase in length of the prestressing cable. Here, two cases arise. Case I : We have to find slope due to prestressing force. M- $\theta_1$ - $\theta_2$ - $\theta_3$ - $\theta_4$ - $\theta_4$ - $\theta_3$ - $\theta_4$ -

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Slope due to prestressing force,  $\theta_1 = \frac{PeL}{2EI}$ 

$$\theta_{1} = \frac{200 \times 10^{3} \times 50 \times 6000}{2 \times 2 \times 10^{13}}$$
$$\theta_{1} = \frac{5 \times 3}{10^{4}} = 1.5 \times 10^{-3}$$

Value of  $\theta_1$  is negative due to upward movement.

Case II : Similarly, we have to find slope due to uniformly distributed load.



#### B.M.D. due to uniformly distributed load

Slope due to uniformly distributed load,  $\theta_2 = \frac{1}{24} \frac{wL^3}{FL}$ 

$$\theta_2 = \frac{1}{4} \times \frac{6^3}{2 \times 10^4} = 2.7 \times 10^{-3}$$

Value of  $\theta_2$  is positive due to downward movement.

Now, net slope of the beam,  $\theta = \theta_1 + \theta_2$ 

$$\theta = -1.5 \times 10^{-3} + 2.7 \times 10^{-3} = 1.2 \times 10^{-3}$$

Net increase in length of the prestressing cable  $= 2 \times \text{Eccentricity} \times \text{Net slope of beam}$ 

$$=2\times e^{2} e^{2} \theta$$

 $= 2 \times 50 \times 1.2 \times 10^{-3} = 0.12 \,\mathrm{mm}$ 

#### **Question 39**

A rough pipe of 0.5 m diameter, 300 m length and roughness height of 0.25 mm, carries water (kinematic viscosity  $= 0.9 \times 10^{-6} \text{ m}^2/\text{s}$ ) with velocity of 3 m/s. Friction factor (*f*) for laminar flow is given by

 $f = 64 / R_e$ , and for turbulent flow it is given by  $\frac{1}{\sqrt{f}} = 2\log_{10}\left(\frac{r}{k}\right) + 1.74$  where,  $R_e$  = Reynolds number,

r = radius of pipe, k = roughness height and  $g = 9.81 \text{ m/s}^2$ . The head loss (in m, up to three decimal places) in the pipe due to friction is \_\_\_\_\_.

Ans. (4.596)

**Sol.** Given : Diameter of rough pipe, D = 0.5 m, length of pipe, L = 300 m

Roughness height of pipe,  $k = 0.25 \text{ mm} = 0.25 \times 10^{-3} \text{ m}$ 

Kinematic viscosity of water,  $v = 0.9 \times 10^{-6} \text{ m}^2/\text{s}$ 

Velocity of water, V = 3 m/s, Acceleration due to gravity, g = 9.81 m/s<sup>2</sup>

To find : Head loss in the pipe due to friction.

Formula for Reynolds number is given by

$$R_e = \frac{VD}{\upsilon}$$



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$$R_e = \frac{3 \times 0.5}{0.9 \times 10^{-6}} = 1.67 \times 10^6$$

We know that Reynolds number, if greater than 2000 then, the flow is said to be turbulent. Here,  $R_e > 2000$ . Therefore, the flow is turbulent.

So, friction factor for turbulent flow is given by the following equation :

 $\frac{1}{\sqrt{f}} = 2\log_{10}\left(\frac{0.25}{0.25 \times 10^{-3}}\right) + 1.74$ 

$$\frac{1}{\sqrt{f}} = 2\log_{10}\left(\frac{r}{k}\right) + 1.74$$
 [Given in question]

where, r = Radius of rough pipe,  $r = \frac{0.5}{2} = 0.25 \text{ m}$ 

Then,

$$\frac{1}{\sqrt{f}} = 6 + 1.74$$
$$\sqrt{f} = \frac{1}{7.74}$$
$$f = \left(\frac{1}{7.74}\right)^2 = 0.0167$$

Head loss in the pipe due to friction,  $h_f = \frac{fLV^2}{2gD}$ 

$$h_f = \frac{0.0167 \times 300 \times 3^2}{2 \times 9.81 \times 0.5} = 4.596 \,\mathrm{m}$$

#### **Question 40**

Three soil specimens (Soil 1, Soil 2, and Soil 3), each 150 mm long and 100 mm diameter are placed in series in a constant head flow set-up as shown in the figure. Suitable screens are provided at the boundaries of the specimens to keep them intact. The values of coefficient of permeability of soil 1, soil 2, and soil 3 are 0.01, 0.003 and 0.03 cm/s respectively.



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Ans.



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Given : Length of all three soil specimens = 150 mm Sol. Diameter of all three soil specimens = 100 mm

Coefficient of permeability of soil 1,  $K_1 = 0.01$  cm/s

Coefficient of permeability of soil 2,  $K_2 = 0.003$  cm/s

Coefficient of permeability of soil 3,  $K_3 = 0.03$  cm/s

Total head loss,  $h_L = 560 \,\mathrm{mm}$ 

**To find :** Value of *h* in the setup.

Since, it is given that all the three soil specimens are placed in series in a constant head flow, the discharge in each specimen is equal.

$$Q_{1} = Q_{2} = Q_{3}$$

$$K_{1}i_{1}A = K_{2}i_{2}A = K_{3}i_{3}A$$

$$K_{1}\frac{h_{1}}{L}A = K_{2}\frac{h_{2}}{L}A = K_{3}\frac{h_{3}}{L}A$$

where,  $h_1$ ,  $h_2$  and  $h_3$  are the head loss of soil 1, 2 and 3. Length and area is same of all the three soil specimens.

$$\therefore \qquad K_{1}h_{1} = K_{2}h_{2} = K_{3}h_{3} = t$$

$$h_{1} = \frac{t}{0.01}, h_{2} = \frac{t}{0.003} \text{ and } h_{3} = \frac{t}{0.03}$$

$$h_{1} + h_{2} + h_{3} = h_{L}$$

$$\frac{t}{0.01} + \frac{t}{0.003} + \frac{t}{0.03} = 560$$

$$t = 1.2$$
Value of  $h_{1} = \frac{t}{0.01} = \frac{1.2}{0.01} = 120 \text{ mm}$ 
Value of  $h_{2} = \frac{t}{0.003} = \frac{1.2}{0.003} = 400 \text{ mm}$ 
Value of  $h_{3} = \frac{t}{0.03} = \frac{1.2}{0.03} = 400 \text{ mm}$ 
Value of  $h_{3} = \frac{t}{0.03} = \frac{1.2}{0.03} = 400 \text{ mm}$ 
Value of  $h_{3} = \frac{t}{0.03} = \frac{1.2}{0.03} = 400 \text{ mm}$ 
Value of  $h_{3} = \frac{t}{0.03} = \frac{1.2}{0.03} = 400 \text{ mm}$ 
Value of  $h_{4} = \frac{t}{0.03} = \frac{1.2}{0.03} = 400 \text{ mm}$ 
Value of  $h_{5} = \frac{t}{0.03} = \frac{1.2}{0.03} = 400 \text{ mm}$ 
Value of  $h_{1} = \frac{t}{0.03} = 560 - (120 + 400)$ 

$$= 560 - 520 = 40 \text{ mm}$$
Question 41
A level instrument at a height of 1.320 m has been placed at a station having a Reduced Level (RL) of 112.565 m. The instrument reads  $-2.835 \text{ m}$  on a levelling staff held at the bottom of a bridge deck. The RL (in m) of the bottom of the bridge deck is
(A) 116.720
(B) 116.080
(C) 114.080
(D) 111.050



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**To find :** Force in the bolt *P*.



Force in the bolt due to direct load,  $F_1 = \frac{P}{r}$ 

$$F_1 = \frac{130}{4} = 32.5 \,\mathrm{kN}$$

Force in the bolt due to moment *M*,

$$F_2 = \frac{P \times e \times r_P}{\sum r_i^2}$$

where,  $r_p$  = Distance of bolt *P* from the C.G.,  $r_p = \sqrt{50^2 + 120^2}$ 

$$r_p = \sqrt{16900} = 130 \,\mathrm{mm}$$

Since, bolts *P*, *Q*, *R* and *S* are at equal distances from the C.G.

*.*..

$$r_P = r_Q = r_R = r_S = 130 \,\mathrm{mm}$$
$$r_i = 130^2$$

Then,

And

$$\sum r_i^2 = 4 \times 130^2 = 67600$$

$$F_2 = \frac{130 \times 200 \times 130}{67600} = 50 \text{ kN}$$

$$\cos \theta = \frac{50}{130} = 0.3846$$

Resultant force,  $F_R = \sqrt{F_1^2 + F_2^2 + 2F_1F_2\cos\theta}$ 

$$F_R = \sqrt{32.5^2 + 50^2 + 2 \times 32.5 \times 50 \cos(0.3846)}$$
$$F_R = \sqrt{4806.2} = 69.32 \,\text{kN}$$

Therefore, force in the bolt P = 69.32 kN.

PAGE 36	GAT	E 2018 [Afternoon Session] Civil Engineering	G A T E Since 2004	GATE ACADEMY steps to success
Questi	ion 43			
	An aerial pho	tograph of a terrain having an average elev	vation of 1400	m is taken at a scale of 1 : 7500.
	The focal length of the camera is 15 cm. The altitude of the flight above mean sea level (in m, up to one			
	decimal place	e) is		
Ans.	(2525)			
Sol.	Given : Aver	age elevation, $h = 1400$ m		
	Scale of photo	ograph = 1:7500		
	Focal length of	of camera, $f = 15 \text{ cm} = 0.15 \text{ m}$		
	To find : Alti	itude of the flight above mean sea level.	ТМ	
	Formula of sc	cale of photograph is given by		
		Scale = $\frac{\text{Focal length}}{\text{Altitude} - \text{Average elevation}}$		
		Scale = $\frac{f}{H-h}$		
	Altitude,	$H = \frac{f}{\text{Scale}} + h$		
		$H = \frac{0.15}{1/7500} + 1400$		
		$H = 1125 + 1400 = 2525 \mathrm{m}$		
Questi	ion 44			
	The value (up to two decimal places) of line integral $\int_c \vec{F}(\vec{r}) \cdot d\vec{r}$ , for $\vec{F}(\vec{r}) = x^2 \hat{i} + y^2 \hat{j}$ along C which is a			
	straight line j	oining (0, 0) to (1, 1) is		
Ans.	(0.67)	Cinco 2		Л
Sol.	<b>Given</b> : $\vec{F}(\vec{r})$	$y = x^2 \hat{i} + y^2 \hat{j}$		4
	Coordinates of straight line = $(0, 0)$ to $(1, 1)$			
	To find : Val	ue of line integral $\int_c \vec{F}(\vec{r}) \cdot d\vec{r}$ .		
		$\vec{F}(\vec{r}) = x^2\hat{i} + y^2\hat{j}$		
	Value of $d\vec{r}$ =	$= dx\hat{i} + dy\hat{j}$		
		$\vec{F}(\vec{r}) \cdot d\vec{r} = \left(x^2\hat{i} + y^2\hat{j}\right) \times \left(dx\hat{i} + dy\hat{j}\right)$		
	$\vec{F}(\vec{r}) \cdot d\vec{r} = x^2 dx + y^2 dy$			
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Integrating both sides and integrating right side equation from (0, 1),

 $\int_{C} \vec{F}(\vec{r}) \cdot d\vec{r} = \int_{0}^{1} x^{2} dx + y^{2} dy$  $\int_{C} \vec{F}(\vec{r}) \cdot d\vec{r} = \int_{0}^{1} x^{2} dx + \int_{0}^{1} y^{2} dy$  $\int_{C} \vec{F}(\vec{r}) \cdot d\vec{r} = \left[\frac{x^{3}}{3}\right]_{0}^{1} + \left[\frac{y^{3}}{3}\right]_{0}^{1}$  $\int_{C} \vec{F}(\vec{r}) \cdot d\vec{r} = \frac{1}{3} + \frac{1}{3}$  $\int_{C} \vec{F}(\vec{r}) \cdot d\vec{r} = \frac{2}{3} = 0.67$ 

#### **Question 45**

A 7.5 m wide two-lane road on a plain terrain is to be laid along a horizontal curve of radius 510 m. For a design speed of 100 kmph, super-elevation is provided as per IRC : 73-1980. Consider acceleration due to gravity as  $9.81 \text{ m/s}^2$ . The level difference between the inner and outer edges of the road (in m, up to three decimal places) is \_\_\_\_\_.

#### Ans. (0.525)

**Sol.** Given : Width of two-lane road, B = 7.5 m

Radius of horizontal curve, R = 510 m

Design speed, V = 100 kmph

Acceleration due to gravity,  $g = 9.81 \text{ m/s}^2$ 

To find : Level difference between the inner and outer edges of the road.

Super-elevation required on horizontal curves should be calculated from the following formula. This assumes that centrifugal force corresponding to  $(3/4^{th})$  the design speed is balanced by super-elevation and rest counteracted by side friction :

$$e = \frac{V^2}{225R}$$

For plain and rolling terrain, value of super-elevation is limited to 7%.

$$e = \frac{100^2}{225 \times 510} = 0.0871 > 0.07$$

Level difference between the inner and outer edges of the road,  $h = e \times B$ 

 $h = 0.07 \times 7.5 = 0.525 \,\mathrm{m}$ 







# PAGE<br/>41GATE 2018 [Afternoon Session]<br/>Civil Engineering $\int_{Since 2004}^{\infty}$ GATE ACAD<br/>Seteps to sulter<br/>steps to sulter<br/>steps to sulterSol.Given : Percentage of sulfur in unburned coal (initial amount) = 2%<br/>Rate of burning = 30 kg/min<br/>Percentage of sulfur in cash = 6% of the initial amount of sulfur<br/>Molecular weight of sulfur (S) = 3.2 gm/mole<br/>Hydrogen (H) = 2 gm/mole<br/>Oxygen (O) = 16 gm/molegm/mole<br/>To find : Annual rate of sulfur oxide (SO2) emission.

Coal burned in one year = 30 kg/min × 24 hours × 60 minutes × 365 days =1.5768×10<sup>7</sup> kg/year =1.5768×10<sup>4</sup> tons/year Sulfur content (in unburnt coal) =  $\frac{2}{100}$ ×1.5768×10<sup>4</sup> = 315.36 tons/year

Sulfur content (in ash) =  $\frac{6}{100} \times 315.36 = 18.92$  tons/year

 $\therefore$  Sulfur converted to SO<sub>2</sub> = 315.36 - 18.92 = 296.44 tons/year

From the chemical formula,

$$S + O_2 \rightarrow SO_2$$

1 mole of S is present in 1 mole of  $SO_2$ .

Molecular weight of S = 32 gm/mole

Then, molecular weight of  $SO_2 = 32 + (16 \times 2) = 64 \text{ gm}$ 

 $\therefore$  32 gm of S is present in 64 gm of SO<sub>2</sub>

Then, rate of SO<sub>2</sub> emission =  $\frac{64 \text{ gm of } \text{SO}_2}{32 \text{ gm of } \text{S}} \times \text{Sulfur converted to SO}_2$ 

$$=\frac{64}{32} \times 296.44 = 592.88$$
 tons/year

#### **Question 51**

In a 5 m wide rectangular channel, the velocity distribution in the vertical direction y is given by  $u = 1.25 y^{1/6}$ . The distance y is measured from the channel bed. If the flow depth is 2 m, the discharge per unit width of the channel is

(A) 
$$2.40 \text{ m}^3/\text{s/m}$$
 (B)  $2.80 \text{ m}^3/\text{s/m}$  (C)  $3.27 \text{ m}^3/\text{s/m}$  (D)  $12.02 \text{ m}^3/\text{s/m}$ 

#### Ans. (A)

**Sol.** Given : Width of rectangular channel, b = 5 m

Flow depth, d = 2 m

To find : Discharge per unit width of the channel.





GATE 2018 [Afternoon Session] PAGE **Civil Engineering** 43 **Given :** Number of piles, n = 9 (3×3 square pattern) Sol. Perimeter of an individual pile = 126 cm = 1.26 mSize of pile group =  $240 \text{ cm} \times 240 \text{ cm} = 2.4 \text{ m} \times 2.4 \text{ m}$ Undrained shear strength of clay, S = 15 kPa Unit weight of clay,  $\gamma = 16 \text{ kN/m}^3$ Negative frictional load acting on the pile group,  $Q_{nf} = SLP + AL\gamma$ where, P = Perimeter of the pile group, P = 4B $P = 4 \times 2.4 = 9.6 \,\mathrm{m}$ For recently filled clay, L = 2 mA = Area of the pile group,  $A = 2.4 \times 2.4 = 5.76 \text{ m}^2$  $Q_{nf} = SLP + AL\gamma$  $Q_{nf} = 15 \times 2 \times 9.6 + 5.76 \times 2 \times 16$  $Q_{nf} = 288 + 184.32 = 472.32 \,\mathrm{kN}$ **Question 53** The rank of the following matrix is :  $\begin{pmatrix} 1 & 1 & 0 & -2 \\ 2 & 0 & 2 & 2 \\ 4 & 1 & 3 & 1 \end{pmatrix}$ (B) 2 (A) 1 **(B)** Ans.  $P = \begin{pmatrix} 1 & 1 & 0 & -2 \\ 2 & 0 & 2 & 2 \\ A & 1 & 2 & 1 \end{pmatrix}$ Sol.

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#### **Question 54**

A schematic flow diagram of a completely mixed biological reactor with provision for recycling of solids is shown in the figure.



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PAGE 44



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Putting all the required values in equation (i), we get

MCRT = 
$$\frac{XV}{Q_w X_u} = \frac{3000 \times 1250}{50 \times 10000}$$
  
MCRT =  $\frac{375}{50} = 7.5$  days

Note :

**MCRT**: The mean cell residence time or MCRT is the amount of time (in days) in which solids or bacteria are maintained in the activated sludge system. The MCRT is also known as the solids retention time (SRT).

#### **Question 55**

The total horizontal and vertical stresses at point X in a saturated sandy medium are 170 kPa and 300 kPa respectively. The static pore-water pressure is 30 kPa. At failure, the excess pore-water pressure is measured to be 94.50 kPa, and the shear stresses on the vertical and horizontal planes passing through the point X are zero. Effective cohesion is 0 kPa and effective angle of internal friction is  $36^{\circ}$ . The shear strength (in kPa, up to two decimal places) at point X is \_\_\_\_\_.

#### Ans. (52.52)





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An angle  $(\alpha)$  is made, when shear failure occurs on a plane, with respect to horizontal.

$$\alpha = 45^{\circ} + \frac{\phi}{2} = 45^{\circ} + \frac{36^{\circ}}{2} = 63^{\circ}$$

Total pore water pressure = (Static + Excess) pore water pressure

= 30 + 94.5 = 124.5 kPa  $\sigma'_{3} = \sigma_{3} - \text{ Total pore water pressure}$   $\sigma'_{3} = 170 - 124.5 = 45.5 \text{ kPa}$   $\sigma'_{1} = \sigma_{1} - \text{ Total pore water pressure}$   $\sigma'_{1} = 300 - 124.5 = 175.5 \text{ kPa}$ Effective normal stress,  $\sigma' = \frac{\sigma'_{1} + \sigma'_{3}}{2} + \frac{\sigma'_{1} - \sigma'_{3}}{2} \cos 2\alpha$   $\sigma' = \frac{175.5 + 45.5}{2} + \frac{175.5 - 45.5}{2} \cos (2 \times 63^{\circ})$   $\sigma' = 110.5 - 65 \times 0.5877 = 72.29 \text{ kPa}$ 

Shear strength at point  $X = C' + \sigma' \tan \phi$ 

 $= 0 + 72.29 \times \tan 36^{\circ} = 52.52 \text{ N/mm}^{2}$ 

\*\*\*\*

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