

Vibration related Formulas

Frequency and Period:

- Frequency = $1/\text{Period} = \frac{1}{T} \frac{\text{Cycles}}{\text{Second}}$ or Hz
- Period = $T = \frac{\text{Second}}{\text{Cycle}}$

Data Sampling:

- $T_{max} \text{ (no overlap)} = \frac{(60)(\#FFT \text{ Lines})}{F_{max} \text{ (CPM)}} = \frac{(60)(\text{Sample Size})}{(2.56)(F_{max})}$
- $T_{max} \text{ (sec) (with overlap)} = \frac{(60)(\#FFT \text{ Lines})}{F_{max} \text{ (CPM)}} + ((\text{NO. Samples with overlap}) * (1 - \text{overlap \%})) * \frac{(60)(\#FFT \text{ Lines})}{F_{max} \text{ (CPM)}}$
- $\# \text{ Revolutions} = \frac{(\#FFT \text{ Lines})(RPM)}{F_{max}}$
- $F_{max} \text{ (CPM)} = \frac{(\#FFT \text{ Lines})(RPM)}{\#Revolutions}$

Where:

- F_{max} = Maximum Spectral Frequency (CPM)
- T_{max} = Sampling period in sec to capture one data sample
- Revolutions = # Revolutions captured in the Time Domain. # Revolutions controlled by Accurex bases on component speed.
- Sample Size = Number of Analog to Digital Conversions used to construct the Time Waveform.

| #Lines | #Samples |
|--------|----------|
| 100 | 256 |
| 200 | 512 |
| 400 | 1024 |
| 800 | 2048 |
| 1600 | 4096 |
| 3200 | 8192 |
| 6400 | 16,384 |
| 12,800 | 32,768 |

Data Sampling Examples:

Accurex LF Spectrum: 800 lines with an Fmax of 12,000 cpm.

Collection time (one sample): $T_{max} = \frac{(60)(800)}{12,000} = 4$ seconds

Collection time 4 samples with 75% overlap:

$$T_{max} = \frac{(60)(800)}{12,000} + ((3*(1-.75)) * \frac{(60)(800)}{12,000})$$

$$= 4 + 3 = 7 \text{ seconds}$$

Accurex constructed Time Waveform # Revolutions:

Whereas revolutions are equal to:

revolutions = (#Signal Points X CPM)/(Sampling Frequency in CPM)

Example:

revolutions = (128,000 X 120)/(600,000 X 2.56)

revolutions = 15,360,000/1,536,000

revolutions = 10

| Shaft Speed RPM | Sampling Frequency | FMax | # Signal Points | Shaft Revolutions in Waveform | Time for 1 Sample (sec.) | Resolution (cpm) |
|--------------------|-----------------------|---------------|--------------------|----------------------------------|-----------------------------|---------------------|
| < 59 | 25.6k Hz | 600,000 CPM | 512k | 19.6 or less | 20 | 1.17 |
| 59-117 | 25.6k Hz | 600,000 CPM | 256k | 9.83-19.5 | 10 | 2.34 |
| 118-120 | 25.6k Hz | 600,000 CPM | 128k | 9.83-10.0 | 5 | 4.7 |
| 121-234 | 51.2k Hz | 1,200,000 CPM | 256k | 10.083-19.5 | 5 | 4.7 |
| 235-468 | 51.2k Hz | 1,200,000 CPM | 128k | 9.79-19.5 | 2.5 | 9.4 |
| 469-899 | 51.2k Hz | 1,200,000 CPM | 64k | 9.77-18.179 | 1.25 | 18.75 |
| 900-1899 | 51.2k Hz | 1,200,000 CPM | 32k | 9.375-19.78 | .625 | 37.5 |
| 1900-3999 | 51.2k Hz | 1,200,000 CPM | 16k | 9.9-20.83 | .3125 | 75 |
| 4000-7500 | 51.2k Hz | 1,200,000 CPM | 8k | 10.42-19.53 | .1563 | 150 |
| >7500 | 51.2k Hz | 1,200,000 CPM | 4k | 9.77 or greater | .078 | 300 |
| | | | | | | |
| Eagle | | | | | | |
| | | | | | | |
| 469-899 | 12.8k Hz | 300,000 CPM | 16K | 9.77-18.179 | 1.25 | 18.75 |
| 900-1899 | 25.6k Hz | 600,000 CPM | 16K | 9.375-19.78 | .625 | 37.5 |
| 1900-3999 | 25.6k Hz | 600,000 CPM | 8K | 9.9-20.83 | .3125 | 75 |
| | | | | | | |

$$\text{Vibration Amplitude} = \frac{\text{Dynamic Force}}{\text{Dynamic Resistance}}$$

RMS vs Peak vs Peak-to-Peak:

- Peak-to-Peak Vibration = 2 times Peak Vibration
- Peak Vibration = 0.5 X Peak-to-Peak Vibration
- Peak Vibration = 1.414 X RMS Vibration
- RMS Vibration = .707 X Peak Vibration

CPM/Hz Conversion:

- $\text{CPM} = \text{Hz} * 60$
- $\text{Hz} = \frac{\text{CPM}}{60}$

Frequency Resolution, Bandwidth, Separating Frequency

- Frequency Resolution = $\frac{\text{Frequency Span}}{\# \text{ FFT Lines}}$
- Separating Frequency (difference between two frequencies to be identified) = $\geq 2 * \text{Frequency Resolution} * \text{Window Noise Factor}$
- Required #FFT Lines = $\frac{2 * \text{Window Noise Factor} * \text{Frequency Span}}{\text{Separating Frequency}}$

Where:

- Window Noise Factor =
 - 1.0 for Uniform or Rectangular Window
 - 1.5 for Hanning Window (Used in Data Collection)

Approximates of Rolling Element Bearing Defect Frequencies

- Approx BPFI = $(N_b/2 + 1.2) \times \text{RPM}$
- Approx BPFO = $(N_b/2 - 1.2) \times \text{RPM}$
- Approx BSF = $\frac{1}{2}(N_b/2 - 1.2/N_b) \times \text{RPM}$
- Approx FTF = $(1/2 - 1.2/N_b) \times \text{RPM}$

Where: N_b = Number of Rolling Elements

Blade Pass Frequency:

- BPF = # Blades * RPM

Gear Mesh Frequency:

- # Gear Teeth * # Gear RPM

Induction Motors:

- N_s = Synchronous Speed = $\frac{120 Fl}{Poles}$
- F_s = Slip Frequency = $N_s - \text{RPM (Actual)}$
- F_p = Pole Pass Frequency = $F_s * \#Poles$
- RBPF = Rotor Bar Pass Frequency = #Rotor Bars * RPM
- F_l = Line Frequency

Belt Frequencies:

Flat or V Belt:

- Belt Speed = $\frac{3.142 * \text{Pulley RPM} * \text{Pulley Pitch Diameter}}{\text{Belt Length}}$

Timing Belt Frequency:

- Pulley RPM * # Pulley Teeth

dB Conversions:

Calculate dB from ratio:

- $20\text{Log}(\text{ratio}) = \text{dB}$

Calculate ratio from dB:

- $10^{(\text{dB}/20)} = \text{Ratio}$