

**DRAINAGE REPORT
GENESSEE PROPERTIES, INC.
SOCIETY TURN PARCEL
SAN MIGUEL COUNTY, COLORADO**

June 30,2022

Prepared for:
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TABLE OF CONTENTS

| SECTION | PAGE |
|--|------|
| 1. INTRODUCTION | 2 |
| 2. HISTORIC DRAINAGE SYSTEM | 2 |
| 3. PROPOSED DRAINAGE SYSTEMS | 3 |
| 4. CONCLUSIONS | 6 |
| 5. CERTIFICATION | 6 |
| 6. REFERENCES | 7 |
| 7. SOFTWARE | 7 |
| APPENDICES | |
| APPENDIX A – SITE MAP | |
| APPENDIX B – NRCS SOILS AND NOAA 14 RAINFALL DATA | |
| APPENDIX C – FEMA FIRMETTE | |
| APPENDIX D.1 – Pre-Developed Conditions Calculations | |
| APPENDIX D.2 – DEVELOPED CONDITIONS CALCULATIONS | |
| APPENDIX E – DRAINAGE PLANS AND DETAILS | |

1. INTRODUCTION

This drainage study was prepared as part of the sketch plan Site Development application for the Society Turn Parcel in San Miguel County, Colorado. This report generally follows the requirements of the San Miguel County Land Use Code, Section 4-302G and Section 5-502AA.

Section 2 of this report discusses the historic hydrologic conditions on the site. Section 3 addresses the developed hydrologic analysis used in sizing detention structures within the project area. Section 4 provides conclusions about the potential impacts of development to the site. The remaining sections provide certification and references employed in the report preparation.

- A. Site Location** - The Society Turn Parcel is in the San Miguel River valley, approximately 3 miles west of the Town of Telluride (see Figure 1 below). It is southwest of the Society Turn intersection (round-about), with Highway 145 on the north and east sides, and Society Drive to the south. The Society Turn Parcel is on mostly gently-sloping terrain that sits on the north side of the San Miguel Valley at the base of a steep slope, which is the toe of Deep Creek Mesa.



Figure1. Google© image of the Society Turn Parcel (outlined in red)

- B. Site Vegetation** - The site is generally cleared but remaining vegetation consists of native grasses, shrubs and scattered elm and cottonwood trees. The areas near the San Miguel River and Remine Creek that are intended to remain as open spaces have concentrations of willows and other wetland plants adjacent to the waterways.
- C. Adjacent Development** – The site is bounded to the south by developed commercial sites and undeveloped land. To the north and east, the parcel is bounded by State Highway 145. The western boundary of the property is bounded by vacant land
- D. Site Description** - The site generally slopes at an average of 1.0% from north to south at elevations from 8712 to 8650 feet above MSL. It is on an elevated terrace of the San Miguel River and has two man-made irrigation ditches crossing the property that are currently in use. The San Miguel River bisects the parcel and flows from east to west at a low gradient. Remine Creek is located on the western portion of the parcel and flows from north to south to its confluence with the San Miguel River. No other water courses are located within 500 feet of the property.
- E. Site Soils** - The project area has been mapped by the NRCS on their Web Soil Survey (WSS) online site to contain two soil units. They are the Cryaquolls-Borochemists complex which covers approximately 19% of the parcel along the San Miguel River corridor and the Cryoborolls-Cryaquolls association which covers the remaining 81% of the project site. Both of these units are classified as Hydrologic Soil Group (HSG) type B soils, which indicates moderately well drained soil with a moderate infiltration rate and low runoff potential. The site is characterized by storm water sheet flows across the entire portion of the site from north to south towards the San Miguel River. Drainage plans for the site are presented in Appendix E of this report. Detailed soil information is presented in Appendix B of this report.
- F. Existing Drainage Facilities** - There are two existing irrigation ditches which generally run from north to south in the western portions of the site. The ditches convey water from the north side of Highway 145 through corrugated metal pipe (CMP) culverts to the elevated portion of the site to provide irrigation for pasture grass. The upper portion of the project site is used seasonally for cattle grazing.
- G. Project Description** – The proposed development of the Society Turn Parcel is a mixed-use phased development of commercial and residential buildings with associated infrastructure improvements including roads, sanitary sewer, water, dry utilities and storm drain systems. Approximately 5.63 acres of the site will be dedicated to open space parks and recreation areas and will remain undeveloped. Domestic water will be supplied by the Town of Telluride under an existing “will serve” agreement with the developer, Genesee Properties, Inc. Sanitary sewer services will also be provided by the Town of Telluride under a service connection agreement.

H. Relevant Flood Hazard and Drainage Studies – The project area is contained on FEMA FIRM panel 08113C0286-C and the San Miguel River channel is located in a FEMA flood Zone A, which indicates that detailed hydraulic analyses have not been performed and that no base flood elevations or depths are shown on the FEMA floodplain maps for this area. The Flood Insurance Study (FIS) for San Miguel County, issued on September 30, 1992, includes the project area. A FIRMette of the project site is included in Appendix C.

2. HISTORIC DRAINAGE SYSTEM

This section of the report reviews the historic or pre-developed conditions on the project site. Historic flows for the site are limited to the 17.61-acre extent of the Society Turn property and are characterized by sheet flows over the vegetated, low sloping terrain from north and south towards the San Miguel River drainage. The pre-developed flows for 10 and 100-year storm events were calculated using the Modified FAA-Rational Method spreadsheet from the USDCM Volume 2 Storage Chapter. The UDFCM Rational Method spreadsheet was used to calculate historic flows for the site. These flows were estimated to be 1.7 cfs for the 10-year storm and 18.96 cfs for the 100-year event assuming 2% impervious cover for undeveloped land. Historic flow patterns for the site are shown on Sheet DR-1 in Appendix E of this report.

3. PROPOSED DRAINAGE SYSTEM

A. Criteria - In order to calculate the required detention storage for the proposed Society Turn development, the following design criteria and assumptions were used:

- Average basin slope = 1.0%
- 12-hour drain time was used due to low runoff type soils (HSG B) as reported by the NRCS-WSS
- Rational Method was used for hydrologic analysis
- Design storms of 10-year, 1-hour (0.773 inches) and 100-year, 1-hour (1.44 inches) were used for analysis using information from the NOAA Atlas Volume 14
- Developed weighted runoff coefficients for 10-yr. and 100-yr return periods were calculated using the UD-Rational workbook
- Infiltration rate of 10 minutes per inch for site soils – HSG = B

B. Hydrologic Data The current NOAA Atlas 14 was consulted for calculations of rainfall depth, intensity, and frequency-duration for the interval storms. The NOAA 14 IDF data for Telluride, Colorado (Station ID 05-8204) with a 90% confidence interval was used for our analysis and is presented in Appendix B.

| RETURN PERIOD | 1-HR TOTAL PRECIPITATION (IN) |
|---------------|-------------------------------|
| 2-year | 0.517 |
| 5-year | 0.641 |
| 10-year | 0.773 |
| 25-year | 0.998 |
| 50-year | 1.21 |
| 100-year | 1.44 |

Table 1. Summary of NOAA Atlas 14 precipitation data for 60-minute duration precipitation events varying recurrence periods in Telluride, CO. Shaded values were used for design and drainage analyses in this report.

| Return Period | 5-min. | 10-min. | 15-min. | 30-min. | 1-hr. | 2-hr. | 3-hr. | 6-hr. | 24-hr. |
|---------------|--------|---------|---------|---------|-------|-------|-------|-------|--------|
| 2-yr | 0.185 | 0.271 | 0.330 | 0.424 | 0.517 | 0.609 | 0.685 | 0.883 | 1.55 |
| 5-yr | 0.234 | 0.342 | 0.418 | 0.535 | 0.641 | 0.747 | 0.832 | 1.07 | 1.87 |
| 10-yr | 0.286 | 0.419 | 0.511 | 0.653 | 0.773 | 0.893 | 0.983 | 1.24 | 2.15 |
| 25-yr | 0.375 | 0.549 | 0.670 | 0.855 | 0.998 | 1.14 | 1.23 | 1.52 | 2.57 |
| 50-yr | 0.457 | 0.670 | 0.817 | 1.04 | 1.21 | 1.37 | 1.46 | 1.75 | 2.91 |
| 100-yr | 0.552 | 0.808 | 0.985 | 1.26 | 1.44 | 1.63 | 1.71 | 2.02 | 3.26 |

Table 2. Summary of NOAA 14 Intensity-Duration-Frequency values for the project site. Rainfall intensity is given in inches per hour

C. Runoff

The developed flow rates for the project area were calculated using the Rational Method as described in Volume 1 of the USDCM. Peak developed runoff flows for the 10-year and 100-year design storms are 9.10 cfs and 19.34 cfs respectively for the portion of the development (Basin #3). Detailed calculation results for pre-developed and developed conditions are presented in Appendices D.1 and D.2 of this report. Developed flow patterns are presented on Sheet DR-2 in Appendix E of this report. Historically, storm drainage has been intercepted by permeable site soils and transmitted in shallow sheet flow across the site from north to south towards the San Miguel River. Developed flows will be drained into storm drains on the side of project roads and designated detention basins and underground detention structures and allowed to percolate naturally into the soils. Field percolation tests performed by Buckhorn Engineering staff during the geotechnical investigation for the project indicate rates of approximately 10 minutes per inch. Storm flows will percolate into the underlying alluvial soil within the prescribed time per Colorado Revised Statutes (CRS) section 37-92-602(8).

The Society Turn parcel was divided into seven (7) drainage basins labeled Basins #1 through Basin #7. Table 3 details those basins' runoff and detention

Society Turn Parcel – Preliminary Plan
 Drainage Report
 San Miguel County, Colorado

calculations. These basins are presented in exhibit DR-2 in Appendix E of this report. Detailed calculation worksheets for each basin are presented in Appendices D.1 and D.2 of this report.

| Phase 2 Basin ID | Drainage Area (Acres) | 10-yr. 1-hr. Runoff (cfs) | 100-yr. 1- hr. Runoff (cfs) | Required 10-yr. Detention Volume (cu. ft.) | Required 100-yr. Detention Volume (cu. ft.) |
|-----------------------------|--------------------------------------|--|--|---|--|
| Basin #1 | 2.06 | 0.20 | 2.22 | None | None |
| Basin #2 | 4.18 | 5.60 | 11.89 | 5,880 | 6,969 |
| Basin #3 | 6.80 | 9.10 | 19.34 | 6,640 | 7,455 |
| Basin #4 | 0.52 | 0.70 | 1.48 | 740 | 830 |
| Basin #5 | 0.48 | 0.64 | 1.37 | 873 | 1045 |
| Basin #6 | 1.80 | 0.17 | 1.94 | None | None |
| Basin #7 | 1.77 | 0.19 | 2.15 | None | None |
| Totals | 17.61 | - | - | 16,421 | 16,654 |

Table 3. Phased Runoff and Retention Values. Weighted c (10-yr) = 0.44, weighted c (100-yr) = 0.55), i (10-yr) = 0.994, i (100-yr) = 1.71. Basins 1, 6 and 7, with no required detention, are to remain as open space and will drain as they have historically towards the San Miguel River.

| Phase 2 Basin ID | Drainage Basin Area (Acres) | Required 100-yr. Detention Volume (cu. ft.) | Provided 100-yr. Detention Volume (cu. ft.) |
|-----------------------------|--|--|--|
| Basin #1 | 2.06 | None | None |
| Basin #2 | 4.18 | 6,969 | 7,088 |
| Basin #3 | 6.80 | 7,455 | 7,623 |
| Basin #4 | 0.52 | 830 | 856 |
| Basin #5 | 0.48 | 1,045 | 1,087 |
| Basin #6 | 1.80 | None | None |
| Basin #7 | 1.77 | None | None |
| Totals | 17.61 | 16,299 | 16,654 |

Table 4. Summary of proposed 100-year retention volume per sub-basin. Provided retention volume is a combination of infiltration trenches and retention ponds.

B. Roads

The majority of rooftop flows will be contained in landscaping at or near the building. The majority of surface storm flows will be from sidewalks, driveways, parking lots and roadways. Those flows will be conveyed in storm drains to detention basins and underground detention structures as described in Section C above. Storm flows will sheet flow from the crown of roads curbs and gutters on both sides of Road B and to distributed detention areas that double as snow storage sites in the winter.

C. Open Channel Flow

Open channel flows through landscaped drainage swales are proposed for the site development to convey flows to designated detention basins and/or underground detention structures. All storm runoff will be routed on the surface to detention facilities as outlined in Section C above. The existing drainage ditches, located in the western portion of the project site, will be graded over in Phase 1 of the proposed development. Vertical curbs with gutters are proposed for project roads. Gutter capacity and curb opening capacity calculations are as follows:

$$\text{Eq. 1} \quad Q = \{0.56/n\} S_x^{5/3} S^{1/2} T^{8/3}$$

Where: Manning's n = 0.013
 Road/Gutter Cross-slope (S_x) = 2%
 Road Longitudinal slope (S) = 0.5%
 Flow width (T) = 18 inches

Therefore: Q = 0.013 cfs for gutter flow rate

Eq. 2 $Q_i = 2.3(L+1.8W_o)d^{1.5}$

Where: Opening length (L) = 1.5 feet
Curb opening width (W_o) = 0.5 feet
Depth of Flow (d) = 0.5 feet

Therefore: $Q_i = 1.95$ cfs

Drainage swales are proposed to convey storm flow from curb openings to adjacent roadway inlets or detention facilities. Calculations for the triangular drainage swales using Manning's equation are:

Eq. 3 $Q = V/A$

$$V = k/n[A/P]^{2/3}S^{1/2}$$

Where: $n = 0.025$
Side slopes = 2H:1V
Longitudinal Slope (S) = 0.01 ft/ft
Flow depth = 1 foot

Solving for velocity and discharge (Q)

Q - 9.51 cfs, $v = 3.48$ ft/sec.

D. Storm Sewers and Culverts

Storm drain inlets along Road B will convey storm flows in 18-inch diameter ADS storm drain pipe to designated outlets at the detention basin and underground detention structures as outlined on Sheet DR-2 in Appendix E. Storm drain systems will be constructed during the initial phase of development to provide storm drainage for the entire project site.

E. Detention Basins and Structures

As shown on Sheet DR-2 in Appendix E, a combination of one above grade detention basin and four (4) underground ADS storm detention structures are proposed to detain storm flows and release them at historic drainage rates. Use of the below grade ADS detention structures will allow parking areas and roadways to be constructed on grade and still provide adequate detention storage. Figure 2. below presents a typical ADS detention structure.

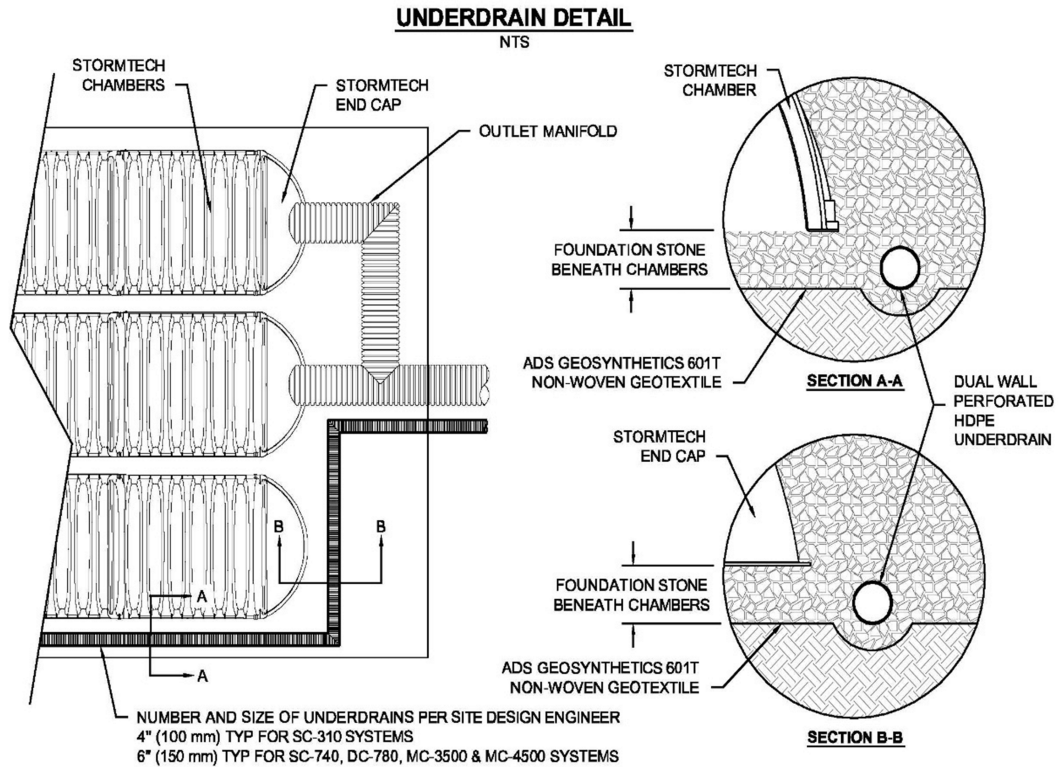


Figure 2. Typical underdrain detail of ADS Stormtech® detention structure

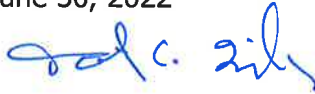
4. CONCLUSION

The proposed development of the Society Turn parcel has been designed in consideration of retaining storm flows on site as required by San Miguel County Land Use Code, Section 4-302G and Section 5-502AA. Drainage will be conveyed by both subsurface storm drains and surface means across the roadways, parking areas and impervious areas to subsurface detention structures or detention basins.

5. REPORT CERTIFICATION

I, Daniel C. Quigley, a duly registered professional engineer in the State of Colorado, (registration #38334), have prepared this report, related documents, and supervised the preparation of the drawings enclosed. The information included is, to the best of my knowledge, accurate and conforming to the requirements of the San Miguel County Land Use Code and current practices for the preparation of drainage reports.

June 30, 2022



Daniel C. Quigley, P.E.
Project Engineer

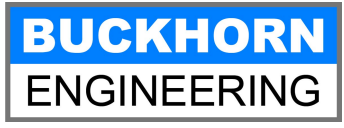


6. REFERENCES

- Urban Drainage and Flood Control District (UDFCD) Criteria Manual, Volumes 1-3, March 2017
- Flood Insurance Study, San Miguel County, September 30, 1992
- NOAA Atlas 14, Volume 8, 2013
- Mays, Larry W., Stormwater Collections Systems Design Handbook, McGraw-Hill, 2001

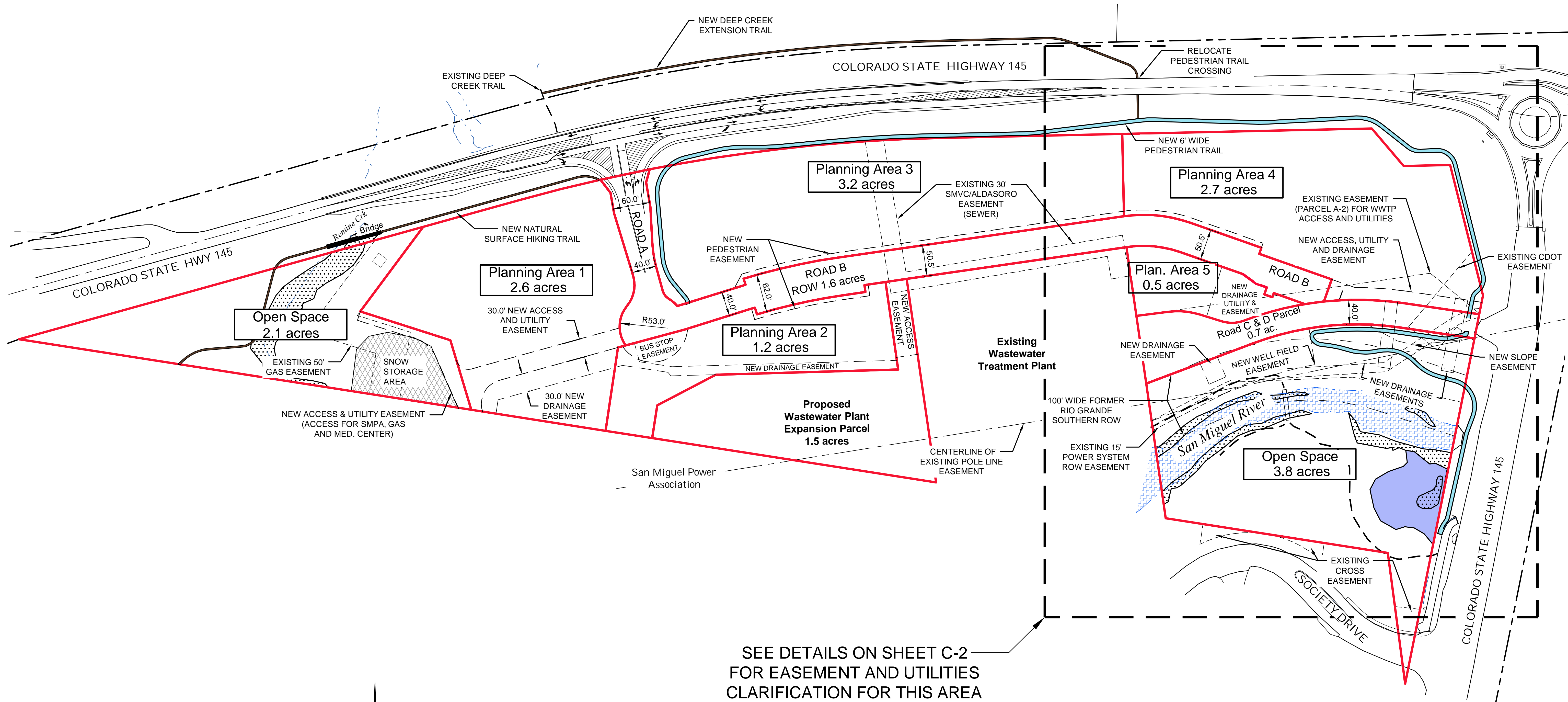
7. SOFTWARE

- UDFCD Detention calculator, v. 3.07, February 2017
- UDFCD Rational calculator, V 2.00, May 2017

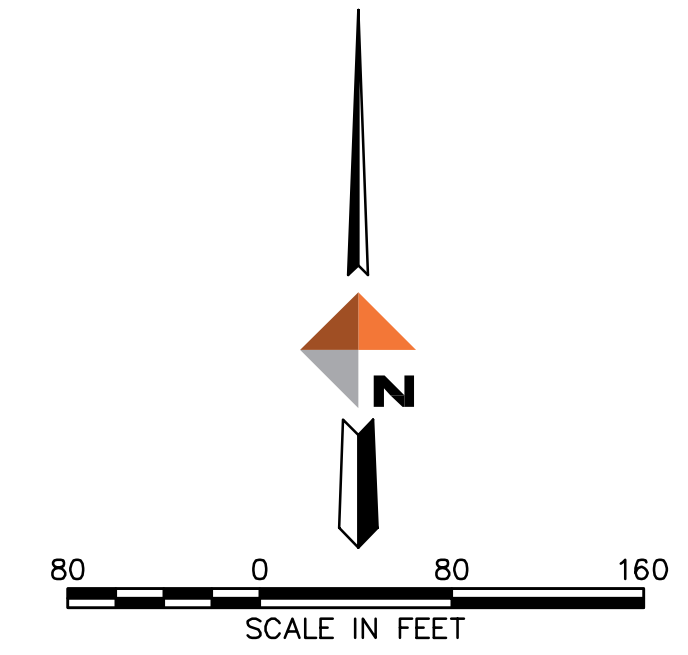


APPENDIX A
SITE PLAN

G:\22\74614-01\65CAD\Civil\Dwg2-Sketch Plan\SC1-Sketch Plan-Site Plans.dwg PLOT DATE 2020-07-27 08:19 SAVED DATE 2020-07-21 08:37 USER: dcastillo



SEE DETAILS ON SHEET C-2 FOR EASEMENT AND UTILITIES CLARIFICATION FOR THIS AREA



| REVISIONS | | | |
|-----------|------|-------------|----|
| REV | DATE | DESCRIPTION | BY |
| | | | |
| | | | |
| | | | |
| | | | |

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 Montrose, Colorado 81401
 970-249-6828

GENESSEE PROPERTIES, INC.
 SOCIETY TURN PARCEL SKETCH PLAN
 GENERAL SITE PLAN

PROJECT 7122-74614
 DATE 07/21/2020

SHEET
C-1
 2 OF 11



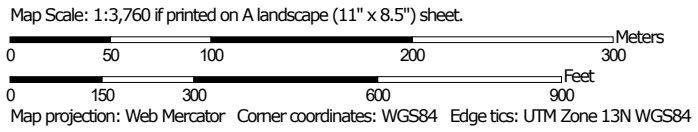
APPENDIX B

NRCS SOILS AND NOAA 14 RAINFALL DATA

Soil Map—Ouray Area, Colorado, Parts of Gunnison, Hinsdale, Ouray, San Juan, and San Miguel Counties
(Society Turn Parcel - Soils Map)




Soil Map may not be valid at this scale.



MAP LEGEND

Area of Interest (AOI)

 Area of Interest (AOI)

Soils

 Soil Map Unit Polygons

 Soil Map Unit Lines

 Soil Map Unit Points

Special Point Features



Blowout



Borrow Pit



Clay Spot



Closed Depression



Gravel Pit



Gravelly Spot



Landfill



Lava Flow



Marsh or swamp



Mine or Quarry



Miscellaneous Water



Perennial Water



Rock Outcrop



Saline Spot



Sandy Spot



Severely Eroded Spot



Sinkhole



Slide or Slip



Sodic Spot



Spoil Area



Stony Spot



Very Stony Spot



Wet Spot



Other



Special Line Features

Water Features



Streams and Canals

Transportation



Rails



Interstate Highways



US Routes



Major Roads



Local Roads

Background



Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service
Web Soil Survey URL:
Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Ouray Area, Colorado, Parts of Gunnison, Hinsdale, Ouray, San Juan, and San Miguel Counties
Survey Area Data: Version 12, Jun 10, 2020

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Nov 26, 2010—Oct 13, 2017

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

| Map Unit Symbol | Map Unit Name | Acres in AOI | Percent of AOI |
|------------------------------------|--|--------------|----------------|
| 109 | Cryaquolls-Borochemists complex, 0 to 5 percent slopes | 6.2 | 18.9% |
| 111 | Cryoborolls-Cryaquolls association, 0 to 15 percent slopes | 26.8 | 81.1% |
| Totals for Area of Interest | | 33.0 | 100.0% |

**NOAA Atlas 14, Volume 8, Version 2
TELLURIDE 4WNW
Station ID: 05-8204**



Location name: Telluride, Colorado, USA*
Latitude: 37.9492°, Longitude: -107.8733°
Elevation:
Elevation (station metadata): 8672 ft**



* source: ESRI Maps
** source: USGS

POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Deborah Martin, Sandra Pavlovic, Ishani Roy, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Michael Yekta, Geoffery Bonnin

NOAA, National Weather Service, Silver Spring, Maryland

[PF tabular](#) | [PF graphical](#) | [Maps & aeriels](#)

PF tabular

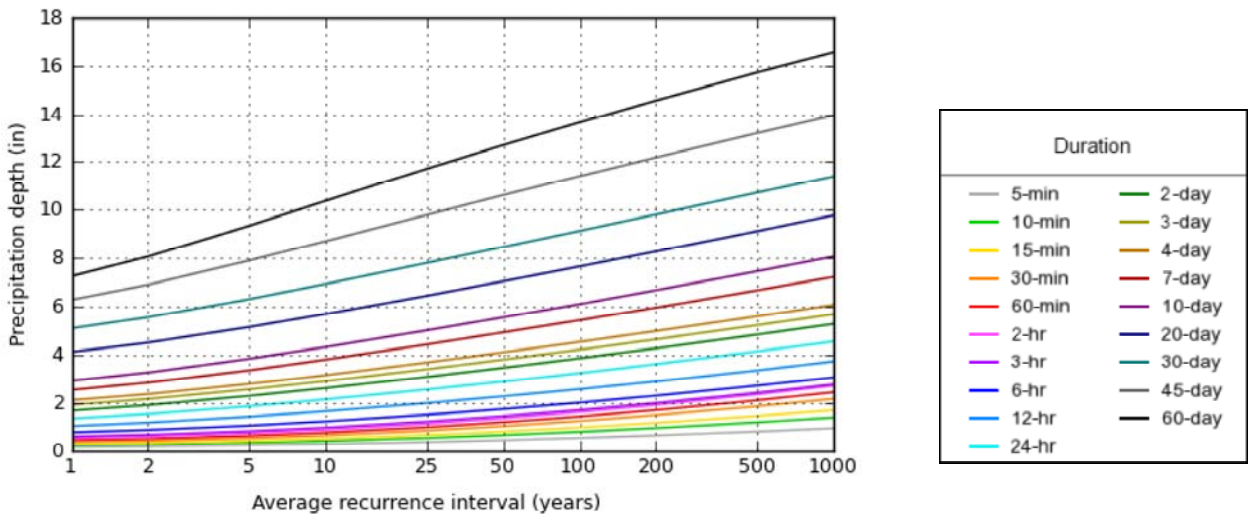
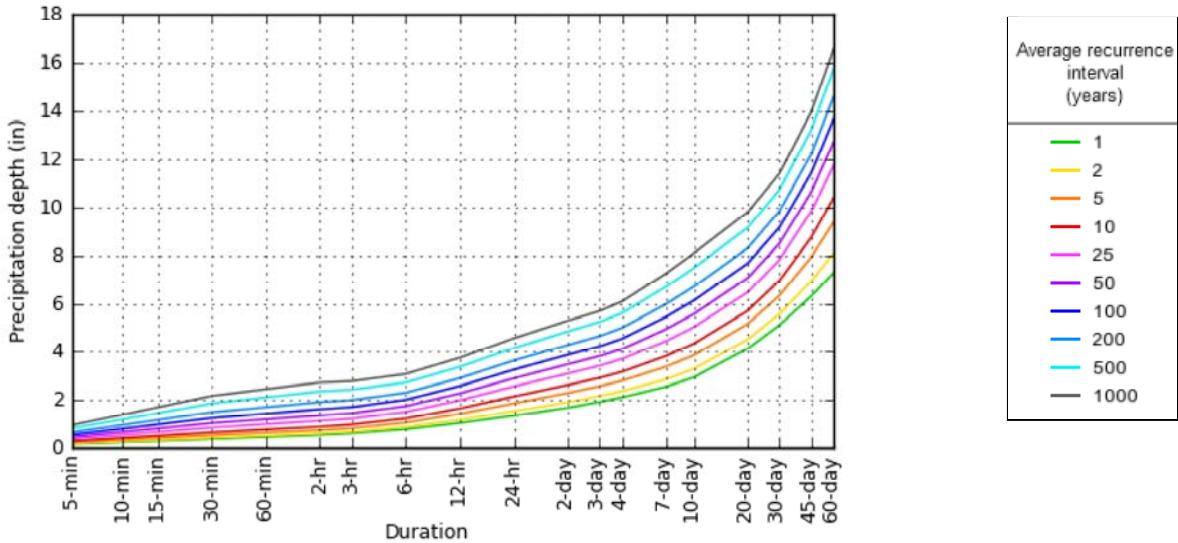
| PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches)¹ | | | | | | | | | | |
|--|--|------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|-----------------------|-----------------------|
| Duration | Average recurrence interval (years) | | | | | | | | | |
| | 1 | 2 | 5 | 10 | 25 | 50 | 100 | 200 | 500 | 1000 |
| 5-min | 0.162 (0.143-0.195) | 0.185 (0.162-0.223) | 0.234 (0.204-0.282) | 0.286 (0.247-0.347) | 0.375 (0.315-0.491) | 0.457 (0.366-0.600) | 0.552 (0.417-0.740) | 0.659 (0.466-0.905) | 0.820 (0.545-1.15) | 0.956 (0.605-1.34) |
| 10-min | 0.238 (0.209-0.286) | 0.271 (0.237-0.326) | 0.342 (0.298-0.413) | 0.419 (0.362-0.508) | 0.549 (0.461-0.719) | 0.670 (0.536-0.879) | 0.808 (0.610-1.08) | 0.965 (0.682-1.33) | 1.20 (0.798-1.69) | 1.40 (0.886-1.96) |
| 15-min | 0.290 (0.255-0.349) | 0.330 (0.289-0.398) | 0.418 (0.364-0.504) | 0.511 (0.441-0.619) | 0.670 (0.562-0.877) | 0.817 (0.654-1.07) | 0.985 (0.744-1.32) | 1.18 (0.832-1.62) | 1.46 (0.973-2.06) | 1.71 (1.08-2.39) |
| 30-min | 0.374 (0.328-0.450) | 0.424 (0.372-0.511) | 0.535 (0.466-0.646) | 0.653 (0.564-0.792) | 0.855 (0.717-1.12) | 1.04 (0.834-1.37) | 1.26 (0.949-1.69) | 1.50 (1.06-2.06) | 1.87 (1.24-2.63) | 2.18 (1.38-3.05) |
| 60-min | 0.459 (0.403-0.553) | 0.517 (0.452-0.622) | 0.641 (0.558-0.774) | 0.773 (0.667-0.938) | 0.998 (0.836-1.30) | 1.21 (0.963-1.58) | 1.44 (1.09-1.93) | 1.71 (1.21-2.35) | 2.12 (1.41-2.97) | 2.46 (1.55-3.44) |
| 2-hr | 0.544 (0.480-0.649) | 0.609 (0.536-0.727) | 0.747 (0.655-0.894) | 0.893 (0.776-1.07) | 1.14 (0.962-1.47) | 1.37 (1.10-1.77) | 1.63 (1.24-2.16) | 1.92 (1.37-2.61) | 2.36 (1.59-3.29) | 2.73 (1.75-3.80) |
| 3-hr | 0.613 (0.543-0.727) | 0.685 (0.605-0.813) | 0.832 (0.731-0.991) | 0.983 (0.857-1.18) | 1.23 (1.04-1.57) | 1.46 (1.18-1.87) | 1.71 (1.31-2.25) | 2.00 (1.44-2.70) | 2.43 (1.65-3.36) | 2.79 (1.80-3.86) |
| 6-hr | 0.787 (0.701-0.926) | 0.883 (0.786-1.04) | 1.07 (0.942-1.26) | 1.24 (1.09-1.47) | 1.52 (1.28-1.90) | 1.75 (1.43-2.22) | 2.02 (1.56-2.61) | 2.31 (1.67-3.07) | 2.73 (1.87-3.73) | 3.08 (2.02-4.23) |
| 12-hr | 1.05 (0.940-1.22) | 1.19 (1.06-1.39) | 1.44 (1.28-1.68) | 1.66 (1.47-1.95) | 2.00 (1.69-2.46) | 2.28 (1.86-2.84) | 2.58 (2.01-3.30) | 2.91 (2.13-3.82) | 3.37 (2.33-4.55) | 3.75 (2.49-5.10) |
| 24-hr | 1.36 (1.22-1.57) | 1.55 (1.39-1.79) | 1.87 (1.68-2.17) | 2.15 (1.91-2.51) | 2.57 (2.18-3.11) | 2.91 (2.39-3.57) | 3.26 (2.55-4.11) | 3.63 (2.68-4.71) | 4.15 (2.90-5.54) | 4.57 (3.07-6.17) |
| 2-day | 1.69 (1.53-1.94) | 1.92 (1.74-2.20) | 2.30 (2.07-2.64) | 2.63 (2.35-3.04) | 3.10 (2.65-3.72) | 3.48 (2.88-4.23) | 3.87 (3.06-4.83) | 4.28 (3.19-5.49) | 4.85 (3.43-6.40) | 5.29 (3.60-7.08) |
| 3-day | 1.93 (1.76-2.20) | 2.17 (1.97-2.48) | 2.58 (2.33-2.95) | 2.93 (2.62-3.36) | 3.42 (2.94-4.07) | 3.82 (3.18-4.61) | 4.22 (3.36-5.24) | 4.65 (3.49-5.93) | 5.23 (3.73-6.87) | 5.69 (3.91-7.59) |
| 4-day | 2.12 (1.93-2.40) | 2.38 (2.16-2.70) | 2.81 (2.54-3.20) | 3.17 (2.86-3.63) | 3.70 (3.19-4.38) | 4.12 (3.44-4.95) | 4.55 (3.63-5.61) | 4.99 (3.76-6.34) | 5.60 (4.01-7.33) | 6.08 (4.20-8.08) |
| 7-day | 2.55 (2.34-2.88) | 2.86 (2.62-3.23) | 3.38 (3.08-3.82) | 3.82 (3.45-4.34) | 4.44 (3.85-5.22) | 4.93 (4.15-5.89) | 5.44 (4.37-6.66) | 5.97 (4.54-7.52) | 6.68 (4.84-8.68) | 7.23 (5.06-9.55) |
| 10-day | 2.94 (2.71-3.30) | 3.28 (3.02-3.68) | 3.85 (3.52-4.33) | 4.34 (3.93-4.90) | 5.02 (4.37-5.87) | 5.56 (4.70-6.60) | 6.11 (4.94-7.45) | 6.69 (5.12-8.39) | 7.46 (5.44-9.65) | 8.07 (5.68-10.6) |
| 20-day | 4.13 (3.82-4.59) | 4.52 (4.17-5.02) | 5.16 (4.74-5.75) | 5.70 (5.20-6.38) | 6.46 (5.67-7.46) | 7.05 (6.01-8.28) | 7.66 (6.26-9.24) | 8.28 (6.42-10.3) | 9.13 (6.74-11.7) | 9.78 (6.99-12.7) |
| 30-day | 5.10 (4.74-5.64) | 5.56 (5.16-6.15) | 6.32 (5.83-7.00) | 6.94 (6.37-7.73) | 7.80 (6.87-8.95) | 8.47 (7.26-9.88) | 9.14 (7.50-10.9) | 9.81 (7.66-12.1) | 10.7 (7.97-13.6) | 11.4 (8.21-14.8) |
| 45-day | 6.29 (5.86-6.91) | 6.91 (6.43-7.60) | 7.90 (7.33-8.71) | 8.71 (8.02-9.65) | 9.79 (8.65-11.1) | 10.6 (9.12-12.3) | 11.4 (9.41-13.6) | 12.2 (9.56-14.9) | 13.2 (9.89-16.7) | 13.9 (10.1-18.0) |
| 60-day | 7.26 (6.78-7.94) | 8.07 (7.53-8.84) | 9.35 (8.69-10.3) | 10.4 (9.57-11.4) | 11.7 (10.4-13.3) | 12.7 (10.9-14.6) | 13.6 (11.3-16.1) | 14.6 (11.5-17.7) | 15.7 (11.8-19.7) | 16.5 (12.1-21.3) |

¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS). Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

[Back to Top](#)

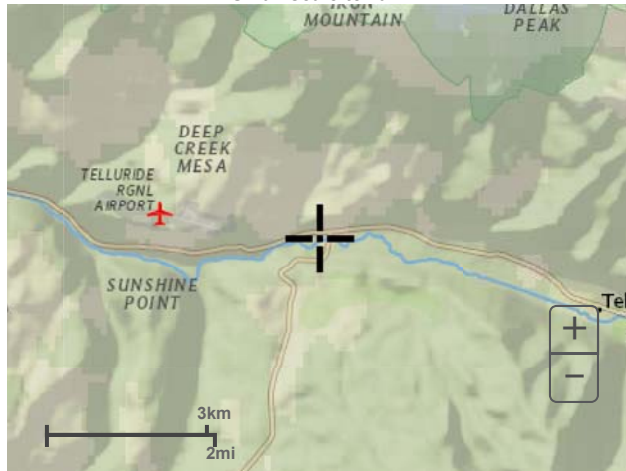
PF graphical

PDS-based depth-duration-frequency (DDF) curves
 Latitude: 37.9492°, Longitude: -107.8733°



Maps & aerals

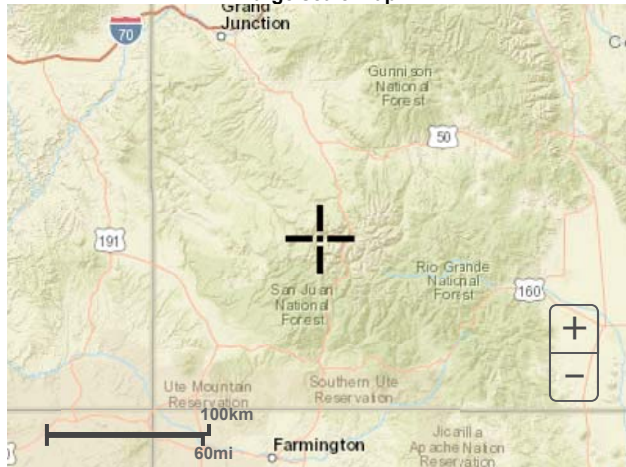
Small scale terrain

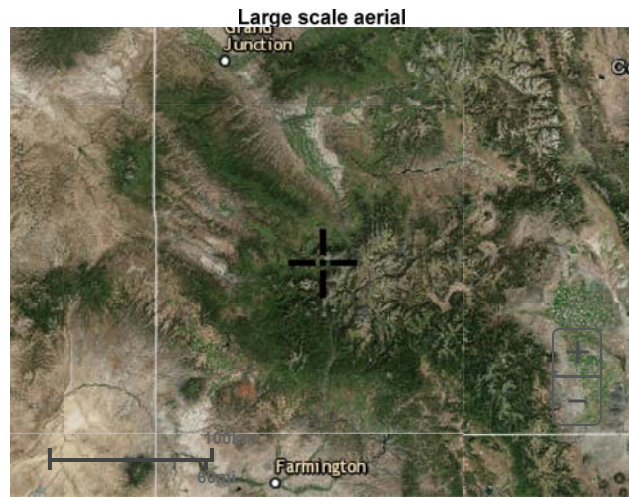


Large scale terrain



Large scale map

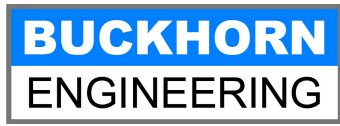




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APPENDIX C
FEMA Firmette



APPENDIX D.1
PRE-DEVELOPED CONDITIONS
CALCULATIONS

Area-Weighted Runoff Coefficient Calculations

Version 2.00 released May 2017

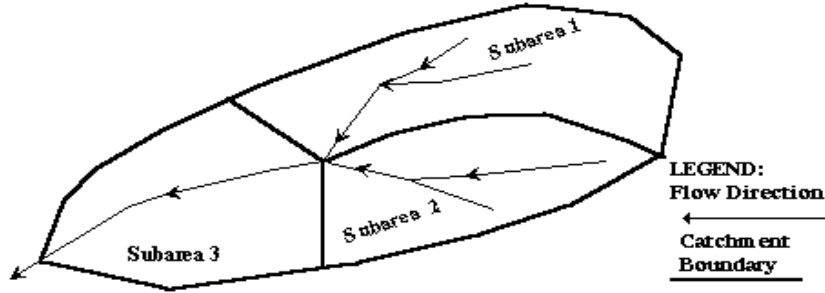
Designer: D. Quigley

Company: DOWL

Date: 8/24/2020

Project: Society Turn - Pre-Developed Conditions

Location: Telluride



| |
|--------------------------|
| Subcatchment Name |
| Society Turn |

| |
|---|
| Cells of this color are for required user-input |
| Cells of this color are for optional override values |
| Cells of this color are for calculated results based on overrides |

See sheet "Design Info" for imperviousness-based runoff coefficient values.

| Sub-Area ID | Area (ac) | NRCS Hydrologic Soil Group | Percent Imperviousness | Runoff Coefficient, C | | | | | | |
|------------------------|--------------|---------------------------------|------------------------|-----------------------|-------------|-------------|-------------|-------------|-------------|-------------|
| | | | | 2-yr | 5-yr | 10-yr | 25-yr | 50-yr | 100-yr | 500-yr |
| Society Trun Parcel | 17.61 | B | 2.0 | 0.01 | 0.01 | 0.07 | 0.26 | 0.34 | 0.44 | 0.54 |
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| Total Area (ac) | 17.61 | | | 0.01 | 0.01 | 0.07 | 0.26 | 0.34 | 0.44 | 0.54 |
| | | Area-Weighted C | | 0.01 | 0.01 | 0.07 | 0.26 | 0.34 | 0.44 | 0.54 |
| | | Area-Weighted Override C | | 0.01 | 0.01 | 0.07 | 0.26 | 0.34 | 0.44 | 0.54 |

Length-Weighted Slope Calculations

Version 2.00 released May 2017

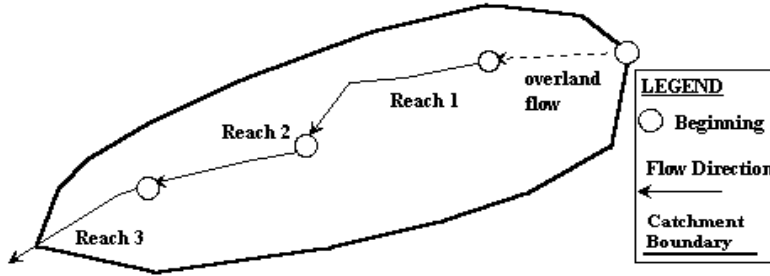
Designer: D. Quigley

Company: DOWL

Date: 8/24/2020

Project: Society Turn - Pre-Developed Conditions

Location: Telluride



| Subcatchment Name | Percent Imperviousness (%) |
|-------------------|----------------------------|
| Society Turn Pre | 2 |

OVERLAND FLOW

| Reach ID | Overland Flow Length L_i (ft) | U/S Elevation (ft) <i>(Optional)</i> | D/S Elevation (ft) <i>(Optional)</i> | Overland Flow Slope S_i (ft/ft) |
|-----------------------------------|---------------------------------|---|---|-----------------------------------|
| Society Turn | 300.00 | | | 0.100 |
| | | | | |
| | | | | |
| | | | | |
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| | | | | |
| | | | | |
| | | | | |
| Total Overland Length (ft) | | 300.00 | Length-Weighted Slope (ft/ft) | 0.100 |

CHANNELIZED FLOW

| Reach ID | Channelized Flow Length L_i (ft) | U/S Elevation (ft) <i>(Optional)</i> | D/S Elevation (ft) <i>(Optional)</i> | Channelized Flow Slope S_i (ft/ft) |
|--------------------------------------|------------------------------------|---|---|--------------------------------------|
| | | | | |
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| | | | | |
| Total Channelized Length (ft) | | | Length-Weighted Slope (ft/ft) | |

Reach-Weighted Time of Concentration Calculations

Version 2.00 released May 2017

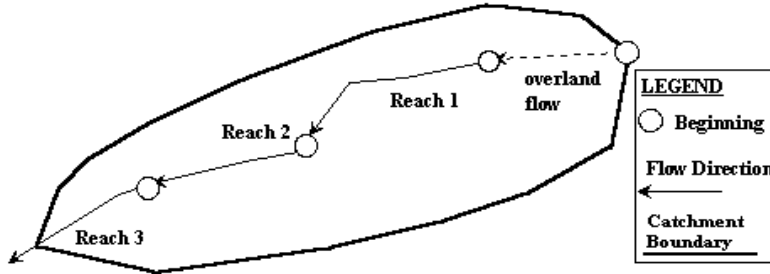
Designer: D. Quigley

Company: DOWL

Date: 8/24/2020

Project: Society Turn - Pre-Developed Conditions

Location: Telluride



| Subcatchment Name | Percent Imperviousness (%) |
|-------------------|----------------------------|
| Society Turn Pre | 2 |

OVERLAND FLOW

| Reach ID | Overland Flow Length L_i (ft) | Overland Flow Slope S_i (ft/ft) | 5-yr Runoff Coefficient, C_s | Overland Flow Time t_i (min) |
|------------------------|---------------------------------|-----------------------------------|--------------------------------|--------------------------------|
| Society Turn Pre | 300.00 | 0.010 | 0.58 | 16.26 |
| | | | | |
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| | | | | |
| | | | | |
| | | | | |
| Weighted Totals | 300.00 | 0.010 | Total t_i (min) | 16.26 |

CHANNELIZED FLOW

| Reach ID | Channelized Flow Length L_i (ft) | Channelized Flow Slope S_i (ft/ft) | NRCS Conveyance Factor K | Channelized Flow Time t_i (min) |
|------------------------|------------------------------------|--------------------------------------|--------------------------|-----------------------------------|
| | | | | |
| | | | | |
| | | | | |
| | | | | |
| | | | | |
| | | | | |
| | | | | |
| Weighted Totals | | | Total t_i (min) | |

| | |
|----------------------|------|
| Computed t_c (min) | 0.00 |
| Regional t_c (min) | |
| Selected t_c (min) | |

APPENDIX D.2
DEVELOPED CONDITION
CALCULATIONS

Calculation of Peak Runoff using Rational Method
 1-hour rainfall depth, P (in) = 0.52 2-yr 0.77 5-yr 1.01 10-yr 1.24 25-yr 1.51 50-yr 1.74 100-yr 1.94 500-yr 2.12
 $I(t/P)^{-0.08}$
 Rainfall Intensity Equations: $I(t/P)^{-0.08}$
 Time of Concentration
 Regional L_c (min) = 2566
 Selected L_c (min) = 1240
 Channelized (Triangular) Flow Time
 Channelized Flow Length L_c (ft) = 0.00
 Channelized Flow Velocity V_c (ft/sec) = 2.00
 NRCs Conversion Factor K_c = 7
 Channelized Flow Time T_c (min) = 0.00
 Overland Flow Length L_o (ft) = 500.00
 Overland Flow Slope S_o (ft/ft) = 0.010
 Overland Flow Time T_o (min) = 43.92
 Total Time of Concentration $T_c + T_o$ = 43.92 min
 Peak Flow Q (cfs) = 0.00

| Subcatchment Name | Area (ac) | Hydrologic Soil Group | Slope (ft/ft) | Runoff Coefficient, C | | | | | | | Overland Flow Length L_o (ft) | Overland Flow Slope S_o (ft/ft) | Overland Flow Time T_o (min) | Channelized Flow Length L_c (ft) | Channelized Flow Velocity V_c (ft/sec) | NRCs Conversion Factor K_c | Channelized Flow Time T_c (min) | US Elevation (ft) (Optional) | US Elevation (ft) (Optional) | Channelized Flow Slope S_c (ft/ft) (Optional) | Regional L_c (min) | Selected L_c (min) | Rainfall Intensity, I (in/hr) | | | | | | |
|-------------------|-----------|-----------------------|---------------|-----------------------|------|-------|-------|-------|--------|--------|---------------------------------|-----------------------------------|--------------------------------|------------------------------------|--|------------------------------|-----------------------------------|------------------------------|------------------------------|---|----------------------|----------------------|-------------------------------|------|-------|-------|-------|--------|--------|
| | | | | 2-yr | 5-yr | 10-yr | 25-yr | 50-yr | 100-yr | 500-yr | | | | | | | | | | | | | 2-yr | 5-yr | 10-yr | 25-yr | 50-yr | 100-yr | 500-yr |
| Basin#1 | 2.06 | B | 2.0 | 0.01 | 0.01 | 0.07 | 0.28 | 0.34 | 0.24 | 0.54 | 500.00 | 0.010 | 43.92 | 0.00 | 2.00 | 7 | 0.00 | 2566 | 1240 | 0.52 | 0.77 | 1.01 | 1.24 | 1.51 | 1.74 | 1.94 | 2.12 | | |
| Basin#2 | 4.18 | B | 8.00 | 0.04 | 0.07 | 0.73 | 0.75 | 0.77 | 0.80 | 0.83 | 300.00 | 0.010 | 13.38 | 0.00 | 2.00 | 20 | 0.00 | 2566 | 1240 | 0.52 | 0.77 | 1.01 | 1.24 | 1.51 | 1.74 | 1.94 | 2.12 | | |
| Basin#3 | 6.80 | B | 8.00 | 0.04 | 0.07 | 0.73 | 0.75 | 0.77 | 0.80 | 0.83 | 300.00 | 0.010 | 13.38 | 0.00 | 2.00 | 20 | 0.00 | 2566 | 1240 | 0.52 | 0.77 | 1.01 | 1.24 | 1.51 | 1.74 | 1.94 | 2.12 | | |
| Basin#4 | 0.52 | B | 8.00 | 0.04 | 0.07 | 0.73 | 0.75 | 0.77 | 0.80 | 0.83 | 300.00 | 0.010 | 13.38 | 0.00 | 2.00 | 20 | 0.00 | 2566 | 1240 | 0.52 | 0.77 | 1.01 | 1.24 | 1.51 | 1.74 | 1.94 | 2.12 | | |
| Basin#5 | 0.48 | B | 8.00 | 0.04 | 0.07 | 0.73 | 0.75 | 0.77 | 0.80 | 0.83 | 300.00 | 0.010 | 13.38 | 0.00 | 2.00 | 20 | 0.00 | 2566 | 1240 | 0.52 | 0.77 | 1.01 | 1.24 | 1.51 | 1.74 | 1.94 | 2.12 | | |
| Basin#6 | 1.80 | B | 2.0 | 0.01 | 0.01 | 0.07 | 0.28 | 0.34 | 0.24 | 0.54 | 500.00 | 0.010 | 43.92 | 0.00 | 2.00 | 7 | 0.00 | 2566 | 1240 | 0.52 | 0.77 | 1.01 | 1.24 | 1.51 | 1.74 | 1.94 | 2.12 | | |
| Basin#7 | 1.77 | B | 2.0 | 0.01 | 0.01 | 0.07 | 0.28 | 0.34 | 0.24 | 0.54 | 500.00 | 0.010 | 43.92 | 0.00 | 2.00 | 7 | 0.00 | 2566 | 1240 | 0.52 | 0.77 | 1.01 | 1.24 | 1.51 | 1.74 | 1.94 | 2.12 | | |

Area-Weighted Runoff Coefficient Calculations

Version 2.00 released May 2017

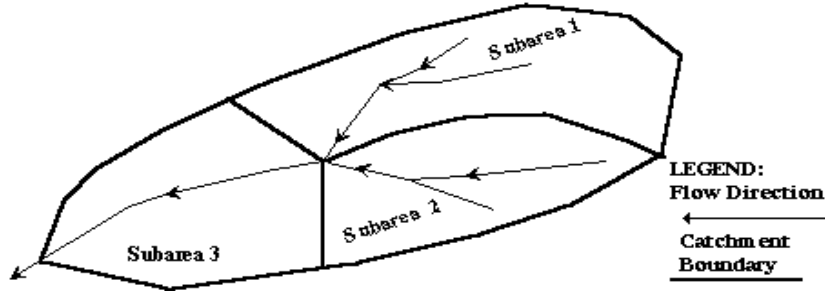
Designer: D. Quigley

Company: DOWL

Date: 8/24/2020

Project: Society Turn - Developed Conditions

Location: Telluride



| |
|--------------------------|
| Subcatchment Name |
| Developed |

| |
|---|
| Cells of this color are for required user-input |
| Cells of this color are for optional override values |
| Cells of this color are for calculated results based on overrides |

See sheet "Design Info" for imperviousness-based runoff coefficient values.

| Sub-Area ID | Area (ac) | NRCS Hydrologic Soil Group | Percent Imperviousness | Runoff Coefficient, C | | | | | | |
|------------------------|--------------|----------------------------|---------------------------------|-----------------------|-------------|-------------|-------------|-------------|-------------|-------------|
| | | | | 2-yr | 5-yr | 10-yr | 25-yr | 50-yr | 100-yr | 500-yr |
| Basin #1 | 2.06 | B | 2.0 | 0.01 | 0.01 | 0.07 | 0.26 | 0.34 | 0.44 | 0.54 |
| Basin #2 | 4.18 | B | 80.0 | 0.64 | 0.67 | 0.70 | 0.75 | 0.77 | 0.80 | 0.83 |
| Basin #3 | 6.80 | B | 80.0 | 0.64 | 0.67 | 0.70 | 0.75 | 0.77 | 0.80 | 0.83 |
| Basin #4 | 0.52 | B | 80.0 | 0.64 | 0.67 | 0.70 | 0.75 | 0.77 | 0.80 | 0.83 |
| Basin #5 | 0.48 | B | 80.0 | 0.64 | 0.67 | 0.70 | 0.75 | 0.77 | 0.80 | 0.83 |
| Basin #6 | 1.80 | B | 2.0 | 0.01 | 0.01 | 0.07 | 0.26 | 0.34 | 0.44 | 0.54 |
| Basin #7 | 1.77 | B | 2.0 | 0.01 | 0.01 | 0.07 | 0.26 | 0.34 | 0.44 | 0.54 |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| Total Area (ac) | 17.61 | | | 0.44 | 0.46 | 0.50 | 0.59 | 0.64 | 0.68 | 0.74 |
| | | | Area-Weighted C | 0.44 | 0.46 | 0.50 | 0.59 | 0.64 | 0.68 | 0.74 |
| | | | Area-Weighted Override C | 0.44 | 0.46 | 0.50 | 0.59 | 0.64 | 0.68 | 0.74 |

Length-Weighted Slope Calculations

Version 2.00 released May 2017

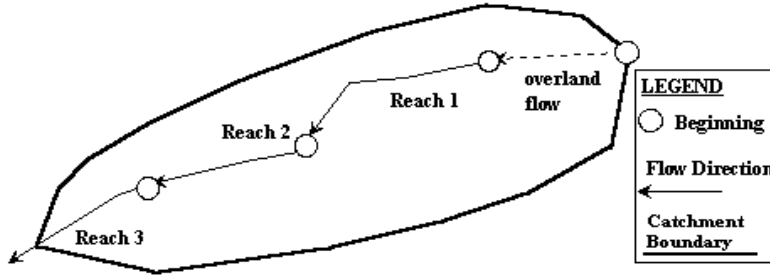
Designer: D. Quigley

Company: DOWL

Date: 8/24/2020

Project: Society Turn - Developed Conditions

Location: Telluride



| Subcatchment Name | Percent Imperviousness (%) |
|-------------------|----------------------------|
| Society Turn Post | 2 |

OVERLAND FLOW

| Reach ID | Overland Flow Length L_i (ft) | U/S Elevation (ft) (Optional) | D/S Elevation (ft) (Optional) | Overland Flow Slope S_i (ft/ft) |
|-----------------------------------|---------------------------------|--------------------------------------|-------------------------------|-----------------------------------|
| Basin #1 | 300.00 | | | 0.010 |
| Basin #2 | 100.00 | | | 0.010 |
| Basin #3 | 100.00 | | | 0.010 |
| Basin #4 | 100.00 | | | 0.010 |
| Basin #5 | 100.00 | | | 0.010 |
| Basin #6 | 300.00 | | | 0.010 |
| Basin #7 | 300.00 | | | 0.010 |
| | | | | |
| | | | | |
| Total Overland Length (ft) | 1300.00 | Length-Weighted Slope (ft/ft) | | 0.010 |

CHANNELIZED FLOW

| Reach ID | Channelized Flow Length L_i (ft) | U/S Elevation (ft) (Optional) | D/S Elevation (ft) (Optional) | Channelized Flow Slope S_i (ft/ft) |
|--------------------------------------|------------------------------------|--------------------------------------|-------------------------------|--------------------------------------|
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| Total Channelized Length (ft) | | Length-Weighted Slope (ft/ft) | | |

Reach-Weighted Time of Concentration Calculations

Version 2.00 released May 2017

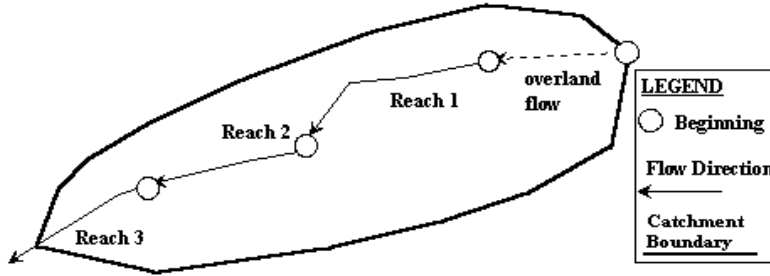
Designer: D. Quigley

Company: DOWL

Date: 8/24/2020

Project: Society Turn - Developed Conditions

Location: Telluride



| Subcatchment Name | Percent Imperviousness (%) |
|-------------------|----------------------------|
| Society Turn Pre | 2 |

OVERLAND FLOW

| Reach ID | Overland Flow Length L_i (ft) | Overland Flow Slope S_i (ft/ft) | 5-yr Runoff Coefficient, C_s | Overland Flow Time t_i (min) |
|------------------------|---------------------------------|-----------------------------------|--------------------------------|--------------------------------|
| Basin #1 | 300.00 | 0.010 | 0.01 | 34.09 |
| Basin #2 | 100.00 | 0.010 | 0.67 | 7.76 |
| Basin #3 | 100.00 | 0.010 | 0.67 | 7.76 |
| Basin #4 | 100.00 | 0.010 | 0.67 | 7.76 |
| Basin #5 | 100.00 | 0.010 | 0.67 | 7.76 |
| Basin #6 | 300.00 | 0.010 | 0.01 | 34.09 |
| Basin #7 | 300.00 | 0.010 | 0.01 | 34.09 |
| | | | | |
| | | | | |
| Weighted Totals | 1300.00 | 0.010 | Total t_i (min) | 133.31 |

CHANNELIZED FLOW

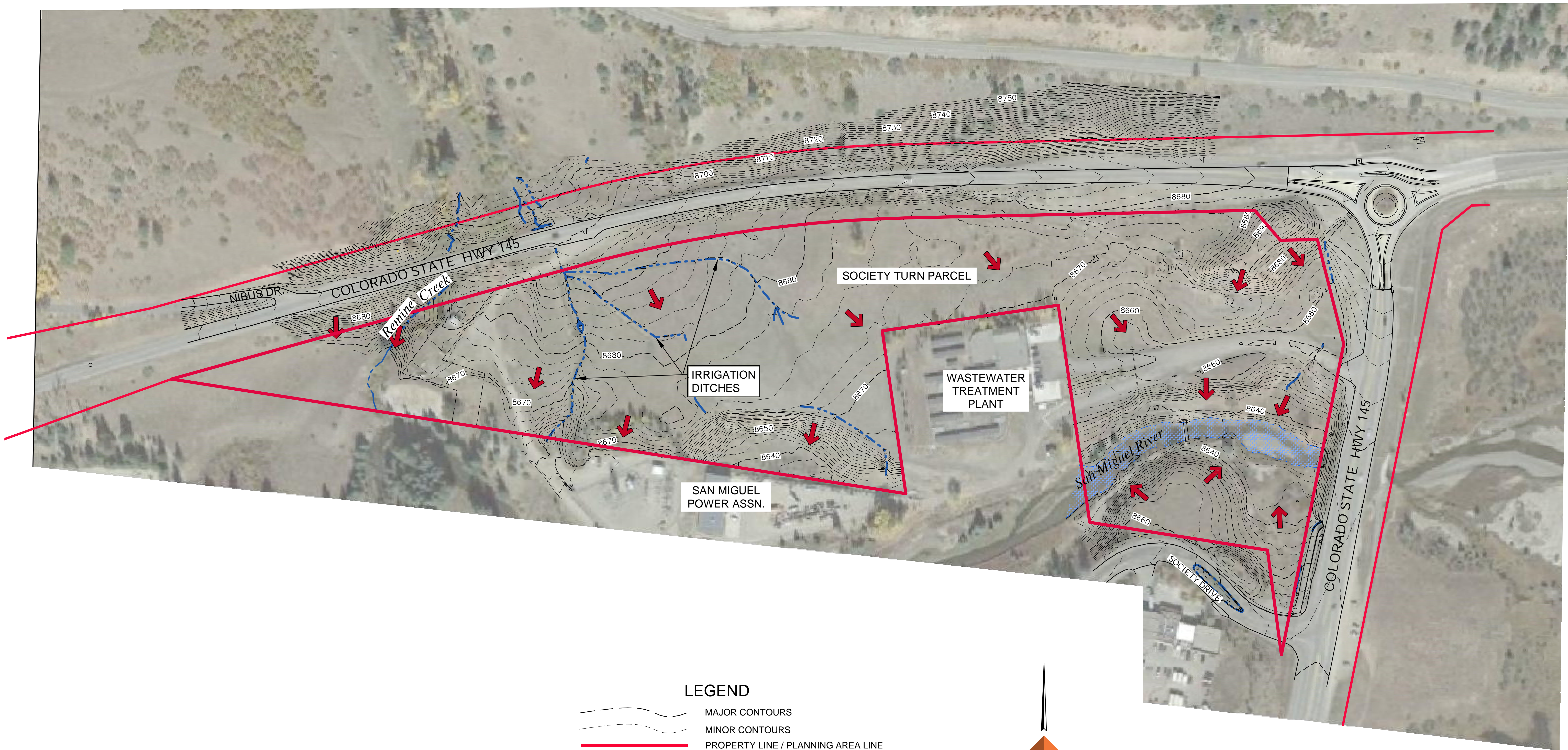
| Reach ID | Channelized Flow Length L_i (ft) | Channelized Flow Slope S_i (ft/ft) | NRCS Conveyance Factor K | Channelized Flow Time t_i (min) |
|------------------------|------------------------------------|--------------------------------------|--------------------------|-----------------------------------|
| | | | | |
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| | | | | |
| Weighted Totals | | | Total t_i (min) | |

| | |
|----------------------|------|
| Computed t_c (min) | 0.00 |
| Regional t_c (min) | |
| Selected t_c (min) | |

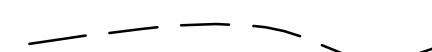
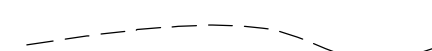




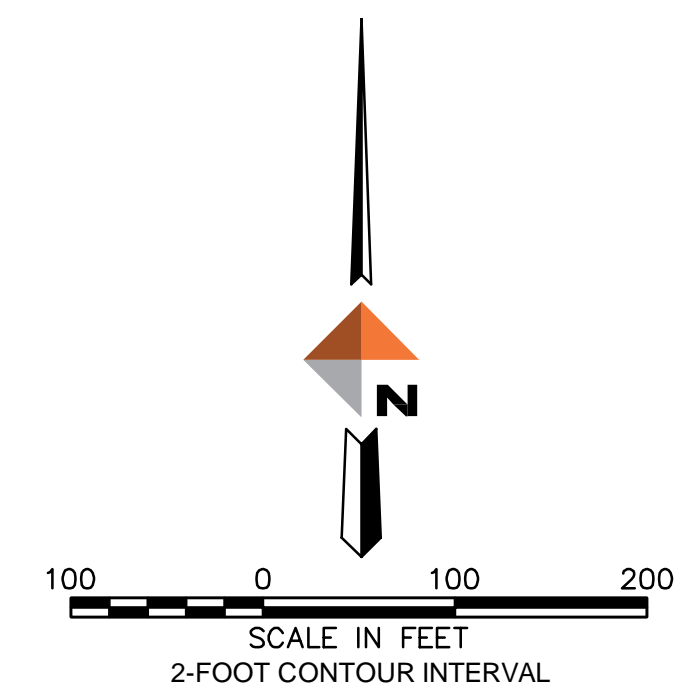
APPENDIX E
DRAINAGE PLANS AND DETAILS

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LEGEND

-  MAJOR CONTOURS
-  MINOR CONTOURS
-  PROPERTY LINE / PLANNING AREA LINE
-  DRAINAGE FLOW ARROW

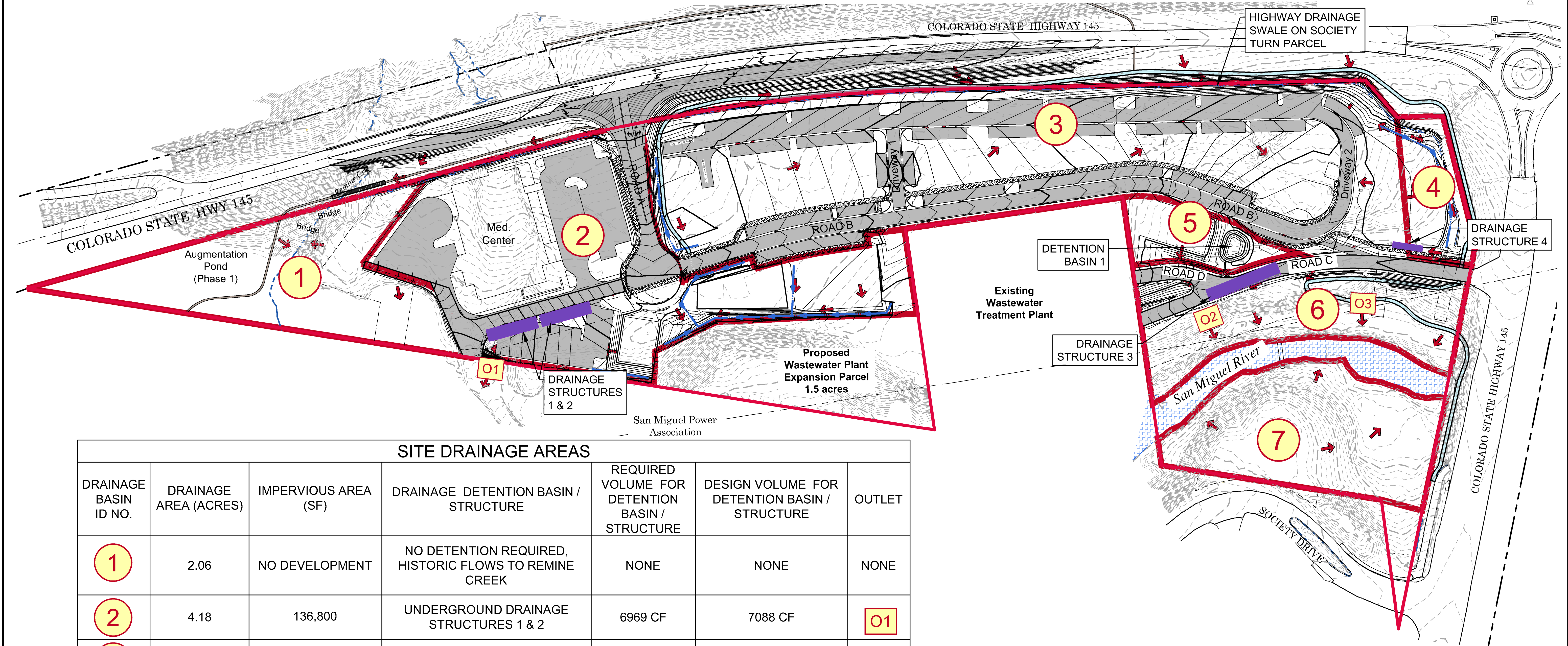


| REVISIONS | | | |
|-----------|------|-------------|----|
| REV | DATE | DESCRIPTION | BY |
| | | | |
| | | | |
| | | | |
| | | | |

DOWL
WWW.DOWL.COM
 222 South Park Avenue
 Montrose, Colorado 81401
 970-249-6828

GENESSEE PROPERTIES, INC.
 SOCIETY TURN PARCEL
 PRE-DEVELOPED DRAINAGE

| | |
|-------------|------------|
| PROJECT | 7122-74614 |
| DATE | 08/21/2020 |
| SHEET | |
| DR-1 | |
| 1 OF 2 | |

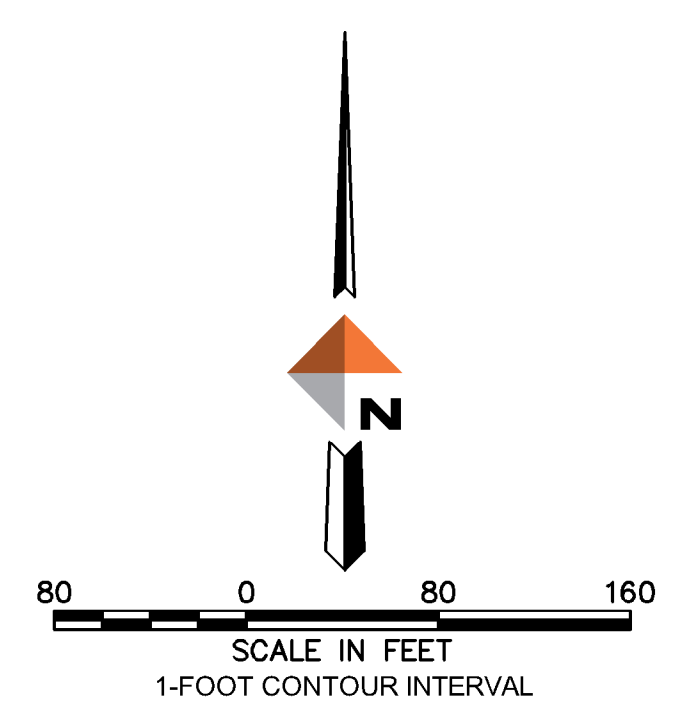


SITE DRAINAGE AREAS

| DRAINAGE BASIN ID NO. | DRAINAGE AREA (ACRES) | IMPERVIOUS AREA (SF) | DRAINAGE DETENTION BASIN / STRUCTURE | REQUIRED VOLUME FOR DETENTION BASIN / STRUCTURE | DESIGN VOLUME FOR DETENTION BASIN / STRUCTURE | OUTLET |
|-----------------------|-----------------------|----------------------|---|---|---|--------|
| 1 | 2.06 | NO DEVELOPMENT | NO DETENTION REQUIRED, HISTORIC FLOWS TO REMINE CREEK | NONE | NONE | NONE |
| 2 | 4.18 | 136,800 | UNDERGROUND DRAINAGE STRUCTURES 1 & 2 | 6969 CF | 7088 CF | O1 |
| 3 | 6.80 | 200,800 | UNDERGROUND DRAINAGE STRUCTURE 3 | 7455 CF | 7623 CF | O2 |
| 4 | 0.52 | 7,472 | UNDERGROUND DRAINAGE STRUCTURE 4 | 830 CF | 856 CF | O3 |
| 5 | 0.48 | 6,871 | DETENTION BASIN 1 | 1045 CF | 1087 CF | O2 |
| 6 | 1.80 | 12,200 (ROAD C & D) | NO DETENTION REQUIRED, HISTORIC FLOWS TO SAN MIGUEL RIVER | NONE | NONE | NONE |
| 7 | 1.77 | NO DEVELOPMENT | NO DETENTION REQUIRED. HISTORIC FLOWS TO SAN MIGUEL RIVER | NONE | NONE | NONE |

LEGEND

- DRAINAGE AREA BOUNDARY LIMITS
- UNDERGROUND DRAINAGE STRUCTURE
- NEW ASPHALT PAVEMENT
- ➔ DRAINAGE FLOW ARROW
- 7 DRAINAGE BASIN ID NO.
- O3 DRAINAGE OUTLET ID NO.



| REVISIONS | | | |
|-----------|------|-------------|----|
| REV | DATE | DESCRIPTION | BY |
| | | | |
| | | | |

DOWL
WWW.DOWL.COM
222 South Park Avenue
Montrose, Colorado 81401
970-249-6828

GENESSEE PROPERTIES, INC.
SOCIETY TURN PARCEL
DEVELOPED DRAINAGE PLAN

PROJECT 7122-74614
DATE 08/21/2020
SHEET
DR-2
2 OF 2

G:\22\74614-01\65CAD\Civil\Draw2-Sketch_Plan\DR1-Drainage_Report.dwg PLOT DATE: 2020-08-24 10:55 SAVED DATE: 2020-08-24 10:48 USER: dcoastillo