

## Noise and Vibration Assessment

CWL01 & 02 – Microsoft Ltd.

03 November 2023

Project No.: 0657169

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## Signature Page

03 November 2023

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CWL01 & 02 – Microsoft Ltd

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## 1. INTRODUCTION

Environmental Resources Management Ltd (ERM) has been appointed by RED Engineering (on behalf of Microsoft Corporation) to undertake an assessment of noise and vibration from the construction, operation, and decommissioning of its Proposed Development. The proposal is for a new data centre complex on the site of the former Quinn Radiators Factory at Celtic Way, Celtic Lakes, Newport, South Wales NP10 8FS.

The aim of this assessment is to determine the existing acoustic climate and predict the sound levels due to three scenarios - normal operation, emergency operation (main power supply failure), and under the generator testing regime of the proposed Development, and to assess these levels against the relevant guidance. Where appropriate, mitigation measures have been recommended to protect the amenity of residents in the locality of the Proposed Development.

## 2. THE PROPOSED DEVELOPMENT

The proposed Development is situated on a 40 acre / 16.49ha site, which lies in the Imperial Park within the business estate in the local planning authority jurisdiction of Newport City Council, which is currently vacant.

Current proposals are for the existing buildings on the site to be demolished and replaced by two single storey data centre buildings. The Development also includes associated offices, back-up generators, substation connection, waste treatment plant, vehicle parking, and security gatehouses.

A layout of the proposed Development is presented in Appendix A.

## 3. LEGISLATION, POLICY, AND RELEVANT GUIDANCE

The assessment takes into account the following legislation and policy:

### 3.1 Legislation

The following legislation are of particular relevance to the assessment:

- The Control of Pollution Act 1974 (CoPA 1974);
- The Environmental Protection Act 1990 (EPA 1990).

#### 3.1.1 *The Control of Pollution Act 1974*

CoPA 1974 provides Local Authorities with powers to control noise and vibration from construction sites.

Section 60 of the CoPA 1974 enables a Local Authority to serve a notice to persons carrying out construction work of its requirements for the control of site noise. This may specify plant or machinery that is or is not to be used; the hours during which construction work may be carried out; the level of noise or vibration that may be emitted; and provides for changes in circumstances.

#### 3.1.2 *The Environmental Protection Act 1990*

The EPA 1990 specifies mandatory powers available to Local Authorities in respect of any noise that either constitutes, or is likely to cause, a statutory nuisance, which is also defined in CoPA 1974. A duty is imposed on Local Authorities to carry out inspections to identify statutory nuisances, and to serve abatement notices against these. Procedures are also specified with regards to complaints from persons affected by a statutory nuisance.

## 3.2 Policy

The following key policies are relevant to this assessment:

- Planning Policy Wales (PPW)<sup>1</sup>;
- The Technical Advice Note (TAN).

### 3.2.1 Planning Policy Wales

The policy document sets out the Government's planning policies for Wales, providing a framework within which local policies can be developed. The key principle of the policy is a presumption in favour of sustainable development. With regards to noise, the document states that in proposing new developments, planning authorities and developers must:

- Address any implications arising as a result of its association with, or location within, air quality management areas, noise action planning priority areas, or areas where there are sensitive receptors.
- Not create areas of poor air quality or inappropriate soundscape; and
- Seek to incorporate measures which reduce overall exposure to air and noise pollution and create appropriate soundscapes.

With regards to industrial development, the policy states: *"...potentially polluting development includes commercial, industrial, energy and agricultural or transport infrastructure. Such development should be located in areas where there is low potential for public exposure, or where its impact can be minimised. Novel or new development types may potentially cause pollution and should be carefully considered, and where appropriate, decisions should be based on the precautionary principle."*

The policy document also highlights sustainability of new developments, stating: *"Taking a sustainable approach will mean balancing short-term needs against long-term objectives to reduce public exposure to airborne pollution and giving particular consideration to the presence of air quality management areas, noise action planning priority areas and areas with sensitive receptors when proposing new development and particularly when preparing development plans."*

The policy document refers to the associated Technical Advice Note on relevant guidance for noise assessments.

### 3.2.2 Technical Advice Note (TAN) 11

Technical Advice Note (TAN) 11<sup>2</sup> provides guidance to local authorities on how the planning system can be used to minimise the adverse impact of noise without placing unreasonable restrictions on development or adding unduly to the costs and administrative burdens of business. It outlines some of the main considerations which local planning authorities should take into account when determining planning applications for development which will either generate noise or be exposed to existing noise sources. TAN 11 also makes reference to guidance and criteria applicable to sources of noise such as industrial and commercial developments, roads and railways.

TAN 11 states that BS 4142 (1997)<sup>3</sup> is the most appropriate methodology to assess noise from industrial and commercial developments. This British Standard has since been updated in 2014. A clarification to TAN 11 was published in 2015 which confirm the updated version should be used.

An update to TAN 11 was published in draft in October 2022, for consultation, following revisions to Planning Policy Wales made in 2018. Consultation on the draft TAN ended in January 2023, however a revised TAN has not been issued for use and so the 1997 TAN remains the current guidance on noise assessment.

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<sup>1</sup> Planning Policy Wales Edition 11 February 2021

<sup>2</sup> Planning Guidance (Wales). Technical Advice Note 11, 1997.

<sup>3</sup> British Standard BS 4142: 1997 'Method for Rating industrial noise affecting mixed residential and industrial areas'

### 3.3 Standards and Guidance

The following standard is relevant to noise generated by the construction phase of the Proposed Development:

- BS 5228:2009+A1:2014 Code of practice for noise and vibration control on construction and open sites.

And the following standards are relevant to noise generated by the operation of the Proposed Development:

- BS 4142:2014+A1:2019: 'Methods for rating and assessing industrial and commercial sound';
- BS 8233: 2014: 'Guidance on sound insulation and noise reduction in buildings'; and
- ISO 9613-2:1996: 'Attenuation of Sound during Propagation Outdoors'.

#### 3.3.1 BS 5228: 2009+A1:2014

BS 5228:2009+A1:2014 *Code of Practice for noise and vibration control on construction and open sites* (BS 5228) refers to the need for the protection against noise and vibration of persons living and working in the vicinity of, and those working on, construction and open sites. The standard:

- Is published in two parts: Part 1 - Noise and Part 2 - Vibration. The discussion below relates mainly to Part 1, however, the recommendations of Part 2 in terms of vibration are broadly very similar;
- Refers to the need for protection against noise and vibration of persons living and working in the vicinity of, and those working on construction and open sites;
- Recommends procedures for noise and vibration control in respect of construction operations;
- Stresses the importance of community relations, and states that early establishment and maintenance of these relations throughout site operations will go some way towards allaying people's concerns;
- Provides recommendations regarding the supervision, planning, preparation and execution of works, emphasising the need to consider noise at every stage of the operation;
- Describes methods of controlling noise at source and its spread; and
- Includes a discussion of noise control targets, and example criteria for the assessment of the significance of noise effects.

#### 3.3.2 BS 8233:2014

BS 8233 is mainly a guidance on sound reduction within domestic and non-domestic dwellings; the standard provides design guidance on acceptable noise levels for a variety of room types. These noise levels apply inside the respective building; for offices, BS 8233 provides a range of noise levels,  $L_{Aeq,T}$  between 35 dB(A) and 50 dB(A) with the upper end of this range recommended for open plan offices. This can be used to derive suitable limits with which to assess potential effects on non-residential receptors. BS 8233 also provides a design target for external areas used for amenity space, such as gardens, of 50 dB  $L_{Aeq,T}$  or 55 dB  $L_{Aeq,T}$  in noisier environments.

#### 3.3.3 BS 4142:2014+A1:2019

BS4142:2014+A1:2019 (BS 4142) describes methods for rating and assessing sound in order to provide an indication of its likely impact upon nearby premises (typically residential dwellings).

The specific sound emitted from the Development (dB,  $L_{Aeq}$ ) is rated by taking into account both the level and character (i.e., tonal elements, impulsivity, intermittency and distinctiveness) of the sound. This is achieved by applying appropriate corrections to the specific sound level externally at the



receptor location, which gives the rating level of the sound in question. This is then assessed against the existing prevailing background sound level (dB, LA90) at that location in order to determine a likely level of impact.

The level by which the rating level exceeds the prevailing background sound level indicates the following potential impacts:

- A difference of 10 dB or more is likely to be an indication of a significant adverse impact, depending on the context;
- A difference of 5 dB or more is likely to be an indication of an adverse impact, depending on the context; and
- Where the rating level does not exceed the background level, this is an indication of the specific sound source having a low impact, depending on the context.

When considering the level of effect, BS 4142 emphasises the importance of the context in which a sound occurs.

### 3.3.4 ISO 9613-2:1996

ISO 9613-2:1996: *Attenuation of Sound during Propagation Outdoors* describes a method for calculating the attenuation of sound during propagation outdoors in order to predict the levels of environmental noise at a distance from a variety of sources. The method predicts the equivalent continuous A-weighted sound pressure level (as described in ISO 1996) under meteorological conditions by taking the octave band sound power level spectrum of the source, and applying a number of attenuation factors that determine the resulting rating level at the receptor location.

ISO 9613-2 is currently being revised; however, the revised version has not yet been published and so the 1996 version remains current.

## 4. CONSULTATION & ASSESSMENT CRITERIA

Newport City Council provided pre-application advice in September 2022.

It was noted in the response to the Pre-Application that the further assessment work identified in the noise preliminary assessment report would be considered an acceptable approach. This included:

- Prediction and assessment of the noise during demolition and construction phases using BS 5228 to predict and assess the noise levels.
- A baseline noise survey in accordance with BS 4142 (and to establish baseline for the construction assessment). Monitoring locations to be selected in discussion with Newport City Council.
- Noise modelling to reflect the current design of the facility and to identify any potential noise impacts.
- Specification of noise mitigation to ensure that noise levels meet appropriate noise standards to avoid significant noise impacts in discussion with Newport City Council.

The noise baseline methodology and monitoring locations were approved by NCC in June 2023. However, it was not possible to arrange access at one of the locations and a suitable alternative was used. This is discussed further in Section 5: Baseline Environment.

NCC asked that the assessment include a 'worst case scenario' of data centre backup power generators activating overnight / early hours, and assessment of all applicable plant & equipment.

NCC have advised that their standard noise condition is:

*“Noise emitted from plant and equipment located at the site shall be controlled such that the rating level, calculated in accordance with BS4142 2014, does not exceed a level of 5dB below the existing background level, with no tonal element to the plant.*

**Reason:** *To ensure that the amenities of occupiers of other premises in the vicinity are protected.”*

Therefore, based on the consultation response by NCC, the assessment criteria for operation noise from the Development is:

- Rating levels from the proposed Development do not exceed 5 dB below the prevailing background levels, with no tonal element to the plant.

## 5. BASELINE ENVIRONMENT

The site is located on an industrial site, previously Quinn Radiator Factory. Buildings remain in place but unused. The land to the north is currently occupied by the NHS. To the east is the continuation of the industrial estate.

The site is bounded by the M4 approximately 700 m to the north and a mainline railway approximately 1 km to the south. A48 also lies to the north of the site, in between the site and the M4.

To the east lies the town of Duffryn with the closest residential properties on its western outskirts situated at a distance of approximately 450 m to the proposed Development. To the South, there is open land with dense vegetation, which appears to be unofficially used by the public (including the use of motorbikes).

The closest residential properties to the site are situated to the west, on Church Lane and Church Crescent at a distance of approximately 280 m from the closest noise producing element on the site. In addition, a number of more isolated properties are situated to the south, with the closest (on a private road off Church Lane), including The Stud Farm, approximately 300 m from the site.

The site is adjacent to several commercial/industrial premises, including:

- Vantage Data centre, which is currently in operation with expansions proposed, approximately 230 m to the north-east of the closest noise producing element on the site;
- IQE – a supplier of semiconductor products, approximately 140 m to the north-east of the closest noise producing element on the site;
- NHS building (storage/pharmacy building), located along the northern boundary of the site and approximately 50 m from the closest noise producing element on the site;
- Other commercial business in the wider business park;
- Parc Golf Club approximately 290 m to the south-west of the closest noise producing element on the site; and
- Hotels and restaurants to the north.

A number of industrial/commercial premises, such as, the IQE industrial unit, and NHS building, are situated close to the site which may contain offices. As the buildings nearby are linked to relatively noisy industrial or commercial uses, they are expected to be of lower noise sensitivity and therefore, the upper end of the guide range has been adopted as outlined in Section 3.3.2. The assessment is undertaken against the upper limit of acceptable noise level within office spaces, assuming a partially open window, which is an equivalent external façade noise level would be 65 dB(A).

Effects from construction noise on users of outdoor spaces such as golf courses and public parks are not significant and not assessed. Baseline noise monitoring was carried out at four locations between 8<sup>th</sup> and the 22<sup>nd</sup> August 2023, to quantify the noise environment at locations close to the Proposed

Development. The monitoring locations were agreed in advance with NCC. The nearest NSRs and noise monitoring locations are shown in Figure 1.

Subsequently, however, it was not possible to arrange access at NSR 7. Instead, noise monitoring was carried out nearby at location ML 7, at the southern end of the site. Although the location is slightly closer to the M4 and A48, the measurement equipment was screened from these noise sources by the (disused) southern building on-site. As a result, noise from these sources is likely to be lower than would be experienced at NSR 7, which is conservative.

A summary of the baseline sound levels adopted for each residential NSR is presented in Table 1. Details of the method and results are presented in Appendix B.

Figure 1 – Noise Sensitive Receptors / Noise Monitoring Locations



**Table 1 – Summary of Baseline Sound Levels at Residential Receptor Locations**

| Receptor Location                         | Construction Baseline, L <sub>Aeq,T</sub> dB / (Adopted 'ABC' Category <sup>(1)</sup> ) |         |        | Operational Baseline, RBSL L <sub>A90</sub> dB <sup>(2)</sup> |       |
|---|---|---------|--------|---|-------|
|   | Day   | Evening | Night  | Day   | Night |
| Nanty-moor Cottages/Blacksmiths Way (ML3) | 57 (A)  | 54 (B)  | 51 (C) | 51  | 46    |
| Church crescent (ML2)                     | 55 (A)  | 54 (B)  | 50 (C) | 52  | 46    |
| Powis Close (ML4)                         | 44 (A)  | 41 (A)  | 39 (A) | 35  | 32    |
| The Stud Farm (ML1)                       | 46 (A)  | 46 (A)  | 44 (B) | 43  | 38    |
| Pencarn Avenue (ML3 Representative)       | 57 (A)  | 54 (B)  | 51 (C) | 51  | 46    |
| The Parc Golf Club (ML1 Representative)   | 46 (A)  | 46 (A)  | 44 (B) | 43  | 38    |

1) 'ABC' category as defined in BS 5228 (see Section 5.1).

2) Representative baseline sound level according to BS 4142 (see Section 5.2).

## 6. METHODOLOGY

### 6.1 Demolition & Construction Noise

#### 6.1.1 Basis of assessment

Noise and vibration from the demolition of the existing buildings and construction of the Proposed Development has the potential to result in significant temporary effects at nearby noise sensitive receptors (NSRs). This assessment considers the main construction activities which are expected to be:

- Demolition of the existing buildings;
- Earthworks;
- Foundation works; and
- Superstructures.

At the time of this assessment, a contractor had not been appointed for the construction works, as such, a detailed construction programme and construction traffic data was not available. Therefore, the potential for effects from construction traffic are only considered subjectively in this assessment.

Studies show that levels of vibration from driven piling fall below the level that may be perceptible in a residential environment within a distance of 100 m <sup>(4)</sup>. Vibration from other construction activities that may be required are expected to generate lower levels of vibration. Therefore, as the nearest sensitive receptors are beyond this distance, vibration during construction has been scoped out of further assessment.

Construction noise has been predicted based on information from the Project engineering team and from experience of other similar projects of the types and numbers of construction plant that will be used. The assessment makes use of the indicative demolition and construction programme; detailing construction activities and the associated plant that will be operating simultaneously.

(4) TRL Report 429. Groundborne Vibration Caused by Mechanised Construction Works. D.M.Hiller & G.I.Crabb. Highways Agency 1995

Table 2 and Table 3 summarise respectively the demolition and construction plant and associated noise levels included in each phase.

**Table 2: Demolition Activities and Sound Power Levels**

| Phase/Activity (duration in weeks)                               | Item                             | BS 5228 Reference | L <sub>Aeq</sub> at 10m | No. of Items | Effective Sound Power Level (L <sub>w</sub> ) |
|--|----------------------------------|-------------------|-------------------------|--------------|---|
| <b>Mobilisation (4w)</b>   | Diesel Generator                 | C.4.76            | 61                      | 1            | 89  |
| <b>Phase 1 Clearance Works (11w)</b>                             | Tracked Excavator 14t            | C.2.07            | 70                      | 2            | 101   |
|  | Telescopic Handler 3.7t          | C.4.55            | 70                      | 1            | 98  |
|  | Mobile Telescopic Crane 50t      | C.4.46            | 67                      | 2            | 98  |
|  | Diesel Scissor Lift 6t           | C.4.59            | 78                      | 1            | 106   |
| <b>Soft Stripping (9w)</b>                                       | Tracked Excavator 21t            | C.4.65            | 71                      | 4            | 105   |
|  | Diesel Scissor Lift 6t           | C.4.59            | 78                      | 1            | 106   |
| <b>Trench Remedial Works (6w)</b>                                | Fuel Tanker Pumping              | C.4.16            | 72                      | 1            | 100   |
| <b>L1 Building Demolition (5w)</b>                               | Tracked Excavator 40t            | C.1.16            | 82                      | 2            | 113   |
|  | Tracked Excavator 40t            | C.1.13            | 86                      | 2            | 117   |
|  | Tracked Crusher 47t              | C.1.14            | 82                      | 1            | 110   |
|  | Tracked Excavator 40t            | C.2.14            | 79                      | 1            | 107   |
| <b>Sprinkler Pump Room (13w)</b>                                 | Water Pump                       | C.2.45            | 65                      | 1            | 93  |
|  | Pulveriser mounted on excavator  | C.1.03            | 80                      | 2            | 111   |
|  | Tracked Crusher 47t              | C.1.14            | 82                      | 1            | 110   |
|  | Tracked Excavator 40t            | C.2.14            | 79                      | 1            | 107   |
| <b>Asphalt Removal (8w)</b>                                      | Tracked Excavator 22t            | C.2.03            | 78                      | 1            | 106   |
| <b>Sewer Diversion Works</b>                                     | Tracked Excavator 40t            | C.2.14            | 79                      | 2            | 110   |
|  | Cement Mixer truck (discharging) | C.4.18            | 75                      | 1            | 103   |
| <b>Phase 1, 2, &amp; 2a Combined effective Sound Power Level</b> |                                  |                   |                         |              | <b>122</b>                                    |
| <b>Main Building Demolition (29w)</b>                            | Tracked Excavator 40t            | C.1.16            | 82                      | 6            | 118   |
|  | Tracked Excavator 22t            | C.2.03            | 78                      | 14           | 117   |
|  | Tracked Excavator 44t            | C.1.12            | 82                      | 6            | 118   |
|  | Tracked Crusher 47t              | C.1.14            | 82                      | 2            | 113   |
|  | Tracked Excavator 40t            | C.2.14            | 79                      | 2            | 110   |
| <b>Phase 3 works Combined effective Sound Power Level</b>        |                                  |                   |                         |              | <b>123</b>                                    |

Phases 1, 2, and 2a works are expected to overlap in duration and dates of activity as such the worst-case scenario of all these activities undertaken simultaneously is assessed as a conservative approach.

**Table 3: Indicative Construction Activities and Sound Power Levels**

| Phase/Activity                              | Item                            | BS 5228 Reference | L <sub>Aeq</sub> at 10m | No. of Items | Effective Sound Power Level (L <sub>w</sub> ) |
|---|---------------------------------|-------------------|-------------------------|--------------|---|
| <b>Substructure</b>                         | 360° excavator                  | C.2.14            | 79                      | 6            | 115   |
|   | Concrete Pump                   | C.3.25            | 78                      | 3            | 111   |
|   | All terrain telescopic forklift | C.4.46            | 67                      | 6            | 103   |
|   | Rigid 6-wheeler tipper (HGV)    | C.8.20            | 79                      | 16           | 119   |
|   | Vibrating roller                | C.2.39            | 74                      | 3            | 107   |
| <b>Combined Effective Sound Power Level</b> |                                 |                   |                         |              | <b>121</b>                                    |
| <b>Superstructure</b>                       | Mobile Crane (250t)             | C.4.38            | 78                      | 2            | 109   |
|   | Mobile Crane (100t)             | C.3.28            | 67                      | 4            | 101   |
|   | Cherry Picker                   | C.4.57            | 67                      | 5            | 102   |
|   | All terrain telescopic forklift | C.4.46            | 67                      | 4            | 101   |
| <b>Combined Effective Sound Power Level</b> |                                 |                   |                         |              | <b>111</b>                                    |
| <b>Envelope</b>                             | Cherry Picker                   | C.4.57            | 67                      | 4            | 101   |
|   | MEWP                            | C.4.53            | 77                      | 6            | 113   |
| <b>Combined Effective Sound Power Level</b> |                                 |                   |                         |              | <b>113</b>                                    |
| <b>Generators</b>                           | Mobile Crane (100t)             | C.3.28            | 67                      | 1            | 95  |
| <b>Fitout</b>                               | Hoist                           | C.4.61            | 68                      | 2            | 99  |
|   | MEWP                            | C.4.53            | 77                      | 30           | 120   |
|   | Mobile Crane (100t)             | C.3.28            | 67                      | 1            | 95  |
| <b>Combined Effective Sound Power Level</b> |                                 |                   |                         |              | <b>120</b>                                    |

As a worst-case, it is assumed that all items of plant for each period are operating 100 % of the time, and are placed at the closest point of the Project Boundary to the relevant NSR,

All construction work will be carried out during daytime hours only, from 07:00 until 19:00 on weekdays, and 08:00 until 13:00 on Saturdays. Night-time construction work is not expected to be required. In exceptional circumstances, some work may be required in the evening and night should works fall behind schedule. This will be limited to works that are not major sources of noise so that levels at NSRs are kept below the relevant criteria. In this event approval from NCC will be sought in advance and local residents informed as part of the considerate contractor scheme.

### 6.1.2 Construction Noise Calculation

Demolition and Construction noise has been calculated in accordance with BS 5228-1. The total effective Sound Power Level from an activity, that may be undertaken simultaneously, is used to determine the sound level at the NSR by calculating sound propagation from the Site boundary to the NSR façade. The propagation calculation accounts for the following factors:

- Quantity of plant;
- Distance to the NSR from the boundary of construction area;
- Height of Source;
- Ground absorption (assumed soft ground between Site and NSRs);

- Plant On-time (assumed %100 as conservative);
- Façade correction (3 dB); and
- Any screening correction (none in this instance).

The sound level is calculated by distance attenuation of total sound with corrections for difference in source height, ground type, screening, and façade correction to determine the sound level at the NSR façade.

## 6.2 Operational Noise

### 6.2.1 Basis of Assessment

The noise and vibration assessment of the operational phase makes use of the following sources of information:

- Preliminary layout of external fixed plant and other noise sources, such as waste treatment plant and Air Handling Units (AHUs), provided by the Project engineering team;
- Equipment noise source data and information regarding assumed at-source mitigation measures provided by the Project engineering team;
- Preliminary design information regarding building construction provided by the Project engineering team (assumptions regarding absorption / transmission values are based on SoundPLAN software library data); and
- Preliminary layout and height information for the main on-site buildings provided by Project engineering team.

No significant vibration generating equipment will be required during operation. Therefore, an operational vibration assessment is scoped out of further assessment.

On-site vehicle movements during operation are expected to be minimal. Off-site vehicles are also expected to be minimal so that significant changes in traffic noise are not likely, and therefore an assessment of road traffic noise during the operation of the Development has been scoped-out.

### 6.2.2 Assessment Scenarios

An assessment of the proposed Development is undertaken for three scenarios of activity:

- **Normal Operation:** this scenario is the typical operation of the data centre powered by the national grid, consisting of the AHU intake and exhaust noise emissions from CWL01 & CWL02 buildings plus the substation noise from the three 150 kV transformers. Generators, and therefore, associated stacks and transformers do not operate during this scenario. Other external plant such as the Waste Treatment Plant (WTP) is enclosed within an external plant room therefore, noise emissions are not expected to be significant.
- **Generator Testing:** A regular (monthly) testing of the generators will be undertaken at the proposed Development, this will involve testing of the generators (with associated transformer, control unit, and stack etc.) over a single day. This scenario has been modelled by inputting noise emissions from the generators closest to respective NSRs (in addition to the normal operation of CWL01 & 02), therefore, demonstrating the worst-case noise levels at each receptor during the testing period.
- **Emergency Mode:** This scenario simulates a complete power supply failure, in such case, all generators are running along with admin office generator and transformer, as well, the generator and transformer for the WTP. This is the worst case which included normal noise emissions from the buildings plus all external generators, stacks, and transformers in operation.



The three scenarios above have been modelled in this assessment; results for each scenario are presented in Section 7.2.

It should be noted that only the normal operation scenario is the typical continuous noise profile of the proposed Development, the generator testing is temporary undertaken over a monthly basis while the emergency mode is worst-case that will only happen during the unlikely event of a power failure, which will be rectified thereafter as soon as possible.

### 6.2.3 Noise Modelling

The specific sound level at the nearest noise-sensitive receptors has been calculated in SoundPlan version 8.2, using the environmental noise propagation model ISO 9613 2:1996 – Acoustics; ‘Attenuation of sound during propagation outdoors – Part 2: General method of calculation’.

The Development comprises the following plant:

- CWL01 Building;
  - 160x AHU unit intake louvres;
  - 160x Relief Air Balcony (RAB) ventilation louvres;
  - 20x Generator units (with 10x exhaust stacks and 20x transformers);
  - 3x Mains 150kV Transformers;
  - 1x Admin office generator unit with transformer; and
  - 1x WTP generator with transformer.
- CWL02 Building;
  - 64x AHU unit intake louvres;
  - 64x RAB ventilation louvres;
  - 8x Generator units (with 4x exhaust stacks and 8x transformers); and
  - 1x Admin office generator unit with transformer.

Noise from Admin office block, UPS control panels, connection load banks, and WTP is not expected to be significant, and as such has not been included as part of the modelling process.

The sound power levels of the plant included in the noise model are presented in Table 4. The octave band spectrum for the AHU intake / exhaust was taken from the manufacturer’s specification reports. The octave band spectrum of a typical plant from our in-house SoundPlan library was scaled and adjusted to sound power levels of the generators, stacks, and transformers of the Development.

**Table 4: Sound Power Levels and Spectrum of Noise Emitting Plant**

| Item                    | A-Weighted Octave Band Frequency Spectrum (Hz) |     |     |     |      |      |      |      | Sound Power Level  |
|-------------------------|--|-----|-----|-----|------|------|------|------|--------------------|
|                         | 63   | 125 | 250 | 500 | 1000 | 2000 | 4000 | 8000 | dB L <sub>WA</sub> |
| Generators (all)        | 91   | 96  | 86  | 88  | 91   | 87   | 84   | 74   | 99                 |
| AHU Intake              | 43   | 63  | 75  | 75  | 76   | 74   | 71   | 63   | 81                 |
| RAB Ventilation Louvres | 40   | 59  | 63  | 74  | 76   | 72   | 67   | 59   | 79 <sup>5</sup>    |
| Transformers (all)      | 13   | 49  | 65  | 64  | 63   | 62   | 57   | 53   | 70                 |
| Stacks (all)            | 43   | 59  | 66  | 75  | 77   | 78   | 85   | 85   | 89                 |

<sup>5</sup> Sound Power level per m<sup>2</sup> of the ventilation louvre (L<sub>WA</sub>/m<sup>2</sup>)

The above sources were modelled at their respective positions and scenarios along with other site buildings such as WTP plant room.

### 6.2.3.1 Model Parameters

The ISO 9613-2 method predicts the level of sound at a receptor by taking the octave band sound power level spectrum of the source, and applying a number of attenuation factors that determine the resulting Specific level at the receptor location. The following parameters were used in the prediction model and are considered to provide a conservative prediction of the noise levels likely to be experienced in practice:

- All plant operating simultaneously and at full capacity;
- Includes local terrain and buildings with respective heights above ground level;
- Ground absorption of  $G=1$  (hard) for hardstanding areas and  $G=0$  (soft ground) for surrounding ground between Development and NSRs;
- Generators modelled as radiating machines; calibrated to 75 dB(A) at 1 m distance;
- All Transformers modelled as point sources;
- AHU louvers (intake and relief air balcony) modelled as transmission areas on the buildings;
- Stacks modelled as point sources at 25,350 mm above ground, two generators exhaust to one stack, therefore, stack noise increased by 3 dB to a total emission of 78 dB(A) at 1 m; and
- Receivers placed at a height of 1.5 m above ground (head height) in front of the NSR façade facing the development

A noise map showing predicted Specific levels (i.e., noise levels prior to any rating corrections) is presented in Appendix C.

### 6.2.4 Rating Level Corrections

BS 4142 states that corrections should be applied to account for certain acoustic features which have the potential to increase the level of noise impact at nearby dwellings.

The acoustic features to be considered in the application of rating corrections are as follows:

- **Impulsivity:** No impulsive characteristics are anticipated from the Development;
- **Tonal Elements:** The main noise sources from the Development are the AHUs intake/outlets for the CWL01 and CWL02 buildings, which are broadband in nature, although transformers will be operational at the site, the transformers are small in size and unlikely to produce tonal noise at the receptors, as such, no tonal penalties have been applied.
- **Intermittency:** The plant will operate 24/7 under normal conditions, the Development will therefore not have “identifiable on / off conditions” in terms of BS 4142; no correction for intermittency was therefore applicable.
- **Distinctiveness:** BS 4142 states that a distinctiveness penalty is applied when no other correction is applicable, but the Development noise may be distinctive against the acoustic climate. Given that the predicted Specific levels are below the background noise level all times, and the Development is situated within an industrial/business park and not out of context of the area, no correction for distinctiveness has been applied.

Based on the above, no correction for acoustic features is applicable. The Rating level at the receptor location is therefore the same as the Specific level.

## 7. ASSESSMENT OF EFFECTS

### 7.1 Construction

Table 5 presents the sound pressure level at the nearest NSRs surrounding the proposed Site for the respective demolition phases. Demolition and construction are only planned to be undertaken during daytime (0700-1900) as such only daytime assessment to respective threshold is undertaken.

**Table 5: Assessment of Demolition Works**

| NSR             | Distance to Site, m | Predicted Sound Pressure Level (at NSR façade), dB, $L_{Aeq,t}$ |         | Difference to Category A Limit (65dB), dB |         |
|-----------------|---------------------|---|---------|---|---------|
|                 |                     | Phase1, 2, 2a   | Phase 3 | Phase1, 2, 2a                             | Phase 3 |
| Church Crescent | 250                 | 64  | 65      | -1  | 0       |
| The Stud Farm   | 340                 | 60  | 62      | -5  | -3      |
| Blacksmiths Way | 420                 | 58  | 60      | -7  | -5      |
| Powis Close     | 480                 | 57  | 58      | -8  | -7      |
| Pencarn Avenue  | 570                 | 58  | 60      | -7  | -5      |

It can be seen from table above that noise from Demolition activity does not exceeds the Limit A category at any NSR during all phases of work.

Table 6 presents the predicted sound pressure level at the nearest NSRs surrounding the proposed Site for the respective construction phases.

**Table 6: Assessment of Construction Works**

| NSR             | Predicted Sound Pressure Level (at NSR façade), dB, $L_{Aeq,t}$ and Difference ( $\Delta$ ) to Category A Limit (65dB), dB |               |                |               |             |               |                        |               |             |               |
|-----------------|--|---------------|----------------|---------------|-------------|---------------|------------------------|---------------|-------------|---------------|
|                 | Substructure   |               | Superstructure |               | Envelop     |               | Generator Installation |               | Fitout      |               |
|                 | $L_{Aeq,T}$  | $\Delta$ , dB | $L_{Aeq,T}$    | $\Delta$ , dB | $L_{Aeq,T}$ | $\Delta$ , dB | $L_{Aeq,T}$            | $\Delta$ , dB | $L_{Aeq,T}$ | $\Delta$ , dB |
| Church Crescent | 63   | -2            | 53             | -12           | 55          | -10           | 37                     | -28           | 62          | -3            |
| The Stud Farm   | 59   | -6            | 49             | -16           | 51          | -14           | 33                     | -32           | 58          | -7            |
| Blacksmiths Way | 58   | -7            | 47             | -18           | 49          | -16           | 33                     | -32           | 56          | -9            |
| Powis Close     | 56   | -9            | 46             | -19           | 48          | -17           | 30                     | -35           | 55          | -10           |
| Pencarn Avenue  | 54   | -11           | 44             | -21           | 46          | -19           | 28                     | -37           | 53          | -12           |

It can be seen that all NSR are below the relative Limit A threshold in terms of BS5228-1, as such, effects from (worst-case) construction noise are not expected to be significant.

#### 7.1.1 Construction Traffic Noise

As stated in Section 6.1.1, a construction programme is not available at this stage, therefore, a construction traffic noise assessment could not be undertaken. Subjectively; the proposed Development is located in an industrial / business park area, the area has two access roads coming off the A48 to the north which is a slip off road from the M4 motorway. Given that the construction traffic will be coming off major roads such as the M4 and A48 directly to the industrial area the change in traffic counts is expected to be negligible and therefore, noise effects to be minimal.

## 7.2 Operation

### 7.2.1 Scenario 1 – Normal Operation

An assessment of the likely impact from normal operation of the proposed Development has been made based on the difference between the Rating levels and representative background levels for daytime and night-time periods, as detailed in Section 3.3.3.

**Table 7: BS 4142 Assessment – Normal Operation**

| Receptor           | Rating Level, dB(A) | Background level, dB, LA90 |       | Difference, dB |       |
|--------------------|---------------------|----------------------------|-------|----------------|-------|
|                    |                     | Day                        | Night | Day            | Night |
| Church Crescent    | 36                  | 52                         | 46    | -16            | -10   |
| The Stud Farm      | 33                  | 43                         | 38    | -10            | -5    |
| Blacksmiths Way    | 32                  | 51                         | 46    | -19            | -14   |
| Pencarn Avenue     | 27                  | 51                         | 46    | -24            | -19   |
| The Parc Golf Club | 25                  | 43                         | 38    | -18            | -13   |
| Powis Close        | 21                  | 35                         | 32    | -15            | -12   |

Table 7 shows that the Rating levels at all receptors are less than the identified assessment criteria in Section 4. Noise from the Development is 5 dB or more below the background levels during both day and night periods at all locations, resulting in ‘no impact’ in terms of BS 4142.

### 7.2.2 Scenario 2 – Generator Testing

An assessment of the likely impact during Generator testing has been undertaken, presented in Table 9 below. As stated in section 6.2.2, the testing is to be undertaken over a single working day, outer generators located near the boundary i.e., generators closest to respective NSR in each direction is modelled, demonstrating worst-case noise output during the generator testing.

**Table 8: BS 4142 Assessment – Generator testing (worst-case)**

| Receptor           | Rating Level, dB(A) | Background level, dB, LA90 |       | Difference, dB |       |
|--------------------|---------------------|----------------------------|-------|----------------|-------|
|                    |                     | Day                        | Night | Day            | Night |
| Church Crescent    | 40                  | 52                         | -     | -12            | -     |
| The Stud Farm      | 36                  | 43                         |       | -7             |       |
| Blacksmiths Way    | 36                  | 51                         |       | -15            |       |
| The Parc Golf Club | 33                  | 43                         |       | -11            |       |
| Pencarn Avenue     | 32                  | 51                         |       | -19            |       |
| Powis Close        | 29                  | 35                         |       | -7             |       |

Table above shows that the rating levels during the generator testing does not exceed more than 5 dB below the background levels at all NSR during daytime. As generator testing will only be undertaken during the day noise impact during night-time is not relevant and as such a night-time assessment is not undertaken.

### 7.2.3 Scenario 3 – Emergency Operation

An assessment of the likely impact during emergency scenario has been undertaken, presented in Table 9 (over).

**Table 9: BS 4142 Assessment – Emergency Mode**

| Receptor           | Rating Level, dB(A) | Background level, dB, LA90 |       | Difference, dB |       |
|--------------------|---------------------|----------------------------|-------|----------------|-------|
|                    |                     | Day                        | Night | Day            | Night |
| Church Crescent    | 45                  | 52                         | 46    | -7             | -1    |
| Blacksmiths Way    | 42                  | 43                         | 38    | -1             | 4     |
| The Stud Farm      | 42                  | 43                         | 38    | -2             | 4     |
| Pencarn Avenue     | 37                  | 51                         | 46    | -14            | -9    |
| The Parc Golf Club | 37                  | 43                         | 38    | -6             | -1    |
| Powis Close        | 36                  | 35                         | 32    | 1              | 4     |

Table above shows that the rating levels during emergency scenario exceed the background levels at Blacksmiths Way and The Stud Farm by 4 dB during the night only and Powis Close during daytime by 1 dB and night-time by 4 dB. As stated in Section 6.2.2, this scenario is based on a power failure emergency event and does not represent the typical operation of the proposed Development.

### 7.2.4 Assessment of Industrial Unit & Offices

As stated in Section 5, directly north of the proposed Development is the NHS unit and offices, although the offices are low sensitivity receptors in terms of noise, the BS 8233 internal noise guide values for office have been adopted in this assessment to show effects from the proposed Development.

The assessment accounts for an open window attenuation of 15 dB  $D_n$ , this value is taken from research results undertaken by Napier University<sup>6</sup> and supporting research findings in the Environmental Research and Public Health journal<sup>7</sup>. The research shows that typical attenuation of slightly open or tilted windows ranges from 14 to 19 dB on average across frequencies, and as such a 15 dB attenuation has been taken as representative. Table 10 below presents the noise levels from the normal operation of the proposed Development.

**Table 10: BS 8233 Assessment of Nearest Offices**

| Receptor    | Predicted Level at facade, dB(A) | Open Window Attenuation, dB | Internal Noise, dB, $L_{Aeq,T}$ | Guide Level, dB(A) | Difference, dB |
|-------------|----------------------------------|-----------------------------|---------------------------------|--------------------|----------------|
| NHS Offices | 50                               | 15                          | 35                              | 50                 | -15            |

As seen above, noise from the normal operation of the Development is considerably less than the upper guide value for offices and will not therefore have significant effects on the offices from the Development operation.

## 7.3 Development Context

The Development is located in an industrial estate / business park area where the acoustic climate consists predominantly of the business unit and activities as well as the traffic noise from the nearby M4 motorway to the north. The proposed Development, as such, will not be out of context or readily distinctive against the existing acoustic environment of the area.

Results from normal operation and generator testing are within the agreed criteria of 5 dB or more below the respective background levels, given that the proposed Development is not out of context of

<sup>6</sup> NANR116: Open/Closed Window Research – Sound Insulation Through Ventilated Domestic Windows: Napier University 2007

<sup>7</sup> Barbara et al. Difference between Outdoor and Indoor Sound Levels for Open, Tilted, and Closed windows: International Journal of Environmental Research and Public Health.

the area, noise emitted from the Development is considered to have no significant impact on the amenity of the local residential dwellings.

Noise during an emergency scenario is expected to exceed the background levels at three NSRs (Table 9) during the night by 4 dB. Although this exceeds the criteria, this scenario will only take place in the unlikely event of a power failure, which will be rectified thereafter as soon as possible. Considering this context, the impact from the emergency scenario would be temporary and unlikely to occur regularly, and therefore, will not result in a significant impact on the quality of life or amenity of the local NSRs.

With regards to generator testing scenario, all residential NSR are within the criteria for this scenario, and for NHS offices directly north of the Development; the closest Generator testing will result in a façade level of 61 dB(A) i.e., an internal level of 46 dB(A), which is below the upper guide value for internal office noise levels and therefore, acceptable in terms of BS 8233.

BS 8233 also provides design targets for amenity spaces of the NSR, ranging from 50 to 55 dB(A) in noisier environments. As seen in Table 7 and Table 8, the highest rating level at the NSR is 40 dB(A), which is 10 dB (A) below the lower target for amenity spaces, therefore, noise within the amenity spaces are unlikely to exceed the target values defined in BS 8233.

## 7.4 Uncertainty

Modelling has been based on preliminary design and manufacturer's datasheets for the selected plant, a number of scenarios have been modelled to present the worst-case noise emissions possible for the proposed Development, modelling parameter have been chosen on the conservative basis (e.g., model assumes downwind conditions for all receptors, closest NSR façade facing the Development directly is chosen to represent receptors results etc.) and monitoring has been undertaken over a long duration (2 weeks) to reduce uncertainty in measured levels as far as reasonably practicable.

A number of conservative approaches have been taken; including assessments of generator testing and emergency mode to show worst-case noise emission scenarios, and long-term background / baseline monitoring for accurate representative levels. Given this conservative approach in the assessment and that rating levels are 5dB or more below the background levels at all receptors during normal operation, the Development noise will have minimal/negligible effects on the acoustic context of the area.

Therefore, the conservative assumptions made in this assessment will likely result in an over-prediction of the level of impact in practice. The uncertainties inherent in the assessment will therefore not have a significant impact on the outcome of the assessment.

## 8. MITIGATION

No mitigation other than those embedded in the design of the proposed Development is required. The demolition and construction noise (assessed as a worst-case) are expected to be within the BS5228-1 lower limit threshold; therefore, no specific mitigation is required for demolition and construction activities. However, the contractor is expected to follow good practice as advocated in BS 5228-1 & 2 to ensure construction activities do not give rise to excessive noise or vibration. Some good practice measures are detailed below which should be implemented to manage the effects of noise and vibration during construction activities:

- The Applicant shall prepare a site-specific Noise Management Plan (NMP) to manage noise during the demolition and construction phases of the Development;
- Construction operations shall be limited to times stated in the NMP, and agreed with the Local Planning Authority;

- Deliveries of HGV to Site to aim to only take place within daytimes (0700 – 1900), during demolition, construction and operation. There may be occasions where it is necessary to make certain deliveries outside these times, for example, where logistical issues result in delivery outside peak times;
- The site contractors shall be required to employ the best practicable means of reducing noise emissions from plant, machinery, and construction activities, as advocated in BS 5228-1:2009;
- Where practicable, the work programme should be phased, which would help to reduce the combined effects arising from several noisy operations;
- Where necessary and practicable, loud noise from fixed plant and equipment should be shielded with suitable acoustic enclosures or acoustic screens;
- All construction traffic should be directed through Celtic Way (off A48 roundabout) which comes through the middle of the business park and will result in the minimum effects to NSRs in the area.

## 9. CONCLUSION

An assessment of potential noise effects associated with the proposed Development has been carried out.

Predicted noise effects from three operational scenarios have been assessed; consisting of noise due to the normal operation of the Proposed Development, noise from generator testing (worst-case), and noise during emergency scenario (main power supply failure).

Predicted noise from all scenarios has been found to be within the acceptable criteria and result in 'low impact, depending on the context' in terms of BS 4142 at all receptors; the external rating levels do not exceed more than 5 dB below the background during the daytime and night-time in the normal operation and generator testing scenarios, and meet the agreed criteria at all receptors.

Demolition and construction noise is predicted on a worst-case basis and do not exceed the lower category BS 5228-1 threshold of 65 dB(A) at any NSR. Works are only expected to be undertaken during the daytime as such only daytime assessment has been undertaken. Given the low exceedance the impact is expected to be manageable by following the best practise principles outlined in Section 8.

Therefore, no significant effects are anticipated from demolition/construction works of the proposed Development or from operation of the Development in the three assessed scenarios, when considering the context.

## 10. GLOSSARY OF TERMS

**Decibel (dB):** The decibel is the basic unit of noise measurement. It relates to the cyclical changes in pressure created by the sound and operates on a logarithmic scale, ranging upwards from 0 dB. 0 dB is equivalent to the normal threshold of hearing at a frequency of 1000 Hertz (Hz). Each increase of 3 dB on the scale represents a doubling of the Sound Pressure and is typically the minimum noticeable change in sound level under typical listening conditions.

**dB(A):** Environmental noise levels are usually discussed in terms of dB(A). This is known as the A-weighted sound pressure level, and indicates that a correction factor has been applied, which corresponds to the human ear's response to sound across the range of audible frequencies. The ear is most sensitive in the middle range of frequencies (around 1000-3000 Hz), and less sensitive at lower and higher frequencies.

**A-Weighting:** The A weighted noise level is derived by analysing the level of a sound at a range of frequencies and applying a specific correction factor for each frequency before calculating the overall level. In practice this is carried out automatically within noise measuring equipment by the use of electronic filters, which adjust the frequency response of the instrument to mimic that of the ear.

**Frequency:** The frequency of a sound is equivalent to its pitch in musical terms. The units of frequency are Hertz (Hz), which represents the number of cycles (vibrations) per second.

**L<sub>A90,T</sub>:** This term is used to represent the A-weighted sound pressure level that is exceeded for 90% of a period of time, t. This is used as a measure of the background noise level.

**Noise:** Unwanted sound. May refer to both natural (e.g., wind, birdsong etc.) and artificial sounds (traffic, industrial noise, aircraft etc.).

**Z-Weighting:** A dB noise level, with no weightings (e.g., A-weighting) applied.

**Noise sensitive receptors:** Locations that may potentially be adversely affected by the addition of a new source of noise, such as residential properties.

**Sound power level (L<sub>w</sub>):** Sound power measured on the decibel scale, defined as the total acoustic energy of a sound emitting source.

**Background Sound:** The background sound level is the underlying level of noise present at a particular location for the majority (usually 90%) of a period of time.

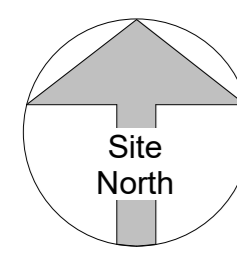
**Rating Level:** Sound levels which have been corrected for certain acoustic features, as required under BS4142 methodology.

**Sound pressure level (L<sub>p</sub>):** Sound pressure measured on the decibel scale, relative to a sound pressure of 2 x 10<sup>-5</sup> Pa.

**Specific Level:** In terms of BS4142 methodology, the specific level is the sound level produced by a source, without corrections for acoustic features.



## **APPENDIX A      PROPOSED DEVELOPMENT PLANS**



### SHEET NOTES

ALL VERTICAL DIMENSIONS ARE RELATIVE TO ASSOCIATED BUILDING SLAB LEVEL.

DO NOT SCALE FROM DRAWINGS. ALL DISCREPANCIES TO BE REPORTED TO GENSLER ARCHITECTS IMMEDIATELY. ALL DIMENSIONS TO BE VERIFIED BY CONTRACTOR ON SITE PRIOR TO ANY WORKS.

#### A-B-11 SHEET NOTES

| Sheet Note Number | Description                  |
|-------------------|------------------------------|
| 01                | SECURITY FENCE               |
| 02                | PRIMARY CAMPUS ENTRANCE      |
| 03                | SECONDARY CAMPUS ENTRANCE    |
| 04                | GUARD HOUSE                  |
| 05                | PRIMARY ENTRANCE BARRIERS    |
| 06                | BACK OF HOUSE GATE           |
| 07                | PARKING                      |
| 08                | BICYCLES                     |
| 09                | BIN STORE                    |
| 11                | CWL 01 ADMIN                 |
| 12                | CWL 01 DATA CENTRE           |
| 13                | LOADING DOCK                 |
| 14                | POND                         |
| 15                | SEWER PUMP STATION           |
| 16                | DAY 1 SUB-STATION            |
| 17                | FUTURE PRIMARY SUBSTATION    |
| 18                | SPRINKLER TANK AND PUMP ROOM |
| 19                | WATER TREATMENT BUILDING     |
| 20                | WATER STORAGE TANKS          |
| 21                | CWL 02 ADMIN                 |
| 22                | CWL 02 DATA CENTRE           |
| 23                | GENERATOR YARD               |
| 24                | SMOKE SHELTER                |
| 25                | EXTERNAL PLANT ROOM          |
| 26                | LIMS / E-HOUSE               |
| 27                | PV AREA TO ADMIN ROOF        |
| 28                | E HOUSE                      |
| 29                | BEE INSECT / BIRD BOX        |



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CWL01-02

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#### Design Team

|                     |          |
|---------------------|----------|
| Design              | GENSLER  |
| Drawn               | Gensler  |
| Checked             | J.E.     |
| Date                | 11.10.23 |
| Company Project No. | P-220340 |
| M.S. Project No.    | P-220340 |

#### Approvals

| CUSTOMER                      | MICROSOFT                               | Date |
|-------------------------------|---|------|
| Microsoft Design Manager      | LEWIS HOLLAND                           |      |
| Microsoft Electrical Engineer | MARK GLEESON                            |      |
| Microsoft Site/Est. Engineer  | ANDREW FREDER                           |      |
| Microsoft Mechanical Engineer | DAVID WREST                             |      |
| CSA                           | SHARON DENNIS, NAEEMU / STUART MCKERRON |      |
| Terrace                       | MARK KELLY / PAUL BISHOP                |      |
| Security Manager              | DAVID BEACLE                            |      |
| Environmental                 | DERONIE GORMAN                          |      |

#### PROJECT MANAGEMENT

|                          |  |      |
|--------------------------|--|------|
| Project Planner          |  | Date |
| Project Manager          |  |      |
| Senior Project Manager   |  |      |
| Development Manager      |  |      |
| Project Manager          |  |      |
| Quality Control Reviewer |  |      |
| Quality Control FT&E     |  |      |

### LEGEND

- SITE BOUNDARY
- - - - - EXISTING COMBINED SEWER TO BE DIVERTED OUTSIDE OF BOUNDARY
- - - - - EXISTING STORM WATER SEWER TO BE DIVERTED OUTSIDE OF BOUNDARY
- - - - - DIVERTED STORM WATER SEWER
- + RETAINED EXISTING TREES

#### SCHEDULE OF APPROX AREAS

|                     |                            |
|---------------------|----------------------------|
| SITE BOUNDARY (RED) | 165,4798.00 m <sup>2</sup> |
| CWL01 GIA           | 24,735.00 m <sup>2</sup>   |
| CWL02 GIA           | 10,230.00 m <sup>2</sup>   |

#### SCHEDULE OF PARKING

|                    |            |
|--------------------|------------|
| OVERALL PARKING    | 121 spaces |
| ELECTRIC PARKING   | 22 spaces  |
| ACCESSIBLE PARKING | 13 spaces  |
| CYCLE PARKING      | 40         |

#### Revisions

| No. | Date     | Description |
|-----|----------|-------------|
| P01 | 31.08.23 | PLANNING    |
| P02 | 12.09.23 | PLANNING    |
| P03 | 11.10.23 | PLANNING    |

#### Registration

#### Bar Code

#### Sheet Title/Number

SITE - PROPOSED  
MASTER PLAN

CWL01-02-  
A-P-07

1:1000@A0

## 01 PROPOSED MASTER PLAN

SCALE: 1:1000



## APPENDIX B      BASELINE NOISE SURVEY

## **B 1. INTRODUCTION**

- 1.1.1.1 Baseline noise monitoring was carried out between 08<sup>th</sup> of August and the 22<sup>nd</sup> of August 2023, to quantify the noise environment at locations close to the Project.
- 1.1.1.2 This section presents details of the data recorded during the survey and the analysis that has been carried out to derive the representative background sound level (RBSL) according to BS 4142<sup>1</sup> as well as other key metrics used to describe the baseline noise environment.
- 1.1.1.3 This appendix is set out as follows:
- Section B 2 presents the survey methodology.
  - Section B 3 presents an overview of the weather data measured over the survey period.
  - Section B 4 presents the results of the monitoring at the south end of the Site), and the analysis used to derive the RBSL.
  - Section B 5 presents the results of the monitoring at 10 Church Crescent, and the analysis used to derive the RBSL.
  - Section B 46 presents the results of the monitoring at Nantymor Cottages, and the analysis used to derive the RBSL.
  - Section B 7 presents the results of the monitoring at 43 Powis Close, and the analysis used to derive the RBSL.

## **B 2. METHODOLOGY**

### **B 1. EQUIPMENT AND SETUP**

- 1.1.1.4 Monitoring was carried out using Class 1 sound level meters (four Rion NL-52s set up as noise loggers). A weather station was set up at one location (at the south end of the Site) to record weather data throughout the survey period. A Rion WS-15 enhanced windshield with a large diameter windshield and a discrete secondary layer to minimize wind effects at the microphone was used with the two noise loggers.
- 1.1.1.5 The microphones were set at a height of approximately 1.5 m above the ground, and three of the four monitoring locations allowed for the measurement to be carried out in free-field conditions (i.e., at least 3.5 m from the nearest hard reflective surface). This was not the case for one of the locations, which it will be discussed further into this chapter.
- 1.1.1.6 The sound level meters were calibrated before the survey. Following the survey collection, the calibration levels were checked. No significant drift (i.e., > 0.5 dB) was observed. Copies of the SLM calibration certificates are available on request.

---

<sup>1</sup> BS 4142:2014 Methods for Rating and Assessing Industrial and Commercial Sound, British Standards Institute.

## B 1.2 DATA RECORDING

- 1.1.1.7 Noise measurements were carried out at four locations around the Project, the noise meters were installed and left to log 15-minute noise levels continuously for a period of approximately fifteen days. The noise monitoring locations are shown in Figure 1 of the main noise report.
- 1.1.1.8 Standard metrics including  $L_{Aeq}$ ,  $L_{A90}$  and  $L_{Amax,f}$  were recorded over the 15-minute intervals. In addition, meteorological data such as precipitation, wind speed and wind direction were continuously logged at one-minute intervals.
- 1.1.1.9 To minimise the influence on the measurements from sources of interference such as wind passing over the diaphragm of the microphone or rain falling on the microphone windshield, measurements made during rainfall events and wind speeds of greater than 5 m/s were discarded during data analysis. This follows the guidance given in BS 4142. The highest one-minute average wind speed recorded during each 15-minute noise measurement period was used to decide whether to discard noise measurements.
- 1.1.1.10 The weather during the survey period was relatively dry albeit with some periods of rainfall, and with wind speeds mostly less than 5 m/s. Consequently, only a very small proportion of the noise measurements had to be discarded.

## B 3. SURVEY WEATHER

- 1.1.1.11 **Error! Reference source not found.** on the following page, details the measurements of wind and rainfall recorded during the survey period. **Error! Reference source not found.**, in the following page details the measurements of wind direction recorded during the survey measured in graphed in degrees.

Figure B1 15-Minute Logged Rain and Wind Data, at the south end of the Site

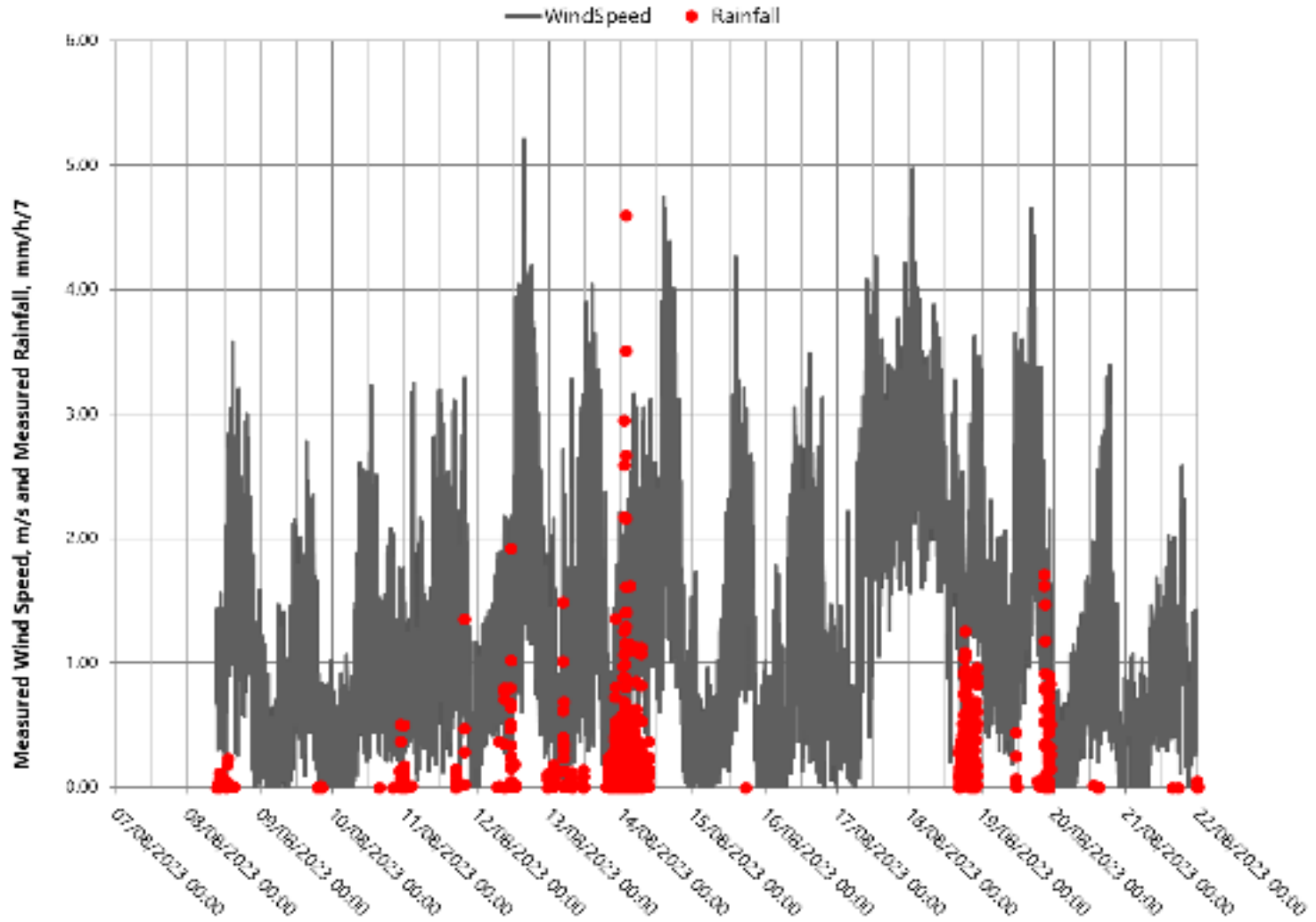
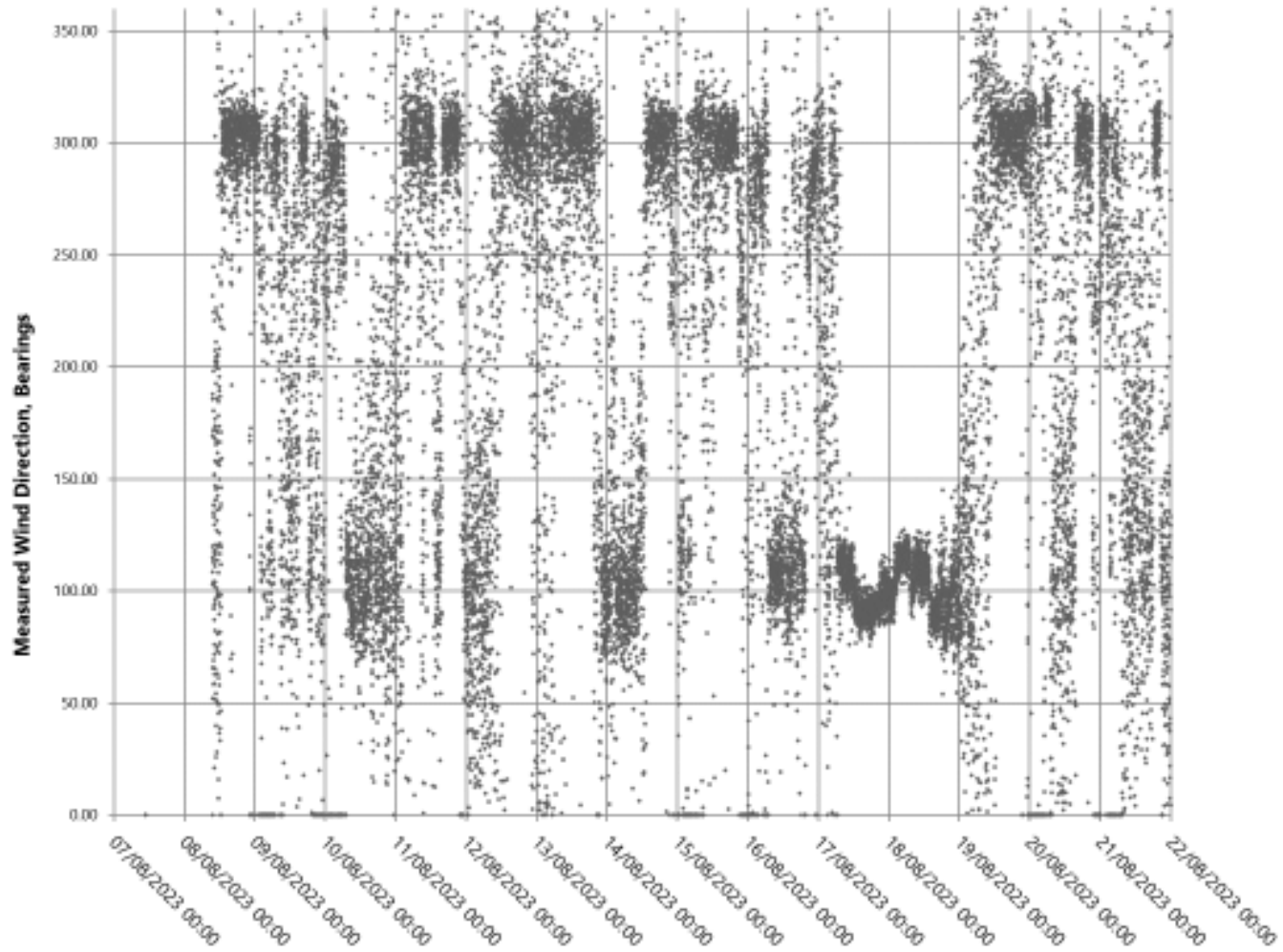


Figure B2 15-Minute Logged Wind Direction Data, at the south end of the Site



## B 4. R1 AT THE SOUTH END OF THE SITE

- 1.1.1.12 The charts below present the following information:
- Figure B4 presents the 15-minute noise measurements logged over the survey period for the key noise metrics;  $L_{Aeq}$ ,  $L_{Amax,f}$  and  $L_{A90}$ .
  - Figure B5 presents the distribution of daytime background  $L_{A90,15mins}$  noise levels over the survey period.
  - Figure B6 presents the distribution of night-time background  $L_{A90,15mins}$  noise levels over the survey period.
  - Table 1 and Figure B7 present the period  $L_{Aeq}$  noise levels over each day, evening, and night-time period.
- 1.1.1.13 Notes regarding the local noise environment, made during installation and collection of the equipment are as follows;
- 1.1.1.14 Dominant sources: constant low-level road traffic noise from the M4 / A48 nearby was the dominant source, as well as intermittent industrial noise from South-Southwest.
- 1.1.1.15 Secondary sources: Occasional faint noise overhead from aeroplanes. Not dominant sources.
- 1.1.1.16 Figure B3 below shows the monitoring equipment set-up at at the south end of the Site.

**Figure B3: Noise Monitoring Setup at the south end of the Site**

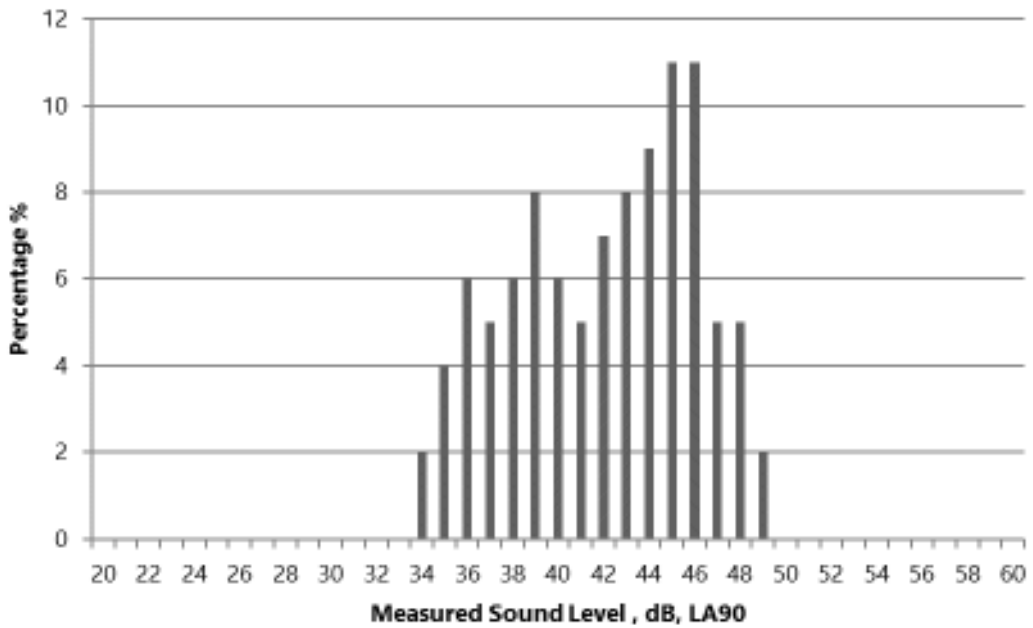




Figure B4 Results of the Noise Monitoring at the south end of the Site)– Noise Levels  $L_{Aeq}$ ,  $L_{A90}$ ,  $L_{max}$ , 15mins

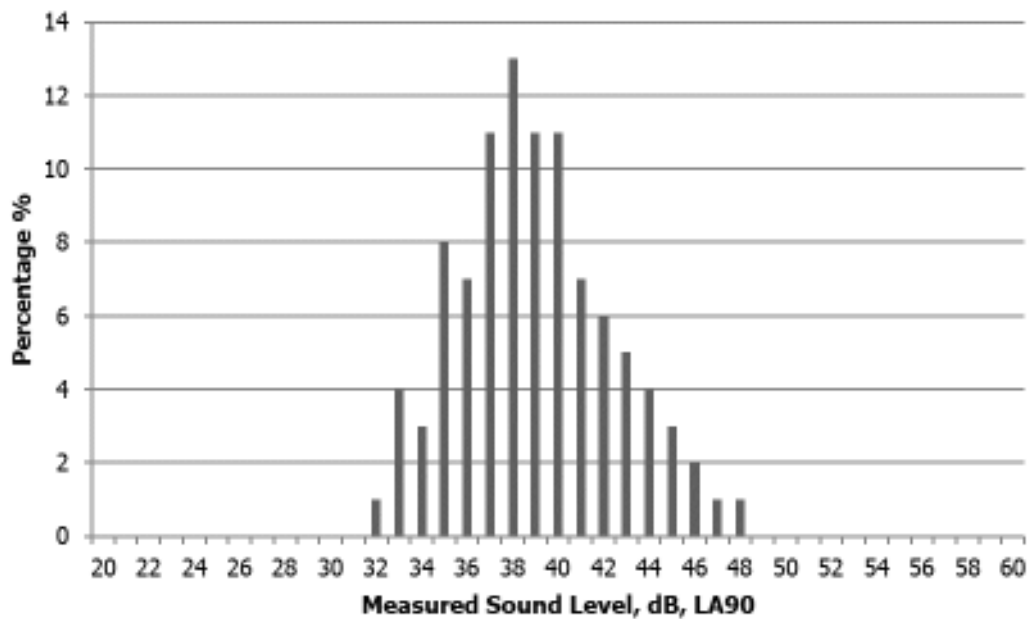


**Figure B5 Distribution of Daytime Background Levels LA90,15mins**



1.1.1.17 LA90 measurements ranged between 34 and 49 dB(A). Two peaks are evident at the values of 45 and 46 dB(A). The 50<sup>th</sup> percentile value is 43 dB(A). The lower of the two values, 43 dB(A), has conservatively been adopted as the RBSL.

**Figure B6 Distribution of Night-time Background Levels LA90,15mins**



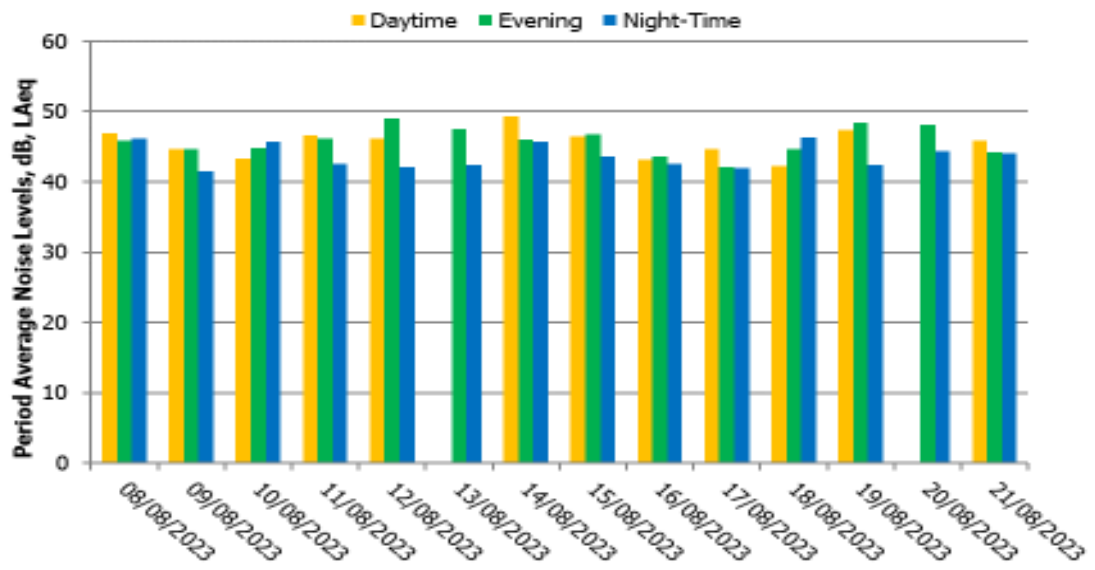
1.1.1.18

LA90 measurements ranged between 32 and 48 dB(A). A peak is evident at the modal value of 38 dB(A). The 50<sup>th</sup> percentile value is 39 dB(A). Therefore 38 dB has been adopted as the RBSL.

**Table 1      Period Average Noise Levels**

| Survey Period  |                | Noise Level, LAeq, period dB(A) |           |            |
|----------------|----------------|---------------------------------|-----------|------------|
| Date           | Day            | Daytime                         | Evening   | Night-Time |
| 08/08/2023     | Tuesday        | 47                              | 46        | 46         |
| 09/08/2023     | Wednesday      | 45                              | 45        | 41         |
| 10/08/2023     | Thursday       | 43                              | 45        | 46         |
| 11/08/2023     | Friday         | 47                              | 46        | 43         |
| 12/08/2023     | Saturday       | 46                              | 49        | 42         |
| 13/08/2023     | Sunday         | -                               | 47        | 42         |
| 14/08/2023     | Monday         | 49                              | 46        | 46         |
| 15/08/2023     | Tuesday        | 47                              | 47        | 44         |
| 16/08/2023     | Wednesday      | 43                              | 44        | 43         |
| 17/08/2023     | Thursday       | 45                              | 42        | 42         |
| 18/08/2023     | Friday         | 42                              | 45        | 46         |
| 19/08/2023     | Saturday       | 47                              | 48        | 42         |
| 20/08/2023     | Sunday         | -                               | 48        | 44         |
| 21/08/2023     | Monday         | 46                              | 44        | 44         |
| <b>Average</b> | <b>14 Days</b> | <b>46</b>                       | <b>46</b> | <b>44</b>  |

Figure B7 Period Average Noise Levels



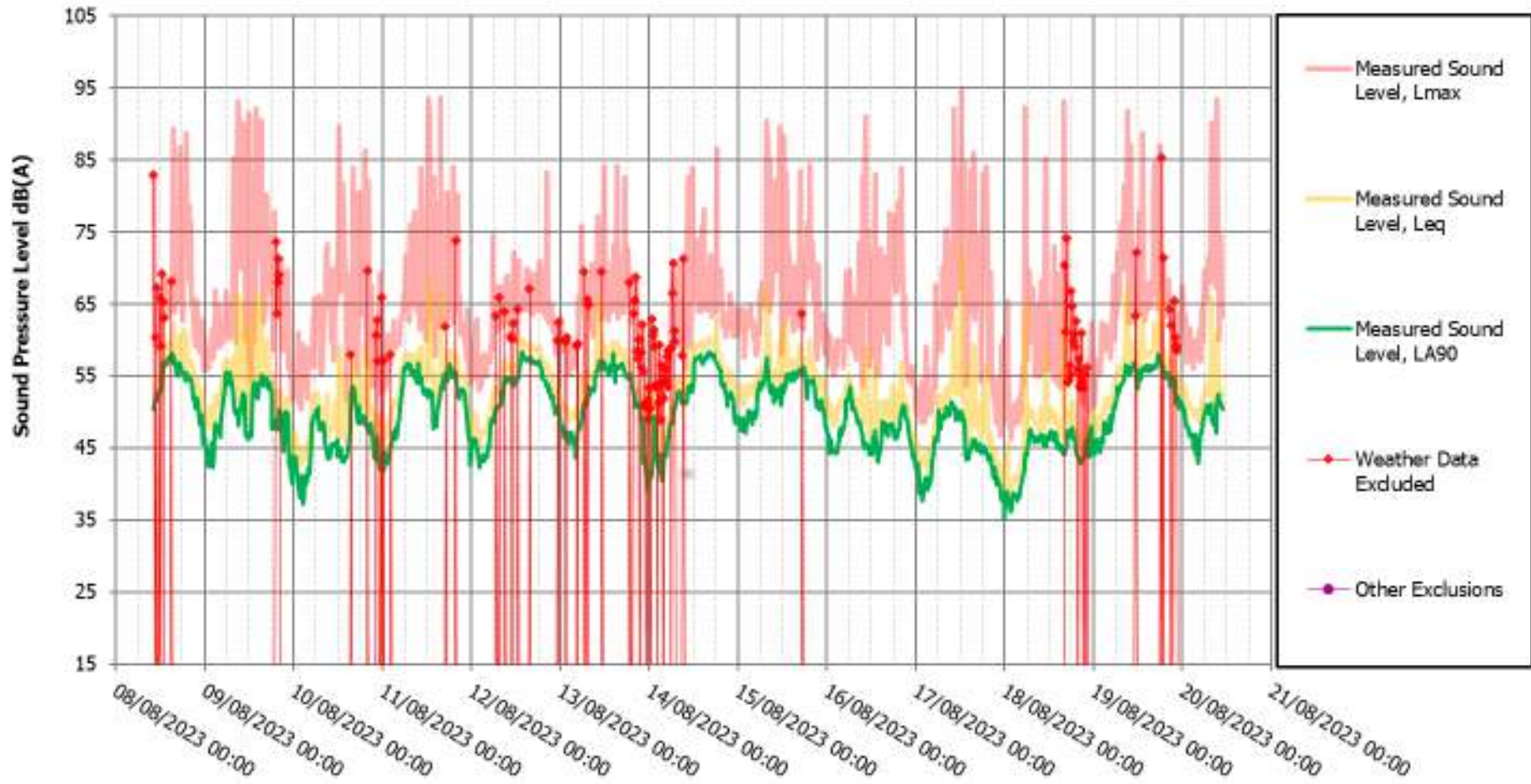
## B 5. R2 10 CHURCH CRESCENT

- 1.1.1.19 The charts below present the following information:
- Figure B10 presents the 15-minute noise measurements logged over the survey period for the key noise metrics;  $L_{Aeq}$ ,  $L_{Amax,f}$  and  $L_{A90}$ .
  - Figure B11 presents the distribution of daytime background  $L_{A90,15mins}$  noise levels over the survey period.
  - Figure B12 presents the distribution of night-time background  $L_{A90,15mins}$  noise levels over the survey period.
  - Table 2 and Figure B13 present the period  $L_{Aeq}$  noise levels over the day, evening, and night-time periods.
- 1.1.1.20 Notes regarding the local noise environment, made during installation and collection of the equipment are as follows;
- 1.1.1.21 Dominant Sources: constant low-level road traffic noise from the M4 / A48 nearby was the dominant source.
- 1.1.1.22 Secondary Sources: birdsong, trees rustling, wind.
- 1.1.1.23 Figure B9 below shows the monitoring equipment set-up at the 10 Church Crescent.

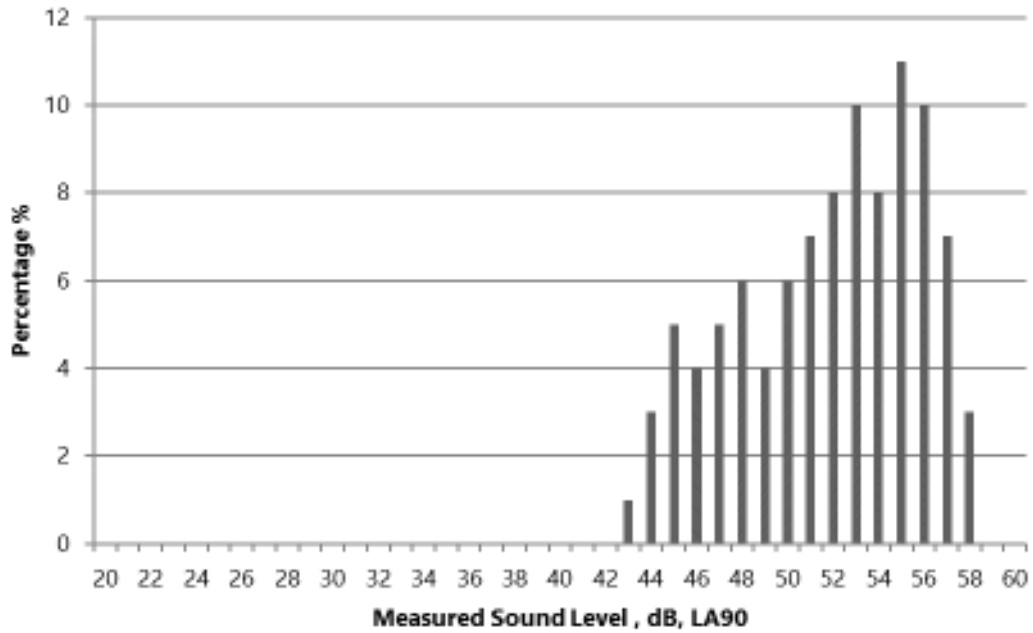
**Figure B1 Noise Monitoring Setup at 10 Church Crescent**



Figure B2 Results of the Noise Monitoring at the 10 Church Crescent – Noise Levels  $L_{Aeq}$ ,  $L_{A90}$ ,  $L_{max}$ , 15mins

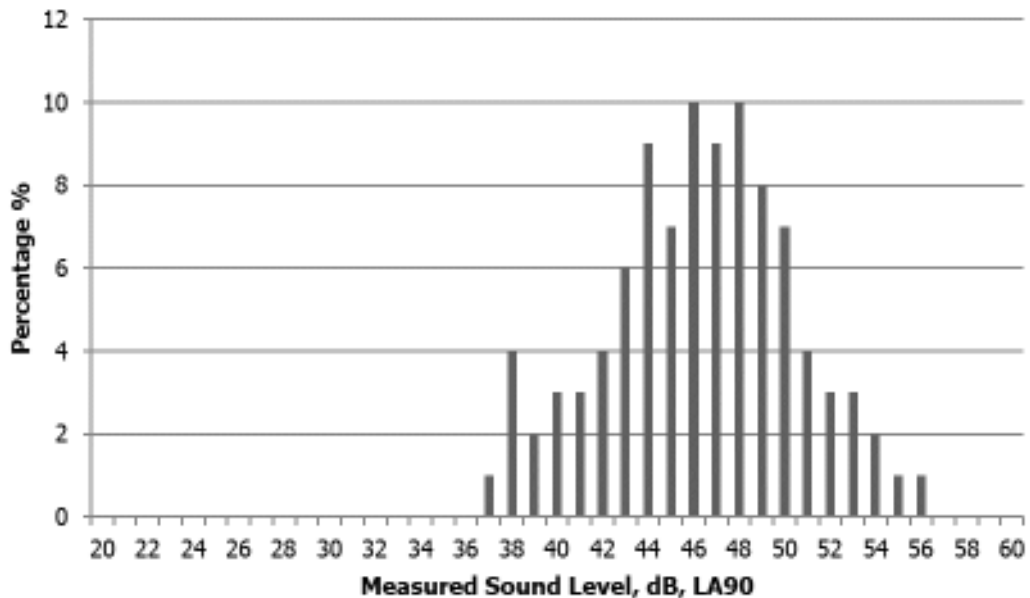


**Figure B3 Distribution of Daytime Background Levels LA90,15mins**



1.1.1.24 LA90 measurements ranged between 43 and 58 dB(A). A peak is evident at the modal value of 55 dB(A). The 50<sup>th</sup> percentile value is 52 dB(A). Therefore, the 52 dB(A) level has been adopted as the RBSL.

**Figure B4 Distribution of Night-Time Background Levels LA90,15mins**

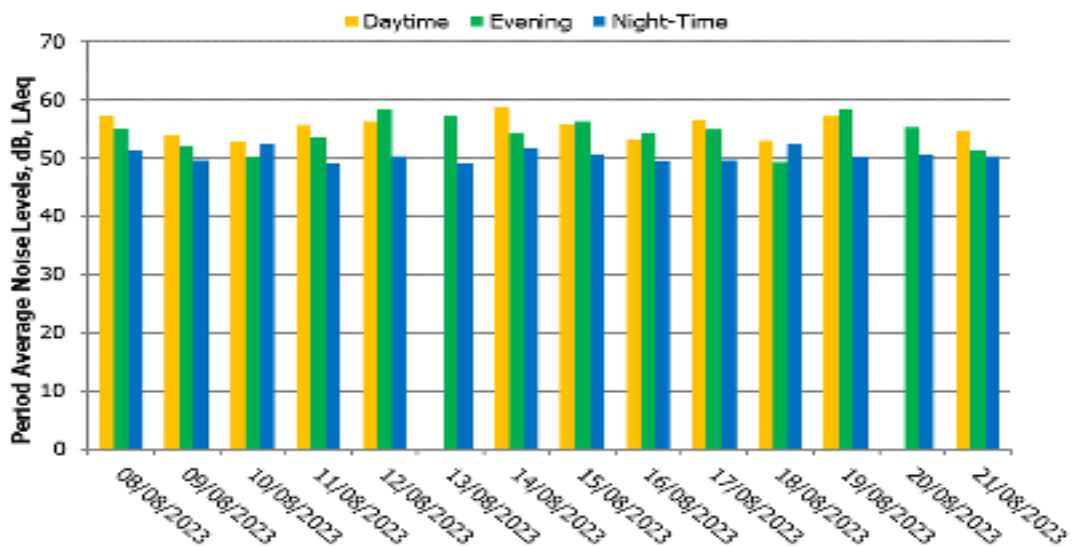


1.1.1.25 LA90 measurements ranged between 37 and 56 dB(A). Two peaks are evident at the values of 46 and 48 dB(A). The 50<sup>th</sup> percentile value is 47 dB(A). The lower peak value of 46 dB(A) has conservatively been adopted as the RBSL.

**Table 2 Period Average Noise Levels**

| Survey Period  |                | Noise Level, $L_{Aeq}$ , period dB |           |            |
|----------------|----------------|------------------------------------|-----------|------------|
| Date           | Day            | Daytime                            | Evening   | Night-Time |
| 08/08/2023     | Tuesday        | 57                                 | 55        | 51         |
| 09/08/2023     | Wednesday      | 54                                 | 52        | 50         |
| 10/08/2023     | Thursday       | 53                                 | 50        | 52         |
| 11/08/2023     | Friday         | 56                                 | 53        | 49         |
| 12/08/2023     | Saturday       | 56                                 | 58        | 50         |
| 13/08/2023     | Sunday         | -                                  | 57        | 49         |
| 14/08/2023     | Monday         | 59                                 | 54        | 52         |
| 15/08/2023     | Tuesday        | 56                                 | 56        | 51         |
| 16/08/2023     | Wednesday      | 53                                 | 54        | 50         |
| 17/08/2023     | Thursday       | 56                                 | 55        | 50         |
| 18/08/2023     | Friday         | 53                                 | 49        | 52         |
| 19/08/2023     | Saturday       | 57                                 | 58        | 50         |
| 20/08/2023     | Sunday         | -                                  | 55        | 51         |
| 21/08/2023     | Monday         | 55                                 | 51        | 50         |
| <b>Average</b> | <b>14 Days</b> | <b>55</b>                          | <b>54</b> | <b>50</b>  |

**Figure B13 Period Average Noise Levels**





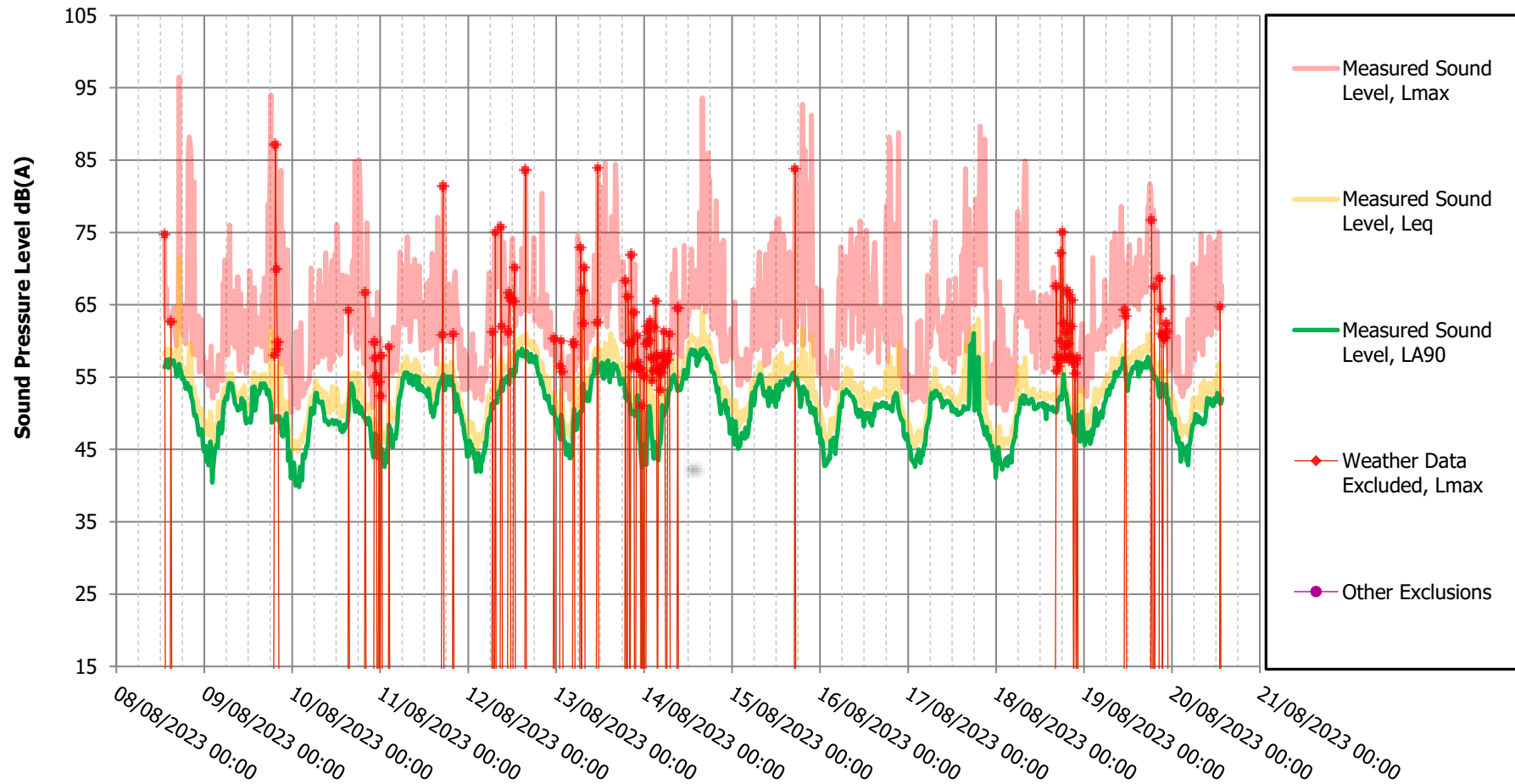
## B 6. R3 2 NANTYMOR COTTAGES

- 1.1.1.26 The charts below present the following information:
- Figure B15 presents the 15-minute noise measurements logged over the survey period for the key noise metrics;  $L_{Aeq}$ ,  $L_{Amax,f}$  and  $L_{A90}$ .
  - Figure B16 presents the distribution of daytime background  $L_{A90,15mins}$  noise levels over the survey period.
  - Figure B17 presents the distribution of night-time background  $L_{A90,15mins}$  noise levels over the survey period.
  - Table 3 and Figure B18 present the period  $L_{Aeq}$  noise levels over each day, evening, and night-time period.
- 1.1.1.27 Notes regarding the local noise environment, made during installation and collection of the equipment are as follows;
- 1.1.1.28 Dominant Sources: constant low-level road traffic noise from the M4 / A48 nearby was the dominant source,
- 1.1.1.29 Secondary sources: dogs barking, trees rustling, wind & birdsong. None of these noise sources were dominant, but all of them were clearly audible sources.
- 1.1.1.30 Figure B14 below shows the monitoring equipment set-up at 2 Nantymor Cottages.

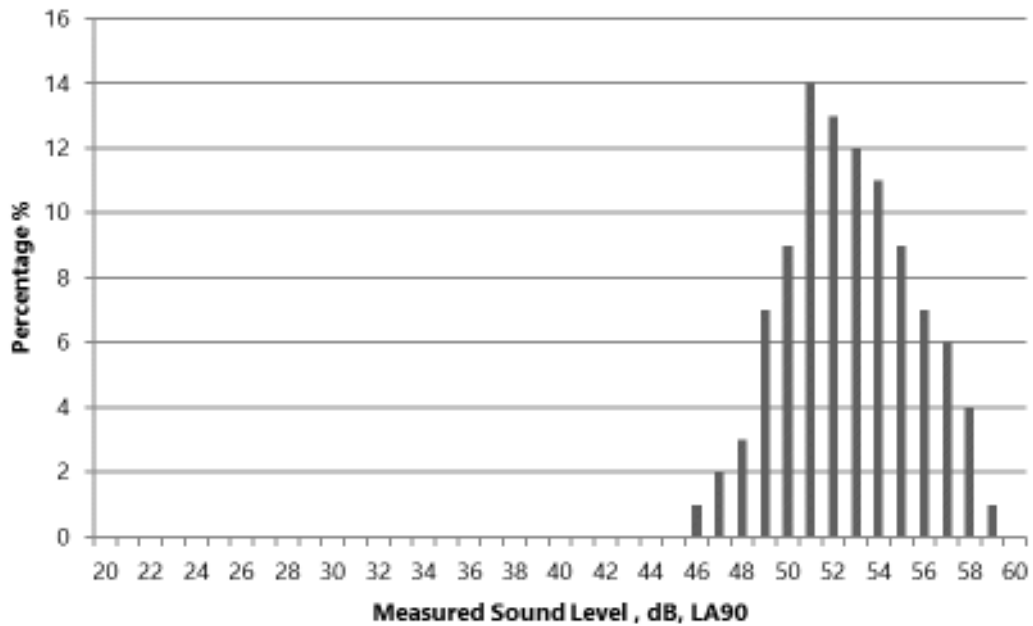
**Figure B14 Noise Monitoring Setup at 2 Nantymor Cottages**



Figure B15 Results of the Noise Monitoring at 2 Nantymor Cottages – Noise Levels  $L_{Aeq}$ ,  $L_{A90}$ ,  $L_{max}$ , 15mins

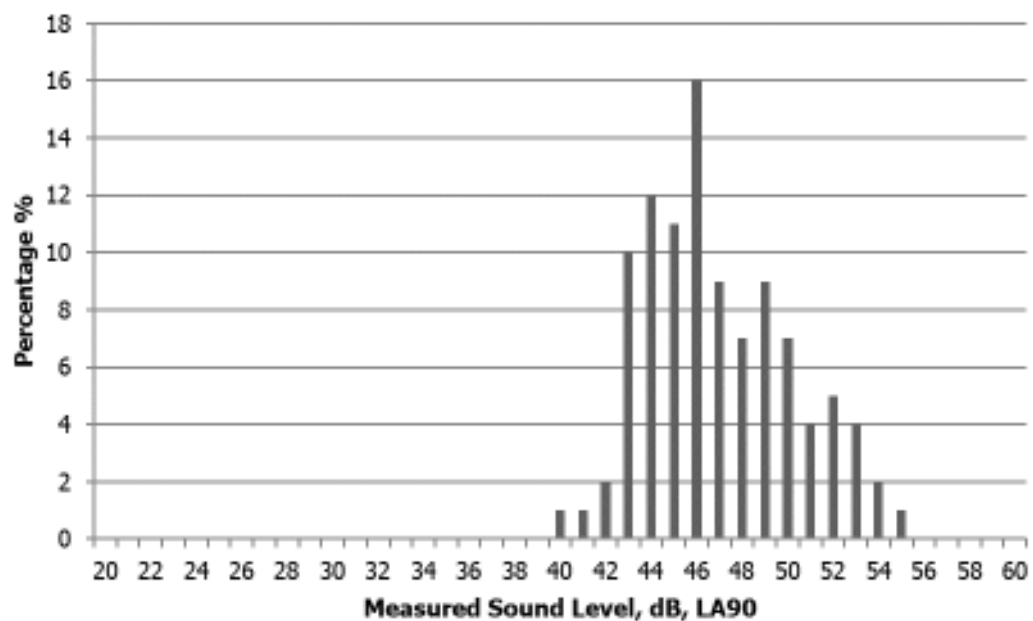


**Figure B16 Distribution of Daytime Background Levels LA90,15mins**



1.1.1.31 LA90 measurements ranged between 46 and 59 dB(A). One peak is evident at the modal value of 51 dB(A). The 50<sup>th</sup> percentile value is 53 dB(A). Therefore, the value of 51 dB(A), has conservatively been adopted as the RBSL.

**Figure B17 Distribution of Night-time Background Levels LA90,15mins**



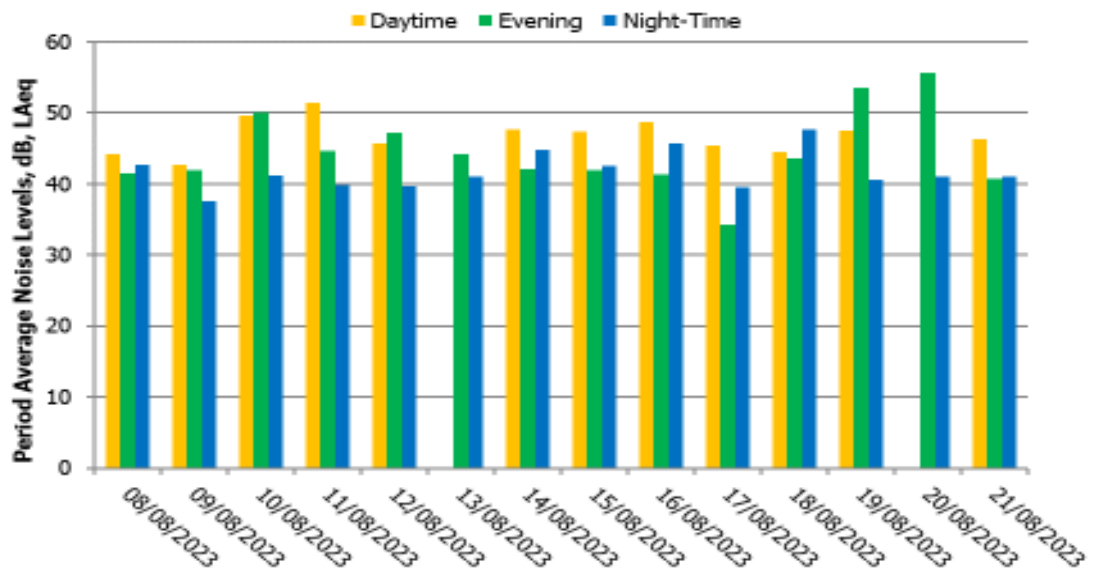
1.1.1.32

LA90 measurements ranged between 40 and 55 dB(A). A peak is evident at the modal value of 46 dB(A). The 50<sup>th</sup> percentile value is 46 dB (A). Therefore, the value of 46 dB(A) has been adopted as the RBSL.

**Table 2      Period Average Noise Levels**

| Survey Period  |                | Noise Level, LAeq, period dB |           |            |
|----------------|----------------|------------------------------|-----------|------------|
| Date           | Day            | Daytime                      | Evening   | Night-Time |
| 08/08/2023     | Tuesday        | 57                           | 56        | 53         |
| 09/08/2023     | Wednesday      | 59                           | 51        | 48         |
| 10/08/2023     | Tuesday        | 52                           | 53        | 53         |
| 11/08/2023     | Friday         | 59                           | 56        | 49         |
| 12/08/2023     | Saturday       | 55                           | 58        | 51         |
| 13/08/2023     | Sunday         | -                            | 58        | 46         |
| 14/08/2023     | Monday         | 58                           | 56        | 54         |
| 15/08/2023     | Tuesday        | 58                           | 56        | 52         |
| 16/08/2023     | Wednesday      | 51                           | 52        | 47         |
| 17/08/2023     | Thursday       | 58                           | 47        | 51         |
| 18/08/2023     | Friday         | 52                           | 46        | 51         |
| 19/08/2023     | Saturday       | 60                           | 59        | 52         |
| 20/08/2023     | Sunday         | -                            | 57        | 52         |
| 21/08/2023     | Monday         | 60                           | 53        | 51         |
| <b>Average</b> | <b>14 Days</b> | <b>57</b>                    | <b>54</b> | <b>51</b>  |

**Figure B18 Period Average Noise Levels**



## B 7. R4 43 POWIS CLOSE

- 1.1.1.33 The charts below present the following information:
- Figure B20 presents the 15-minute noise measurements logged over the survey period for the key noise metrics;  $L_{Aeq}$ ,  $L_{Amax,f}$  and  $L_{A90}$ .
  - Figure B21 presents the distribution of daytime background  $L_{A90,15mins}$  noise levels over the survey period.
  - Figure B22 presents the distribution of night-time background  $L_{A90,15mins}$  noise levels over the survey period.
  - Table 4 and Figure B23 present the period  $L_{Aeq}$  noise levels over each day, evening, and night-time period.
- 1.1.1.34 Notes regarding the local noise environment, made during installation and collection of the equipment are as follows;
- 1.1.1.35 It was not possible to position the sound level meter 3.5 m from all surfaces because of the size of the garden. The meter was set up approximately 2 m from either side of the garden and approximately 3 m from garden shed. BS 4142 suggests a correction of -3 dB is applied when the noise meter at a distance of 1 m from a façade (and when measured noise sources are distant). This is to account for increases in the measured sound level due to reflections. Although the noise meter installation position was further from the nearest surfaces than 1 m, there were several nearby surfaces. Therefore the full correction of -3 dB has been applied to the sound level measurements carried out at this location.
- 1.1.1.36 Dominant Sources: constant low-level road traffic noise from the M4 and A48 was the dominant source.
- 1.1.1.37 Secondary sources: faint noise from overhead aeroplanes. A wooden garden windchime produced sporadic noise. None of these noise sources were dominant.
- 1.1.1.38 Figure B19 below shows the monitoring equipment set-up at 43 Powis Close.

**Figure B19 Noise Monitoring Setup at 43 Powis Close**

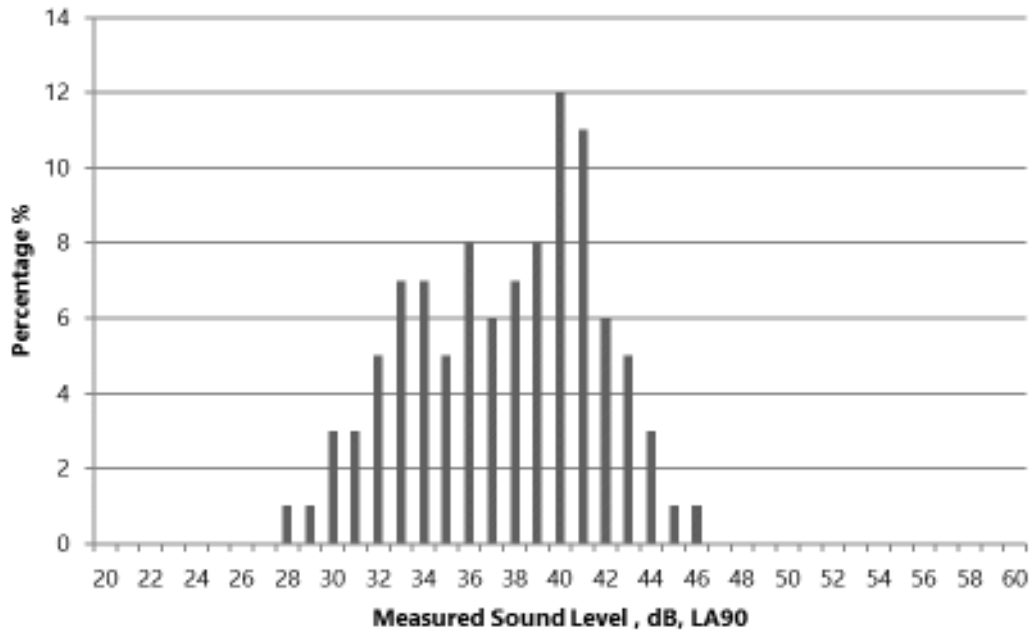


Figure B20 Results of the Noise Monitoring at 43 Powis Close – Noise Levels  $L_{Aeq}$ ,  $L_{A90}$ ,  $L_{max}$ , 15mins



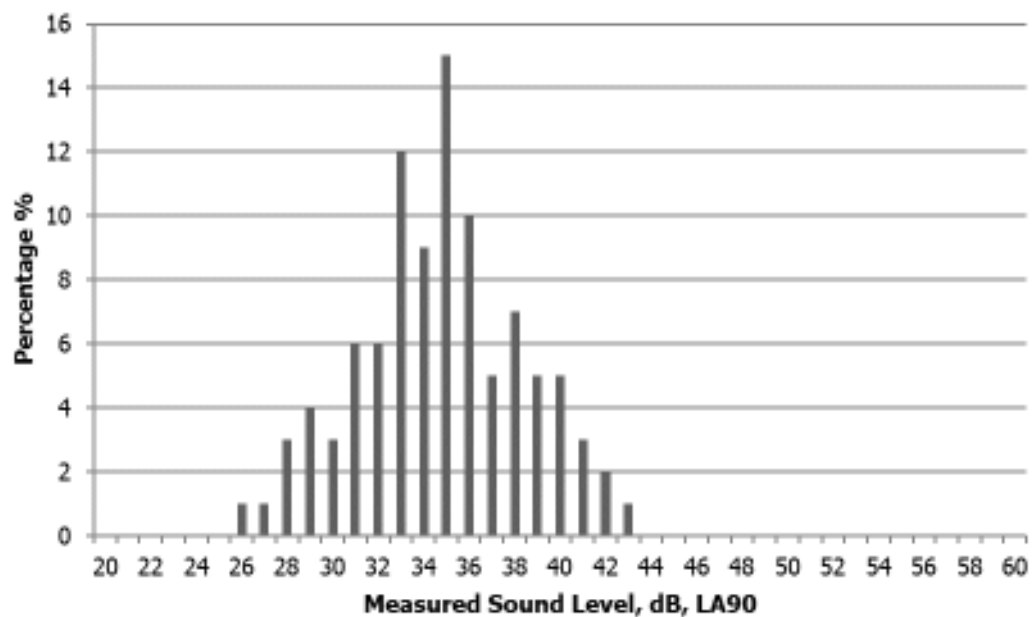


**Figure B21 Distribution of Daytime Background Levels LA90,15mins**



1.1.1.39 LA90 measurements ranged between 28 and 46 dB(A). One peak is evident at the modal value of 40 dB(A). The 50<sup>th</sup> percentile value is 38 dB(A). The 50<sup>th</sup> percentile value has conservatively been adopted. Applying a correction of -3 dB for reflections (as discussed above) results in a RBSL of 35 dB(A).

**Figure B22 Distribution of Night-time Background Levels LA90,15mins**



1.1.1.40 LA90 measurements ranged between 26 and 43 dB(A). A peak is evident at the modal value of 35 dB(A). The 50<sup>th</sup> percentile value is 35 dB (A). Applying

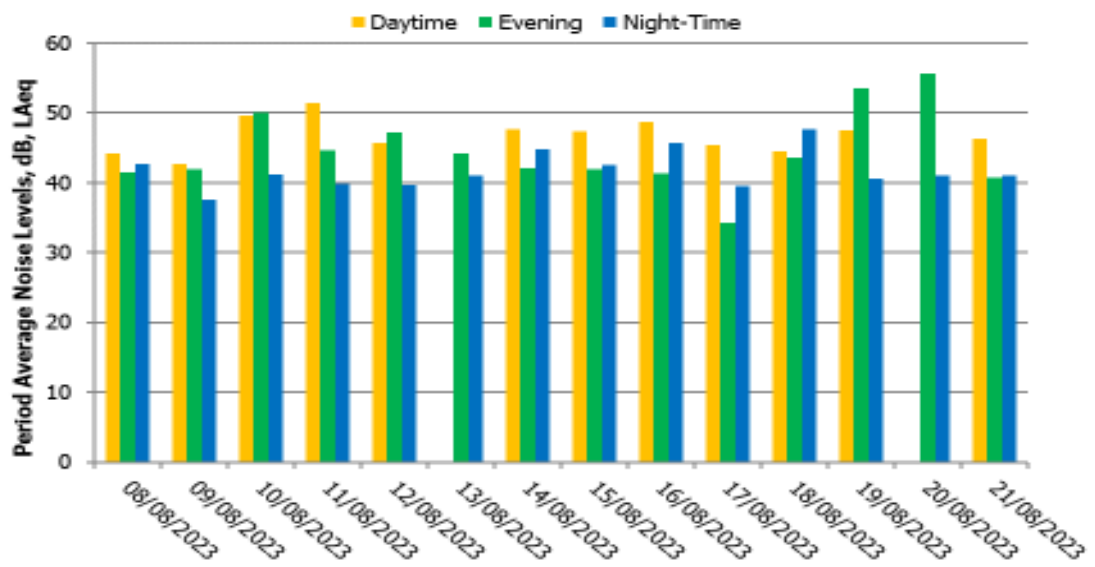
a correction of -3 dB for reflections (as discussed above) results in a Therefore, the level of 35 dB(A) has been adopted as the RBSL. Applying a correction of -3 dB for reflections (as discussed above) results in value of 32 dB(A) which has been adopted as the RBSL.

**Table 3 Period Average Noise Levels**

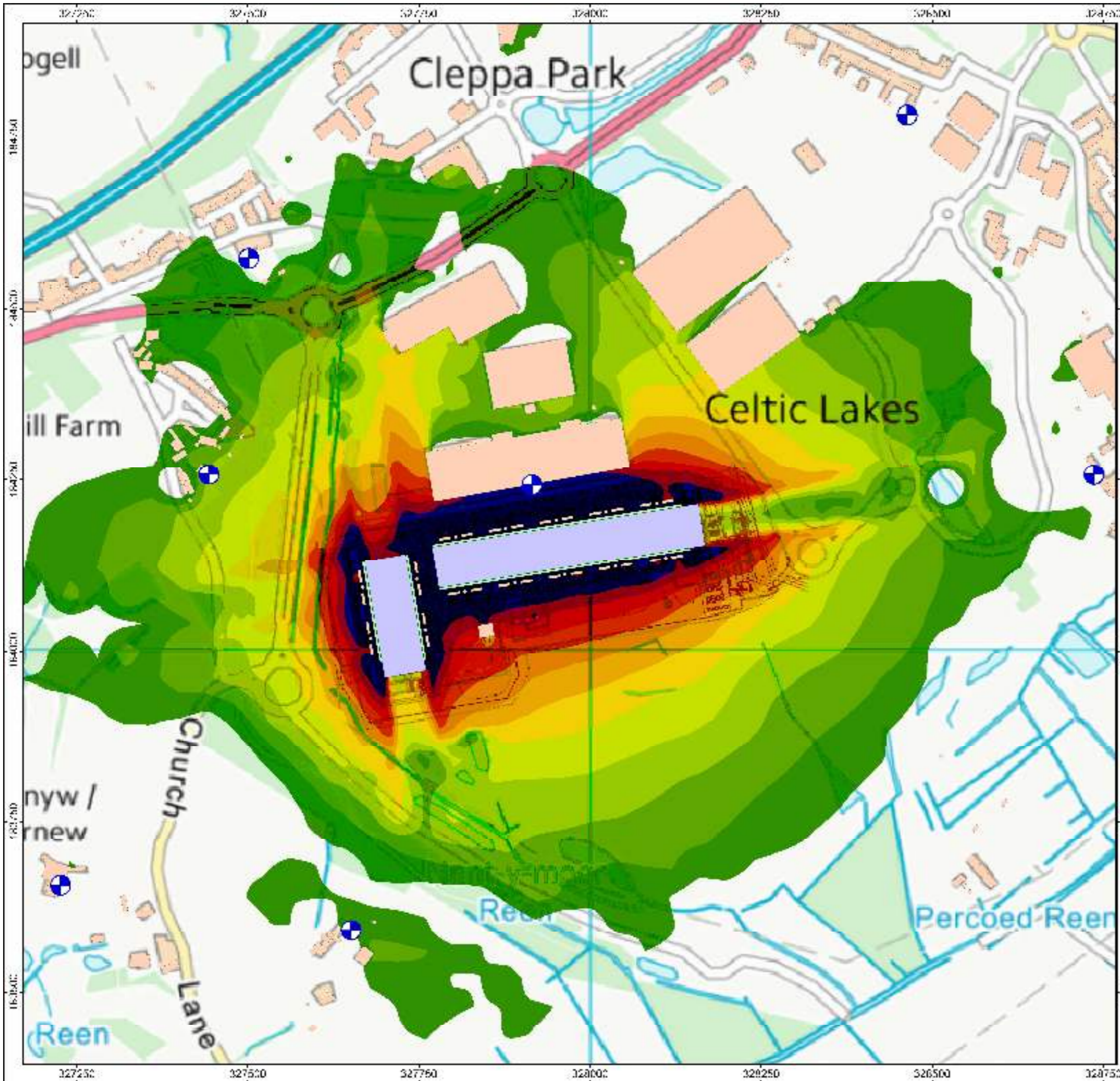
| Survey Period                 |                | Noise Level, $L_{Aeq, period}$ dB |           |            |
|-------------------------------|----------------|-----------------------------------|-----------|------------|
| Date                          | Day            | Daytime                           | Evening   | Night-Time |
| 08/08/2023                    | Tuesday        | 44                                | 41        | 43         |
| 09/08/2023                    | Wednesday      | 43                                | 42        | 38         |
| 10/08/2023                    | Thursday       | 50                                | 50        | 41         |
| 11/08/2023                    | Friday         | 51                                | 45        | 40         |
| 12/08/2023                    | Saturday       | 46                                | 47        | 40         |
| 13/08/2023                    | Sunday         | -                                 | 44        | 41         |
| 14/08/2023                    | Monday         | 48                                | 42        | 45         |
| 15/08/2023                    | Tuesday        | 47                                | 42        | 43         |
| 16/08/2023                    | Wednesday      | 49                                | 41        | 46         |
| 17/08/2023                    | Thursday       | 45                                | 34        | 39         |
| 18/08/2023                    | Friday         | 44                                | 44        | 48         |
| 19/08/2023                    | Saturday       | 47                                | 54        | 41         |
| 20/08/2023                    | Sunday         | -                                 | 56        | 41         |
| 21/08/2023                    | Monday         | 46                                | 41        | 41         |
| <b>Average <sup>(1)</sup></b> | <b>14 Days</b> | <b>44</b>                         | <b>41</b> | <b>39</b>  |

1) As discussed above, a correction of -3 dB has been applied to account for reflections in the measured sound levels.

Figure B23 Period Average Noise Levels



## APPENDIX C      NOISE CONTOUR MAP



Customer: Red Engineering (Microsoft)  
 Project: Newport Quinn Datacentre  
 Project-No. 0654550



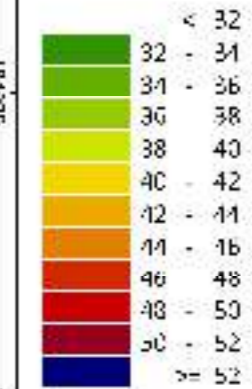
Appendix

C

NormalOP-NoiseMap\_V1\_BA  
 Result number 5  
 Calculation in 1.5 m above ground

Project engineer: BA  
 Created: 05/10/2023  
 Processed with: SoundPLAN 8.2, Update 16/07/2020

Levels Lr24hr  
 in dB(A)

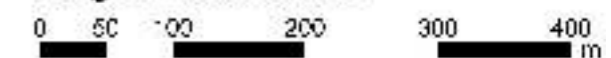


Signs and symbols

- Main building
- Wall
- Transparency wall areas
- Point receiver
- Transformers/Stacks
- CW2 & CW22 Building
- A.L. Louies



Length scale 1:5700



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