Gas Turbine Introduction and Vibration Diagnostic Basics

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Gas Turbine Introduction

Styles of Gas Turbines

- Micro-turbines typically produce tens to hundreds of kW. Some corporations advertise micro-turbines up to 1 MW, but that size of this style of machine is rare to date with most being in sizes less than 400 kW.
- Aero-derivative gas turbines Typically range in size from one MW to tens of MW. There is considerable use of this technology presently being used to improve performance efficiencies of larger 'frame' size gas turbines.
- Large frame gas turbines Typically range in size from just under 100MW to over 300 MW with current technology

Today's topic will be the large frame gas turbines



Gas Turbine Introduction

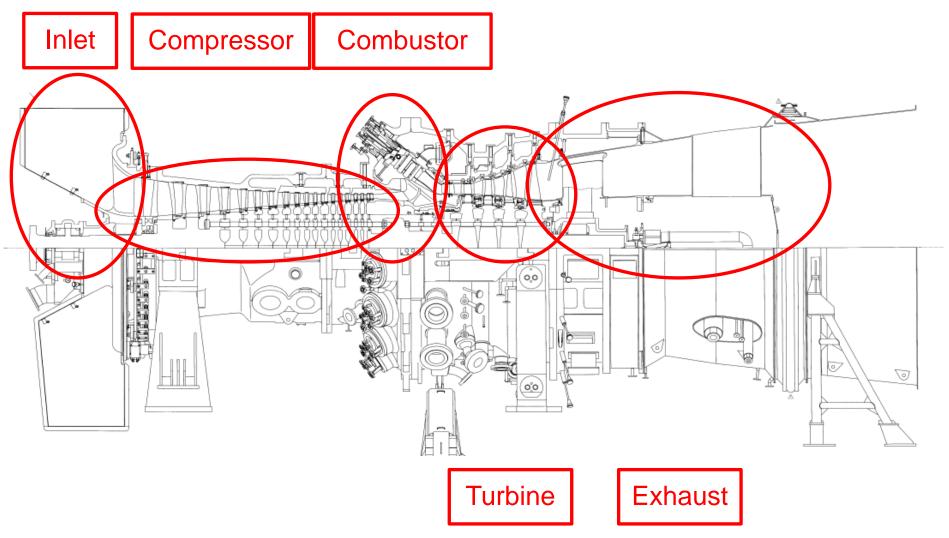


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Gas Turbine Basics – Major Sections

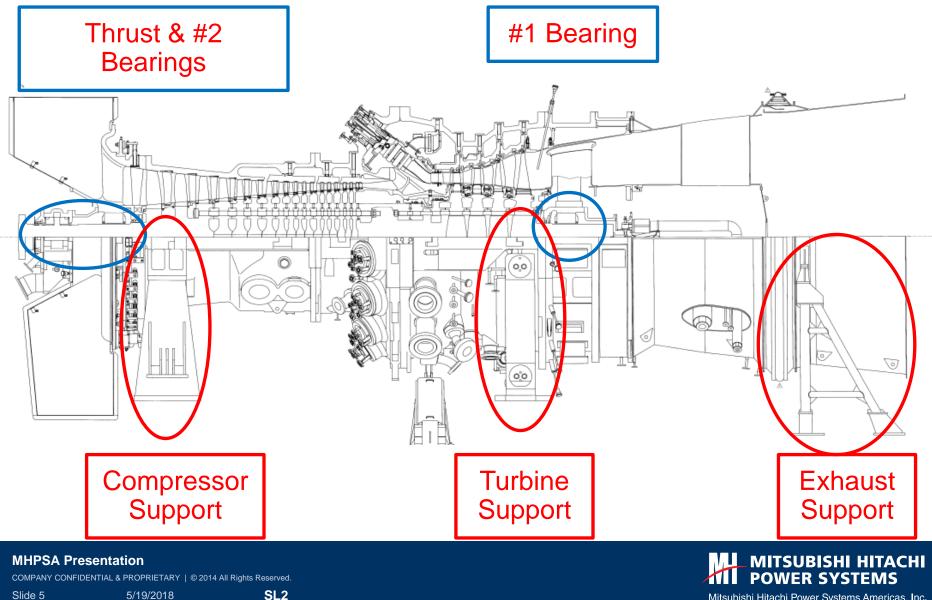


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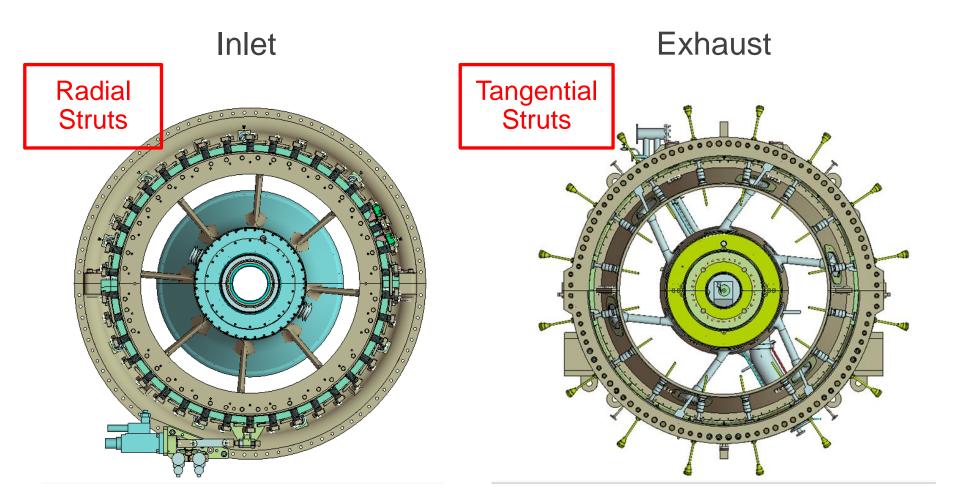
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Gas Turbine Basics – Structural Support



Gas Turbine Basics – Bearing Support



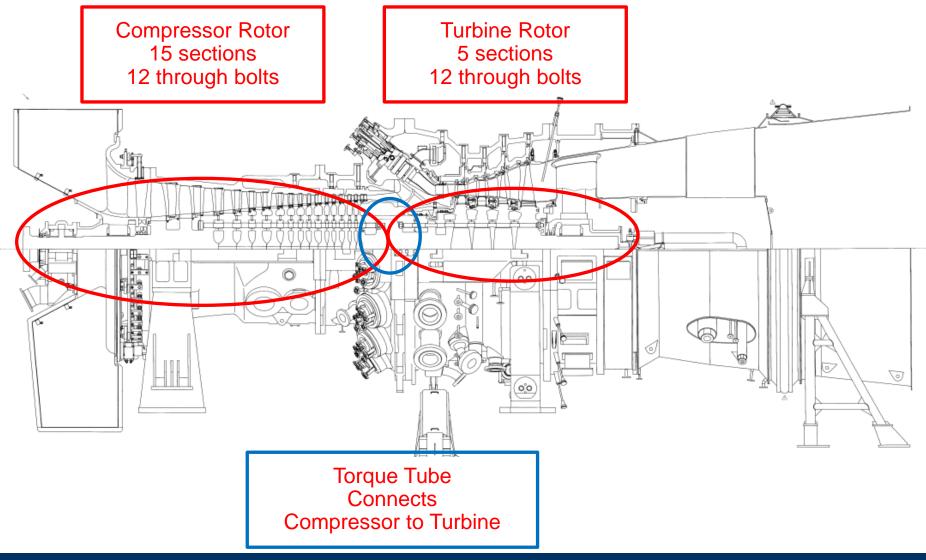
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Gas Turbine Basics - Rotor

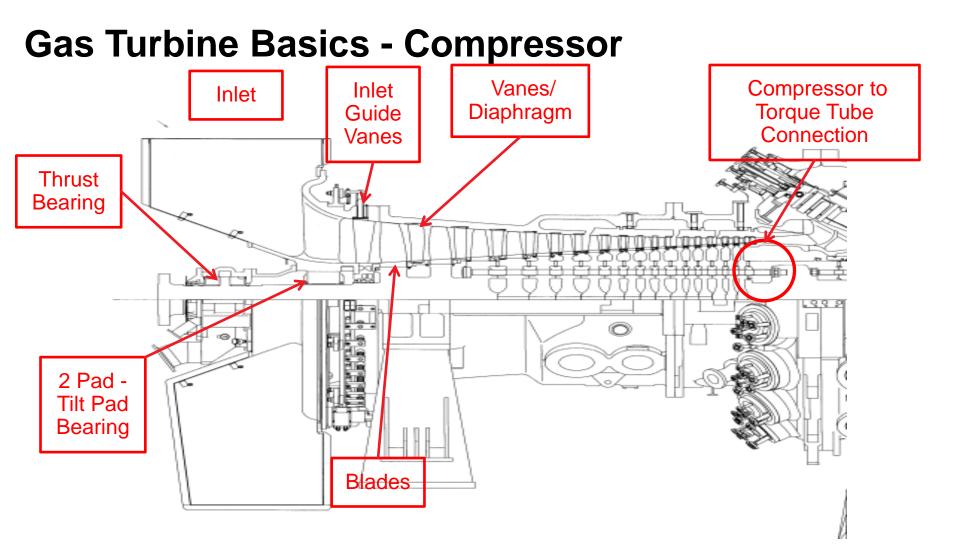


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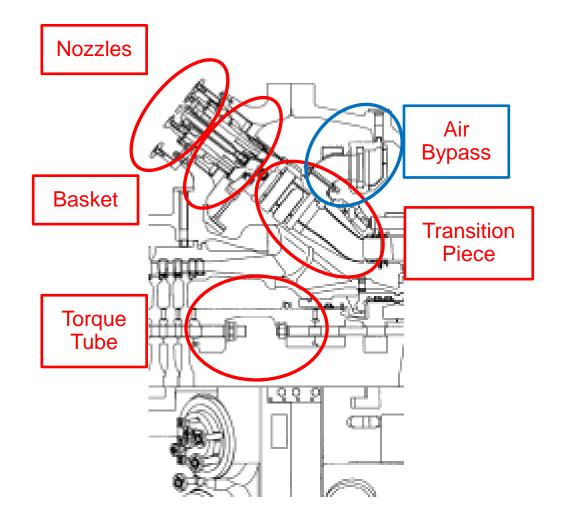


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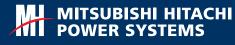


Gas Turbine Basics – Combustor Section

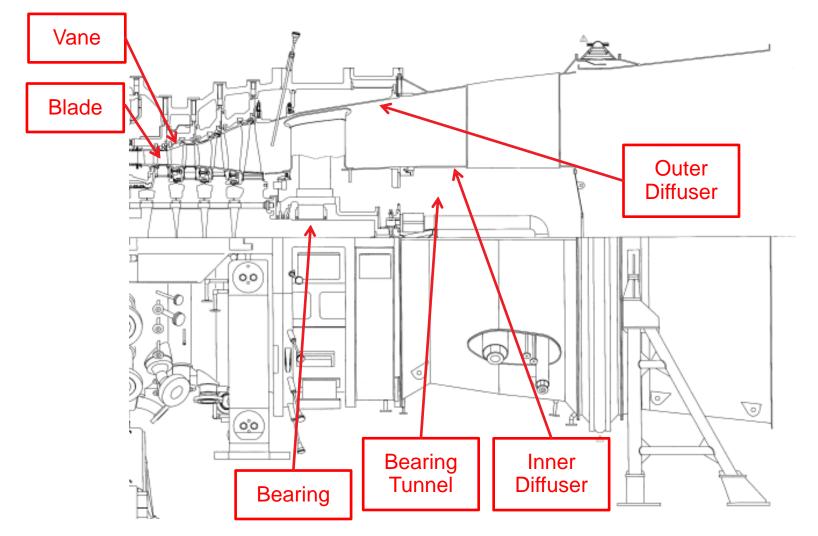


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Gas Turbine Basics

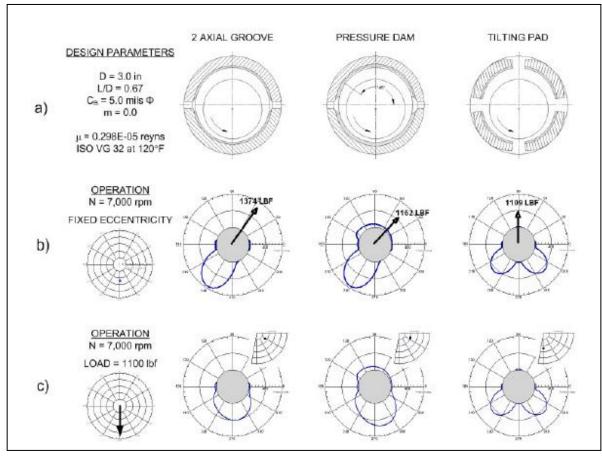


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Gas Turbine Basics



Know your bearings. Different bearings designs produce different operational characteristics.

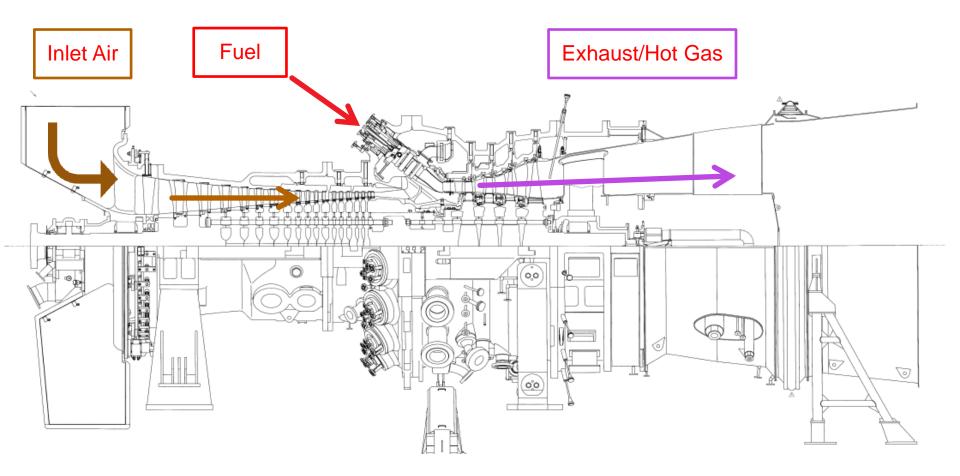
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Gas Turbine Basics – Air and Fuel flows



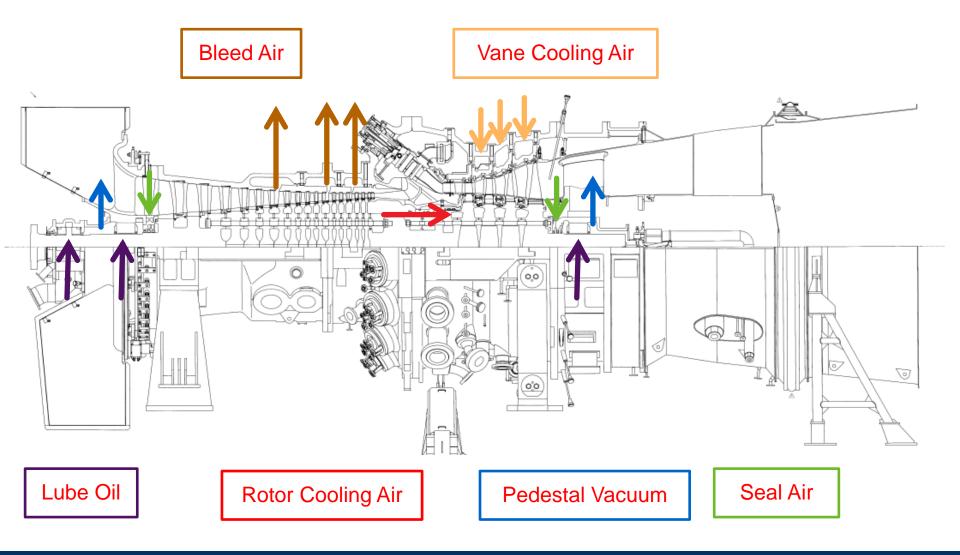
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Gas Turbine Basics – Auxiliary Systems



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Gas Turbine Basics

Characteristics of Gas Turbines Rotors

- Rotor Flexibility
- Will typically operate above the 2nd critical
- Bearing supports The connection from the bearings to the foundation are much more complex than other large turbo-machinery. This affects bearing foundation stiffness and thus rotor and machine operational characteristics
- At 3600 rpm 'Full Speed No Load' a gas turbine is still near 2/3 of total power coming from the turbine end to drive the compressor. So even at full speed/no load these machines are not truly idling, and the operational data is meaningful. Although there is still thermal transient to go through during startup conditions that depending on insulation condition, ambient temperatures, etc. will still take many hours to stabilize. Foundations can take a full day or more to stabilize.



Forces on the machine

- Forces that act on a machine
 - Internal influences interaction with parts of itself
 - Support forces in bearings
 - Forces resulting from shaft deflection
 - Fluid dynamics and subsequent forces
 - External influences forces that are applied to the rotor system
 - Axial Restraint Rub
 - Casing distortion Rub
 - Static radial loads Rotor to rotor Misalignment
 - Unbalance typically considered and handled as an external force



Rotor System Parameters

- Rotor System Parameters
 - Mass
 - Stiffness
 - Damping

The equation below describes how displacement, force, and dynamic stiffness are related.

$$\overrightarrow{\text{Displacement}} = \frac{\sum \overrightarrow{\text{Forces}}}{\sum \overrightarrow{\text{Dynamic Stiffness}}}$$

A change in displacement (vibration) is due to a change in the force applied or stiffness of the system. The equation below shows the relationship between frequency, stiffness, and mass.

$$F_n = \frac{1}{2}\Pi \times \sqrt[2]{\frac{k}{M}}$$

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Rotor System Parameters

Using the foundation of the previous information the following equation was developed to describe the motion of a shaft:

Rotor Equation of Motion (for fluid film bearings):

Fs +Ft +Fd +Fp =Mr

Spring stiffness + Tangential stiffness + Damping force + Pertubation force = mass x acceleration

 $-Kr + jD\lambda\Omega r - D\dot{r} + mr_{\mu}\omega^2 e^{j(\omega t + \delta)} = M\ddot{r}$

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Reference: Fundamentals of Rotating Machinery Diagnostics – Charles T. Hatch & Donald E. Bently

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- Instrumentation Error
- Unbalance
- Misalignment
 - Rotor to rotor
 - Casing to rotor
 - Radial
 - Axial
- Bearing Damage or excessive clearance
- Rotor Bow
- Looseness
- Fluid Induced Instability
- Shaft Crack
- Resonance

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- Instrumentation Error
 - Loose connections spikey signal
 - Failing sensor
 - Drift change in scale factor
 - Improperly matched components change in scale factor
 - Incorrect calibration change in scale factor

• Unbalance

- Initial/Residual unbalance condition
- Loss of balance weight
- Loss of blade mass
- Increase in blade mass





- Misalignment
 - Rotor to rotor
 - Change in relative bearing position
 - Rotor to casing
 - Radial
 - Axial
- Bearing Damage or excessive clearance
 - Babbitt damage
 - Tilt pad tilting/rocking mechanism wear
- Rotor Bow
 - Assembly issue
 - Thermal distortion (also known as thermal sensitivity)





- Looseness
 - Bearing components
 - Bearing to pedestal
 - Pedestal to foundation
 - **Rotor Components**
- Fluid Induced Instability
 - Bearing Whirl
 - **Bearing Whip**
 - Tilt pad flutter
- Shaft Crack
 - Shaft stiffness change
- Resonance
 - Is resonance itself a problem?

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Data Acquisition for Machinery Diagnostics

Parameters

- Bearing Temperatures
- Operating conditions Speed, MW, MVars, Blade path temps,
- Lube oil system operating conditions supply pressure and temperature, drain temperatures
- Seismic vibration probes velocity, accelerometer, velomitor
- Relative vibration probes note installation location/orientation
- Transient and Steady State Data vibration and operational parameters

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Defining Terms

Steady State Conditions: The machinery is operating under steady conditions; steady load, speed, etc.

Transient Conditions: The machinery is operating under changing conditions; changing speeds (startup, coast down), changing loads

Static Data is any data that can be represented by a single number or status. Examples include vibration amplitude filtered vibration amplitude, filtered vibration phase lag, transducer gap voltage, etc.

Plot Examples: Tabular List, Trend, Spectrum

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Dynamic Data is the actual vibration waveform. Sampling of the waveform and processing to provide both time domain (Orbit or Timebase plots) and frequency domain (Spectrum plots). Dynamic data cannot be characterized by a single number.

Plot Examples – Bode, Polar, Shaft Centerline, Timebase, Orbits, Cascade, Waterfall



Digital Control System (DCS) Data

Target Operating Range Alarm/Trip SetPoints Historical Operating Information



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Operating Conditions

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Lube Oil System Operating Conditions

Target Operating Range Alarm/Trip SetPoints Historical Operating Information



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Bearing Temperatures

Target Operating Range Alarm/Trip SetPoints Historical Operating Information



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Bearing Temperatures

Target Operating Range Alarm/Trip SetPoints Historical Operating Information



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Bearing Temperatures

Target Operating Range Alarm/Trip SetPoints Historical Operating Information



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Note the different items available

Tabular List

CH#	Channel Na	me Machine	Name S	tatus	Angle	Direction	Run Type	Date						Speed Units((P) Amp Un	it Phase Unit		
1	1X TVLL	TVLL	0	K	45°	Right	Start Up	30May2015	17:44:30.000	To 30M	ay2015	18:41:16.	800	rpm	mil pp	deg		
2	2X TVLC	TVLC	0	K	45°	Right	Start Up	30May2015	17:44:30.000	To 30M	ay2015	18:41:16.	800	rpm	mil pp			
3	3X GENLC	GENLC	0	K	45°	Right	Start Up	30May2015	17:44:30.000	To 30M	ay2015	18:41:16.	800	rpm	mil pp			
4	3Y GENLC	GENLC	0	K	45°	Left	Start Up	30May2015	17:44:30.000	To 30M	ay2015	18:41:16.	800	rpm	mil pp	deg		
5	4X GENLE	GENLE	0	K	45°	Right	Start Up	30May2015	17:44:30.000	To 30M	ay2015	18:41:16.	800	rpm	mil pp			
6	4Y GENLE	GENLE	0	К	45°		Start Up	30May2015	17:44:30.000	To 30M	ay2015	18:41:16.	. 800	rpm	mil pp			
7	5X EXC	EXCITAD		K	45°	-			17:44:30.000		-				mil pp			
8	5Y EXC	EXCITAD			45°				17:44:30.000						mil pp			
9	Kph 1		0	К	45°	Right	Start Up	30May2015	17:44:30.000	To 30M	ay2015	18:41:16.	800	rpm	V рр	deg		
CH#	Chann	Sample# [Date			Speed(P)	Direct	A	vg Gap	1XAm	plitude	1X Pha	se 2	2XAmplitude	2X Phase	nX-1Amplitude	nX-1 Phase	Speed
1	1X TVLL	460	30May2015	5 18:23	:29.700	3600	5.5	69	-7.300		5.063	341		0.247	60	0.016	225 BMA	
2	2X TVLC	460	30May2015	5 18:23	:29.700	3600	4.9	65	-7.531		4.806	278		0.087	324	0.062	OBMA	
3	3X GENLC	460	30May2015	5 18:23	:29.700	3600	2.9	63	-7.336		1.521	333		0.293	295	0.170	205 FNX	
4	3Y GENLC	460	30May2015	5 18:23	:29.700	3600	2.2	77	-8.227		0.843	43		0.221	112	0.031	OBMA	
5	4X GENLE	460	30May2015	5 18:23	:29.700	3600	3.6	57	-7.397		2.930	330		0.159	310	0.087	201FNX	
6	4Y GENLE		30May2015				1.9		-8.313		1.059	340		0.072	270	0.041	194BMA	
7	5X EXC		30May2015				7.8		-9.094		6.446	56		0.586	195	0.303	24FNX	
8	5Y EXC		30May2015				4.5		-9.533		3.444	191		0.632	83	0.062	149BMA	
9	Kph 1	460	30May2015	5 18:23	:29.700	3600	5.5	69INV	-7.300INV									3600

Compare samples Look for slow roll stability Compare data of different runs

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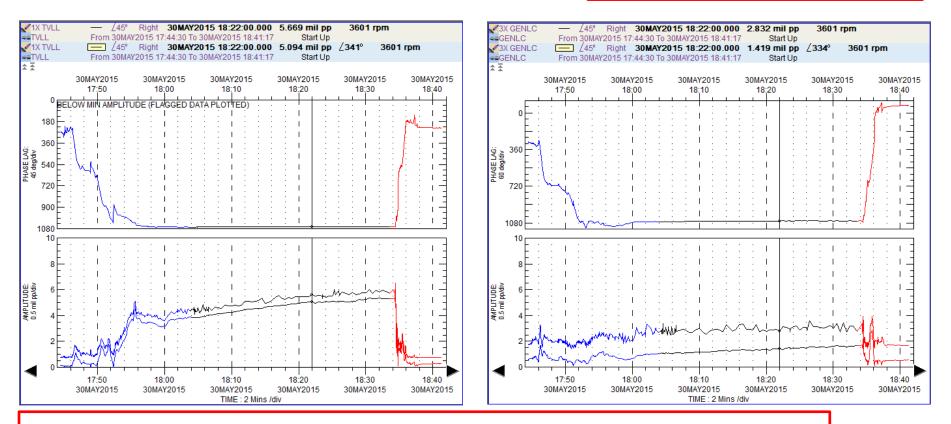
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Trends

These are more advanced trends that apply not only overall but 1X amplitude and phase for review and analysis



Blue trace - startup; black - loaded/steady state; red - coast down

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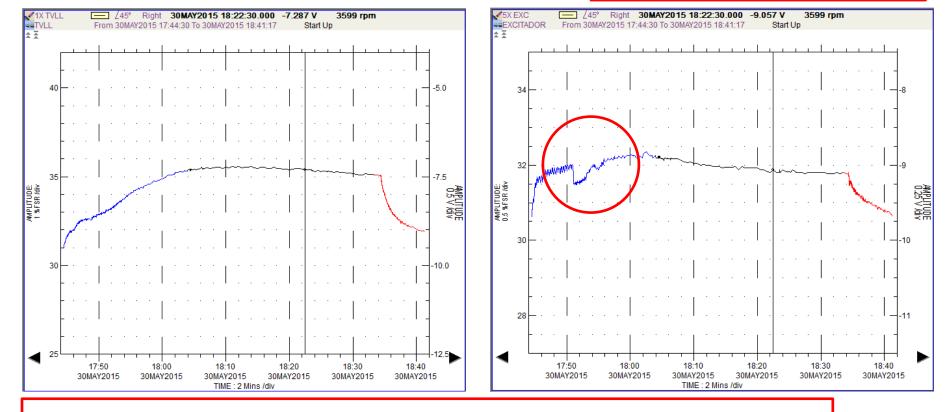
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Trends – Gap Voltage

These are the raw gap voltages that are used to develop shaft centerlines. Smooth movements are desirable. Anything else could indicate a potential issue



Blue trace - startup; black - loaded/steady state; red - coast down

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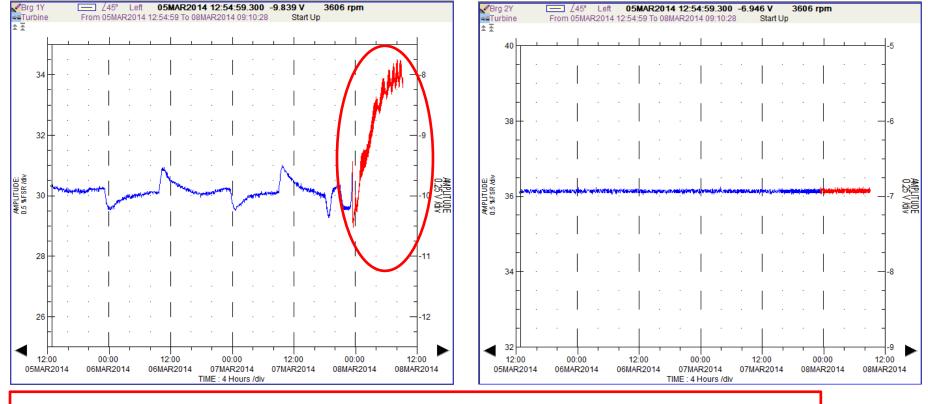
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Trends

These are the raw gap voltages that are used to develop shaft centerlines. Smooth movements are desirable. Anything else could indicate a potential issue



These are abnormal plots

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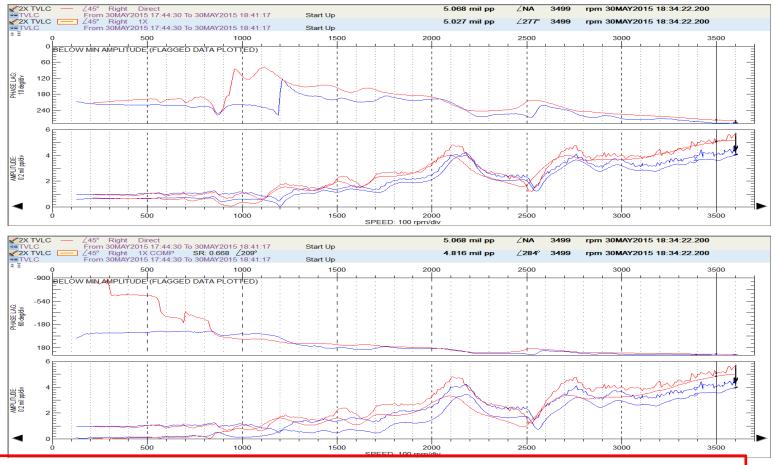
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Start-up and coast down comparison Amplitude shifts; phase shifts Overall and 1X amplitude and phase

Bode



Blue trace - startup; black - loaded/steady state; red - coast down

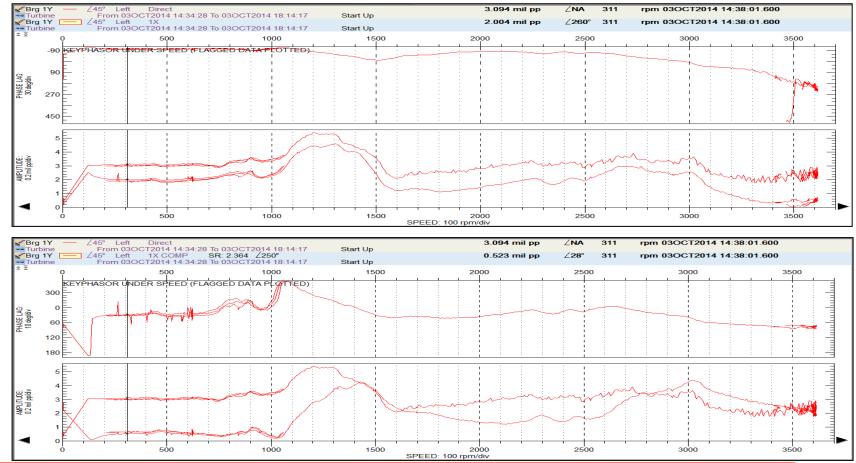
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Start-up and coast down comparison Amplitude shifts; phase shifts Overall and 1X amplitude and phase Slow roll change due to a rub





Blue trace – startup; black – loaded/steady state; red – coast down

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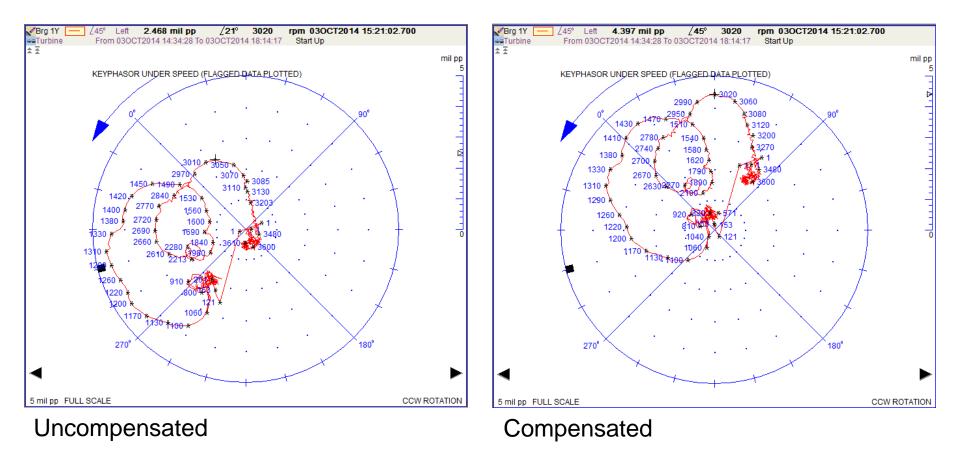
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Polar

Coast down comparison between compensated and uncompensated shows phase and amplitude shifts And peak critical speed shift



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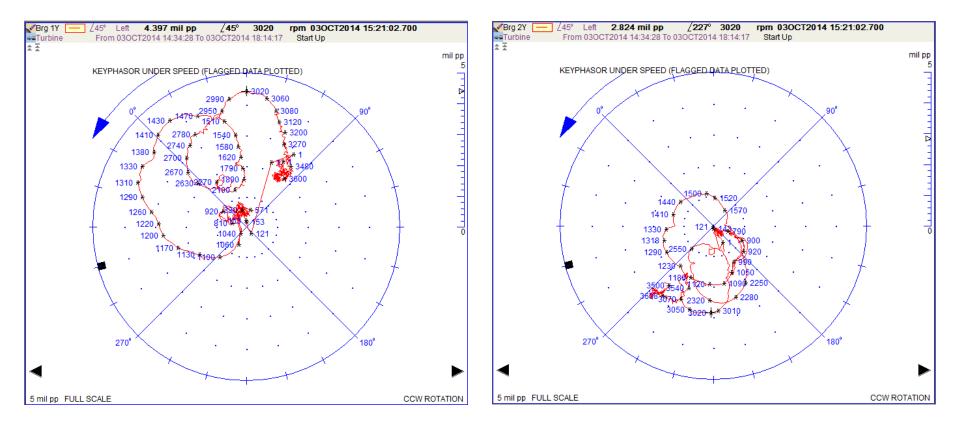
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Polar

Compensated data showing vibration signature differences between the two ends of the machine



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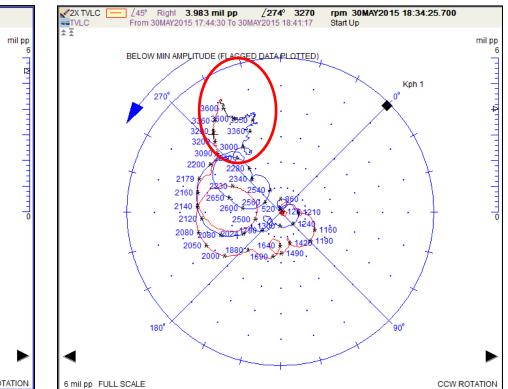
ZX TVLC Right 5.461 mil pp /327° 3270 1X TVLL 245° rpm 30MAY2015 18:34:25.700 ∠45° From 30MAY2015 17:44:30 To 30MAY2015 18:41:17 Start Up ±Ξ mil pp BELOW MIN AMPLITUDE (FLAGGED DATA PLOTTED Kph 1 270 220 316 2179 310 2160

1230 * * 1220 180[°] 906 6 mil pp FULL SCALE CCW ROTATION

Vibration Data

Polar





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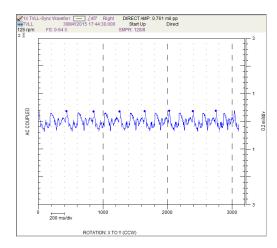
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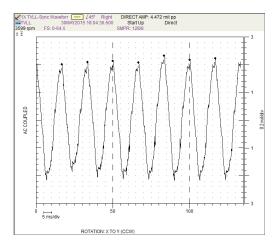
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Waveforms





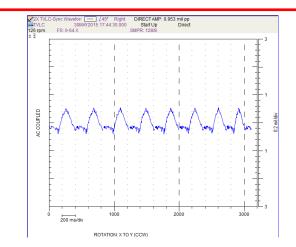
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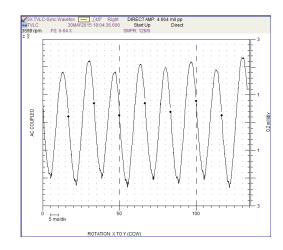
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Top two plots are slow roll noise levels for those channels Bottom two plots are uncompensated 3600 rpm data Same scales

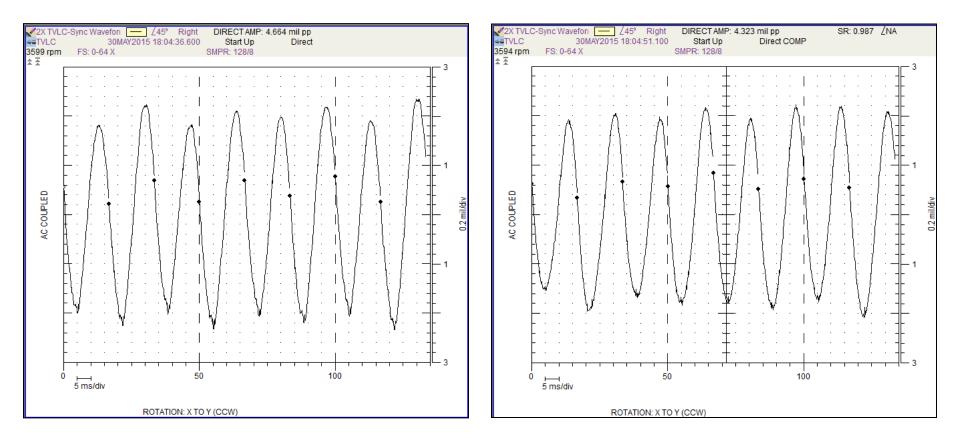




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Waveforms

Compensated plots from previous slide show less than 0.5 mils of change in amplitudes



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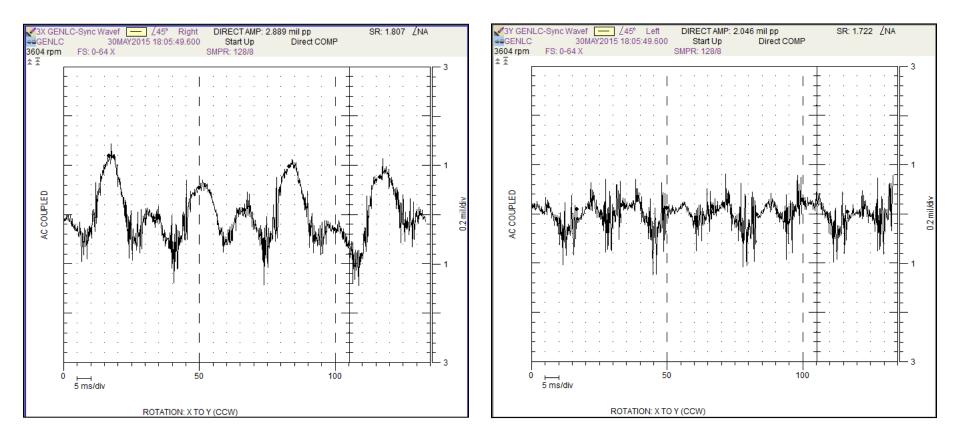
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Waveforms

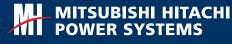
Example of another machine with higher noise levels. Plots below are 3600 rpm



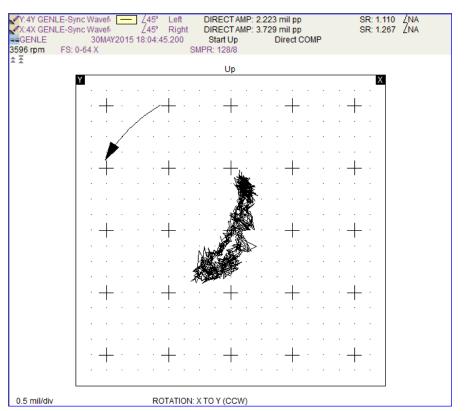
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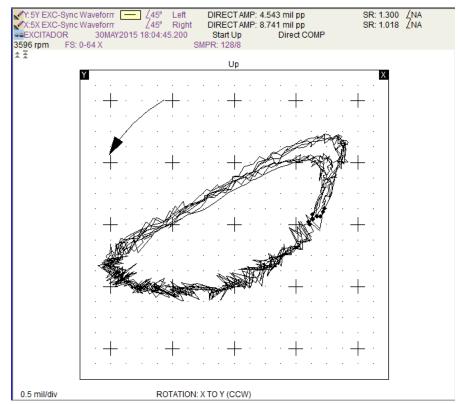
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Orbits



Example of a machine with preload on two of it's bearings looking at the Direct Orbits. Left side plot with banana shape; right side plot with 'flattened' side.



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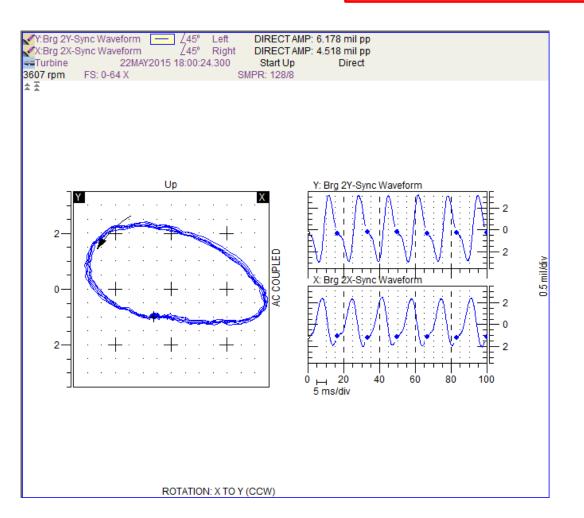
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Example of a machine showing the Direct Timebase and Orbit plots. Uneven travel through Timebase resulting in uneven elliptical shape

Orbits



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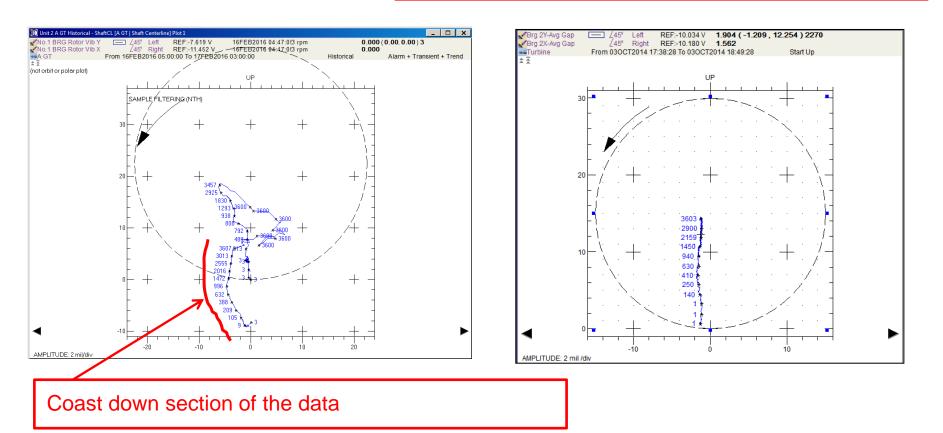
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Shaft Centerlines

Shaft Centerline plots of a startup and coast down on a large frame gas turbine. Left side plot is exhaust or #1 bearing; right side is compressor or #2 bearing.

Abnormal movement of #1 bearing is due to thermal growth of the startup. During coast down, there was a horizontal preload indicated.



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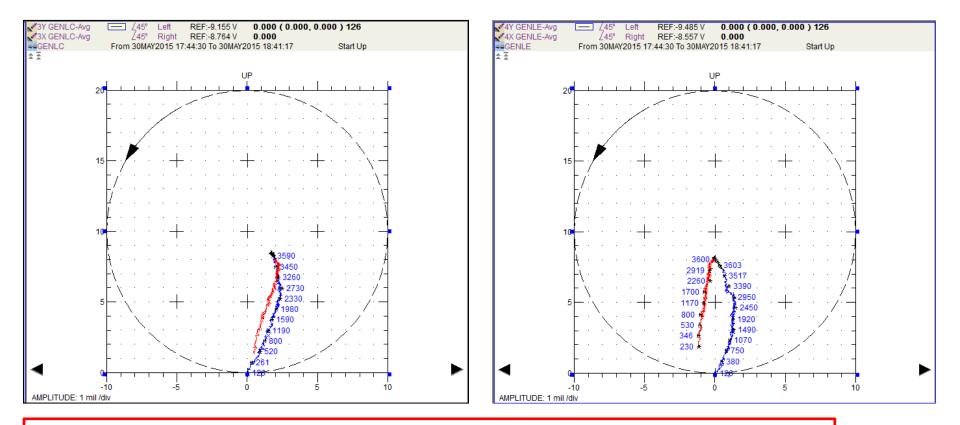
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Shaft Centerlines

Shaft Centerline movements of a gas turbine that are more typical. Some horizontal preload, further evaluation of other data plots would be recommended



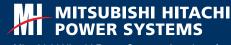
Blue trace - startup; black - loaded/steady state; red - coast down

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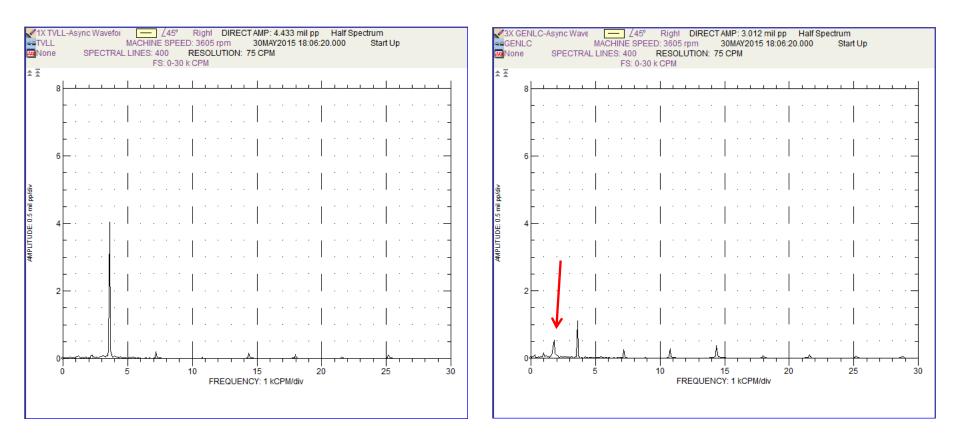
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Typical Spectral data for a Gas Turbine bearing and a Generator bearing. Generator bearing on right was indicating some sub-synchronous energy.

Vibration Data

Spectrums



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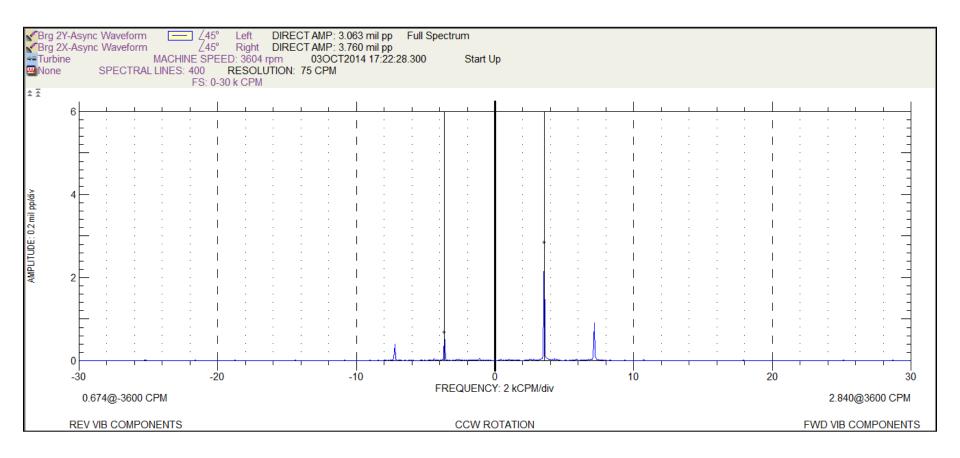
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Full Spectrum

Typical Full Spectrum data for a compressor bearing in a Gas Turbine. Some reverse precession energy indicated. Orbit plot would be elliptical



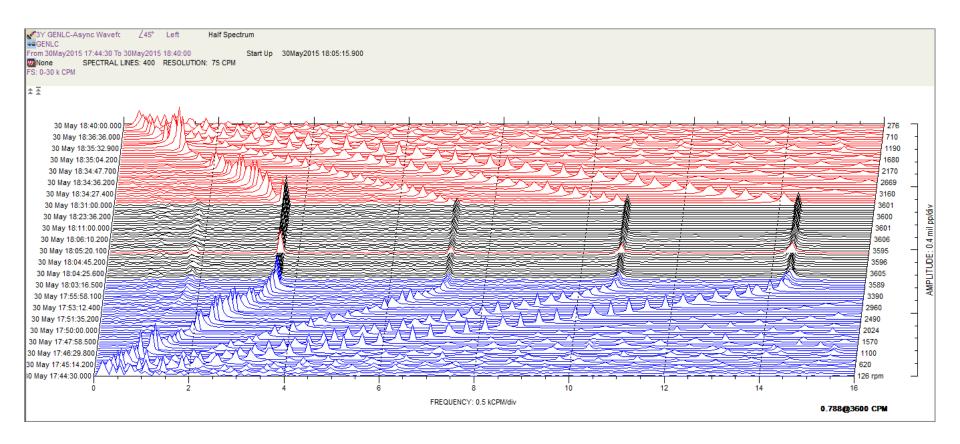
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Waterfall

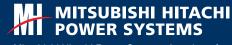
Spectral plot shown during startup, loaded operation, and coast down. Lack of change in synchronous multiples during the speed transients indicated that this is 'glitch' in the signal and not actual vibration energy.



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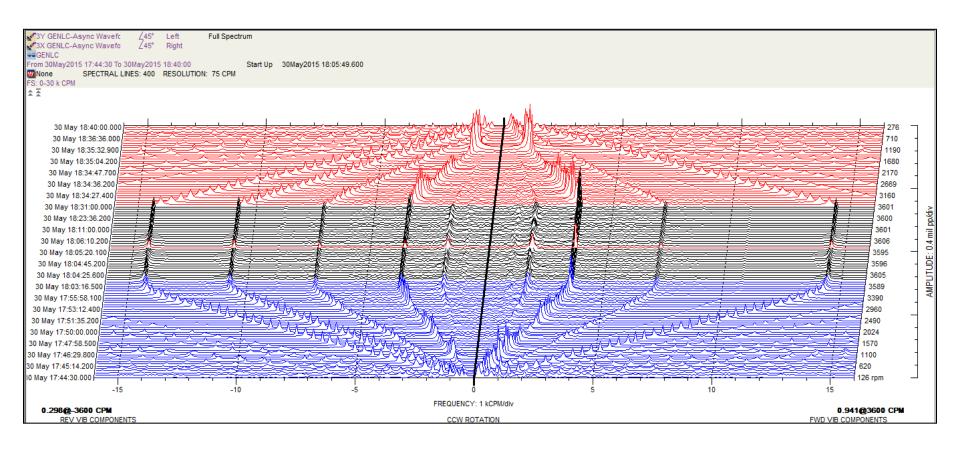
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Full Waterfall

Full Spectrum Waterfall shown (same data as previous slide) during startup, loaded operation, and coast down. Lack of change in synchronous multiples during the speed transients indicated that this is 'glitch' in the signal and not actual vibration energy.



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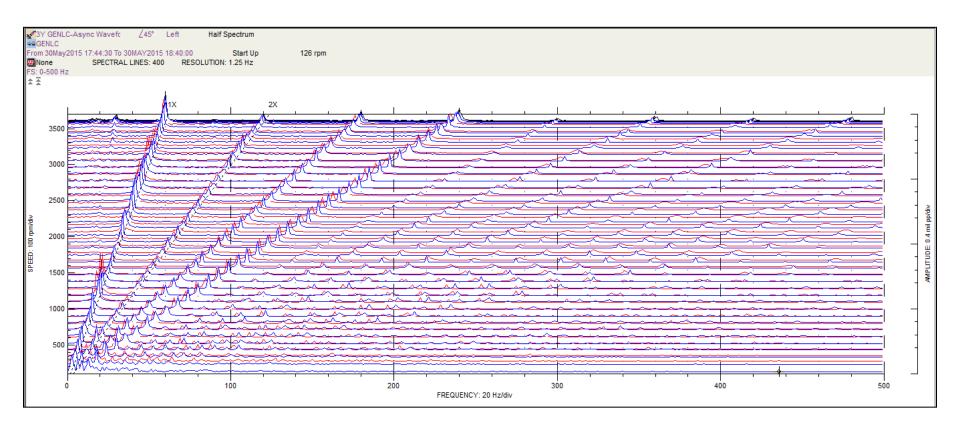
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Cascade

Cascade plot (same data as previous slide) during startup, loaded operation, and coast down. Lack of change in synchronous multiples during the speed transients indicated that this is 'glitch' in the signal and not actual vibration energy.



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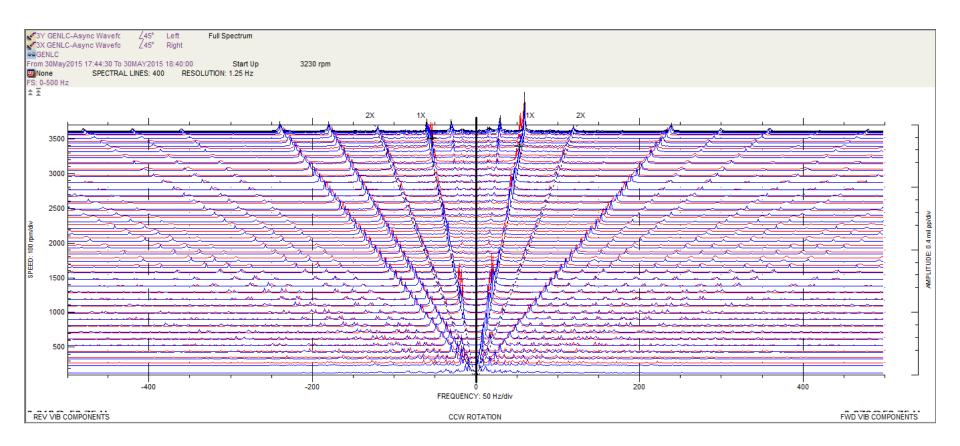
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Full Cascade

Full Spectrum Cascade shown (same data as previous slide) during startup, loaded operation, and coast down. Lack of change in synchronous multiples during the speed transients indicated that this is 'glitch' in the signal and not actual vibration energy.



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SL2



Instrumentation Issues



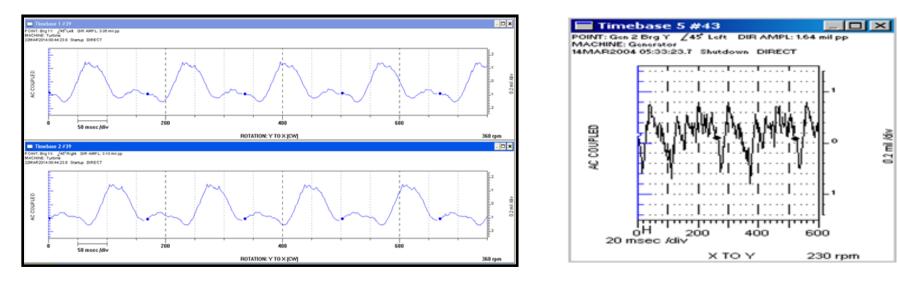
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MITSUBISHI HITACHI POWER SYSTEMS

Instrumentation Issues



Proximity Probe - Elevated Slow Roll amplitudes

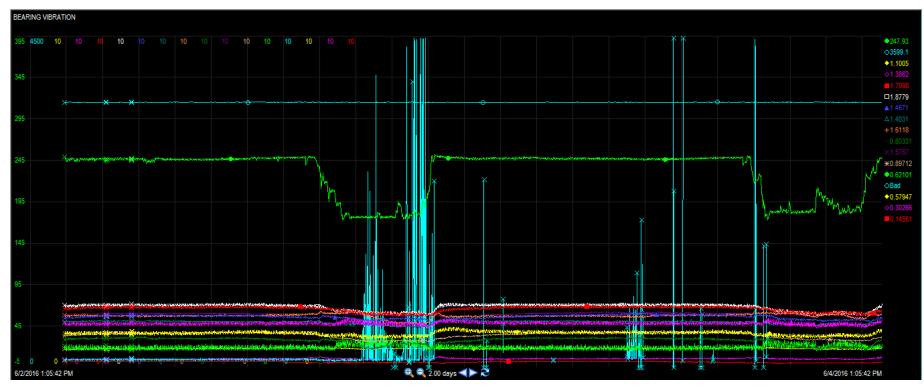
- **Mechanical Runout**
- **Electrical Runout**

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Instrumentation Issues



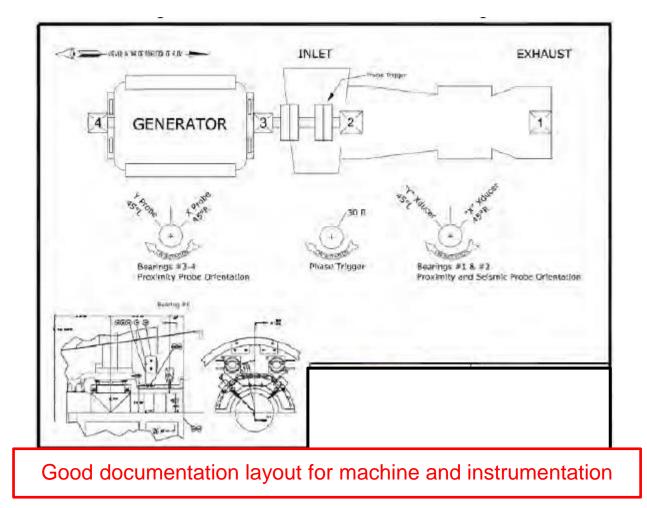
Wiring/Connection Noise

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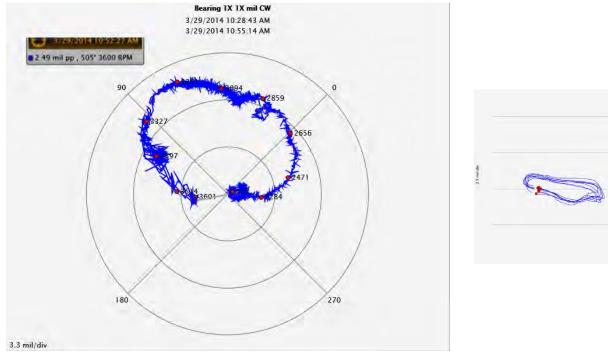


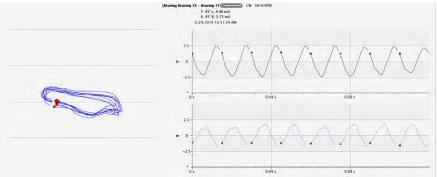


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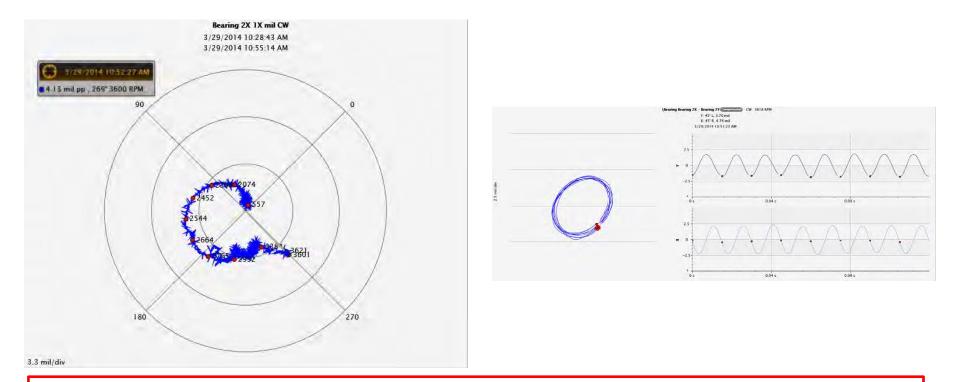
Startup and initial loaded operation; clean 2nd critical; but some vertical preload as it reached full speed; #1 bearing

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Startup and initial loaded operation; clean 2nd critical; but some vertical preload as it reached full speed - #2 bearing on the same machine.

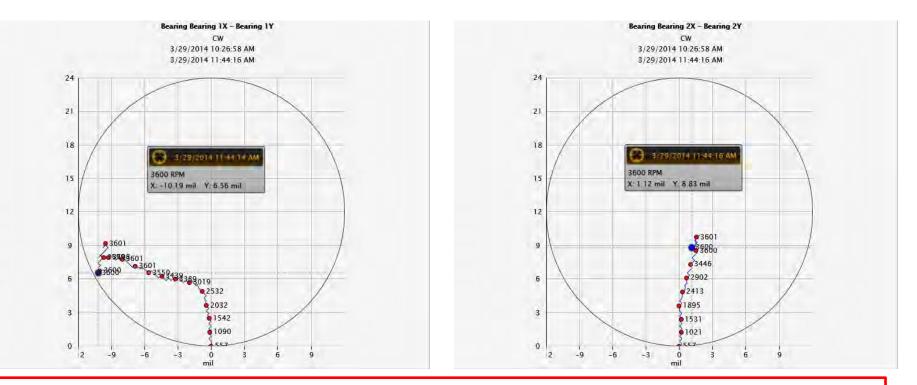
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SL2





Shaft Centerlines on the same machine during coast down. Rub on the #1 bearing was confirmed with the unusual shaft centerline movement.

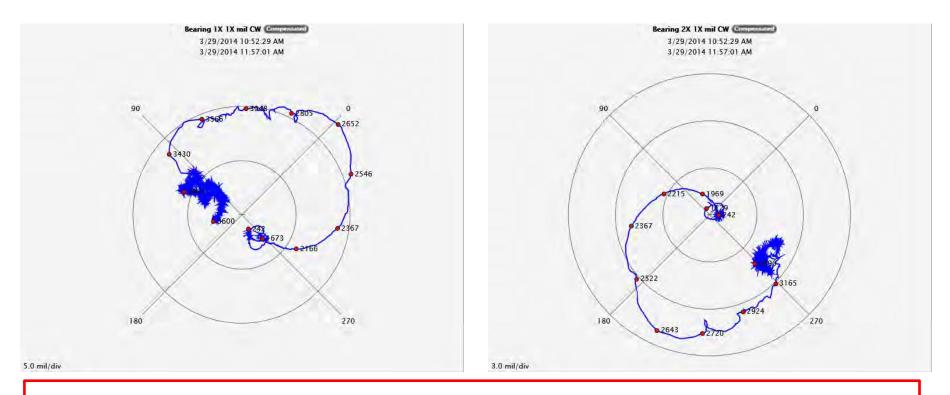
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Polar plots – Bearing 1 on the left; bearing 2 on the right during coast down. Shows 180 degree phase shift between ends at the 2nd critical.

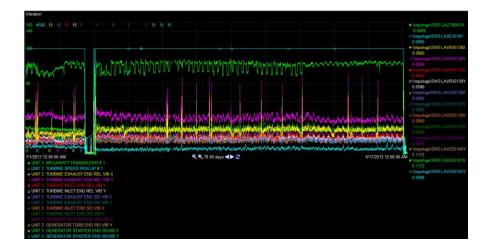
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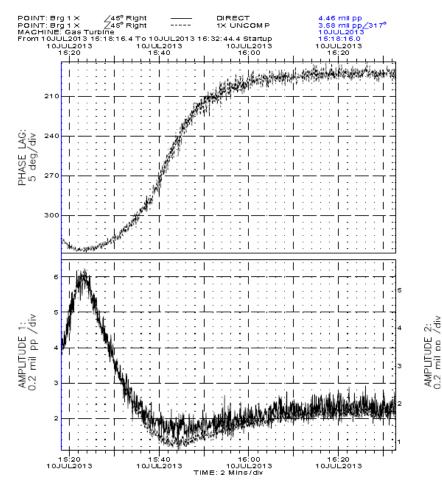
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Intermittent rub indication from trend data above. Amplitude increases occurred on an infrequent basis.



One amplitude increase was caught on dynamic data collection showing both amplitude swing and phase shifting



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CH#	Channel Name	Machine Name	Status	Angle	Direction	Run Type	2	Date			Sp	eed Units(P) Sp	eed Units(S)	Amp Unit Phase Uni	t
1	EXH X REL	CT1 START 4 C	OCT15 OK	45°	Left	Steady S	itate	01Jan198	6 12:27:33.200	To 01Jan1601 (00:00:00.004 rp	n rp	m	milpp deg	
2	EXH Y REL	CT1 START 4 C	OCT15 OK	45°	Right	Steady S	itate	01Jan198	6 12:27:33.200	To 01Jan1601 (00:00:00.004 rp	n rp		milpp deg	
3	GEN EXC X	CT1 START 4 C	OCT15 OK		Left	Steady S	itate	01Jan198	6 12:27:33.200	To 01Jan1601 (00:00:00.004 rp	ո որ		milpp deg	
4			OK	90°	Right	Steady S	itate	01Jan198	6 12:27:33.200	To 01Jan1601 (00:00:00.004 rp	ո որ		milpp deg	
5		CT1 START 4 C	OCT15 OK		Left	Steady S	itate	01Jan198	6 12:27:33.200	To 01Jan1601 (00:00:00.004 rp	n rp		milpp deg	
		CT1 START 4 C		45°	Right	Steady S	itate	01Jan198	6 12:27:33.200	To 01Jan1601 (00:00:00.004 rp	n rp	m	milpp deg	
7	GEN TURB END X	CT1 START 4 C	OCT15 OK	30°	Left	Steady S	itate	01Jan198	6 12:27:33.200	To 01Jan1601 (00:00:00.004 rp	n rp	m	milpp deg	
8	GEN TURB END Y	CT1 START 4 C	OCT15 OK	60°	Right	Steady S	itate	01Jan198	6 12:27:33.200	To 01Jan1601 (00:00:00.004 rp	n rp	m	milpp deg	
9	Kph 1		OK	0°	None	Steady S	state	01Jan198	6 12:27:33.200	To 01Jan1601 (00:00:00.004 rp	n rp	m	V pp deg	
 CH#	Channel Nam	e Sample#	Sample Cau	use Date	2		Spe	ed(P)	Direct	Avg Gap	Inst Gap	1XAmplitude	1X Phase	2XAmplitude	2X Phase
1	EXH X REL	9	DR-T	01Ja	n1986 12:	27:47.000		280	0.360	-10.327	0.000IN	/ 0.185	333BMA	0.000INV	OINV
2	EXH Y REL	9	DR-T	01Ja	n1986 12:	27:47.000		280	0.349	-9.851	0.000IN		216BMA	0.000INV	OINV
3	GEN EXC X	9	DR-T	01Ja	n1986 12:	27:47.000		280	0.840	-10.168	0.000IN	0.478	6	0.000INV	OINV
4		9	DR-T	01Ja	n1986 12:	27:47.000		280	0.000	0.000	0.000IN	0.000	OBMA	0.000INV	OINV
5	INLET X REL	9	DR-T	01Ja	n1986 12:	27:47.000		280	0.658	-8.337	0.000IN	0.411	354	0.000INV	OINV
6	INLET Y REL	9	DR-T	01Ja	n1986 12:	27:47.000		280	0.637	-8.215	0.000IN	0.411	252	0.000INV	OINV
7	GEN TURB	. 9	DR-T	01Ja	n1986 12:	27:47.000		280	0.576	-9.497	0.000IN	0.524	351	0.000INV	OINV
8	GEN TURB	. 9	DR-T	01Ja	n1986 12:	27:47.000		280	0.586	-9.265	0.000IN	0.462	257	0.000INV	OINV
9	Kph 1	9	DR-T	01Ja	n1986 12:	27:47.000		280	0.360INV	-10.327INV	0.000IN	/			

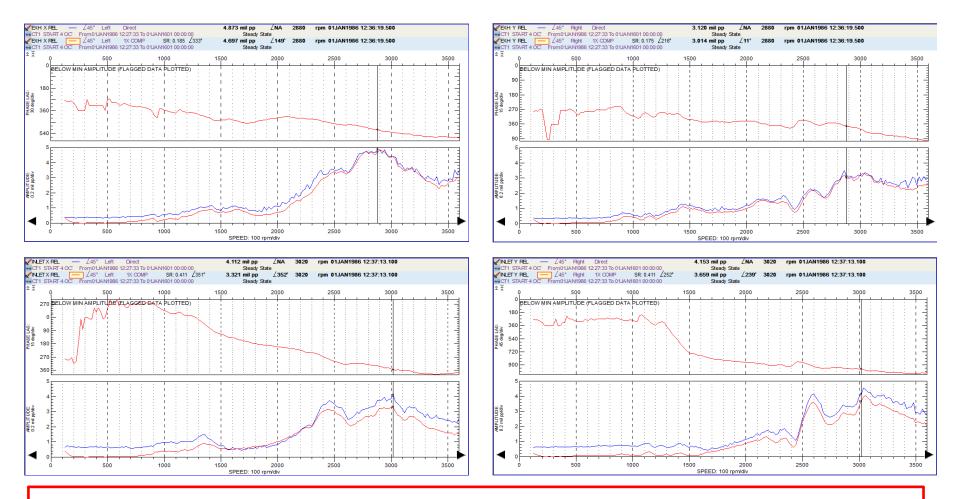
Tabular list used for slow roll data compensation selection and comparison between operational data points. Note all the different information that is available

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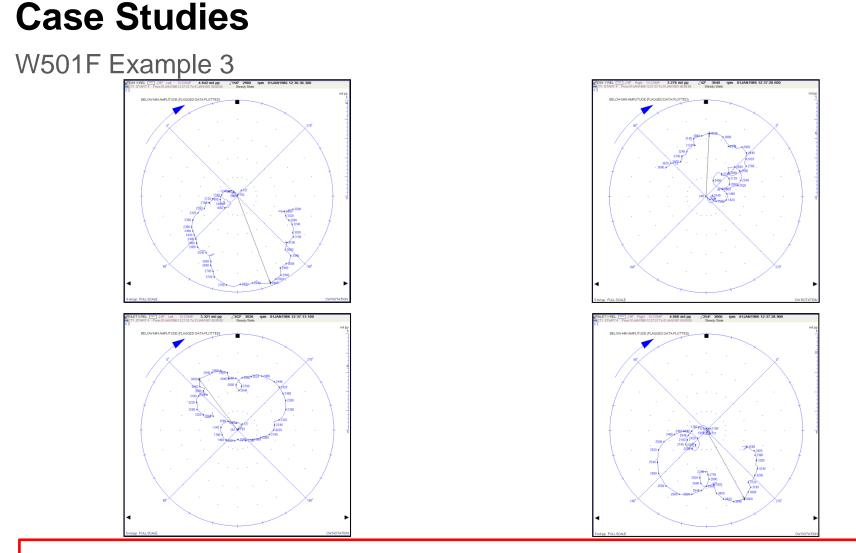
Bode plots showing 1st and 2nd critical responses and increased response after 2nd critical

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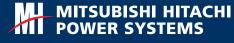


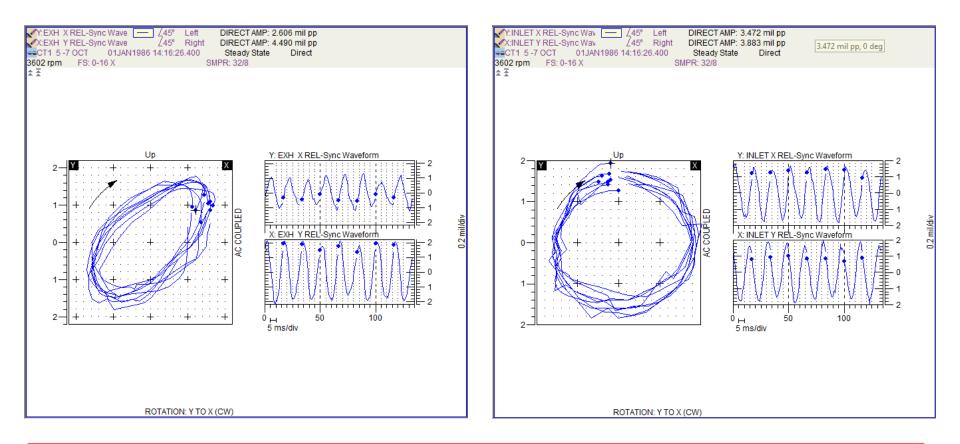


Polar plots showing 1st and 2nd critical responses and increased response after 2nd critical.

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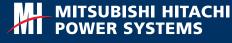


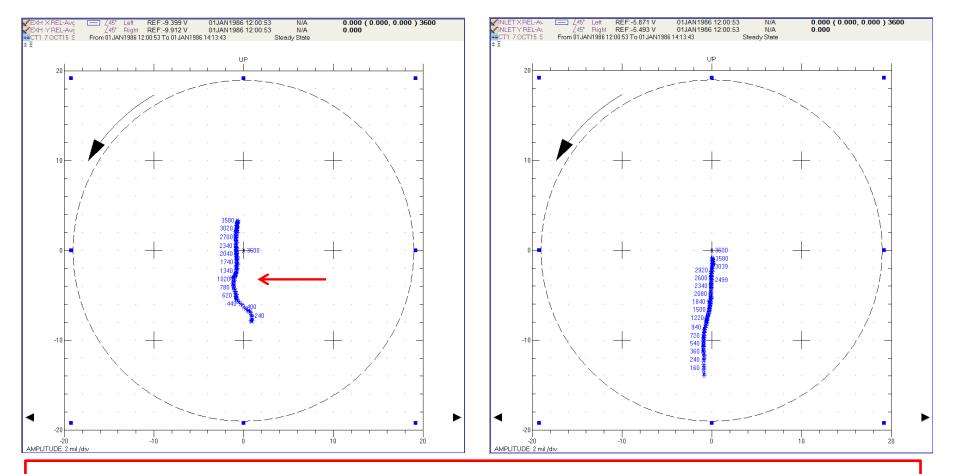
#1 bearing preloaded when compared to #2 bearing. Variation in Orbit shape from one revolution to the next would be good to do further investigation

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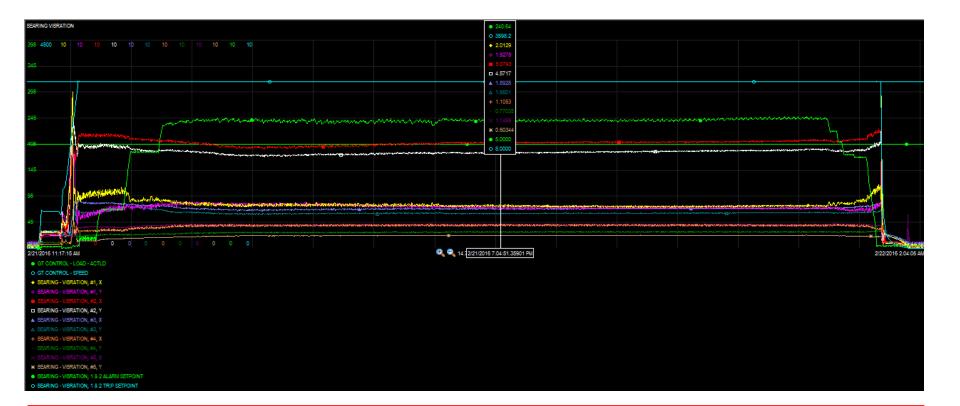
#1 bearing horizontally preloaded when compared to #2 bearing.

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Overall Vibration levels after a row 2 turbine blade replacement. Note blades were changed on turbine end, higher vibration incurred on compressor end.

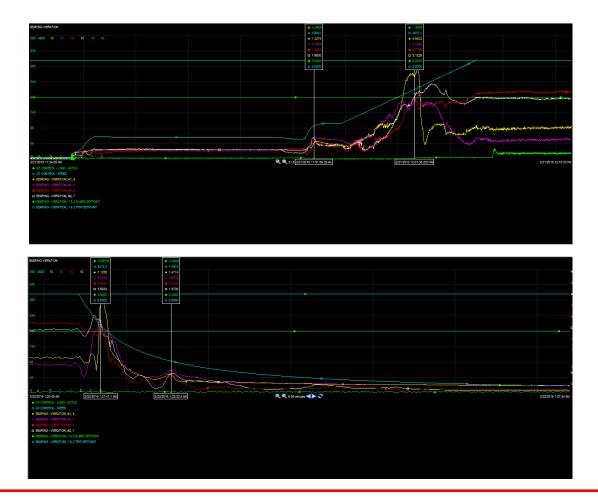
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SL2





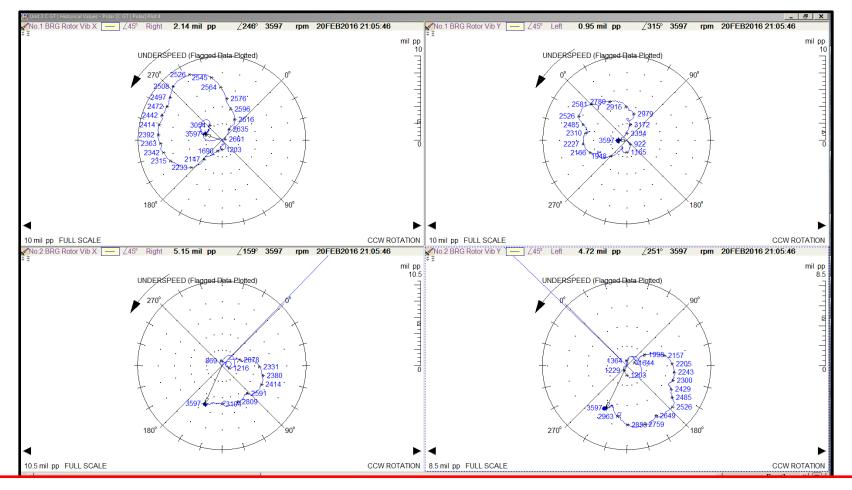
Startup and coast down overall trend behavior after the row 2 turbine blade replacement

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Coast down Polar plot behavior after the row 2 turbine blade replacement

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Overall Vibration levels after balancing was performed by installing trim balance weights in the turbine end of the machine.

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Startup and coast down overall trend behavior after trim balancing was performed by adding weights in the turbine end of the machine

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- ISO 7919 Mechanical Vibration
- API 670 Machinery Protection systems
- Metrix Machinery Diagnostic Services



End

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