

EXCELLENT PIPES



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A Member of Hedley Industrial Group

**Excellent Pipes
Company L.L.C**

FIBERBOND™
Glass-Fiber Reinforced
Thermosetting
Resin Pipes (GRP)



Installation
Guide

Installation Guide

EXCELLENT

Pioneering Excellence in Piping Systems

EXCELLENT PIPES COMPANY L.L.C

Excellent Pipes Company is part of the Hedley Industrial Group that operates state of the art manufacturing plants in United Arab Emirates. Established in 2000, Excellent Pipes Co. (EXCELLENT) is a leading manufacturer and supplier of high quality GRP, RC, uPVC, ABS and PE piping systems that are widely used in municipal, industrial and infrastructure development projects throughout the Gulf region.

EXCELLENT adopts a policy of continuous development as an integral part of its operation. We have in place advanced technology coupled with extensive research & development and assured quality. **FIBERBOND™** GRP products are used for a wide range of applications including sanitary sewerage, industrial waste water & effluents, sea water, cooling water, fire water lines and potable water.

We offer support services to our clients and assist them with their project implementation from conception to successful commissioning.

FIBERBOND™ GRP pipes are manufactured to close dimensional tolerance with an uncompromising emphasis on quality and performance. As an industrial offshoot of Hedley Industrial Group, we enjoy a unique standing in the business community, capitalizing on the group's long history of successful achievements and awards. Our group's road to success is marked with several recognitions, including the Shaikh Khalifa industrial and Excellence Awards, American Concrete Pipe Association Certificate, American Petroleum Institute Monogram, triple certification under ISO 9001, 14001 & 18001 and the highly acknowledged BSI Kitemark certification.

Our technical and operational expertise supported by technology from leaders in the pipe industry, bring EXCELLENT to the forefront of international pipe manufacturers, providing value to our customers, in line with our motto of **"PIONEERING EXCELLENCE IN PIPING SYSTEMS"**.





FIBERBOND™

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GLASS-FIBER REINFORCED PLASTIC PIPE

INSTALLATION GUIDE

1. INTRODUCTION

This manual deals with handling, laying and testing of FIBERBOND pipes and joints at installation site. Pipe diameters range from 25 mm to 2600 mm with standard pressure classes of 1, 3, 6, 10, 12, 16, 20, 25 and 32 bar and stiffness classes of 2500, 5000 and 10000 Pa. Pipes can be either solid wall type or with reinforcing ribs. Standard pipe lengths are as per the following table.

Table 1: Standard Pipe Length

Nominal Pipe Diameter (mm)	Standard Pipe Length (m)
25	3
40 - 80	4 / 6
100 - 300	9
350 - 600	9 / 12
700 and above	12

This manual should be carefully read by the Contractor as well as the Design Engineer prior to laying the pipes. The information given in this manual should be considered only as guidelines. The Engineers or others involved in the pipeline design or installation should establish the requirements and procedure suited to the specific site conditions. For studying the site conditions Sound Engineering practices are recommended.

2. HANDLING

2.1 Receiving of Pipes

The pipes will be handed over to the Contractor or his representative at the factory or at the job site as agreed upon in the purchase order. In the case of an Ex-works delivery, the pipes and fittings shall be loaded on the Contractor's trucks by the factory loading staff. If the loading staff considers the transport unsuitable, they will advise the contractor or his representative accordingly. Thorough inspection is made by the factory loading staff of the goods being loaded. Nevertheless the Contractor or his representative may make their own inspection of the goods during dispatch.

The Contractor should make the following inspection at the time of receiving the goods:

- a- Each item should be inspected with care upon its arrival at installation site.
- b- Total quantity of pipes, coupling, rubber rings, fittings, etc... should be carefully checked against the delivery notes.
- c- Any damaged or missing item must be pointed out to the dispatcher or driver and noted on the delivery note.

Materials that have been damaged during transportation should be isolated and stored separately on site, until the material is checked by the manufacturer and repaired or replaced.

Note: Damaged material must not be used before it is repaired and inspected.

2.2 Unloading of Pipes

Unloading at the job site must be carried out carefully under the control and responsibility of the Contractor. Care should be taken to avoid impact with any solid object, i.e., other pipes, ground stones, truck side etc.

2.2.1 Unloading by hand

Unloading by hand with two men is only allowed for small diameters pipes of weight not exceeding 60 kg.

2.2.2 Mechanical unloading

Mechanical unloading is required for pipes heavier than 60 kg. Flexible slings or straps should be used in combination with a mobile crane. When unloading is done with a mobile crane, care must be taken that the pipes do not slide off the slings. Therefore, it is recommended to use two slings or nylon lifting straps to hold and lift the pipes. Steel cables must not be used for lifting or handling of the pipes.

The pipes can also be lifted with one sling or strap balanced in the middle with the aid of a guiding rope.

Caution: Hooks must not be used at the pipe ends to lift the pipes, nor should the pipe be lifted by passing a rope or sling through the pipe.

2.3 Unloading of Couplings

Couplings shall also be unloaded with care. They must not be thrown off the truck on the ground. In general, couplings are strapped and bundled in the factory and can be off loaded like the pipes.

2.4 Storage of Rubber Gaskets on Site

Rubber gaskets are delivered in closed bags from the factory and must be stored in a cool shaded area protected from direct sunlight, until they are ready for use.

2.5 Storage of Pipes at site

2.5.1 Distribution along the trench

It is preferable to unload the pipes alongside the trench directly from the truck. If the trench is opened, string out the pipes on the opposite side to the excavated earth. Allow sufficient space between pipes and the trench for excavator, cranes, etc. Avoid placing the pipes where they can be damaged by traffic or blasting operations.

If possible, store pipes on the soft level ground (e.g. sand), timber bearers, or sand bags.

Caution: Pipes must not be stored on rocks.

2.5.2 Storing in stock piles

Care must be taken that the storage surface is leveled, firm, and clear of rocks or solid objects that might damage the pipes. Store the pipes in the separate stockpiles according to their class and nominal diameter. If it is necessary to stack pipes, it is best to stack on flat timber supports at the maximum 6 meters spacing (3 meters for small diameters, up to 600 mm). The maximum stack height is approximately 2 meters. Stacking of pipes larger than 1400mm diameter is not recommended. This height is limited for safety purpose and to avoid excessive loads on the pipe during storage.

Wooden wedges, which are used in order to prevent the pipe stack from sliding, should be placed on both sides of the stack on the timber bearers, as shown in figure below.

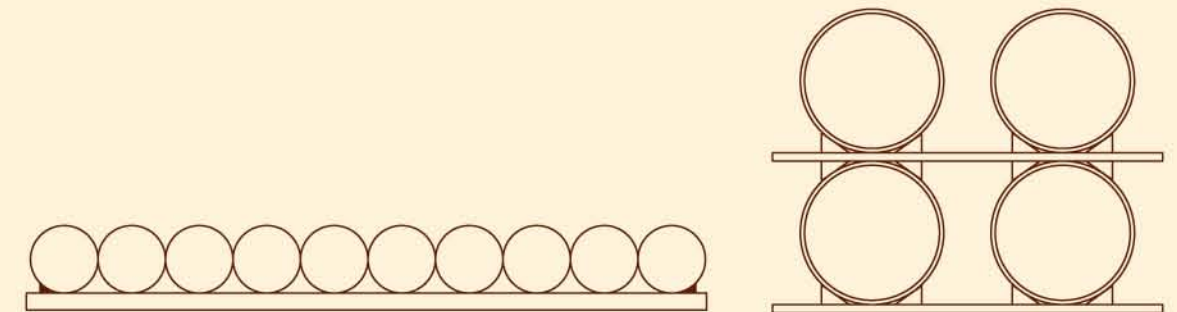


Fig. 1: Pipe Storage

2.6 Handling of nested pipes

Pipes may be delivered nested (i.e. one or more small diameter pipes inside a larger diameter pipe). Special handling procedures must be followed when handling and de-nesting such pipe loads.

When handling nested pipes, never use a single sling or strap. Nested pipes must always be lifted using at least two straps or slings. A spreader bar will help insure the load is lifted uniformly. Mobile lifting equipment should move slowly when handling nested pipes and all such movements should be kept to a minimum to insure the safety of site personnel. The Contractor should insure that the crane operator realizes that the smaller pipes inside the larger nested pipes may slip out and fall during movement. All necessary precautions should be taken.



De-nesting a load is easily accomplished by inserting a forklift fork into a padded boom. The forklift lifting capacity should be appropriate to handle the weight and length of the pipes being de-nested. Proper padding on the boom is essential. Rubber, several wraps of corrugated cardboard sheets, or PVC or a PE pipe slipped over the boom are all suitable options to avoid damaging the inside of the nested pipes.

The Forklift operator should lift the inner most pipe sufficiently so the pipes do not touch each other when the inner pipe is being pulled out.

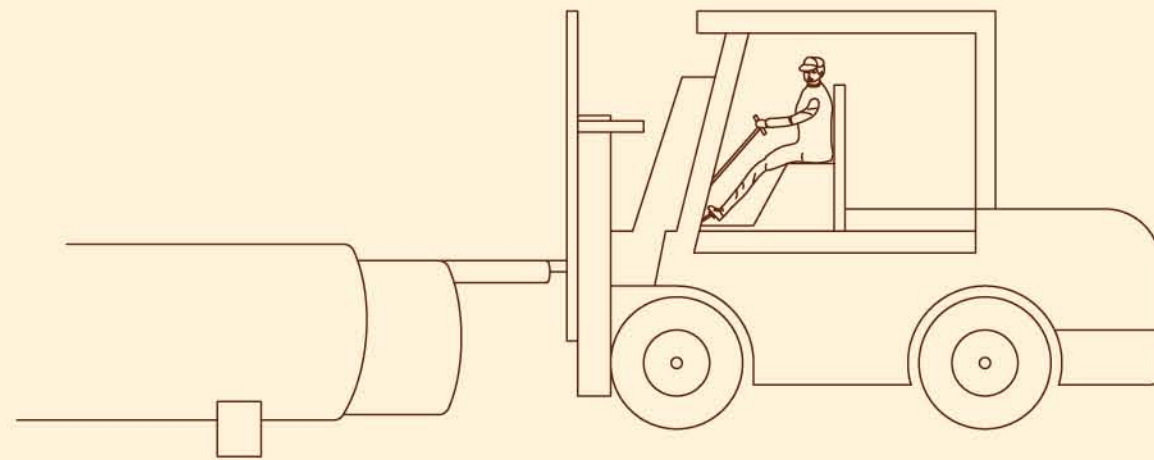


Fig. 2: De-nesting of Pipes

2.7 Lowering of the pipe into the trench

Hand loading should be executed by at least two men. It is recommended that the weight carried by one man do not exceed 30 kg. Pipes weighing up to 175 kg can be lowered by means of two ropes. The ropes must be anchored to stakes as indicated below.

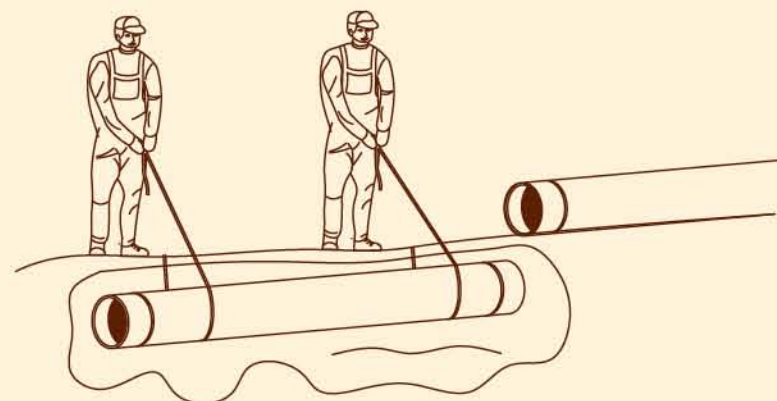


Fig. 3: Lowering of the pipe using ropes

Mechanical lowering is used for large diameter pipes, especially when combined with pipe assembly in the trench. Two straps or slings can be used from an excavator boom if no separate lifting equipment is available.

3. TRENCH SPECIFICATIONS

3.1 The Trench

The trench excavation should be not be too far ahead of the pipe-laying team to ensure a better control of the trench and for safety reasons. The excavated soil should be placed on one side of the trench leaving the other side clear for equipment and pipe handling. If the trench consists of various layers of soils, these should be placed separately in order to use the stone-free granular material for backfill.

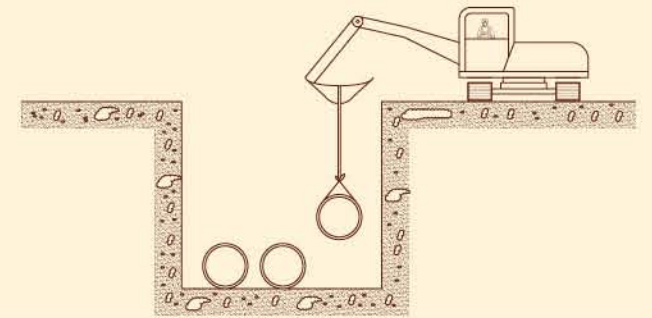
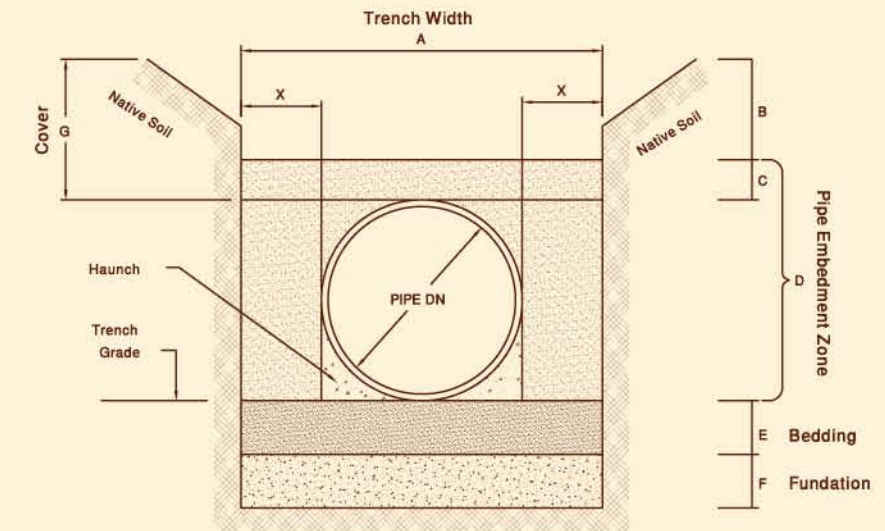


Fig. 4: Mechanical lowering with excavator

3.2 Minimum Trench Width

The trench width must be maintained within certain limits. A very wide trench will increase the volume of backfill material required, and compaction labor and effort. A very narrow trench will render laying, handling and joining of pipes, as well as compaction of side backfill difficult. The minimum recommended trench width is given below.



X = 300 mm for DN80-1000, X = 450 mm for DN1100-1500, X = 600 mm for DN1600-2600

Fig. 5: Minimum Trench Width

Notes:

1. In poor native soil conditions and depending on pipe stiffness and burial depth, a wide trench (up to 4 x DN) might be required. See section 4.7 for additional details.
2. The distance between the pipe and the trench wall should be at least 10 cms wider than the width of the equipment used for compaction of the backfill material.

3.3 Parallel pipes installed in the same trench

Where two or more pipes are installed in parallel in the same trench, the following minimum distance should be maintained in order to allow for sufficient room to place and compact the backfill material under the pipe haunches, for all the pipes in the trench. The distance between the pipes should be at least 10 cm wider than the width of the equipment used for compaction of the backfill material.

Where pipes of the same or different diameters are installed in the same trench, a minimum spacing, X equal to (DN of pipe a + DN of pipe b)/4, but not smaller than 300mm, is required.

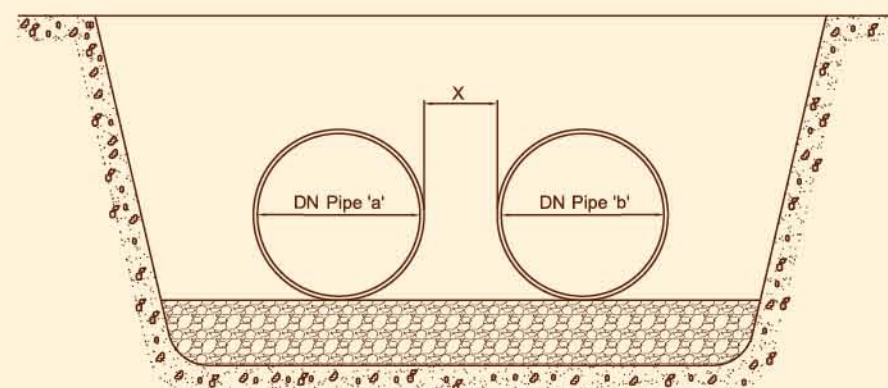


Fig. 6: Pipes in the same trench

3.4 Trench depth

3.4.1 Minimum cover depth

Generally the cover depth of pipe is specified by the Design Engineer. When there is no traffic load over the pipe, the minimum burial depth is 0.6 m. in the presence of traffic loads, a minimum cover above the pipes shall always be maintained as follows for all stiffness classes.

Table 2: Minimum Cover Depth

Load Type	Traffic (Wheel Load)		Minimum Burial Depth
	kN	Lbs	
AASHTO H20 (C)	72	16,000	1
BS 153 HA (C)	90	20,000	1.5
ATV LKW 12 (C)	40	9,000	1
ATV SLW 30 (C)	50	11,000	1
ATV SLW 60 (C)	100	22,000	1.5

High Water Table: In case of high ground water table, a minimum cover depth equal to 0.75 times the pipe diameter of granular soil (minimum dry density of 1300 Kg/m³) must be provided to prevent pipes from floating. Always ensure that this minimum cover is available before turning off dewatering systems.

3.4.2 Maximum cover height

The maximum cover height depends on the pipe stiffness, type of installation, backfill material and its compaction, as well as native soil conditions.

4. BACKFILL AND INSTALLATION SELECTION

4.0 Backfill and Installation Selection

The installation type and choice of Pipe Embedment Zone material is normally specified by the Design Engineer based on the specified pipe stiffness class (SN), maximum burial depth, vacuum requirements and native soil conditions.

4.1 Acceptable pipe foundation and Pipe Embedment Zone backfill materials

Most coarse-grained soils are generally acceptable as backfill material for the foundation and pipe embedment zone. The following may be used if compacted to the required degree.

Table 3: Acceptable Backfill Material

Soil Category	Symbol (as per ASTM D 2487)
Crushed Rock/Gravel	GW, GP, GW-GC, GW-GM, GP-GC, GP-GM, GM, GC
Sand	SW, SP, SW-SC, SW-SM, SP-SC, SP-SM, SM, SC

The maximum particle size is as follows:

Table 4: Maximum particle size

Pipe Diameter	Maximum particle Size
DN less than 600 mm	13 mm
DN between 600 and 1600 mm	19 mm
DN larger than 1600	25 mm

Note:- If the native soil meets the specifications in tables 3 and 4 above, the same soil may not be used in the Pipe Embedment Zone.

4.2 Migration

When backfill materials such as gravel and crushed rocks are placed in a trench adjacent to finer native material, the finer material may migrate into the coarser material under the flow pressure force of the ground water table. Migration can also occur when selected sand is used as backfill in a trench where the native soil is coarser.

Significant hydraulic gradients may arise in the pipeline trench during construction, when water levels are controlled by various pumping or well-pointed methods.

Gradients may also arise after construction, when permeable under drain or when the open graded embedment materials act as a “French” drain under high ground water levels. Migration can result in significant loss of pipe support and increasing pipe deflections that may eventually exceed the design limits.

The gradation and relative size of the embedment and adjacent native soils must be compatible in order to minimize migration. In general, where the ground water table is above the foundation or bedding level and when the native soil is finer than the backfill, avoid using open graded materials such as crushed rocks and gravel unless a geo textile filter fabric is used to line the trench bottom and sides.

4.3 Determination of native soil properties

In order to choose the appropriate installation type and to identify the allowed burial depth limits, it is necessary to determine native soil properties. Proper soil investigation along the pipeline route is an engineering practice that should be executed by the Contractor in case no soil data is provided by the end user. When no soil data is available, borehole samples should be taken along the pipeline route at intervals of not more than 500 meters. If the native soil properties and appearance are not consistent over this distance, shorter intervals for sampling should be adopted. Soil samples must be taken from a depth that provides the necessary information at the pipe embedment zone level of the pipeline.

Important soil properties

- Physical characteristics appearance and gradation
- Water table location
- Blow counts (N) as per ASTM D1586 (Standard Penetration Test)

4.4 Classification of native soils

Native soils can be classified into five main groups and two sub-groups - Cohesive and Granular.

Table 5: Native soil groups

	1	2	3	4	5
Blow counts (N) ASTM D 1586	>30	16-30	8-15	4-7	1-3
Cohesive Soils	Hard	Very Stiff	Stiff	Medium	Very Soft
Granular Soils	Dense	Compact	Slightly Compact	Loose	Very Loose

4.5 Standard Installation

Installation selection unless otherwise specified by the end user, shall be based on the native soil properties, pipe stiffness class (SN) and burial depths. Figures 7A to 7D illustrate the four installation types. Tables 6A and 6B specify the maximum burial depth without and with traffic loads respectively for pipes with a stiffness class of SN 2500, SN 5000, and SN 10000 in native soil groups of 1 to 5.

Installation type I

Full gravel/crushed stones surround, compacted to 70% Relative Density

Installation type II

Full sand, with less than 12% fines surround compacted to 90% SPD

Installation type III

Full sand, with more than 12% fines surround compacted to 90% SPD

Installation type IV

Full sand, with more than 12% fines surround compacted to 80% SPD

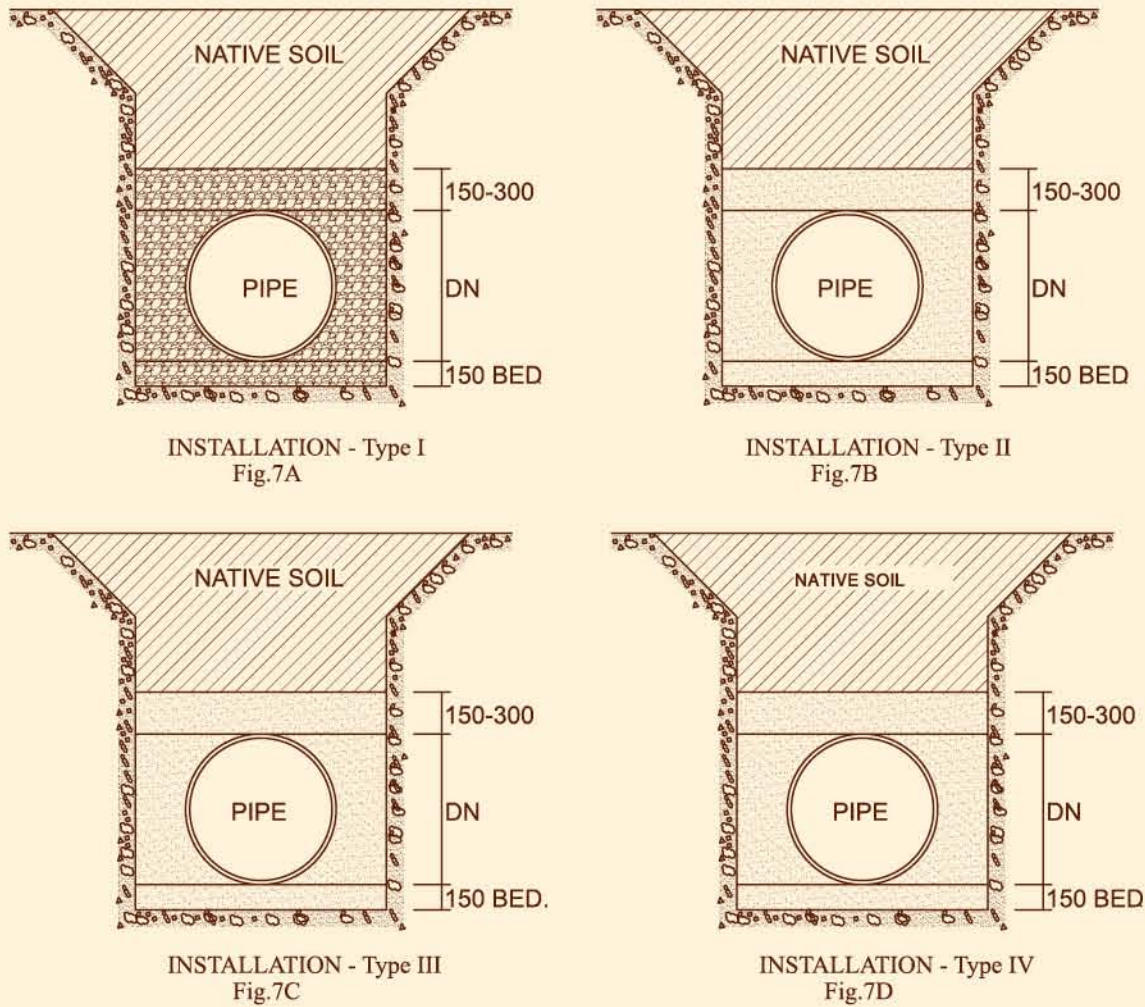


Table 6A
Standard Trench
Maximum Burial Depth (meters) Without Traffic Load

Installation Type	Native Soil Group				
	1	2	3	4	5
Large Diameter DN>250					
Water and Sewer Pipe					
Pipe Stiffness 2500					
1	14	8	6	5	NR
2	9	5	4	3	NR
3	6	4	3	2	NR
4	3	2.5	2	1.5	NR
Pipe Stiffness 5000					
1	16	10	8	6	2.5
2	10	6	5	4	1.5
3	7	5	4	3	NR
4	5	4	2.5	2	NR
Pipe Stiffness 10000					
1	18	12	11	9	4
2	15	9	7	6	2.5
3	8	7	6	4	1
4	6	5	4	3	NR
Small Diameter DN < 300					
Water Pipe					
Pipe Stiffness 5000					
1	16	10	8	6	2.5
2	10	6	5	4	1.5
3	7	5	4	3	NR
4	5	4	2.5	2	NR
Pipe Stiffness 10000					
1	18	12	11	9	4
2	15	9	7	6	2.5
3	8	7	6	4	1
4	6	5	4	3	NR
Sewer Pipe					
Pipe Stiffness 5000					
1	10	6	5.5	4	2.5
2	4	3	2.5	2	1
3	3	2.5	1.5	NR	NR
4	2	1.5	1	NR	NR
Pipe Stiffness 10000					
1	15	10	8	6	3
2	7	5	4	3	2
3	4	3.5	3	2	NR
4	3	2.5	2	1.5	NR

Note: NR - Not Recommended

Table 6B
Standard Trench
Maximum Burial Depth (meters) With Traffic Load

Installation Type	Native Soil Group				
	1	2	3	4	5
Large Diameter DN>250					
Water and Sewer Pipe					
Pipe Stiffness 2500					
1	14	8	6	5	NR
2	8	4	3	2.5	NR
3	6	4	2.5	1	NR
4	3	2.5	2	NR	NR
Pipe Stiffness 5000					
1	16	10	8	6	2
2	10	5	4	3	NR
3	7	5	4	3	NR
4	4	3	2	2	NR
Pipe Stiffness 10000					
1	18	12	11	9	2
2	15	9	7	5	2
3	8	7	6	4	1
4	5	4	3	2	NR
Small Diameter DN < 300					
Water Pipe					
Pipe Stiffness 5000					
1	16	10	8	6	2.5
2	10	5	4	3	NR
3	7	5	4	3	NR
4	4	3	2	2	NR
Pipe Stiffness 10000					
1	18	12	11	9	3
2	15	9	7	5	2
3	8	7	6	4	1
4	5	4	3	2	NR
Sewer Pipe					
Pipe Stiffness 5000					
1	10	6	5.5	4	1
2	4	2.5	2	1.5	NR
3	3	2	1.5	NR	NR
4	2.5	1.5	1	NR	NR
Pipe Stiffness 10000					
1	15	10	8	6	2.5
2	7	5	4	3	1
3	4	3	2.5	2	1
4	3	2.5	2	1.5	NR

4.6 Alternative Installations

If the burial depth requirement for the selected pipe stiffness installation type and native soil group exceeds the limits given in tables 6A and 6B, then the following three alternative installation methods may be considered:

- Wider Trench
- Permanent Sheeting
- Cement Stabilized backfill

4.6.1 Wider Trench

Increasing the trench width allows a deeper installation. Tables 7A and 7B specify the maximum cover depth allowed for large diameter pipes, without and with traffic loads respectively. Tables 8A and 8B specify the maximum cover depth allowed for small diameter pipes, without and with traffic loads respectively.

Table 7A
Wider Trench - Large Diameter Pipes
Maximum Burial Depth (meters) Without Traffic Load

Trench Width	3 x DN			4 x DN	
Installation Type	Native Soil Group				
	3	4	5	4	5
Pipe Stiffness 2500					
1	8	6	NR	12	NR
2	5	4	NR	5	NR
3	4	3	NR	4	NR
4	2.5	2	NR	2.5	NR
Pipe Stiffness 5000					
1	10	8	4	14	6
2	6	5	2.5	6	3.5
3	5	4	2	5	3
4	3	2.5	1	3	1.5
Pipe Stiffness 10000					
1	16	12	6	18	10
2	9	8	4	10	6
3	7	5	3	6	4
4	3.5	3	1.5	3.5	2

Table 7B
Wider Trench - Large Diameter Pipes
Maximum Burial Depth (meters) With Traffic Load

Trench Width	3 x DN			4 x DN	
Installation Type	Native Soil Group				
	3	4	5	4	5
Pipe Stiffness 2500					
1	8	6	NR	12	NR
2	4	3	NR	4	NR
3	3.5	1.5	NR	3	NR
4	2.5	NR	NR	1	NR
Pipe Stiffness 5000					
1	10	8	4	14	6
2	6	5	2	6	3.5
3	5	4	1	5	2
4	3	2	NR	2	NR
Pipe Stiffness 10000					
1	16	12	6	18	10
2	9	7	4	10	5
3	7	5	2	6	3
4	3.5	2.5	1	3	1.5

Table 8A
Wider Trench - Small Diameter Pipes
Maximum Burial Depth (meters) Without Traffic Load

Trench Width	4 x DN		5 x DN	
Installation Type	Native Soil Group			
	4	5	4	5
Water Pipe				
Pipe Stiffness 5000				
1	14	6	15	10
2	6	3.5	7	4
3	5	3	6	3
4	3	1.5	3	2
Pipe Stiffness 10000				
1	18	10	19	16
2	10	6	11	6
3	6	4	7	4
4	3.5	2	3.5	2.5
Sewer Pipe				
Pipe Stiffness 5000				
1	7	3.5	10	6
2	2.5	1.5	3	2.5
3	1	NR	1.5	1
4	NR	NR	1	NR
Pipe Stiffness 10000				
1	10	5	18	10
2	4	3	5	4
3	3	1	3.5	1.5
4	2	NR	2.5	1

Table 8B
Wider Trench - Small Diameter Pipes
Maximum Burial Depth (meters) With Traffic Load

Trench Width	4 x DN		5 x DN	
Installation Type	Native Soil			
	4	5	4	5
Water Pipe				
Pipe Stiffness 5000				
1	14	6	15	10
2	6	3.5	7	4
3	5	2	5	3
4	2	NR	NR	NR
Pipe Stiffness 10000				
1	15	10	18	16
2	9	5	10	6
3	5	3	6	3.5
4	2	1.5	3	1.5
Sewer Pipe				
Pipe Stiffness 5000				
1	7	3.5	10	6
2	2.5	NR	2.5	2
3	2	NR	2	1
4	1	NR	1	NR
Pipe Stiffness 10000				
1	10	5	18	10
2	4	2.5	5	4
3	3	2	4	3
4	2	1	2	2

4.6.2 Permanent Sheet piling

Permanent sheet piling can be used to distribute the pipe's lateral loads appropriately. The sheet piling should be at least 300 mm higher than the pipe crown level and driven below the foundation level. The sheet piling system is to be designed by a specialist and the material to be of quality to last the lifetime of the pipe.

4.6.3 Cement Stabilized Sand backfill

Cement stabilized sand is a mixture of one sack of cement (50 kg) and one ton of clean sand. This backfill material provides excellent support to the pipes where native soil conditions are poor. The mixture should be placed in the foundation, bedding, haunches and Pipe Embedment Zone in layers of 15-20 cm. Each layer should be wetted with clean water and compacted with plate vibrators before the cement sets.

4.7 Pipe bedding and foundation

To ensure a firm support for the pipe, proper bedding must be provided under the pipe. During trench excavation, a pipe bedding thickness of at least 150mm must be provided. In case of very poor native soils (silt, clay or mud) additional 150mm thick foundation layer must be provided below the bedding. Selected backfill material should be placed at the foundation and bedding levels and thoroughly compacted by plate vibrators or by hand tamping. Wetting of sand bedding/foundation materials prior to compaction will improve and facilitate the achievement of the degree of compaction required.

Pipe laying should always take place in dry trenches. It is not acceptable to lay pipes in flooded trenches. The Contractor should provide the necessary dewatering equipment to enable installation to proceed in a dry trench. Dewatering equipment should be removed and pumps turned off only after completion of backfilling of the Pipe Embedment Zone and sufficient backfill has been provided to prevent pipes from floating if the normal ground water level is above the pipe invert.

Prior to lowering the pipe into the trench small holes should be dug under each joint location so that the pipe does not rest on the joints. The bedding material should provide firm and continuous support over the entire length of the pipe, excluding the joint area.

The Contractor should lower the pipe into position after checking the proper levels and alignment of the pipeline.

4.8 Pipe Embedment Zone

The selected backfill material should be evenly placed and properly compacted on both sides of the pipe. Appropriate hand or mechanical tamping shall be carried out by the contractor to achieve the specified degree of compaction required by the selected installation type. During the first one or two lifts, special care should be taken to place and to compact the backfill material under the pipe haunches. The best way to achieve this compaction is to do it manually with the mean of a wooden board. This is one of the most important installation steps and should be executed with care. Failure to place and to compact the backfill material under the pipe haunches may cause ovalization, localized loads and over deflection of the pipes

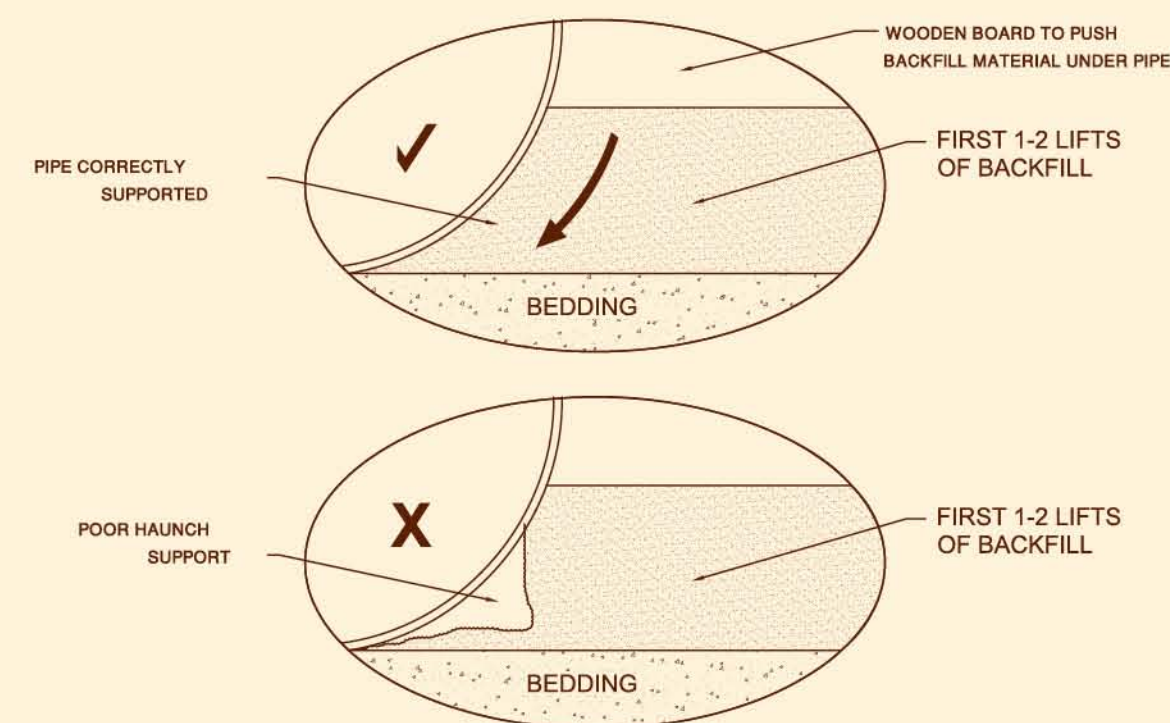


Fig.8: Backfilling of pipe haunches

Pipes joined in the trenches should not be left for long periods without backfilling as some joints may rupture as a result of the daily expansion and contraction of the pipes due to ambient temperature fluctuation. However, if the pipes are sufficiently restrained to prevent movement, the joints may be left exposed for an easy visual inspection during the field hydrotest. These joints must be backfilled immediately after the test to avoid damages.

The contractor should note that the compaction of clean and mixed sand is best achieved when the material is at its optimum moisture content. While the wetting of sand is recommended prior to compaction, trench flooding should be avoided to prevent pipes from floating.

Following the first two layers where the backfill has been sufficiently placed, compaction should proceed from the sides of the trench towards the pipe. The pipe Embedment zone backfill should proceed in 150 to 300 mm lifts depending on backfill type see section 4.1. The pipe Embedment Zone backfilling and compaction should continue until the backfill reaches at least 15 cm above the pipe crown. For pipes larger than 1000 mm diameter, backfilling the pipe embedment zone should continue to 300 mm above the pipe crown.

After completion of backfilling in the pipe embedment zone, native material excavated from the trench may be used to complete backfilling to final grade. No compaction is required in these final backfilling layers except where specified by the engineer, or in the case of traffic or other high external loads over the pipes where settlement of the native backfill is to be avoided.

CAUTION: Sand layers of more than 300 mm cannot be compacted properly and may result in loss or reduced support for the pipes. The best compaction results are achieved with wet sand near its optimum moisture content. But flooding of the trench must be avoided as pipe floatation may occur. A minimum of one pipe diameter of granular backfill is normally required to prevent the pipes from floating.



4.9 Backfilling where temporary sheet piles or shoring is used

Special attention and care from the contractor's side is required when the pipes are backfilled in sheeted trenches. If sheeting or trench shoring is withdrawn after compaction, hollow spaces will be left and soil pipe support will be lost or reduced,

CAUTION: Sheet piles must be withdrawn in stages as backfilling progresses in such a way that all hollow spaces left behind the sheeting are filled with compacted backfill material.

4.10 Offshore Pipelines

This installation method is used for the offshore portion of FIBERBOND pipes. The pipes joints are assembled under the water. Steel angle irons lugs will be provided on the two ends of pipe to allow divers to assemble the standard Reka coupling joints under water. It may be possible to assemble on the barge up to 3 lengths of pipe and to lower the assembled section (total length of 36 m) into the excavated sea bed trench.

CAUTION: Standard pipe is not designed to be assembled on-shore in long lengths and then dragged out to the sea.

Installing FIBERBOND pipe under water requires a trench similar to the onshore trench, except the fact that the trench width is larger. The typical underwater trench width is equal to $2 \times \text{DN}$, but in no case less than $\text{DN} + 1$ meter. The cover over the pipes shall not be less than 1 meter above the pipes on the normal seabed.

The divers should make backfilling with excavated granular seabed materials in the maximum 300 cm lifts, paying particular attention to the backfilling and compaction of the backfill under the pipe haunches. Backfilling should be made evenly on both sides of the pipe to avoid pipe displacement.

Protection shall be allowed for the backfilled seabed over the pipe trench. Large stones or rocks (rip-rap) may be used for this purpose.

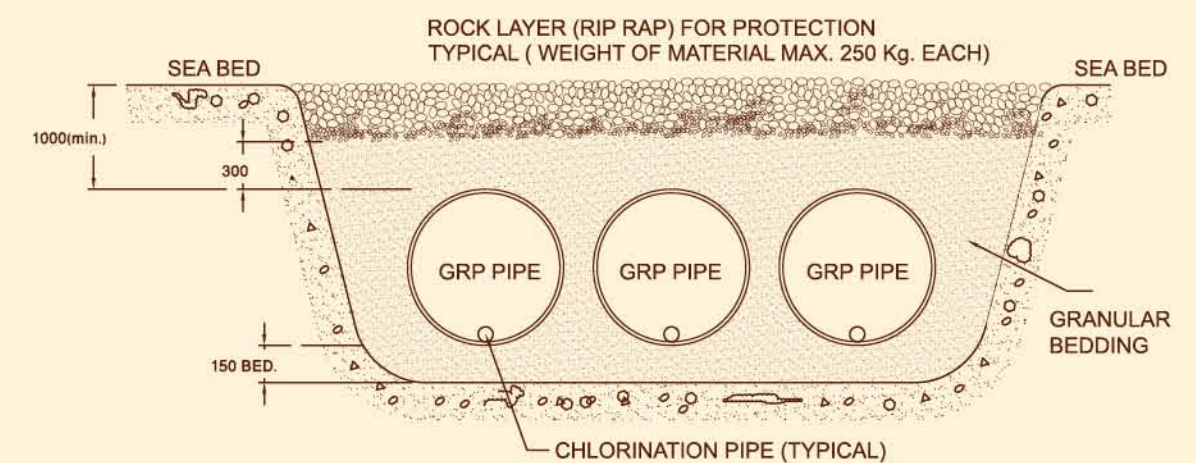


Fig. 9: Offshore pipelines installation

4.11 Thrust boring and micro-tunneling installations

This method is used when the ground above or around the pipe cannot be distributed. This is the case for crossings under highways, railways, airport runways, rivers etc. This method might be economical for very deep sewer lines where the cost of opened trench excavations may become excessive due to the ground conditions where extensive sheet pilings and dewatering might be required.

Standard FIBERBOND pipes can be provided in short lengths to be encased in a concrete jacket. In this case, the outer concrete pipes take the jacking load while the inner FIBERBOND pipe provides the corrosion resistance and the required joint tightness.

5. JOINTS

5.1 Double Bell Coupling

5.1.1 Joint Angular Deflection

Double bell coupling joints, used to join FIBERBOND pipes, allows for a certain angular deflection. The maximum allowed angular deflection, distributed equally on both sides of the joint, and the resulting offset and the radius of curvature are given with respect to the pipe nominal diameter and section length, in table 9.

Table 9: Allowable Double Bell Coupler Joint Angular Deflection

DN (mm)	Joint deflection (degree)	Offset (mm)			Radius (meters)		
		L=3m	L=6m	L=12m	L=3m	L=6m	L=12m
<500	3	157	314	628	57	115	229
500 to 800	2	104	209	419	86	172	344
900 to 1700	1	52	104	209	172	344	688
> 1700	0.5	26	52	104	344	688	1375

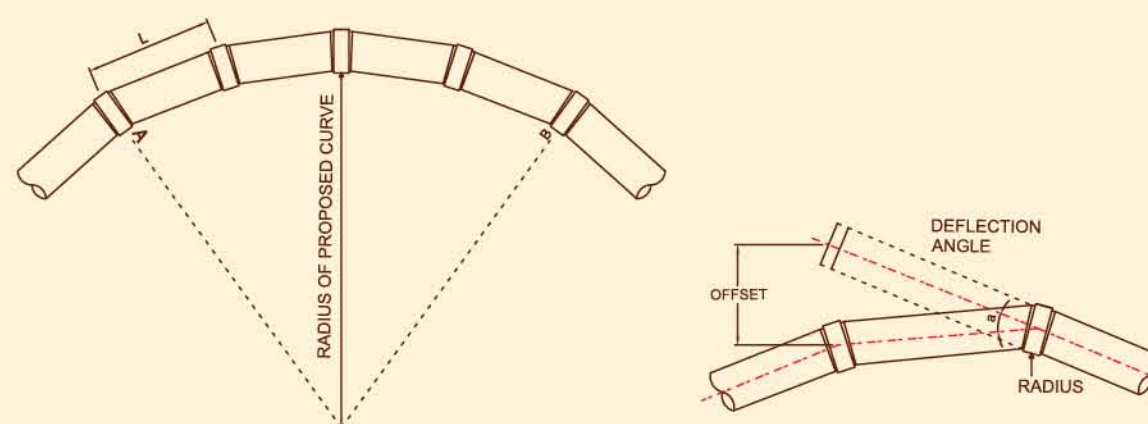


Fig. 10: Double Bell Coupler Joint Angular Deflection

Note: The angular deflection can occur in the horizontal as well as in the vertical plane. It is recommended that above limits not to be reached during installation.

5.1.2 Lubricant consumption

For lubricant, use only a vegetable based on soft soap. In dusty conditions lubricate generously the coupling only. The recommended amount of joint lubricant required is shown below.

Table 10: Lubricant Consumption

DN (mm)	Amount of lubricant required per joint (kg)
80 - 300	0.05
350 - 500	0.1
600 - 800	0.12
900 - 1000	0.2
1100 - 1200	0.25
1300 - 1400	0.3
1500 - 1600	0.4
1700 - 1900	0.45
2000 - 2200	0.5
2400	0.75
2600	1

CAUTION: Never use petroleum-product grease or automotive oils to lubricate the joint, as they will damage the rubber rings.

5.1.3 Preparation of the FIBERBOND coupling (Double bell Coupler)

In order to avoid damage, the sealing rubber ring must be fitted into the Reka FIBERBOND coupling just before the laying starts.

- For large diameters lay the coupling horizontally for better control and safety.
- Clean the groove in the coupler and the rubber ring before inserting it.
- Insert the rubber ring into the groove, leaving uniform loops extending out of groove. There should be one loop for every 500 mm of ring circumference. Do not lubricate the rubber of the groove at this stage.
- With uniform pressure, push all the loops simultaneously into the groove.
- Make sure that the compression in the ring is uniformly distributed all around the circumference.



5.1.4 Mounting the coupler

This operation can be carried out either inside or outside the trench. In the latter case it is recommended to lower the pipe with the free end towards the laid portion of the line. Clean coupling and pipe ends with a firm brush and inspect them thoroughly. Lubricate the pipe end and the coupling rubber ring by means of a dry clean piece of cloth or a sponge.

For small diameter pipes (DN≤350mm) the coupling can be mounted by hand or with a crow bar. Use a timber block to protect the coupling and force the coupling up to the correct position that is indicated by the home line on the pipe spigot.

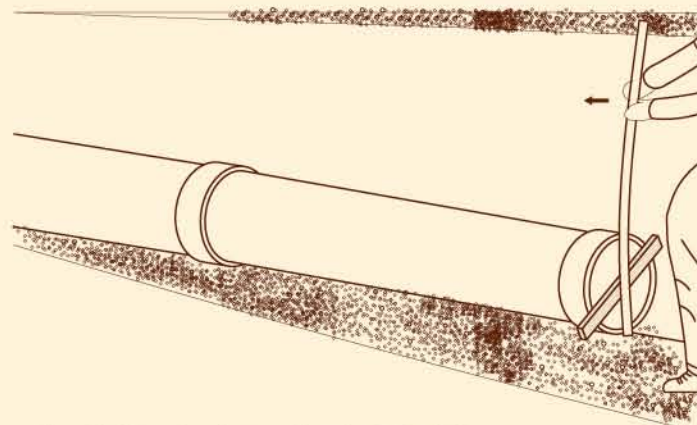


Fig. 11: Mounting the coupling for DN ≤ 350 mm

For pipes with diameters above 350mm, a come-along type puller is used. This apparatus is fixed to the outside of the pipe by friction.

CAUTION: Under no circumstances should brute force be applied to mount the coupling. The pipes and couplings are dimensioned within tolerances that allow jointing to be carried out without using excessive effort.

5.1.5 Inserting the pipe in the coupling

Joints should be made inside the trench following the procedures shown in figures 12 and 13. A steel strap with rubber lining must be fixed on the installed pipe at the home line in order to stop insertion of the pipe in the coupler at the pipe home line. Alternatively, a wooden spacer may be used inside the couplings to maintain the correct spacing. All spacers must be removed immediately after jointing the pipes. Spacers may damage air valves fitted in the system if they are not removed before the hydrostatic test. Before insertion, the two pipes should be perfectly aligned and levelled to avoid any damage to the rubber rings.

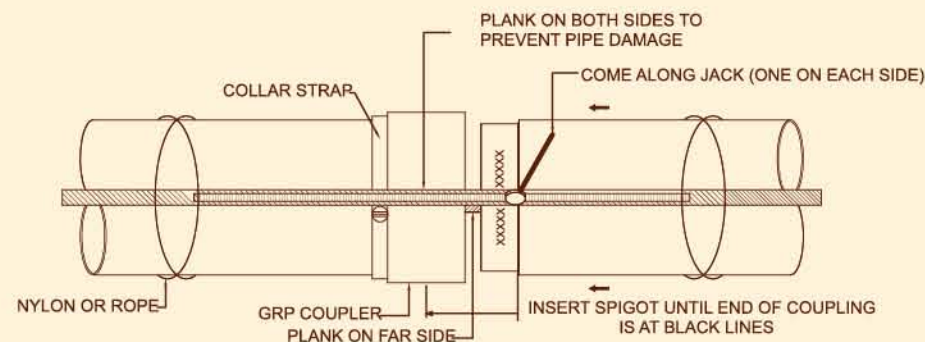


Fig. 12: Pipe Jointing using a "come along" jack

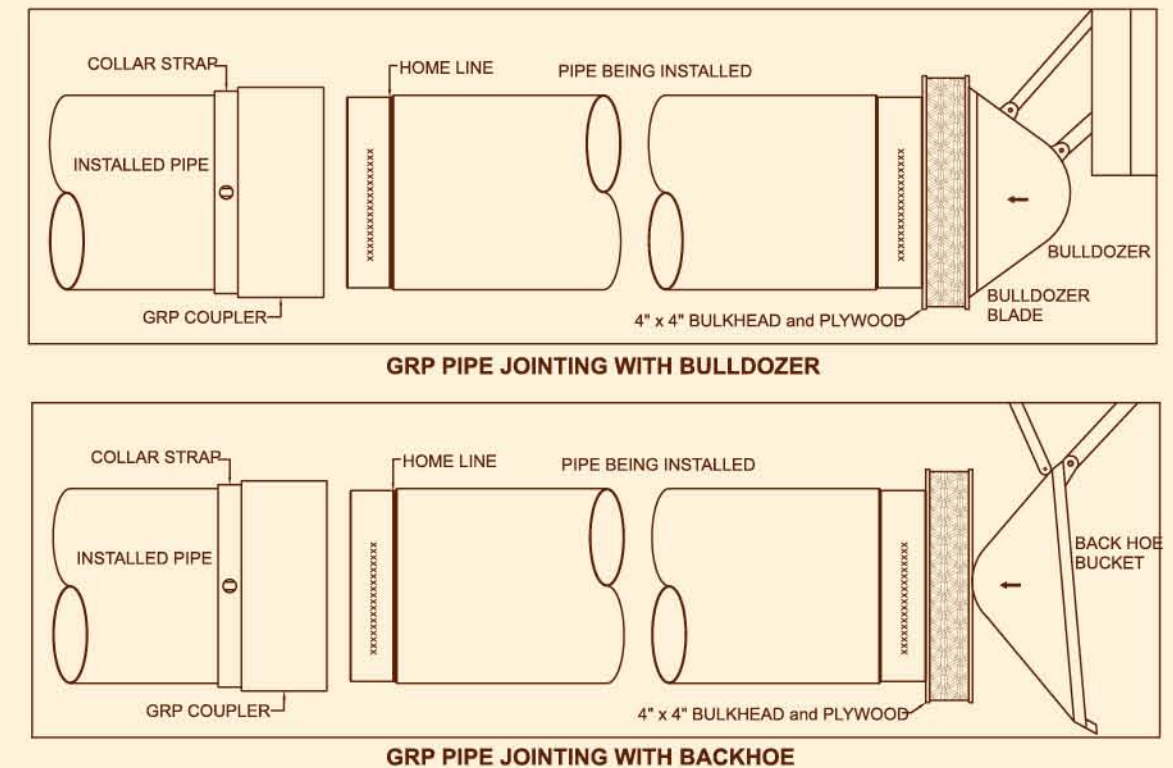


Fig. 13: Pipe jointing using construction equipments

Working with mounting equipment, although very efficient, should not be carried out by unskilled laborers. Risks of damaging or dislodging a rubber ring should not be disregarded. It is essential to push the coupling not beyond the home line. Otherwise the pipes in the coupling will touch each other and will consequently not allow for any expansion or deflection inside the joint. Only skilled operators should attempt to use the boom of an excavator to push either coupling or pipe, as the direction of the applied force is not under control and might damage the pipes and/or the coupling. No steel tools should come into direct contact with the edges of the pipe or its external surface. Pipe edges should be protected with a timber.

5.2 Lamination Joints

This joint is made from glass fiber reinforced embedded in polyester resin. The length and thickness of the joint depends on the diameter and the pressure.

This type of joints requires special working condition and should be performed only by skilled workers. Always consult the pipe manufacturer before performing lamination joints.

5.3 Flanged Joints

Flanged pipes and fitting can be provided for use inside valve chambers. Contact our engineers for flange thickness before ordering flange bolts as they are thicker than steel flanges.

6. SPECIAL REQUIREMENTS

6.1 Standard short length pipes

Standard short pipe lengths are required in various situations, such as:

- For outside rigid structure (i.e., water reservoirs, pumping station, thrust blocks, valve chamber, Manholes, etc)
- To connect the pipes to a line fitting such as bends or tees inside thrust blocks.

Standard short length pipes shall be planned ahead by the contractor. The recommended length (L) of standard short pipe is $1.5 \times \text{DN}$ with a maximum of 2000mm and a minimum of 500 mm.

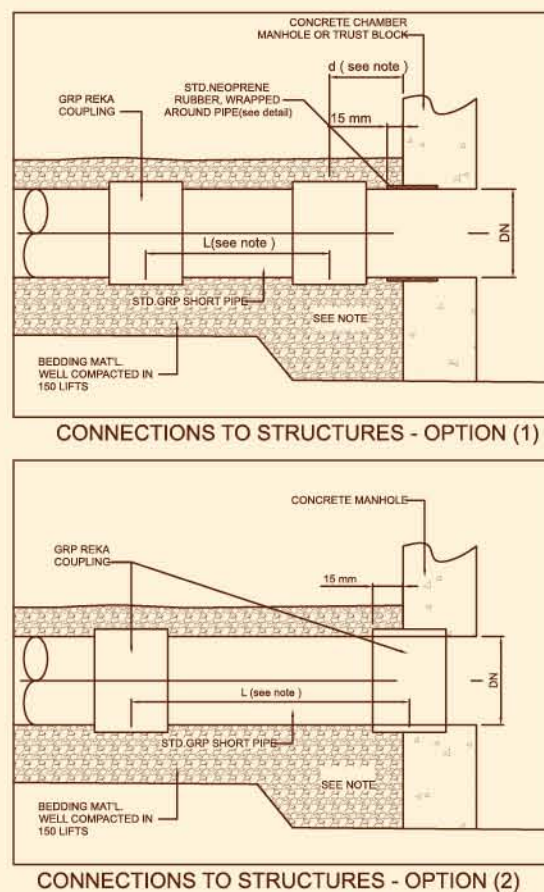


Fig. 14: Standard Short Pipe

6.2 Pipeline closures

For a closure in a line it is required to order a special short pipe from the factory with double width calibration. The contractor should clearly indicate in his order that a short pipe closure is required. In closure pipes, the length of the machining is equal at least to the width of the Reka coupling plus 30mm.

Before ordering a closure pipe, the contractor should measure accurately the gap between the two ends of the line. The length of the pipe to be fitted must be 32 mm less than the measure length to allow a gap of 16 mm between the jointed ends in both couplings. Mark the home line on the machined ends if necessary and lubricate them abundantly. The assembly of the short length pipe is made as indicated in figure 15 below.

CAUTION: When pulling the couplings over the insertion piece it is necessary to pull the second rubber ring smoothly over the chamfer of the pipe to avoid damaging it. For that purpose, use approved lubricants abundantly. To locate a fitting exactly, it is recommended to place it at the required position, to assemble the first pipe in full length, and then to make a closure as indicated above.

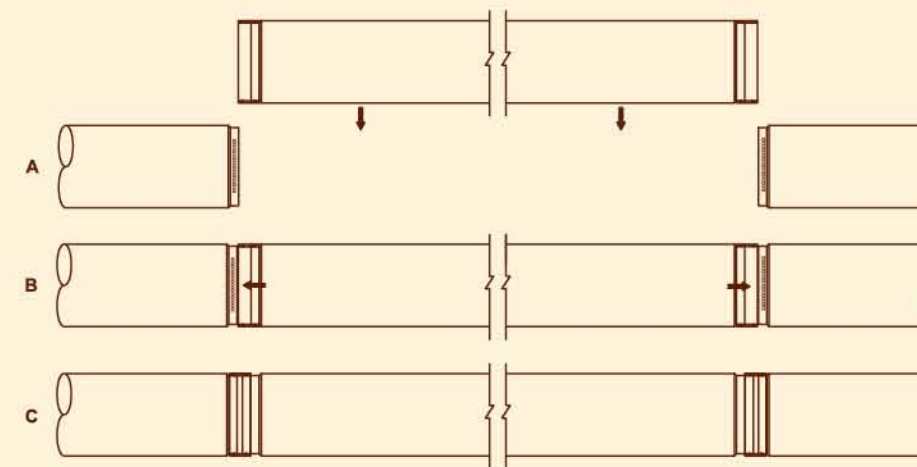


Fig. 15: Pipeline Closure

6.3 Thrust blocks and anchoring

Thrust blocks must be used in pipeline systems with non restrained joints such as the double bell coupling wherever thrust loads are expected, such as at:

- Changes of direction (Bends, Tees, Wyes)
- Cross section changes (Reducers)
- Valves and hydrants
- Dead ends

The thrust blocks can be dimensioned and designed according to the expected thrust load as well as native soil properties. Thrust block space must be foreseen in the design and trench excavations. At vertical bends, the line or the bend must be anchored by thrust blocks or other means to resist outward thrusts. Thrust blocks must be cast against undisturbed trench walls (native soil) and must completely encase the fitting (except at the joint area). The maximum allowable displacement of fittings is 0.5% of the diameter, or 6mm; whichever is less. The outlet part of the encased fitting in the concrete block shall be rubber wrapped as shown in figure 16. See Appendix II for additional information about thrust blocks.

Note: Gravity lines up to 1 bar pressure do not require thrust blocks.

Caution: Always provide a standard short pipe length outside thrust blocks (see section 6.1) to protect the pipeline from differential settlement-

Nozzle connections should be concrete encased. Nozzle are tee branches meeting all the following criteria:

1. Nozzle diameter $\leq 300\text{mm}$
2. Header diameter ≥ 3 times nozzle diameter
3. If the nozzle is not concentric and/or not perpendicular to the header pipe axis, the nozzle diameter shall be considered to be the longest cord distance on the header pipe wall at the nozzle/pipe intersection.

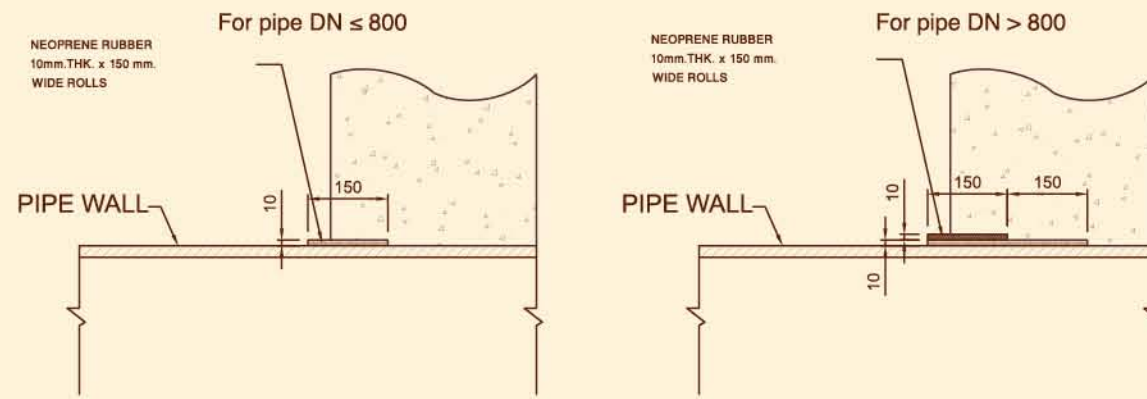


Fig. 16: Rubber wrapping

6.4 Concrete Encasement

Pouring concrete around the pipe results in uplifting forces that can damage the pipe and/or joint. To avoid such movement, the pipe should be anchored downward by straps hooked to a rigid base. The straps should be flat material of minimum 25mm width. The distance between straps should not exceed 4 meters, with a minimum of one strap per section length. Straps should not be over-tightened.

6.5 Fittings for valve chambers

One of the advantages of FIBERBOND pipe systems is customized fittings. Using a piping system greatly simplifies the valve chamber design and eliminates unnecessary flanged joints as shown in figure 17. Valves must be sufficiently anchored to take the thrust force.

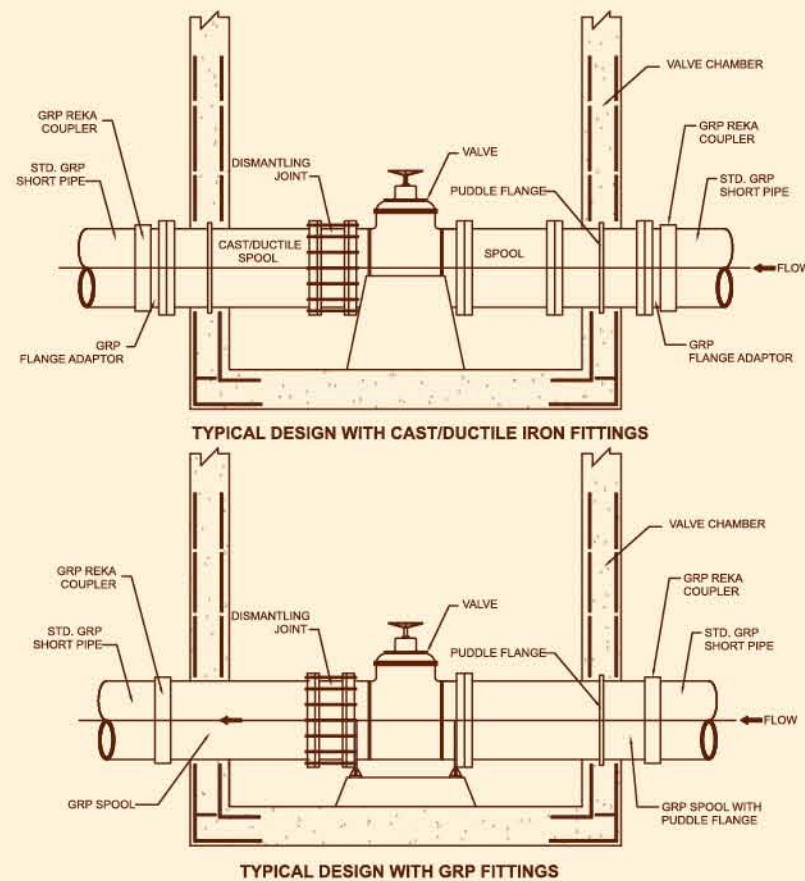


Fig. 17: Valve chamber

7. PIPE DEFLECTION

The deflection of pipe depends on the pipe diameter, pipe medium and native soil classification. pipe deflection is defined as the percentage reduction in vertical diameter after installation as shown below in figure 18.

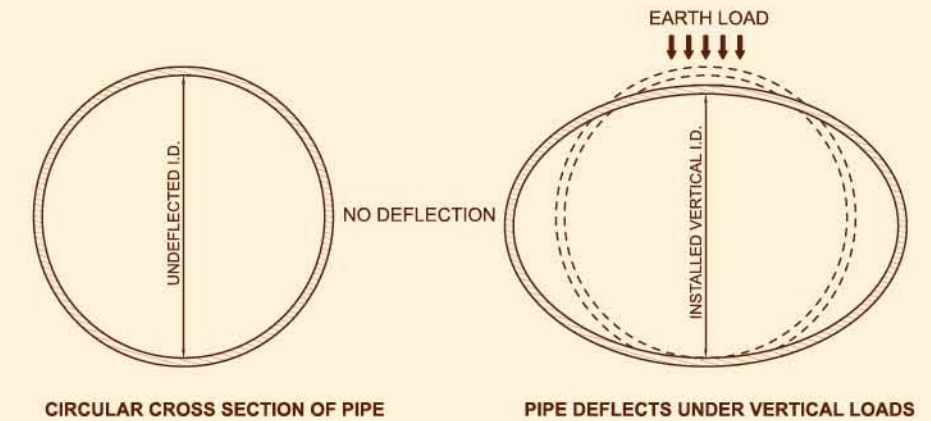


Fig. 18: Pipe Deflection

$$\% \text{ Deflection} = 100 \times \frac{(\text{Actual undeflected pipe ID} - \text{Installed ID})}{\text{Actual undeflected pipe ID}}$$

To ensure that the long-term deflection does not exceed the maximum allowable limit, the preliminary & initial deflection of the pipe must be monitored and controlled in site by the contractor, maintaining the deflection within allowable limits is achieved by proper selection of pipe stiffness, installation method related to the native soil conditions, and maximum burial depth.

Measuring pipe deflections is easy and is the best way for the contractor to check if the installation was executed properly.

FIBERBOND pipes deflection is measured in the following manner:

For pipe sizes 800mm and larger, where human entry inside the pipes is possible, the installed vertical pipe ID can be measured by means of a manual micrometer at 3 to 4 m intervals. An electronic deflectometer is used to measure the deflection of the pipes of diameter within the range of 400 to 800 mm. A probe with sensed arms is pulled through the line, recording the pipe ID on a data logger kept outside the line. The results are then presented on a computer generated report.

A wooden disc (Pig ball), with an outside diameter equal to the maximum acceptable deflected pipe ID, may be pulled through the pipes. If the pig passes freely, it means that the pipe deflection has not exceeded the limit set by the pig OD. Please check the figure 19 for a typical configuration of a wooden Pig.

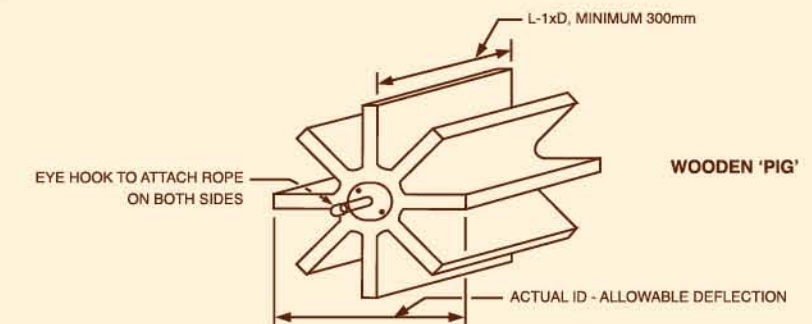


Fig. 19: Pipe pig ball

Note: It is important that pipe deflection measurements are done at the same time of pipe laying operations and not after. This will allow for early detection of any installation deficiencies and allow corrective action to be taken quickly in order to reduce the time and expenses necessary to rectify defective installations.

Table 11: Maximum allowable deflection

	Deflection (% of Pipe Diameter) in a native soil of group				
	1	2	3	4	5
Large Diameter Pipes, DN> 250 - Water and Sewer					
Initial	4	3.5	3	2.5	2
Long Term	5	5	5	5	5
Small Diameter Pipes, DN<300					
Water					
Initial	3	3	2.5	2	2
Long Term	5	5	5	5	5
Sewer					
Initial	2.5	2.5	2	1.5	1.5
Long Term	4	4	4	4	4

7.1 Preliminary Deflection

This measurement should be taken when backfill reaches 30cm above pipe crown. At this stage the measured deflection should be slightly negative, but not exceeding - 2%. A negative deflection means the pipe vertical ID has increased because of the compaction forces/stresses coming from the side backfill.

A positive deflection at this stage indicates inadequate compaction in the Pipe Embedment Zone, hence improvement in the quality of installation and compaction is required. In such, it is advisable to remove the backfill to about 1/3 of the pipe ID from the invert level and to re-compact the backfill in stages up to the top of the pipe zone, with special care to the compaction of the pipe haunches backfill area. After this rectification, the preliminary deflection should be measured again.

7.2 Initial Deflection

This measurement should be done immediately after backfilling reaches the final grade and after all temporary sheeting has been withdrawn and all de-watering systems have been turned off for two days-The initial deflection limits are set to account for creep and soil consolidation with time (determined by the deflection log factor).

If the initial deflection exceeds the allowable limits up to 8% of the pipe diameter, the contractor should re-excavate the trench (by hand from 0.3 m above pipe crown), remove the Pipe Embedment Zone backfill and start re-backfilling the pipe, paying attention to the pipe haunches and backfilling in appropriate lifts to reach the required compaction. If the deflection slightly exceeds the allowable limits, the deflection may be monitored over the following 6 months period with monthly deflection measurements. If deflections at the end of 6 months period do not exceed the following long-term deflection limit, the pipeline section may be considered as accepted.

Any recently installed pipe exhibiting deflections equal or greater than 9% (7% for pipes SN 10,000) must be replaced. Such pipe must not be re-installed nor incorporated in any permanent works on site.

7.3 Final Deflection

This measurement should be done at least 6 months after the initial test is done. The maximum deflection at this stage should not exceed the limits specified in table 11.

8. FIELD TESTING

8.1 Line Hydrostatic Testing

8.1.1 Preparations

Prior to the hydrostatic test, several points must be checked in order to avoid failures:

- While the contractor tends to test long sections to increase his efficiency, the length of the test section should be short enough to allow an easy detection of any possible leak. It is also difficult to fill a very long line with out risk of air entrapment.
- The backfilling must have carried out properly and reached a level that would restrain the pipes to avoid movements during testing. The joints may be left exposed for visual inspection. The thrust blocks, which are part of the pressure test section, should be of permanent constructions and concrete should be poured at least 7 days before testing.

Check whether all testing apparatus are available and operational.

- The open ends of a line must be sealed temporarily with GRP or steel/cast iron end-caps. GRP testing end-caps can be purchased from the manufacturer with the pipes and the fittings. All the end-caps should have an inlet for water filling and an outlet for venting. See figure 20 for a typical arrangement of a test section and apparatus. The approximate end thrust force is given in the table below.

DN (mm)	Cross Section Area (cm ²)	End Thrust Force (Kg)							
		Test Pressure (bar)							
		4.5	9	12	15	18	20	24	30
80	64	286	573	763	954	1,145	1,272	1,527	1,909
100	95	428	855	1,14	1,425	1,711	1,901	2,281	2,851
150	201	905	1,81	2,413	3,013	3,619	4,021	4,825	6,032
200	346	1,559	3,177	4,156	5,195	6,234	6,927	8,313	10,391
250	539	2,426	4,852	6,47	8,087	9,704	10,783	12,939	16,174
300	769	3,463	6,925	9,233	11,542	13,85	15,389	18,467	23,083
350	1,052	4,734	9,469	12,625	15,781	18,938	21,042	25,25	31,563
400	1,366	6,146	12,291	16,389	20,486	24,583	27,314	32,777	40,972
450	1,787	8,042	16,083	21,444	26,805	32,166	35,74	42,888	53,61
500	2,099	9,447	18,894	25,191	31,489	37,787	41,986	50,383	62,978
600	2,988	13,446	26,892	35,856	44,82	53,784	59,76	71,712	89,64
700	4,043	18,195	36,389	48,519	60,649	72,779	80,866	97,079	121,298
800	5,281	23,765	47,529	63,372	79,215	95,058	105,62	126,744	158,43
900	6,684	30,077	60,154	80,205	100,257	120,308	133,676	160,411	200,513
1000	8,252	37,132	74,264	99,019	123,774	148,528	165,032	198,038	247,547
1100	9,984	44,93	89,86	119,813	149,766	179,719	199,688	239,626	299,5332
1200	11,882	53,47	106,941	142,587	178,234	213,881	237,646	285,175	356,468
1300	13,945	62,753	125,507	167,342	209,178	251,013	278,903	334,684	418,355
1400	16,173	72,779	145,558	194,077	242,597	291,116	323,462	388,154	485,193
1500	18,566	83,547	167,095	222,793	278,491	334,189	371,321	445,585	556,982
1600	21,124	95,058	190,116	253,489	316,861	380,233	422,481	506,977	633,722
1800	26,735	120,308	240,616	320,822	401,027	481,232	534,703	641,643	802,054
2000	33,006	148,528	297,057	396,076	495,095	594,114	660,127	792,152	990,19
2200	39,938	179,719	359,439	479,252	599,065	718,878	798,753	958,504	1,198,130
2400	47,529	213,881	427,762	570,349	712,937	855,524	950,582	1,140,699	1,425,873
2600	55,781	251,013	502,026	669,368	836,71	1,004,053	1,115,614	1,338,737	1,673,421

Table 12 - End thrust during pressure testing

(Values are given in kilograms - some diameter/pressure combinations might not be available)

Note : for the Diameters between 2000 mm and 2600 mm please consult the manufacturer)

8.1.2 Bracing test-ends and set-up

Due to the thrusts occurring at the testing end-caps, temporary blocks must be used to brace the pipe end-caps in order to prevent line displacement as indicated in figure 20.

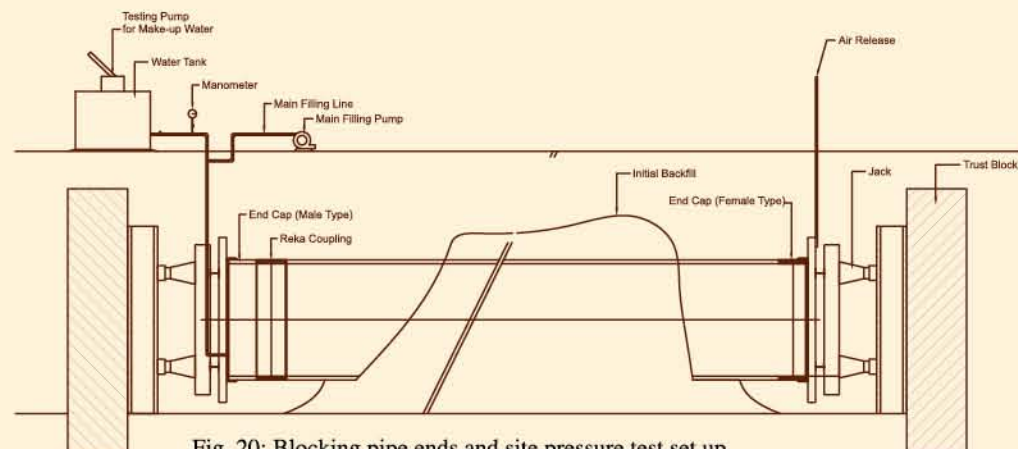


Fig. 20: Blocking pipe ends and site pressure test set up

In the gap between the end of the pipeline and the block, jacks should be placed as shown in figure 20. The last pipe length should also be wedged on both sides, at the top and at the bottom, in order to prevent lateral and vertical movements. Sandbags can be used for this purpose.

Note: It may be possible to reduce the size of the concrete blocks by driving into the ground, several meters deep, two or more steel piles back to back. Sheet piles so positioned behind the concrete blocks will provide additional bracing.

8.1.3 Filling the line with water

The pipeline should be filled slowly and evenly with water from the lowest end point. At high points, air vents will be installed to release the entrapped air. After filling the line with water, the test section should be left for stabilization. The filling rate of the line with water should be controlled to ensure a proper venting and to keep the flow velocity below the allowable limit. Following the stabilization period and after expelling all the entrapped air out of the pipe test section, the air vents should be closed.

8.1.4 Volume of water required

Table 13 indicates the approximate volume of water required in order to fill FIBERBOND pipes per 100 meter of pipeline.

Table 13: Volume of water required

DN (mm)	Water volume (m³) / 100m of pipeline	DN (mm)	Water volume (m³) / 100m of pipeline
80	0.5	900	63.6
100	0.8	1000	78.5
150	1.8	1100	95
200	3.1	1200	113
250	4.9	1300	132.7
300	7.1	1400	153.7
350	9.6	1500	176.7
400	12.6	1600	201
450	15.9	1700	226
500	19.6	1800	254.4
600	28.3	2000	314.1
700	38.5	2200	380.1
800	50.3	2400	452.4
		2600	530.9

8.1.5 Pressurizing

After the stabilization period, the pressure shall be raised gradually until the intended test pressure at the lowest point reached.

Unless otherwise specified by the Engineer, the test pressure shall be equal to 1.5 times the intended working pressure of the pipeline section, but shall not exceed the pipe pressure class. Once the required test pressure is reached, the pressure should be maintained for a holding period.

During the pressure test, all joints should be visually inspected (where ever possible), and all visual leaks should be repaired. In case the test is not satisfactory, the locations of the leaks shall be determined and rectified, and the line should be re-tested in the same manner as specified above. The test section shall be accepted only after successfully passing the above leakage test.

During the holding period, if the pressure drops, make sure that the thermal effect and the air entrapped is not the cause.

Notes:

1. The contractor should note that while pressure testing large diameter FIBERBOND pipe on site at pressure generally above 10 bars, there is a possibility of a slight rotation/pivoting of the FIBERBOND coupling, and is inevitable during normal joint assembly where a perfectly centered and aligned joint can never be achieved. In the unlikely event that one or more joints start to rotate or to shift slightly during the pressure test, it is advisable to reduce the pressure, and to backfill the joints completely using selected, properly compacted backfill prior to resumption of the pressure test. Any joint that has shifted significantly should be centered again before resuming the pressure test.

2. Test pressure of pipelines are related to the intended working pressure (Pw) in the pipes but not to the rated pressure class of the pipes (PN)

8.2 Joint Hydrostatic Testing

Joint testing is applicable only for diameters of 800 mm and above. This method is recommended in the case of..

- Non availability of a sufficient water supply source
- Unstable soils, which is a potential problem in the case of section testing
- Large diameter pipelines where traditional pipe section pressure test is not feasible

Please contact our engineers for more information about the joint tester.

As laying proceeds, each coupling is tested for its water tightness by applying internal hydrostatic pressure by means of a mobile joint testing apparatus fitted internally and designed to seal internally the gap between the pipe ends. When the pressure is applied, it results in high thrust, and the pipes must be solidly anchored and wedged laterally.

The last pipe laid must be at least 2 pipes ahead of those to be tested. Prior to the test, the pipe sections must have at least 1xD of cover above the pipe crown, with a minimum of 300mm and a maximum of 1m. It is not essential to leave the joints exposed to ambient atmosphere in this test method. The test pressure shall be 1.5 times the intended working pressure of the pipes.

Caution: Pipe joint testing shall be performed in well ventilated pipelines only. The safety of the operators inside the pipe must always be assured. For safety considerations, the operators must preferably work at the free end of the joint tester (near to the pipe access). All operators must be securely hooked to a guide rope with other workers terminating, outside the pipeline to allow pulling them out from the pipes in case of an emergency.

8.3 Pressure Testing of Gravity Lines

Two methods are available for testing gravity lines, a low-pressure air test or a low head water test.

8.3.1 Low Head Water Test

The contractor should plug both ends of the pipeline section (between two manholes) with suitable plugs. The test section should not exceed 200 meters. The plugs should have connections for a stand pipe (typically 50 or 75 mm in diameter) connected to the pipe plug with a 90° elbow, At the upstream manhole, the stand pipe shall extend 1.2 m above the crown of the gravity pipe, or 1.2m above the existing ground water level, This level is called the test level. The test section shall be filled slowly from the upstream manhole while releasing the air out. Allow the water to stand for about 1 hour for stabilization, then add water until the test level is again reached in the stand pipe at the upstream manhole. Start the test, and over the next 30 minutes. The amount of water necessary to maintain a constant test level water head shall be measured using graduated containers of water. The line shall pass the test if the exfiltration amount does not exceed 15 liters per 24 hours per mm of pipeline diameter per kilometer of pipe. A typical test set up is shown in figure 21.

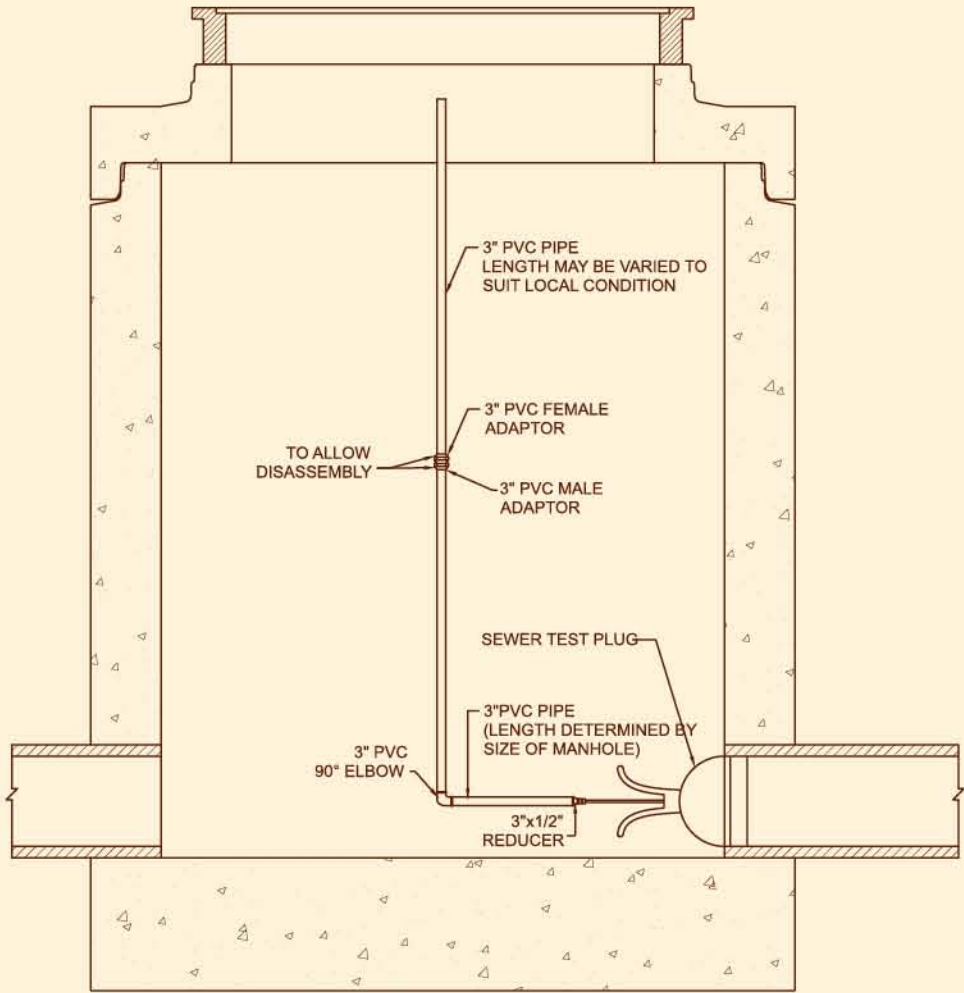


Fig. 21: Low head water test

8.3.2 Air test

The Contractor should plug both ends of the pipeline section (between two manholes) with suitable plugs. The plugs should have connections for air and a manometer or air pressure gauge. Air shall be pumped into the line until a pressure of 25 kPa is indicated on the manometer or air pressure gauge. After 5 minutes stabilization period, air may be added to restore the pressure up to 25 kPa. During the test period shown in table 14, if the pressure drop does not exceed 7 kPa gauge, the line shall be considered as having passed the air test.

Table 14: Low pressure air test

DN (mm)	Test time (hours)/ 100 m	DN (mm)	Test time (hours)/ 100 m
100	0.9	350	6.5
150	2	400	7.2
200	3.5	450	7.7
250	4.7	500	9.3
300	6	600	10

Note: In case where the pipes are laid below the ground water table, the test pressure shall be increased by 10 kPa gauge. For every 1 meter of ground water above the pipe crown. If the resulting air test pressure exceeds 35 kPa, the air test method should not be used and the infiltration method is recommended.

Caution: Air test can be dangerous if the line is not prepared properly and safety precautions are not taken. It is very important to install the test plugs properly and brace them to prevent blowouts. Air pressure must always be relieved before attempting to remove the test plugs. The test equipment should include a pressure relief valve designed to release air and prevent pressure from exceeding 42 kPa gauge.

9. PIPELINE COMMISSIONING

After completing the hydraulic test, the line must be thoroughly flushed out and disinfected (in case of potable water lines), as specified by the engineer or local regulations. In the absence of any such regulations, the guidelines may be followed.

Disinfecting potable water lines is normally performed using either of the following chemical mediums:

- Liquid Chlorine
- Sodium Hypochlorite solution
- Calcium Hypochlorite granules or tablets

This application gives a solution containing at least 20 to 25 mg/l of free chlorine initially. The disinfecting period is normally 24 hours after which the residual chlorine should not be less than 10 mg/l. After the 24 hours disinfecting period, the line is flushed and filled with potable water.

When commissioning a pipeline, first ensure that all air valves are fully opened to release entrapped air. Fill the line very slowly and evenly at velocities not exceeding 0.3 m/s. Do not open valves quickly and fully during filling. After releasing all air, close air valves and hydrants and open inlet valve fully. If the line is coupled to a pump, the inlet valve should be closed when the pump starts running. Later on, the inlet valve shall be opened slowly. The discharge valve should be closed slowly before shutting down the pump.

10. AIR IN PIPELINES, AIR VALVES AND SURGE CONTROL

Air in pressure pipelines can cause major operational problems. Typical problem induced by the presence of such air are the reduction in flow capacity because of reduced cross sectional areas and fluctuation in flow caused by expansion and contraction of the air pockets in the line. High surge pressures can result from the flow fluctuations, which cause sudden movements of the air from one location to another, followed by slugs of water. Also surge (water hammer) can occur in pipelines from opening and closing valves and from start up and shutdown of pumps.

Air can enter a pipeline from many locations like :

- Line Drains
- Negative surges (vacuum) causing air to enter at air valves in the pipeline
- Intake source
- Release of dissolved air from the water by temperature and pressure variation.
- Draining parts of the pipeline or the pipe system during normal shut down

In the first instance air shall be prevented from entering the line. This will reduce operational difficulties.

Suggested solutions for controlling entrapped air in pipelines are as follows:

- The intake point should be provided with low water level pump cut-off.
- Release of air: Air dissolved in the water at the intake and released due to temperature and pressure fluctuations cannot be prevented. However, the quantities of such air are not large and provisions for releasing the air can be made by the means of air valves. Proper selection of air valves is essential.
- While draining the line, air cannot be prevented from entering the line. Large orifice air valves should be provided for exhausting the air during refilling, Long filling times will allow the complete release of air.
- Negative surges (vacuum) – Large volumes of air may be involved here and can cause serious operational problems. The best way to prevent air from entering under these conditions is by proper design to eliminate the possibility of water column separation.

Studies have shown that suddenly released entrapped air under apparently static conditions creates a situation similar to a water hammer. Generated pressures can be of the order of several times the pipeline test pressure. Any pipeline material can be seriously affected by the quick increase in the magnitude of pressure loads.

Remedial actions against entrapped air and water hammer are as follows:

1. Lay the pipeline essentially to grade wherever is possible, avoiding major slopes. It may be advantageous to create artificial high points by providing a small slope of around 1-2 mm per m to facilitate air collection at high points.
2. Automatic continual acting air release valves should be used at all major high points. Almost all the air release valve manufacturers limit the maximum distance between air release valves to around 750 meters.
3. Air should be sucked out from the pipeline slowly.
4. Maximum filling velocity of the pipeline is 0.3 m/s.
5. Use $d/D = 1/10$ to $1/15$.
 d = diameter of air release valve
 D = pipe diameter
6. Using motorized actuated valves is an effective means of limiting positive surges to an acceptable level by controlling the rate of opening and closing of the valves.
7. Flywheels on pump motors allow the pump to keep on running for a short period of time after any power shutdown, before it gradually stops.

11. REPAIR AND REPLACEMENT OF A PIPE

The repair of a pipe or a fitting in a double bell coupling joints system is similar to that of a closure (i.e. laying the last length of pipe or fitting which closes or completes the line or a section of the line)

To replace a damaged pipe, cut out a ring from its length and pull out the remaining two sections from the couplers that connect it to the adjacent pipes. Pull out these couplers and replace the sealing rings.

Insert the new pipe as indicated below:

- Carefully measure the gap where the replacement piece has to be fitted. The replacement piece must be 32mm shorter than the length of the gap. The pipe must be well centered, and an equal clearance of 16mm must be left between the inserted pipe and the adjacent ones.
- Use a special pipe with double calibrated ends especially ordered from FIBERBOND manufacturer.
- Mount the couplers into the calibrated ends of the new pipe after abundantly lubricating the ends and the sealing ring. It will be necessary to gently help the second sealing ring over the chamfered end of the pipe.
- After cleaning them thoroughly, lubricate the ends of the two adjacent pipes.
- Insert the pipe in its final position and pull each coupler over the adjacent pipe up to the home line.

12. TAPPING FIBERBOND WATER MAINS

FIBERBOND pressure pipes, which require tapping, should have a minimum stiffness of SN 5,000 N/m².

'Live' FIBERBOND water pipe can be tapped while pressurized and in service to obtain service connections to consumers. Typically, ¾" (20mm) service connections are made. Also 2" and 1" service taps are available.

Wide band gunmetal saddles or HDPE saddles may be used to tap FIBERBOND pipes. Saddles are normally provided with a threaded outlet of the required size (e.g. ¾")

The following general procedures should be adhered to:

- The outside surface of the FIBERBOND pipe, where the saddle will be mounted, in particular where the outlet will be located, should be cleaned and all soil, sand, etc. should be removed by a brush, before mounting the saddle.
- Insert the stopcock into the threaded outlet of the saddle before mounting on the pipe, using Teflon tape where necessary. Screw the stopcock in until a tight seal is obtained.
- Attach a rubber or PE hose/pipe to the outlet of the stopcock. The hose should be sufficiently long so that water run-off will be outside the trench area.
- The saddles should be assembled in accordance with the manufacturer's instructions, making sure that the rubber O ring seal is well seated and centered between the threaded outlet and the outside surface of the pipe. Do not over-tighten the saddle to avoid damaging or distorting the pipe.
- Using a commercial tapping machine, attach the correct hole cutting tool into the tapping machine and screw the assembly quickly into the open stopcock.
- Follow the tapping machine operating instruction and after drilling is complete, use the hose and pressurized water to flush out any debris.
- Unscrew the tapping machine and close the stopcock, then connect the permanent house connection pipe (typically PE) to the stopcock using a male adaptor.
- Backfill pipe following the standard instructions making sure that the backfill material is placed and compacted under the pipe haunches.

Appendix I

Approximate Weight of Pipes and Coupling

DN (mm)	SN 2500 (kg/m)	SN 5000 (kg/m)	SN 10000 (kg/m)	Coupling (kg/pc)
80		2	2	1
100		3	3	1
150		4	4	2
200		6	8	3
250	7	9	11	4
300	9	11	13	5
350	11	14	17	12
400	14	19	23	13
450	18	23	26	15
500	22	28	34	18
600	32	38	49	24
700	43	50	65	30
800	55	70	85	36
900	70	85	105	42
1000	88	105	130	49
1100	96	120	150	56
1200	125	155	185	63
1300	135	175	210	70
1400	165	210	250	77
1500	175	230	275	83
1600	220	260	320	90
1700	245	300	360	97
1800	265	330	400	104
2000	325	410	480	118

Note: For diameters above 2000mm and up to 2600mm, pipe and coupler weight is to be advised by the manufacturer as the pipe can be designed either solid wall type or ribbed.

Appendix II

Design considerations for pipelines anchoring

The anchorage of pressure pipelines with rubber gasket joints is an important consideration for the safe and reliable operation of pressure pipelines.

If pressure pipelines are not anchored properly, the thrust loads can lead to displacement of pipes and fitting sections. Thrust loads occur in pipelines wherever there is a change in diameter (e.g. reducers), a change in direction (elbow, tee, and wye, etc.) or at dead ends (e.g. blind flanges, closed valves, bulk heads).

The determination of the thrust occurring in these situations is relatively simple. The figures and formulas in the following sections show the values of thrust occurring in various types of fitting configurations, common to all pressure pipelines. It is not the intention of this section to provide the design methods of thrust blocks. Specialized engineers should do these kinds of studies. The main design considerations of thrust blocks are as follows:

- The pressure is assumed to be acting on the joint area and not on the internal pipe cross sectional area.
- Where concrete thrust blocks are used, they should be poured against undisturbed native soil. This is required to ensure proper load distribution, and that pressures induced by the surrounding soil do not exceed the maximum design bearing capacity. A soil investigation is recommended to establish the proper soil bearing capacities.
- Upward thrust forces can be absorbed by a combination of pipe weight, water in the pipe and the soil on top of the pipe. If these restraining forces are not sufficient, concrete blocks can be used to provide additional weight on top of the pipe.
- In the case of a horizontal thrust (the most common case), concrete blocks, both non-reinforced and reinforced are typically used. Pilings may be used where native soils are unstable. It may also be possible to provide special axially reinforced pipes and to tie several sections of pipe together on both sides of an elbow for example. Tied pipe sections plus the weight of water plus the soil weight provide support which resists by friction the thrust forces in the pipeline. Tying of FIBERBOND pipe and fitting sections is normally done by laminated joints or alternatively by rubber gasket locked joints.
- The ground on which the pipes are laid normally absorbs downward thrust forces. The designer should note that where instable soils are present, a proper foundation and bed constructed with good granular material shall be provided.
- The typical coefficients of friction (f) used for design purposes are the following:

- Concrete on concrete	0.65
- Concrete on dry clay	0.50
- Concrete on wet clay	0.33
- Concrete on gravel	0.65
- Concrete on sand	0.40

- The table below provides typical soil bearing capacities (horizontal) when may be used for the design of thrust blocks. The designer should note that proper evaluation and identification of native soil is essential to determine the proper soil bearing capacity values.

Soil type	Bearing capacity (strength) (kN/m²)
Soft clay	48
Silt	72
Sandy silt	144
Sandy Silt	191
Sandy clay	287
Hard clay	430

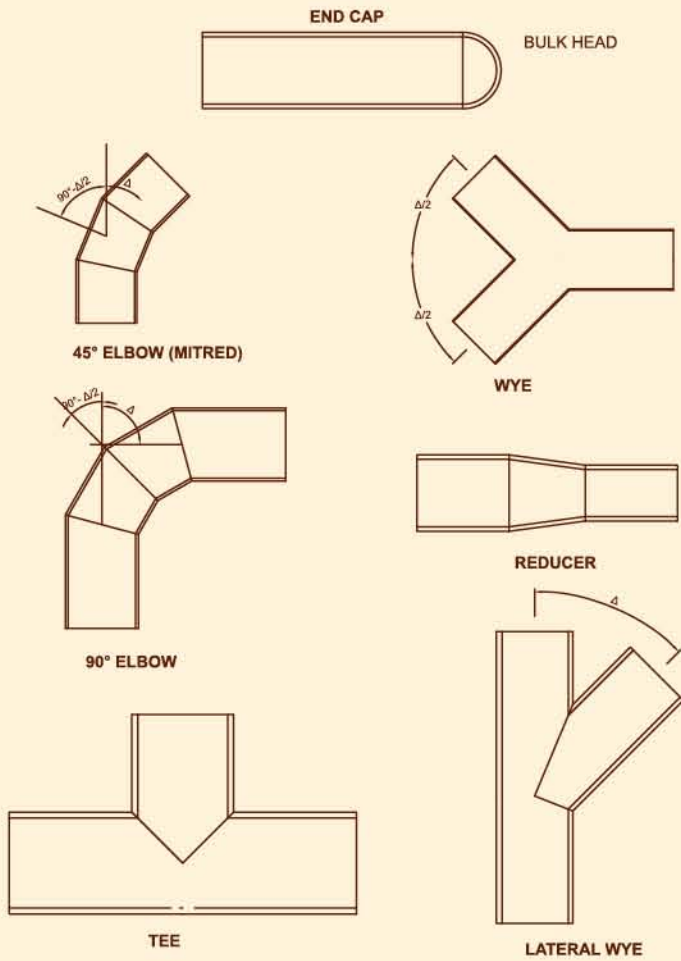


Figure II-1: Thrust in Fittings

Appendix II

Design considerations for pipelines anchoring

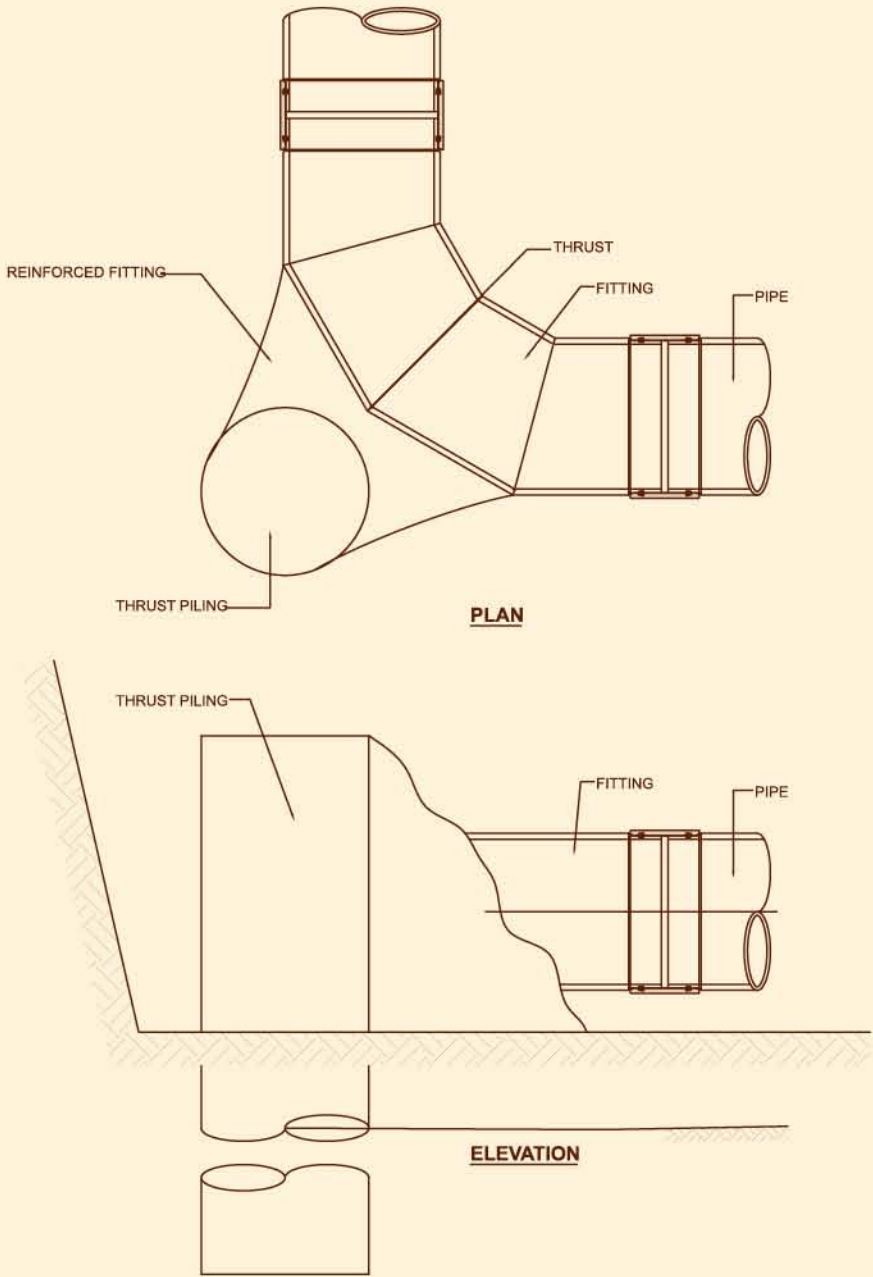


Figure II-2: Thrust Piling

Appendix III

List of references

- Fiberglass Pipe Institute Fiberglass Pipe Handbook.
- ASTM C924 M-89 Standard Practice for Testing Concrete Pipe Sewer lines by Low-pressure Air Test Method [M]
- ASTM C969 M-94 Standard Practice for Infiltration and Exfiltration Acceptance Testing of Installed Precast Concrete Sewer Lines
- ASTM D1586 Standard Method for Penetration Test and Split Barrel Sampling of Soils.
- ASTM D2487 Classification of Soils for Engineering Purposes
- ASTM D3839 Standard Practice for Underground Installation of "Fiberglass" Pipe.
- AWWA C950 Standard Specification for Fiberglass Pipe.
- AWWA Manual M45 Fiberglass Pipe Design.
- BS 8010 Part 1:89 Pipelines on Land - General
- BS 8010 Part 2.5:89 Pipelines on Land – Design, Construction & Installation – GRP Pipelines.
- BS 8010 Part 3:93 Pipelines – Sub-sea: Design, Construction & Installation.



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While the information, opinions, advice and recommendations contained in this publication have been prepared with proper care, they are offered only in pursuance of the objective to provide useful information and assist those interested in technical matters associated with pipeline design, selection and installation.

The information contained herein is not intended to be an exhaustive statement of all relevant data as the successful installation in each case may depend on numerous factors outside the control of Excellent Pipes Company L.L.C e.g. particular design requirements, site preparation, quality of workmanship during installation, etc. EXCELLENT accepts no responsibility for or in connection with the quality or standard of any pipeline or installation nor its suitability for any purpose when installed.

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A large, white, cylindrical GRP pipe is being transported by a yellow scissor lift in a large industrial factory. The pipe is positioned horizontally, and the lift is moving it across the floor. The background shows the complex steel structure of the factory and other industrial equipment. The text "FIBERBOND™ GRP pipes" is overlaid at the bottom of the image.