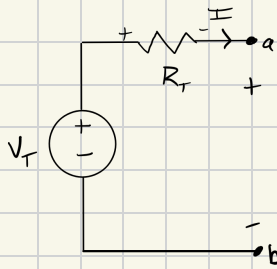


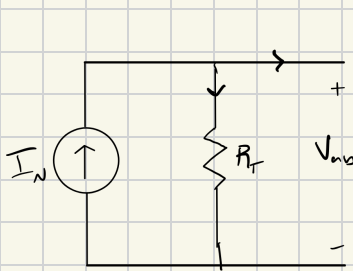


How to make thevenin and Norton circuits



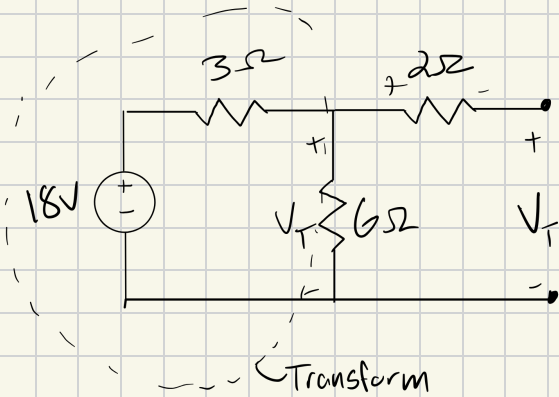
KVL: $-V_T + IR_T + V_{AB} = 0$

$V_{AB} = \underbrace{V_T}_{\text{Open circuit voltage}} - R_T I$



KCL: $I_N = \frac{V_{AB}}{R_T} + I$
 ↳ short-circuit current

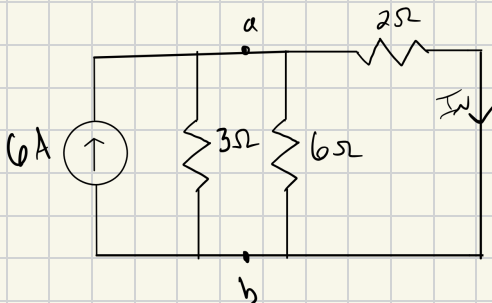
Example:



Voltage Division

$V_T = 18 \left(\frac{6}{6+3} \right) = 12V$

↳ short the circuit for I_N

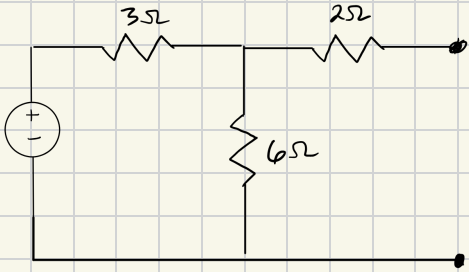


Current Division:

$I_N = 6A \left(\frac{R_p}{2\Omega} \right) = 6 \left(\frac{1}{2} \right) = 3A$

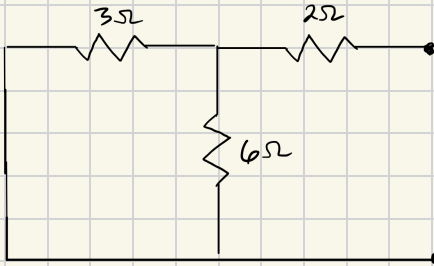
$R_T = \frac{V_T}{I_N} = \frac{12V}{3A} = 4\Omega$

How to get R_T directly:



① Source suppression
- remove independent sources

② Find R_{eq} :



→



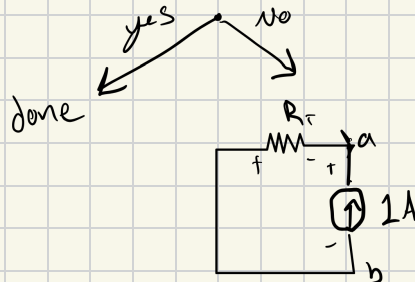
$$R_T = 4\Omega$$

• Test Signal Method

- What if you can't simplify to a single resistor?

① Source suppression

② Check if we can reduce to single resistor



$$KVL: R_T I + V_{ab} = 0$$

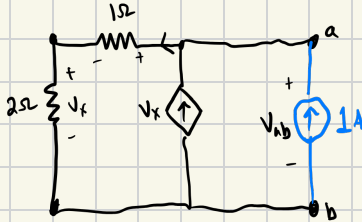
$$R_T = \frac{-V_{ab}}{I} = \frac{-V_{ab}}{-1} = V_{ab}$$

Example: Obtain V_T, I_N, R_T for the following circuit.

V_T : No independent sources: $V_T = 0V$

I_N ' ' $I_N = 0A$

Get R_T :



KCL:

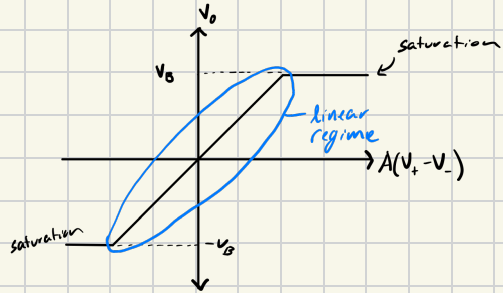
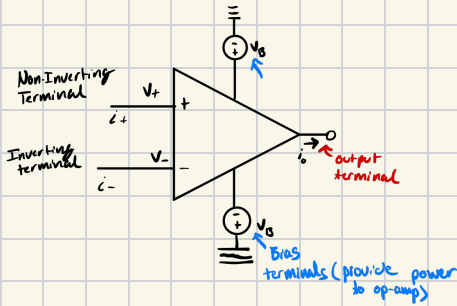
$$1 + V_x = I_{2\Omega} = \frac{V_x}{2} \Rightarrow V_x = -2V$$

KVL:

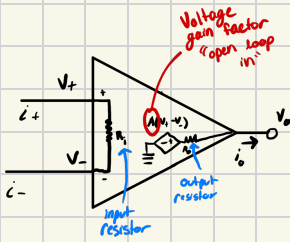
$$-V_x - 1\left(\frac{V_x}{2}\right) + V_{ab} = 0$$

$$V_{ab} = \frac{3}{2}V_x = -3V \Rightarrow R_T = -3\Omega$$

• Operational Amplifier (Op-amp)



OP-Amp in linear regime:



- $|V_+ - V_-| \ll (\ll 10 \mu V)$
- $R_i \gg (\gg 10^6 \Omega)$
- $R_o \ll (\ll 10 \Omega)$
- $A \gg (\gg 10^6)$

Ideal op-amp approximations

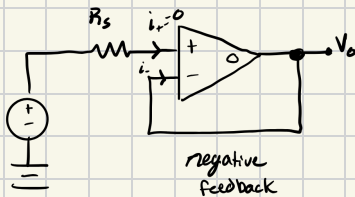
- $i_+ = i_- = 0 \rightarrow$ within pA
- $V_+ = V_- \rightarrow$ within μV

Example 1: Voltage follower

• Obtain V_o in the following circuit assuming the ideal op-amp approx:

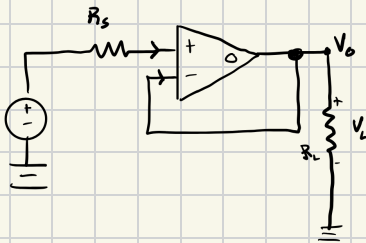
$$\bullet V_+ = V_-$$

$$\bullet i_+ = i_- = 0$$



$$V_o = V_- = V_+ = V_s$$

Consider attaching a load

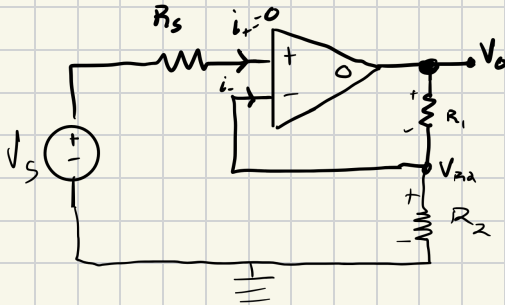


$$\bullet P_L = \frac{V_L^2}{R_L} = \frac{1}{R_L} \left(V_s \frac{R_L}{R_L + R_s} \right)^2 = \frac{V_s^2}{R_L} \left(\frac{R_L^2}{(R_L + R_s)^2} \right)$$

• Op-Amp acts as a buffer between the source and the load

Example 2: non-inverting amplifier

- Obtain V_o in the following circuit assuming the ideal op-amp approx



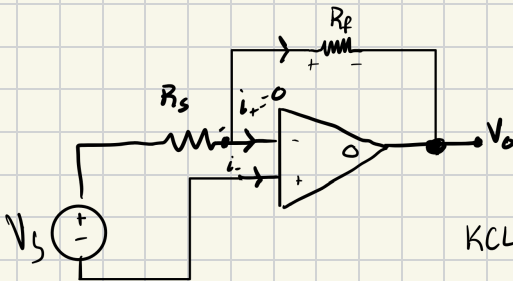
$$V_o = V_{R_1} + V_{R_2} = i_+ R_1 + V_s$$

$$V_{R_2} = V_- = V_+ = V_s$$

- Never do KCL @ ground in op-amps
- $i_o = 0$ (in general)

Example 3: Inverting Amplifier

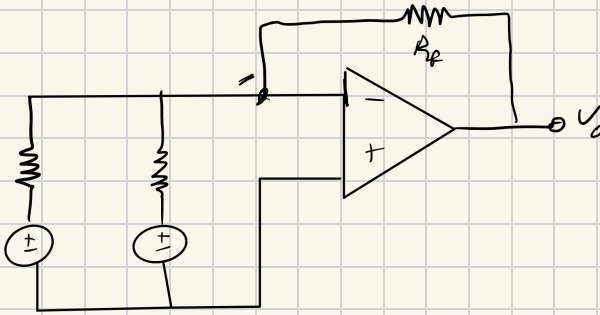
- Obtain V_o in the following circuit



KCL @ (-)

$$\frac{V_s}{R_s} = \frac{-V_o}{R_f} \Rightarrow -V_s \left(\frac{R_f}{R_s} \right) = V_o$$

Example 4: Adder



$$\frac{V_1}{R_1} + \frac{V_2}{R_2} = \frac{-V_o}{R_f}$$

Linearity, time-invariance and LTI systems

$$\begin{aligned}
 V_o(t) &= -\frac{R}{L} \int_{-\infty}^t V_s(x) dx = \xrightarrow{f(t)} \boxed{\text{system}} \xrightarrow{y(t)} \\
 &= \underbrace{-\frac{R}{L} \int_{-\infty}^0 V_s(x) dx}_{V_o} - \frac{R}{L} \int_0^t V_s(x) dx \\
 &= V_o - \frac{R}{L} \int_0^t V_s(x) dx \\
 &\xrightarrow{\text{zero input response (when } V_s(t)=0 \text{ (no input))}} V_{ZI}(t) + V_{ZS}(t) \xleftarrow{\text{zero-state response when } V_o=0 \text{ (no initial state)}}
 \end{aligned}$$

Zero state:

- no initial state
- a weighted sum of inputs produces a similarly weighted sum of corresponding zero-state outputs, consistent with superposition principle

if

$$f_1(t) \rightarrow \boxed{\text{zero state linear}} \rightarrow y_{ZS,1}(t)$$

$$f_2(t) \rightarrow \boxed{\text{zero state linear}} \rightarrow y_{ZS,2}(t)$$

then

$$f_3(t) = K_1 f_1(t) + K_2 f_2(t) \rightarrow \boxed{\text{zero state linear}} \rightarrow y_{ZS,3}$$

Example:

- Consider a system with input $f(t)$, initial state $y(0) = y_0$ and input-output rule given by

$$y(t) = y_0 e^{-t} - \int_0^t f(x) dx$$

- Determine if the system is linear or not

Q: Zero-state linear or not? $\Rightarrow y_0 = 0 \Rightarrow y_{zs}(t) = -\int_0^t f(x) dx$

$$f_1(t) \rightarrow \boxed{} \rightarrow y_1(t) = -\int_0^t f_1(x) dx$$

$$f_2(t) \rightarrow \boxed{} \rightarrow y_2(t) = -\int_0^t f_2(x) dx$$

$$\begin{aligned} K_1 f_1(t) + K_2 f_2(t) &\rightarrow \boxed{} \rightarrow K_1 y_1(t) + K_2 y_2(t) \\ &= -\int_0^t f_3(x) dx = -\int_0^t (K_1 f_1 + K_2 f_2) dx = \\ &\quad K_1 \underbrace{\left(-\int_0^t f_1 dx\right)}_{y_1} + K_2 \underbrace{\left(-\int_0^t f_2 dx\right)}_{y_2} \end{aligned}$$

Is
linear

Q: zero input linear? $\Rightarrow f(t) = 0 \Rightarrow y_{zi}(t) = y_0 e^{-t}$

$$\boxed{y_0} \rightarrow y_{zi,0}(t) = y_0 e^{-t}$$

$$\boxed{y_1} \rightarrow y_{zi,1}(t) = y_1 e^{-t}$$

$$\boxed{y_3 = K_1 y_0 + K_2 y_1} \rightarrow y_{zi,3}(t) = K_1 y_{zi,0}(t) + K_2 y_{zi,1}(t)$$

Example: $y(0) = y_0$

$$y(t) = y_0^2 + f^2(t)$$

① zero-state linear? $\Rightarrow y_0 = 0 \Rightarrow y_{zs}(t) = f^2(t)$

LTI - Linear + Time Invariant

Time Invariance: delayed inputs cause equally delayed outputs for zero initial state and any delay t_0 . So

if

$$f_1(t) \rightarrow \boxed{\text{time-invariant}} \rightarrow y_1(t)$$

$$f_2(t) = f(t - t_0) \rightarrow \boxed{\text{time-invariant}} \rightarrow y_2(t) = y_1(t - t_0)$$

Example:

$$y(0) = y_0 \quad y(t) = y_0^2 + 2f(t)$$

$$\text{zero-state} \Rightarrow y_0 = 0 \Rightarrow y_{zs}(t) = 2f(t)$$

$$f_1(t) \rightarrow \boxed{\phantom{\text{time-invariant}}} \rightarrow y_1(t) = 2f_1(t)$$

$$f_2(t) \rightarrow \boxed{\phantom{\text{time-invariant}}} \rightarrow y_2(t) \stackrel{?}{=} y_1(t - t_0)$$

$$\parallel \\ f(t - t_0)$$

$$= 2f_1(t - t_0)$$

same TI system

$$y_1(t - t_0) = 2f_1(t - t_0)$$

Ex: $y(0) = y_0 \quad y(t) = y_0^2 + f(t^2)$

$$\text{zero state} \Rightarrow y_0 = 0 \Rightarrow y_{zs}(t) = f(t^2)$$

$$f_1(t) \rightarrow \boxed{\phantom{\text{time-invariant}}} \rightarrow y_1(t) = f_1(t^2)$$

$$f_2(t) \rightarrow \boxed{\phantom{\text{time-invariant}}} \rightarrow y_2(t) \stackrel{?}{=} y_1(t - t_0)$$

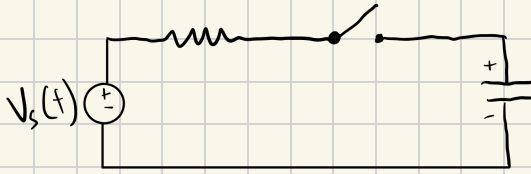
$$\parallel \\ f_2(t - 3)$$

$$f_2(t^2) = f_1(t^2 - 3) \neq$$

$$y_1(t - 3) = f_1((t - 3)^2) \neq \text{TI}$$

$t_0 = 3s$
for simplicity.
Must work for
any t_0

• First Order RC and RL circuits



Initial Conditions:

$$V_c(0^-) = V_c(0) = V_c(0^+) = -I_c$$

$t > 0$

KVL: $-V_s(t) + i(t) \cdot R + V_c(t) = 0$

$i(t) = C \frac{dV_c}{dt}$

$$RC \frac{dV_c}{dt} + V_c(t) = V_s(t)$$

$$\frac{dV_c}{dt} + \frac{1}{RC} V_c(t) = \frac{V_s(t)}{RC}$$

How to solve:

• Start with a simple case:
Constant input

$$f(t) = K \Rightarrow K = \frac{dy}{dt} + ay(t) \Rightarrow K = 0 + aB \Rightarrow B = \frac{K}{a}$$

$$y(t) = B - \text{constant}$$

$$K = \frac{dy}{dt} + ay(t)$$

$$y(t) = \frac{K}{a} + y_h(t)$$

particular solution

homogeneous solution

$$K = \frac{d}{dt} \left(\frac{K}{a} + y_h(t) \right) + a \left(\frac{K}{a} + y_h(t) \right)$$

$$K = \frac{d}{dt} y_h(t) + K + ay_h(t)$$

$$\frac{dy_h(t)}{dt} + ay_h(t) = 0 \rightarrow -aAe^{-at} + aAe^{-at} = 0$$

$$y_h = Ae^{-at}$$

$$y(t) = \frac{K}{a} + \underbrace{Ae^{-at}}_{\substack{\text{when} \\ t=0}}$$

$$y(t) = \underbrace{\frac{K}{a}}_{y_p} + \underbrace{\left(y(0^+) - \frac{K}{a} \right)}_{y_h} e^{-at}$$

$$y_p = \frac{K}{a} = V_s$$

$$y_h = \left(y(0^+) - \frac{K}{a} \right) e^{-at} = (V_c(0^+) - V_s) e^{-\frac{t}{RC}}$$

$$V_c(t) = (V_c(0^+) - V_s) e^{-\frac{t}{RC}} + V_s$$

$t > 0$

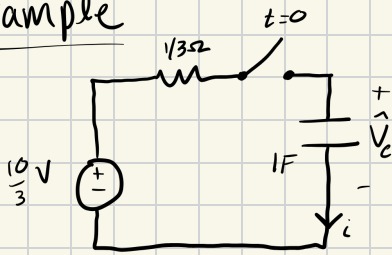
First Order linear ordinary differential equation (ODE) with constant coefficients, which governs RC circuit for $t > 0$

→ can also use $\mu(t) = e^{\frac{t}{RC}}$

$$(e^{\frac{t}{RC}} V_c(t))' = e^{\frac{t}{RC}} \frac{1}{RC} V_s(t)$$

$$\Rightarrow \underbrace{\frac{V_s}{RC}}_K = \frac{dV_c}{dt} + \underbrace{\left(\frac{1}{RC} \right)}_a V_c(t)$$

Example



$$\textcircled{1} \frac{dV_c}{dt} + \underbrace{\left(\frac{1}{RC}\right)}_{a=3} V_c(t) = \underbrace{\left(\frac{V_s}{RC}\right)}_{=10}$$

$$\textcircled{2} \frac{dV_c}{dt} + 3V_c(t) = 10 \Rightarrow 0 + 3B = 10 \quad B = \frac{10}{3}$$

$$\textcircled{3} y(t) = y_p + y_h = B + Ae^{-at}$$

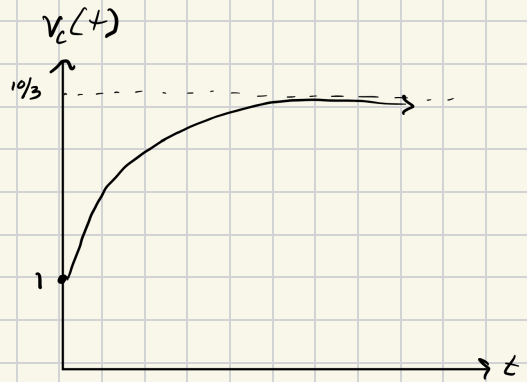
$$\textcircled{4} V_c(t) = \frac{10}{3} + Ae^{-3t}$$

$$\textcircled{5} \text{Find } A$$

$$V_c(0^-) = V_c(0^+) = 1$$

$$1 = \frac{10}{3} + A \Rightarrow A = -\frac{7}{3}$$

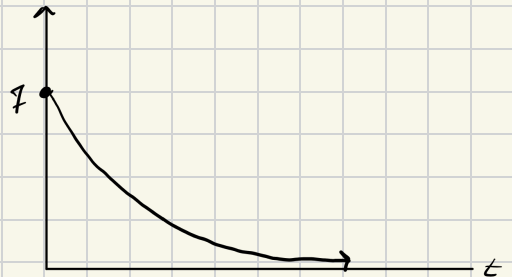
$$\textcircled{6} V_c(t) = \left(\frac{10}{3} - \frac{7}{3}e^{-3t}\right) \text{ Volts}$$



$$\textcircled{7} i_c(t) = C \frac{dV_c}{dt} = 7e^{-3t} \text{ Amps}$$

$$i_c(0^+) = 7A$$

$$i_c(0^-) = 0A$$



Time-Constant

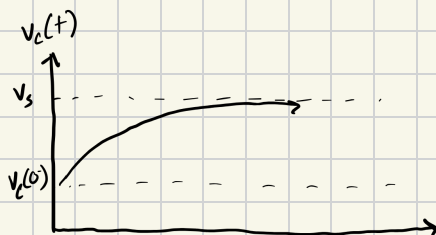
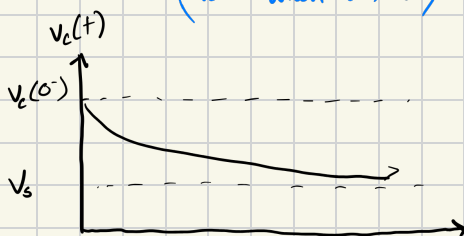
Recall

$$y(t) = \frac{K}{a} + (y(0^+) - \frac{K}{a}) e^{-at}$$

$$V_c(t) = \underbrace{(V_c(0^-) - V_s) e^{-\frac{t}{\tau_c}}}_{\text{transient response}} + \underbrace{V_s}_{\text{steady state response}}$$

transient response
(a part which goes to 0 when $t \rightarrow \infty$)

which is left after transient response has vanished



Rate of decay is controlled by a time const.

$\tau \Rightarrow$ slower decay

$$\tau = RC [s] \quad \leftarrow \text{unit = seconds}$$

Simple Solution Method:

(only works for first order ode with const coefficients and const inputs)

$$y(t) = B + Ae^{-at}$$

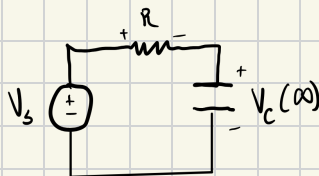
$$a = \frac{1}{\tau_c} = \frac{1}{RC}$$

$$V_c(t) = B + Ae^{-\frac{t}{\tau_c}}$$

Need to evaluate:

$$\bullet V_c(\infty) = B + Ae^{-\frac{\infty}{\tau_c}} = B$$

$$\bullet V_c(0^-) = B + A$$



$$i_c(t) = C \frac{dV_c}{dt}$$

at the DC steady-state ($t \rightarrow \infty$) capacitor acts as an open-circuit ($i_c = 0$)

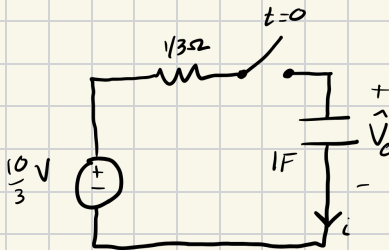
$$\Delta \quad B = V_s$$

$$A = V_c(0^-) - B = V_c(0^-) - V_s$$

$$V_c(t) = V_s + (V_c(0^-) - V_s)e^{-t/\tau}$$

Redo example w/ shortcut:

$V_c(0^-) = 1V$, determine $V_c(t)$ for $t > 0$



$t > 0$

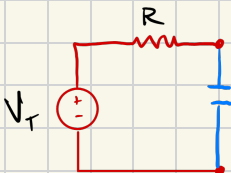
$$V_c(t) = B + Ae^{-t/\tau}$$

$$V_c(\infty) = \frac{10}{3}V = B$$

$$V_c(0^-) = B + A = 1 \Rightarrow A = \left(1 - \frac{10}{3}\right) = -\frac{7}{3}$$

$$V_c(t) = \frac{10}{3} - \frac{7}{3}e^{-3t}$$

If a resistive circuit w/ a single capacitor;



Find Thévenin circuit
as seen by the
Capacitor

• Zero-input (ZI), zero-state (ZS)

$$y(t) = \underbrace{\frac{K}{a}}_{\text{particular}} + \underbrace{(y(0^+) - \frac{K}{a})}_{\text{hom}} e^{-at}$$

$$\frac{K}{a} - \frac{K}{a} e^{-at}$$

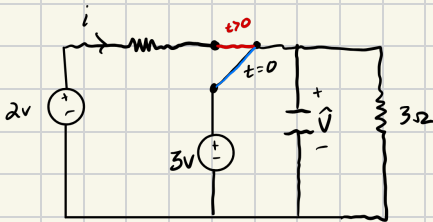
First order circuits are when there are only one power storage device in a circuit.

Zero state is easiest to do.

Recall

$$y(t) = \frac{K}{a} + (y(0^+) - \frac{K}{a})e^{-at}$$

zero state: $\frac{K}{a}$



$t < 0$

capacitor acts as open circuit.

$$V_c(0^-) = 3V$$

$t > 0$

$$V_c(t) = B + Ae^{-t/\tau}$$

Find τ : $\tau = R_T C \rightarrow$ Find R_T from perspective of the cap.

$$R_T = (\frac{2}{3} + \frac{1}{3})^{-1} = \frac{3}{4}\Omega$$

Must find V_c at ∞ and initial conditions

$$V_c(\infty) = B = 2V(\frac{3}{3+1}) = \frac{3}{2}V$$

$$V_c(0^+) = V_c(0^-) = B + A \Rightarrow A = (V_c(0^-) - \frac{3}{2})$$

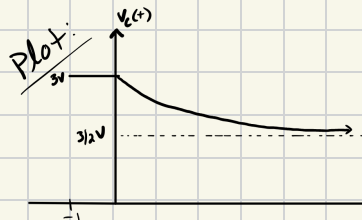
$$V_c(t) = B + Ae^{-t/\tau} =$$

$$\frac{3}{2} + (V_c(0^-) - \frac{3}{2})e^{-t/3} = \frac{3}{2} + V_c(0^-)e^{-t/3} - \frac{3}{2}e^{-t/3}$$

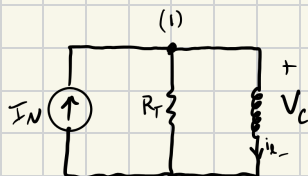
$$= y_{ZS}(t) = \frac{3}{2} - \frac{3}{2}e^{-t/3} V$$

$$+ y_{ZI}(t) = V_c(0^-)e^{-t/3} = 3e^{-t/3} V$$

$$V_c(t) = \frac{3}{2} + \frac{3}{2}e^{-t/3} V$$



Ex with inductor



KCL @ Node 1 : $I_N = \frac{V_L}{R_T} + i_L$
 $= \frac{L}{R_T} \frac{di_L}{dt} + i_L \times \frac{R_T}{L}$

$$V_L = L \frac{di}{dt}$$

↳ In DC-Steady state, inductor acts as a short circuit.

$$\frac{di_L}{dt} + \frac{R_T}{L} i_L = \frac{R_T}{L} I_N$$

$$\tau = \frac{L}{R_T}$$

$$\alpha = \frac{1}{\tau}$$

Solution should be in the form:

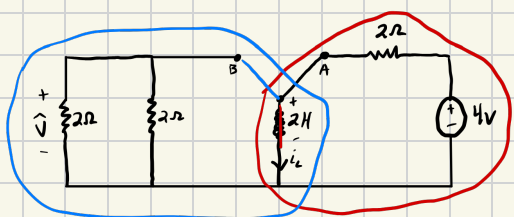
$$i_L(t) = B + A e^{-\alpha t}$$

$$i_L(t) = B + A e^{-t/\tau}$$

$$i_L(\infty) = B$$

$$i_L(0^+) = i_L(0^-) = B + A$$

Example:



$t < 0$

$$i_L(0^-) = \frac{4V}{2\Omega} = 2A$$

$t > 0$

$$i_L(t) = B + A e^{-t/\tau}$$

$$\tau = \frac{L}{R_T}$$

First Find τ : $\tau = \frac{L}{R_T}$

$R_T = 1\Omega$ (From perspective of the inductor)

$$\tau = \frac{2H}{1\Omega} = 2s$$

$$i_L(\infty) = B = 0A \text{ (no source)}$$

$$i_L(0^+) = i_L(0^-) = 2A$$

$$i_L(t) = i_L(0^-) e^{-t/\tau} \text{ Amps}$$

$$\{ i_{2s}(t) = i_L(0^-) e^{-t/\tau} \text{ Amps}$$

$$\{ i_{2s}(t) = 0 \text{ (force } i_L(0^-) \text{ to be 0)}$$

$$i_{2s}(t) = i_L(0^-) e^{-t/\tau} = 2e^{-t/2} \text{ Amps}$$

What if the circuit goes from $A \rightarrow B \rightarrow A$

$t < 0$

$$i_L(0^-) = \frac{4}{2} = 2A$$

$0 < t < 2$

$$i_L(t) = B + Ae^{-t/\tau} ; \tau = 2s$$

$$i_L(\infty) = B = 0$$

$$i_L(0^+) = i_L(0^-) = A = 2$$

$$i_L(t) = 2e^{-t/2} \text{ amps}$$

Now going
back to pos A
→

$t > 2$

$$i_L(t) = \hat{B} + \hat{A}e^{-t/\tau}$$

Consider the particular solution:

$$y_p(t) = \frac{1}{2} \cos(t) + \frac{1}{2} \sin(t) = H \cos(t + \varphi)$$
$$= H \cos(\varphi) \cos(t) - H \sin(\varphi) \sin(t) \Rightarrow H \cos(\varphi) = \frac{1}{2}$$
$$-H \sin(\varphi) = \frac{1}{2}$$

Determine H and φ

Get φ :

$$\frac{H \sin(\varphi)}{H \cos(\varphi)} = \frac{-1/2}{1/2} = -\tan(\varphi) = -1 \Rightarrow$$
$$\varphi = -\frac{\pi}{4} \text{ or } \frac{3\pi}{4}$$

Get H

$$H \cos(\varphi) = 1/2$$

$$H \cos(\frac{3\pi}{4}) = \frac{1}{2}$$

$$H = \frac{\sqrt{2}}{2} \text{ or } -\frac{\sqrt{2}}{2}$$

$$y_p(t) = \frac{\sqrt{2}}{2} \cos(t - \frac{\pi}{4})$$

Transient Response v.s. Steady-State Response

Transient: $y_{tr}(t) \forall$
 $t \rightarrow \infty$

$$y_{tr}(t) \rightarrow 0$$

Steady state: $y_{ss}(t)$ is what's left after $y_{tr} \rightarrow 0$

$$y(t) = y_{tr}(t) + y_{ss}(t)$$

Recall

$$y(t) = \overbrace{Ae^{-at}}^{\text{transient}} + \underbrace{B}_{ss}$$

$$y(t) = \underbrace{Ae^{-at}}_{\text{transient}} + Be^{-pt}$$

$$y(t) = \underbrace{Ae^{-at}}_{\text{transient}} + \underbrace{H \cos(\omega t + \varphi)}_{\text{steady state}}$$

Last Week:

$$\frac{dy}{dt} + \frac{y}{t} = C_1 \Rightarrow y(t) = K_1 e^{-1/t} + K_2$$

Lets make a particular solution table

What if:

$$\frac{dy}{dt} + \frac{y}{t} = f(t)$$

$$y = y_h(t) + y_p(t)$$

s.t. $\frac{dy_h}{dt} + \frac{y_h}{t} = 0$

$f(t)$	$y_p(t)$
C_1	C_2 * constants
$Kt + b$	$\alpha t + \beta$
polynomial of degree "n"	polynomial of same degree "n" with all other lower terms.
$\cos(\omega t)$ or $\sin(\omega t)$	$A \cos(\omega t) + B \sin(\omega t)$
Ae^{ct}	if $\begin{cases} c \neq -\frac{1}{t}; Be^{ct} \\ c = -\frac{1}{t}; Bte^{ct} \end{cases}$

Example:

$$\frac{dy}{dt} + y = e^{-2t}$$

$$y_h = Ae^{-t/\tau}, \tau = 1$$

$$= Ae^{-t}$$

$$y = Ae^{-t} - e^{-2t}$$

use I.C. (initial conditions)
to find A.

plug into original eq where $y = y_p$

$$\begin{cases} y_p: c \neq -\frac{1}{t} \\ y_p = Be^{-2t} \\ \frac{dy_p}{dt} = -2Be^{-2t} \end{cases}$$

$$-2Be^{-2t} + Be^{-2t} = e^{-2t} \rightarrow B = -1$$

$$-Be^{-2t} = e^{-2t}$$

$$\Delta y_p = -e^{-2t}$$

Example:

$$\frac{dy}{dt} + y = e^{-t}$$

$$y_p = Bte^{-t}$$

$$-Bte^{-t} + Bte^{-t} + Bte^{-t} = e^{-t}$$

$$\frac{dy_h}{dt} + y_h = 0$$

$$\Rightarrow \frac{dy_h}{dt} = B(-te^{-t} + e^{-t})$$

$$Be^{-t} = e^{-t}$$

$$B = 1$$

$$y_p = te^{-t}$$

$$r = 1$$

$$y_h = Ae^{-t}$$

Δy :

$$y = y_h + y_p \Rightarrow y = Ae^{-t} + te^{-t}$$

Particular is at the same order as homogeneous we must multiply by t .

Example:

$$\frac{dy}{dt} + y = t^2$$

$$y_p = Bt^2 + Ct + D$$

ply in

$$2Bt + C + Bt^2 + Ct + D = t^2$$

$$y_h = Ae^{-t}$$

$$\frac{dy_p}{dt} = 2Bt + C$$

$$Bt^2 + 2Bt + Ct + C + D = t^2$$

$$r = 1$$

$$y_p = t^2 - 2t + 2$$



$$B = 1$$

$$2B + C = 0$$

$$C + D = 0$$

$$2 + C = 0 \Rightarrow C = -2$$

$$D = -C \Rightarrow D = 2$$

$$y = Ae^{-t} + t^2 - 2t + 2$$

Ex w/ Sinusoidal input

$$\frac{dy}{dt} + y = \cos(t)$$

$$y_h = Ae^{-t}; r = 1$$

$$y_p = B\cos(t) + C\sin(t)$$

$$-B\sin(t) + C\cos(t) + B\cos(t) + C\sin(t) = \cos(t)$$

$$\frac{dy_p}{dt} = -B\sin(t) + C\cos(t)$$

$$C + B = 1$$

$$C = \frac{1}{2} \quad B = \frac{1}{2}$$

$$C - B = 0$$

$$C = B$$

$$y_p = \frac{1}{2}\cos(t) + \frac{1}{2}\sin(t)$$

$$C\cos(t) + D\sin(t) = K\cos(t + \theta)$$

$$K = \sqrt{C^2 + D^2}$$

$$\theta = \tan^{-1}\left(\frac{-D}{C}\right)$$

$$K = \sqrt{\frac{1}{4} + \frac{1}{4}} = \sqrt{\frac{2}{4}} = \frac{\sqrt{2}}{2}$$

$$\theta = \tan^{-1}\left(\frac{-1}{1}\right) = \tan^{-1}(-1) = -\frac{\pi}{4}$$

$$y_p = \frac{\sqrt{2}}{2}\cos\left(t - \frac{\pi}{4}\right)$$

$$y = Ae^{-t} + \frac{\sqrt{2}}{2}\cos\left(t - \frac{\pi}{4}\right)$$

• Dissipative Systems

- has a transient zero-state response

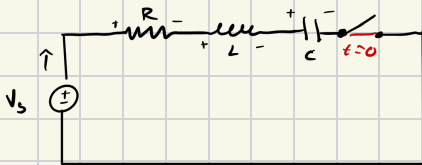
$$y_{zi}(t) \rightarrow 0 \\ t \rightarrow \infty$$

- the ss response to a cosinusoidal input applied at $t = -\infty$ will be cosinusoidal independent of the initial state

$$y(t) = Ae^{-at} + \underbrace{H \cos(\omega t + \gamma)}_{y_{ss}(t)}$$

• n^{th} order LTI systems

- Determine the ODE governing the capacitor voltage in the following circuit:



$$-V_s + V_R + V_L + V_C = 0$$

$$-V_s + iR + L \frac{di}{dt} + V_C = 0$$

$$-V_s + R\left(C \frac{dv_c}{dt}\right) + L \frac{d}{dt}\left(C \frac{dv_c}{dt}\right) + V_C = 0$$

• In general: $\frac{\partial^n y}{\partial t^n} + a_1 \frac{\partial^{n-1} y}{\partial t^{n-1}} + \dots + a_n y = f(t)$

Where n - number of energy storage elements (L, C)

• Solution is

$$y(t) = y_p(t) + y_h(t)$$

└ same as in 1st order ODE

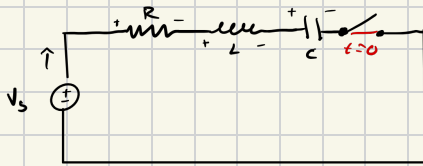
if $P_1 = P_2$

$$A_1 e^{-P_1 t} + t A_2 e^{-P_2 t} + \dots$$

Example:

For $t > 0$, obtain $v_c(t)$

$V_s = 0V$, $R = 0\Omega$, $i_c(0^-) = 0A$, $v_c(0^-) = 1V$, $L = 1H$, $C = 1F$



$$\frac{V_s}{LC} = \frac{d^2 v_c}{dt^2} + \frac{R}{L} \frac{dv_c}{dt} + \frac{v_c}{LC} - 1$$

$$0 = \frac{d^2 v_c}{dt^2} + v_c$$

now we find A_1 and A_2 :

$$v_c(0^-) = v_c(0^+) = 1V$$

$$1 = A_1 + A_2 \quad (1)$$

$$i_c(0^+) = 0A$$

$$i_c(t) = C \frac{dv_c}{dt} = -jA_1 e^{-jt} + jA_2 e^{jt}$$

$$i_c(0^+) = -jA_1 + jA_2 = 0 \quad (2)$$

$$\text{Solving (1) and (2)} \Rightarrow A_1 = A_2 = \frac{1}{2}$$

Solution:

$$\frac{d^2 v_c}{dt^2} + v_c = 0$$

$$y_h(t) = e^{st}$$

$$s^2 e^{st} + e^{st} = 0$$

$$s^2 + 1 = 0$$

$$s = \pm \sqrt{-1} = \pm j$$

$$y_h = A_1 e^{-jt} + A_2 e^{jt}$$

$$y_h = \frac{1}{2} e^{-jt} + \frac{1}{2} e^{jt}$$

$= \cos(t) \rightarrow$ zero-input response

is not transient

$$i_c(t) = -\sin(t) \text{ Amps}$$

system
is non-dissipative

Friday Lecture: to watch

Last time:

must convert sin into cos

-phasors are cos-based objects

Phasor Superposition

- The weighted superposition
- Don't have to have same magnitude, must have same frequency

Derivative Principle

The derivative

$$g(t) = \frac{d}{dt} f(t)$$

of cosinusoid $f(t) = \text{Re}[F e^{j\omega t}]$ is also a co-sinusoid with phasor

$$G = j\omega F$$

Note: N^{th} derivative

$$\frac{d^n f}{dt^n} = (j\omega)^n F$$

Consider

$$f(t) = 3\cos(2t + \frac{\pi}{4}) \rightarrow F = 3e^{j\frac{\pi}{4}} = 3(\frac{1}{\sqrt{2}} + j\frac{1}{\sqrt{2}})$$

Determine $f'(t)$

$$= \frac{3}{\sqrt{2}} + j\frac{3}{\sqrt{2}}$$

$$g(t) = \text{Re}[G e^{j\omega t}]$$

$$\begin{aligned} \uparrow \\ G = j\omega F &= j 2 (\frac{3}{\sqrt{2}} + j\frac{3}{\sqrt{2}}) \\ &= j\frac{6}{\sqrt{2}} - \frac{6}{\sqrt{2}} = \end{aligned}$$

$$A = \sqrt{(\frac{6}{\sqrt{2}})^2 + (\frac{6}{\sqrt{2}})^2} = 6$$

$$\theta = \pi + \tan^{-1}(-1) = \pi - \frac{\pi}{4} = \frac{3\pi}{4}$$

Determine the steady state solution to the following diff eq.

$$\frac{d^2 y}{dt^2} + 2 \frac{dy}{dt} + y = -5 \sin(2t)$$

↓ phasors

*turn this to pos by shifting π
 - then convert to cos by subtracting $\frac{\pi}{2}$*
turn into phasor
 $= 5 \cos(2t + \frac{\pi}{2})$
 $= 5e^{j\frac{\pi}{2}} = 5j$

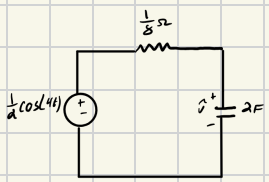
$$(j\omega)^2 + 2j\omega y + y = 5j$$

$$-4y + j4y + y = j5$$

$$y = \frac{j5}{-3+j4} = \frac{5e^{j\frac{\pi}{2}}}{5e^{j\frac{3\pi}{4}}} = 5e^{j(\frac{\pi}{2} - \frac{3\pi}{4})}$$

$$y_{ss} = 1 \cos(2t + \frac{\pi}{2} - \frac{3\pi}{4}) = \cos(2t - \frac{\pi}{4})$$

Determine $\hat{v}_{ss}(t)$ using phasors



KVL: $\frac{-1}{2} \cos(4t) + \frac{1}{4} \frac{d\hat{v}}{dt} + \hat{v} = 0$

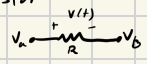
$$\frac{1}{4} \frac{d\hat{v}}{dt} + \hat{v} = \frac{1}{2} \cos(4t)$$

$$\frac{1}{4}(j\omega)\hat{v} + \hat{v} = \frac{1}{2} \Rightarrow \frac{1}{2}e^{j\pi} = -\frac{1}{2}$$

$$j\hat{v} + \hat{v} = -\frac{1}{2}$$

V-I relationships in phasors

• Resistor

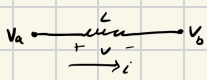


$$V(t) = R \cdot i(t)$$

$$V = IR$$

$$|V|e^{j\theta_V} = R \cdot |I|e^{j\theta_I} \Rightarrow \theta_V = \theta_I \text{ (voltage and current are in-phase)}$$

• Inductor



$$V(t) = L \frac{di}{dt}$$

↓ phasors

$$V = (Lj\omega)I = ZI = V$$

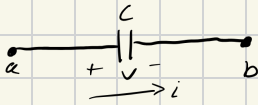
Z-impedance [ohms]

$$|V|e^{j\theta_V} = L\omega e^{j\frac{\pi}{2}} |I|e^{j\theta_I} = \theta_V = \theta_I + \frac{\pi}{2}$$

$$\theta_V = \theta_I + \frac{\pi}{2}$$

Voltage leads current by $\frac{\pi}{2}$, or current lags voltage by $\frac{\pi}{2}$

• Capacitor



$$i = C \frac{dV}{dt}$$

↓ phasors

$$I = C j\omega V \rightarrow \frac{1}{j\omega C} I = V$$

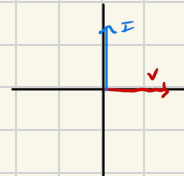
$$Z = \frac{1}{j\omega C} = \frac{-j}{\omega C}$$

$$V = Z \cdot I$$

$$|V|e^{j\theta_v} = \frac{1}{\omega C} e^{-j\frac{\pi}{2}} |I|e^{j\theta_i}$$

$$\theta_v = \theta_i - \frac{\pi}{2}$$

$$\theta_i = \theta_v + \frac{\pi}{2}$$

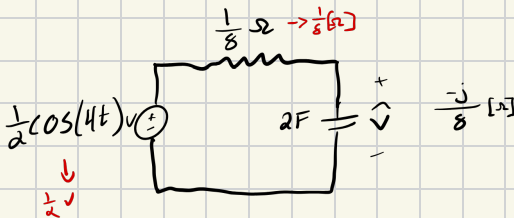


Current leads
Voltage by
 $\frac{\pi}{2}$

• V-I relationships in phasors

$$\text{Impedance, } Z = \begin{cases} R & \text{resistor} \leftarrow \text{purely resistive} \\ j\omega L & \text{inductor} \\ \frac{1}{j\omega C} = \frac{-j}{\omega C} & \text{capacitor} \leftarrow \text{purely reactive} \end{cases}$$

• Determine $\hat{V}_{ss}(t)$ using phasors

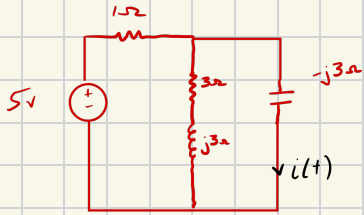
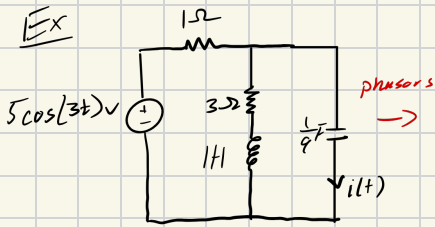


Voltage
Division

$$\hat{V} = \frac{1}{2} \left(\frac{-j/8}{-j/8 + \frac{1}{2}} \right) = \frac{1}{2} \left(\frac{-j}{-j+1} \right) = \frac{1}{2} \left(\frac{e^{-j\frac{\pi}{2}}}{\sqrt{1+0}e^{j\frac{\pi}{4}}} \right) = \frac{1}{2\sqrt{2}} e^{-j\frac{3\pi}{4}}$$

$$\hat{V}_{ss}(t) = \frac{1}{2\sqrt{2}} \cos(4t - \frac{3\pi}{4}) [V]$$

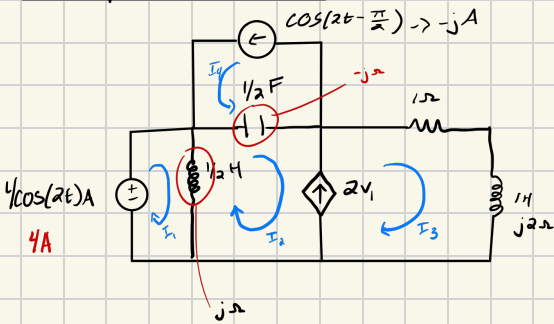
Ex



current division

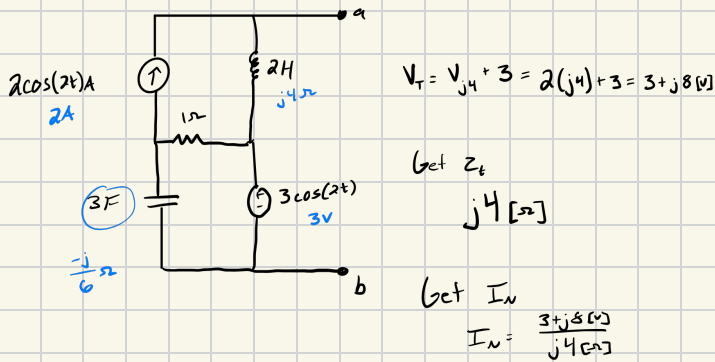
current division $5A \left(\frac{Z_P}{-j3} \right) =$

Multiple Sources



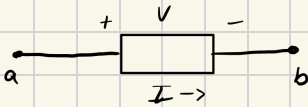
Can use node-voltage method or loop current

- We can still find Thevenin equivalents



• Average power

- Recall $P = IV$



- If v and i are time varying, then the instantaneous power is
 $p(t) = v(t)i(t)$

- For periodic signals with period T , the average power is:

$$P = \frac{1}{T} \int_T p(t) dt = \frac{1}{T} \int_T \underbrace{v(t)i(t)}_{\frac{1}{2} (\text{Re}\{V e^{j\omega t}\} + \text{Re}\{V^* e^{-j\omega t}\})} dt$$

Average Power for Phasor

$$P = \frac{1}{T} \int_T P(t) dt = \frac{1}{T} \int_T v(t) i(t) dt$$

$$P = \frac{1}{T} \int_T \frac{1}{2} (\operatorname{Re}\{V I e^{j\omega t}\} + \operatorname{Re}\{V I^*\}) dt =$$

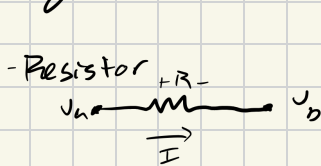
$$= \frac{1}{2T} \int_T \operatorname{Re}\{V I e^{j\omega t}\} dt + \frac{1}{2T} \int_T \operatorname{Re}\{V I^*\} dt$$

$$= \frac{1}{2T} \int_T |V I| \cos(\omega t + \angle V I) dt + \frac{1}{2} \operatorname{Re}\{V I^*\}$$

$$P = \frac{1}{2} \operatorname{Re}\{V I^*\}$$

angle of $V I$
Average of a cos over 2 cycles is zero

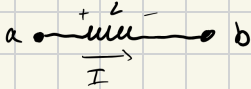
• Average Absorbed Power



$$P = \frac{1}{2} \operatorname{Re}\{V I^*\} = \frac{1}{2} (\operatorname{Re}\{R \cdot I \cdot I^*\})$$

$$= \frac{1}{2} R(I^2) = \frac{1}{2} \frac{|V|^2}{R}$$

Inductor

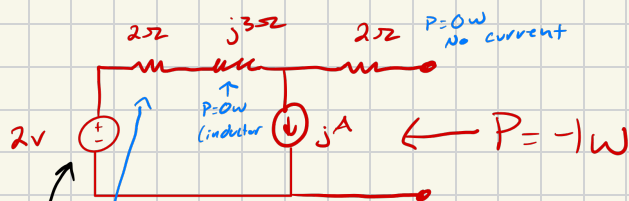
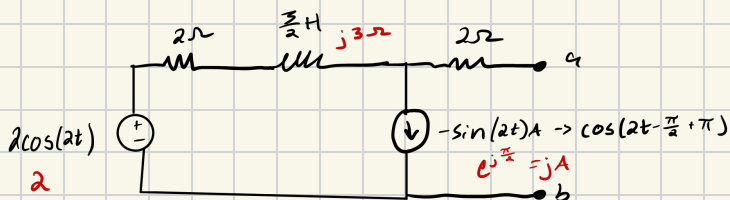


$$P = \frac{1}{2} \operatorname{Re}\{V I^*\} = \frac{1}{2} \operatorname{Re}\{j\omega L |I|^2\} = 0$$

Capacitor $\rightarrow P = 0W!$

OW since they store energy then end up discharging it (1 cycle charge, 1 cycle discharge)

• Determine Avg Power for each element



$$P = \frac{1}{2} |I|^2 \cdot R$$

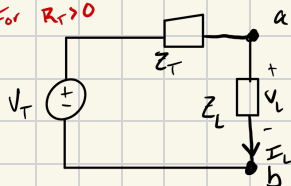
$$= \frac{1}{2} |j|^2 \cdot 2$$

$$= \frac{1}{2} \cdot 1^2 \cdot 2 = 1W$$

$$P = \frac{1}{2} \text{Re}\{VI^*\} = \frac{1}{2} \text{Re}\{2 \cdot (-j)^*\} = 0W$$

• Available Power

For $R_T > 0$



$$Z_T = R_T + jX_T$$

$$Z_L = R_L + jX_L$$

$$P_L = \frac{1}{2} \text{Re}\{V_L \cdot I_L^*\} = \frac{1}{2} \text{Re}\left\{\frac{V_T \cdot Z_L}{Z_T + Z_L} \cdot \frac{V_T^*}{(Z_T + Z_L)^*}\right\} =$$

$$I_L = \frac{V_T}{Z_T + Z_L}$$

$$V_L = V_T \left(\frac{Z_L}{Z_T + Z_L}\right)$$

$$= \frac{1}{2} \text{Re}\left\{\frac{|V_T|^2 Z_L}{|Z_T + Z_L|^2}\right\}$$

$$= \frac{1}{2} \frac{|V_T|^2 \cdot R_L}{|Z_T + Z_L|^2} =$$

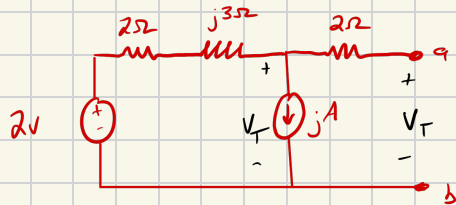
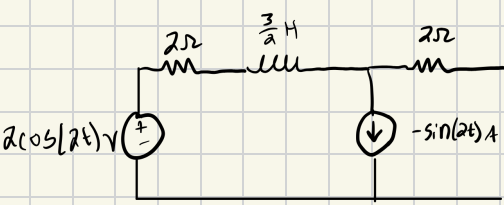
$$= \frac{1}{2} \frac{|V_T|^2 \cdot R_L}{(R_T + R_L)^2 + (X_T + X_L)^2}$$

$$Z_L = R_T - jX_T = Z_T^* \quad \begin{cases} X_L = -X_T \\ R_L = R_T \end{cases}$$

$$P_a = \frac{|V_T|^2}{8R_T} = \left(\frac{1}{2}\right) \frac{|V_T|^2}{4R_T}$$

only real part of Z_T
From phasors

Example:



Get V_T :

$$\text{KVL: } -2 + 2j + j(j3) + V_T = 0$$

$$V_T = 5 - j2V$$

Get Z_T

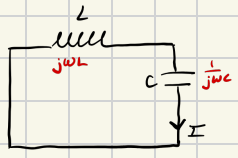
$$Z_T = 2 + j3 + 2 = 4 + j3\Omega$$

$$P_a = \frac{1}{2} \frac{|V_T|^2}{4R_T} = \frac{1}{2} \frac{\sqrt{5^2 + (-2)^2}^2}{4 \cdot 4} = \frac{29}{32} W \quad \text{only if}$$

$$Z_L = Z_T^* = 4 - j3\Omega$$

• Resonance

- Circuit below with $v_c(0^-) = 1V$, $i_L(0^-) = 0A$, $v_c(t) = 4\cos(t + \theta)$



$$\text{KVL: } v_L + v_C = 0$$

$$j\omega L \cdot I + \frac{1}{j\omega C} I = 0$$

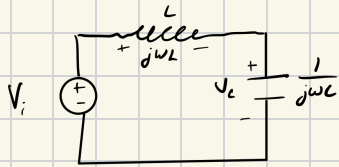
$$I(j\omega L - \frac{1}{j\omega C}) = 0$$

Can be satisfied by any I as long as $j\omega L - \frac{1}{j\omega C} = 0$

$$\omega L = \frac{1}{\omega C}$$

$$\omega_0 = \frac{1}{\sqrt{LC}} \quad \text{resonant frequency}$$

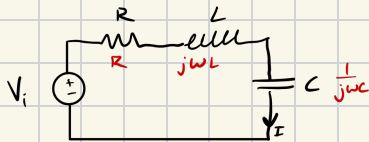
What if we add a source



$$V_c = V_i \left(\frac{\frac{1}{j\omega C}}{\frac{1}{j\omega C} + j\omega L} \right) = \frac{V_i}{- \omega^2 LC + 1}$$

if $\omega = \frac{1}{\sqrt{LC}}$

What if we also add a resistor?



$$V_c = V_i \left(\frac{\frac{1}{j\omega C}}{\frac{1}{j\omega C} + j\omega L + R} \right) = \frac{V_i}{1 - \omega^2 LC + j\omega RC}$$

$$V_c = \frac{V_i}{j\omega RC} = -j \sqrt{\frac{L}{C}} \cdot \frac{1}{R} \cdot V_i$$

$$V_L = V_i \left(\frac{j\omega L}{j\omega L + \frac{1}{j\omega C} + R} \right) = j \sqrt{\frac{L}{C}} \cdot \frac{1}{R} V_i = -V_c$$

complex conjugate of one another

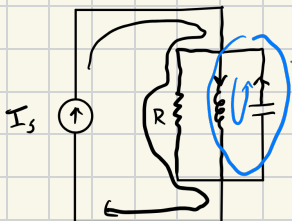
$$V_c + V_L = 0$$

(net zero voltage)

$$Z_s = R + j\omega L - \frac{j}{\omega C}$$

$= 0$ if $\omega = \frac{1}{\sqrt{LC}}$

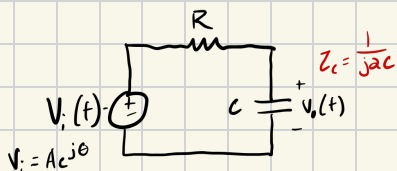
• What if the elements are in parallel: **Parallel Resonance**



they act as open circuit,
but they still have current.
It goes around just between L and C

Chapter 5 Frequency Response $H(\omega)$ of LTI Systems

Example:



$$V_o = V_i \left(\frac{\frac{1}{j\omega C}}{R + \frac{1}{j\omega C}} \right) = V_i \left(\frac{1}{j\omega RC + 1} \right)$$

$$= \frac{|V_i| e^{j\angle V_i}}{\sqrt{1 + (\omega RC)^2} e^{j \tan^{-1}(\omega RC)}}$$

$$V_o = \frac{|V_i|}{\sqrt{1 + (\omega RC)^2}} e^{j(\angle V_i - \tan^{-1}(\omega RC))}$$

Let $V_i(t) = A \cos(\omega t + \theta)$

Determine $V_{o,ss}(t)$

$$H(\omega) = |H(\omega)| e^{j\angle H(\omega)}$$

Amplitude response: $\frac{1}{\sqrt{1 + \omega^2 R^2 C^2}} = |H(\omega)|$

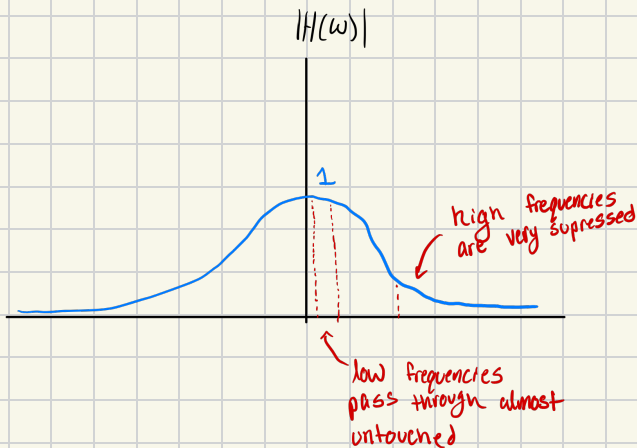
Phase response: $-\tan^{-1}(\omega RC) = \angle H(\omega)$

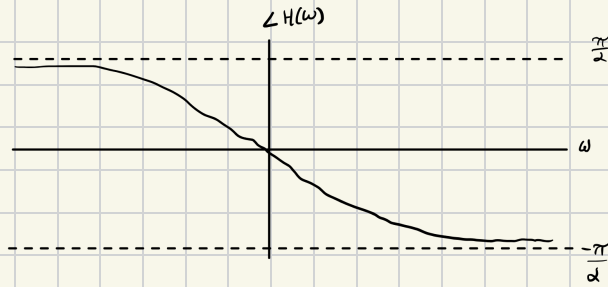
$$V_o = V_i H(\omega)$$

$\uparrow$ $\uparrow$
 output phasor input phasor

$$V_i = |V_i| e^{j\angle V_i}$$

$$V_o = |V_i| |H(\omega)| e^{j(\angle V_i + \angle H(\omega))}$$





• Recall from example above:

$$|H(\omega)| = \frac{1}{\sqrt{1 + (\omega RC)^2}}$$

$$\angle H(\omega) = -\tan^{-1}(\omega RC)$$

Find $V_o(t)$ if $V_i(t) = 2 \cos(3t + \frac{\pi}{3})$

$$V_o = |V_i| |H(3)| \cos(3t + \frac{\pi}{3} - \tan^{-1}(3RC))$$

Find $V_o(t)$ if $V_i(t) = 3 \sin(6t + \frac{\pi}{6})$
 $= 3 \cos(6t - \frac{\pi}{3})$

$$V_o(t) = 3 |H(6)| \cos(6t - \frac{\pi}{3} - \angle H(6))$$

• For LTI systems with

input $f(t) = \text{Re}\{F e^{j\omega t}\}$

output $y(t) = \text{Re}\{Y e^{j\omega t}\}$

$$f(t) \rightarrow \boxed{\text{LTI}} \rightarrow y(t)$$

$$F \rightarrow \boxed{H(\omega)} \rightarrow Y = F \cdot H(\omega)$$

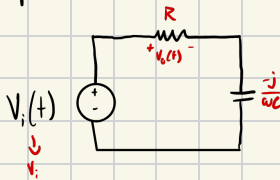
We have:

$$Y = F H(\omega)$$

$$F = |F| e^{j\angle F}$$

$$Y = |F| |H(\omega)| e^{j(\angle F - \angle H(\omega))}$$

Example

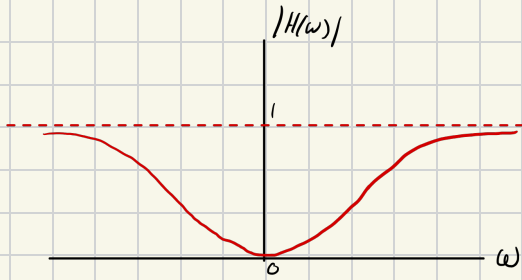


Let $V_i(t) = A \cos(\omega t + \theta)$

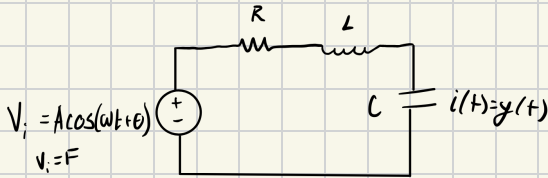
$$V_o = V_i \left(\frac{R}{R + \frac{1}{j\omega C}} \right) = V_i \frac{j\omega RC}{j\omega RC + 1} \quad \text{where } H(\omega) = \frac{j\omega RC}{j\omega RC + 1}$$

$$|H(\omega)| = \frac{|\omega| RC}{\sqrt{1 + \omega^2 R^2 C^2}}$$

$$\angle H(\omega) = \begin{cases} \frac{\pi}{2} - \tan^{-1}(\omega RC) & \text{if } \omega > 0 \\ -\frac{\pi}{2} - \tan^{-1}(\omega RC) & \text{if } \omega < 0 \\ 0 & \text{if } \omega = 0 \end{cases}$$



Example:



$$H(w) = \frac{Y}{F} = \frac{I}{V_i}$$

$$I = \frac{V_i}{R + j\omega L + \frac{1}{j\omega C}}$$

Consider the ODE

$$\frac{dy}{dt} + y = 3f(t) \quad ; \quad \text{let } f(t) = A \cos(\omega t + \theta)$$

$$j\omega Y + Y = 3F \quad \rightarrow \quad Y = \frac{3F}{j\omega + 1}$$

Find $H(w)$, $|H(w)|$, and $\angle H(w)$

$$H(w) = \frac{Y}{F} \quad ; \quad Y = FH(w)$$

$$|H(w)| = \frac{3}{\sqrt{1 + \omega^2}}$$

$$\angle H(w) = 0 - \tan^{-1}(\omega) = -\tan^{-1}(\omega)$$

comes from $\frac{Y}{F} \leftarrow \text{angle of } Y \text{ minus angle of } F$

• General First Order filters and second order filters

• Low pass

$$|H(0)| = C$$

$$|H(\infty)| = 0$$

$$|H(\omega)| \approx \frac{1}{\sqrt{1+\omega^2}}$$

• High Pass

$$|H(0)| = 0$$

$$|H(\infty)| = C$$

$$|H(\omega)| \approx \frac{|\omega|}{\sqrt{1+\omega^2}}$$

• Band Pass (only for dissipative systems)

$$|H(0)| = 0$$

$$|H(\infty)| = 0$$

in between
 $H(t) \neq 0$

$$|H(\omega)| \approx \frac{|\omega|}{\sqrt{\omega^2 + (1-\omega^2)^2}}$$

Note: $H(0)$ is a real number

• Properties of $H(\omega)$ for real valued LTI systems

- Conjugate Symmetry $H(\omega) = H^*(\omega)$

- Even Amplitude Response $|H(\omega)| = |H(-\omega)|$

- Odd Phase Response $\angle H(\omega) = -\angle H(-\omega)$

- Real-Valued DC Response $H(0) \in \mathbb{R}$

- Steady-State response to complex exponential

$$f(t) = A e^{j(\omega t + \theta)} \quad H(\omega) A e^{j(\omega t + \theta)}$$

$\xrightarrow{\quad} \boxed{H(\omega)} \uparrow$

• What if you have multiple frequencies

Let $f(t) = \cos(\frac{1}{2}t) + 3\cos(2t + \frac{\pi}{4}) + 2\sin(3t)$

$\downarrow$ input $\downarrow \omega_1$ $\downarrow \omega_2$ $\downarrow \omega_3$

$$y(t) = \frac{d}{dt} f(t)$$

$$Y = j\omega F$$

• Find $y_{ss}(t)$

① $H(\omega), |H(\omega)|, \angle H(\omega)$

$$H(\omega) = \frac{Y}{F} = j\omega$$

$$|H(\omega)| = |\omega|$$

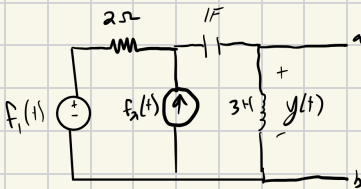
② $y_{ss}(t) = 1 \cdot |H(\frac{1}{2})| \cos(\frac{1}{2}t + \angle H(\frac{1}{2})) + 3 |H(2)| \cos(2t + \frac{\pi}{4} + \angle H(2)) +$

$$2 |H(3)| \sin(3t + \angle H(3)) =$$

$$= \frac{1}{2} \cos(\frac{1}{2}t + \frac{\pi}{2}) + 3 \cdot 2 \cos(2t + \frac{\pi}{4} + \frac{\pi}{2}) + 2 \cdot 3 \sin(3t + \frac{\pi}{2})$$

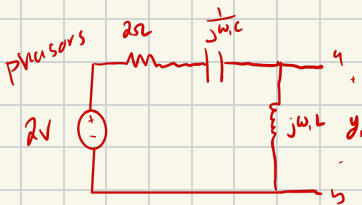
Example:

$f_1(t) = 2\cos(\frac{1}{3}t) \text{ V}$ and $f_2(t) = 3\sin(t) \text{ A}$



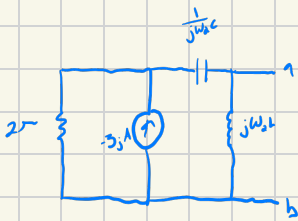
Look at each source individually
and add in time domain

$$y_{ss}(t) = y_{ss_1}(t) + y_{ss_2}(t)$$



$$y_1 = \frac{1}{\sqrt{2}} e^{j \frac{3\pi}{4}} \rightarrow \text{convert to time domain} = \frac{1}{\sqrt{2}} \cos(\frac{1}{3}t + \frac{3\pi}{4}) \text{ V}$$

Only $f_a(t)$



$$Y_a = \frac{9}{\sqrt{2}} e^{-j\frac{\pi}{4}} \rightarrow y_{ss} = \frac{9}{\sqrt{2}} \cos\left(t - \frac{\pi}{4}\right) \text{ V}$$

$$y_{ss} = y_{ss_1} + y_{ss_2} = \frac{1}{\sqrt{2}} \cos\left(\frac{1}{3}t + \frac{3\pi}{4}\right) + \frac{9}{\sqrt{2}} \cos\left(t - \frac{\pi}{4}\right)$$

Looking back at Schun's lectures

Frequency Response

$$f(t) \rightarrow \boxed{\text{system}} \rightarrow y(t)$$

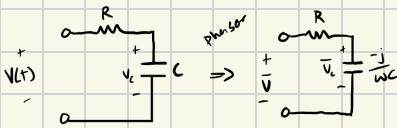
$$f(t) = F_p \cos(\omega t) \longleftrightarrow \bar{F} = F_p \angle 0^\circ$$

$$F_p \angle 0^\circ \rightarrow \boxed{\text{system}} \rightarrow Y_p \angle \theta$$

$$H(\omega) \leftarrow \text{frequency response (complex)}^*$$

$$\bar{Y} = H(\omega) \bar{F} \Rightarrow H(\omega) = \frac{\bar{Y}}{\bar{F}}$$

Ex: RC Circuit



$$\begin{aligned} \bar{V}_c &= \left(\frac{-j}{\omega C} \right) \bar{V} \Rightarrow \left(\frac{-j \omega C (R + j/\omega C)}{R^2 + \frac{1}{\omega^2 C^2}} \right) \bar{V} = \left(\frac{1}{(\omega C)^2} - j \frac{R}{\omega C} \right) \bar{V} \stackrel{\omega_c}{=} \left(\frac{1}{\omega^2 R^2 + \frac{1}{\omega^2}} \right) \bar{V} = \\ &= \left(\frac{1}{R^2 + \frac{1}{(\omega C)^2}} \right) \bar{V} \quad \omega_c = \frac{1}{RC} \Rightarrow \underbrace{\left(\frac{\omega_c^2 - j \omega \omega_c}{\omega^2 + \omega_c^2} \right)}_{H(\omega)} \bar{V} \end{aligned}$$

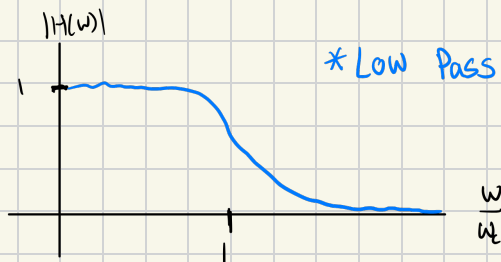
$$\rightarrow H(\omega) = \frac{\omega_c^2 - j \omega \omega_c}{\omega^2 + \omega_c^2}$$

$$|H(\omega)| = \sqrt{Re^2 + Im^2} = \sqrt{\left(\frac{\omega_c^2}{\omega^2 + \omega_c^2} \right)^2 + \left(\frac{-\omega \omega_c}{\omega^2 + \omega_c^2} \right)^2} = \sqrt{\frac{\omega_c^4 + \omega^2 \omega_c^2}{(\omega^2 + \omega_c^2)^2}} = \sqrt{\frac{\omega_c^2 (\omega^2 + \omega_c^2)}{(\omega^2 + \omega_c^2)^2}} = \sqrt{\frac{\omega_c^2}{\omega^2 + \omega_c^2}} =$$

$$|H(\omega)| = \sqrt{\frac{1}{1 + \left(\frac{\omega}{\omega_c} \right)^2}}$$

$$\frac{\omega}{\omega_c} \rightarrow 0, |H(\omega)| \rightarrow 1$$

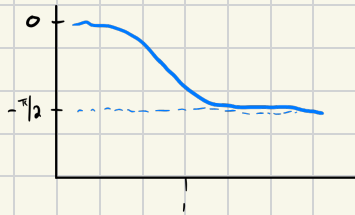
$$\frac{\omega}{\omega_c} \rightarrow \infty, |H(\omega)| \rightarrow 0$$



* Low Pass Filter *

$$\Theta(\omega) = \tan^{-1}\left(\frac{\text{Im}}{\text{Re}}\right) \rightarrow \Theta(\omega) = \tan^{-1}\left(\frac{-\omega\omega_c}{\omega_c^2}\right) = \tan^{-1}\left(\frac{-\omega}{\omega_c}\right)$$

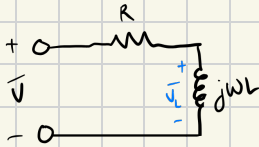
$$\frac{\omega}{\omega_c} \rightarrow 0, \Theta \rightarrow 0 \quad \frac{\omega}{\omega_c} \rightarrow \infty, \Theta \rightarrow -\frac{\pi}{2}$$



RL Low Pass



R-L High Pass

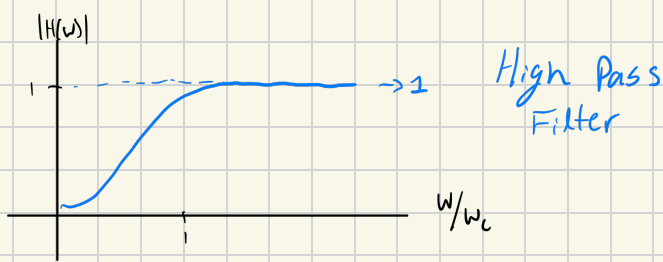


$$\begin{aligned} \bar{V}_L &= \left(\frac{j\omega L}{R + j\omega L} \right) \bar{V} \\ &= \left(\frac{j\omega L(R - j\omega L)}{R^2 + (\omega L)^2} \right) \bar{V} = \frac{j\omega LR + \omega^2 L^2}{R^2 + \omega^2 L^2} \bar{V} = \frac{j\omega(\frac{L}{R}) + \omega^2(\frac{L}{R})^2}{1 + \omega^2(\frac{L}{R})^2} \bar{V} \\ &\downarrow \\ &= \underbrace{\frac{j\left(\frac{\omega}{\omega_c}\right) + \left(\frac{\omega}{\omega_c}\right)^2}{1 + \left(\frac{\omega}{\omega_c}\right)^2}}_{H(\omega)} \bar{V} \end{aligned}$$

$$\begin{aligned} |H(\omega)| &= \sqrt{\left(\frac{\left(\frac{\omega}{\omega_c}\right)^2}{1 + \left(\frac{\omega}{\omega_c}\right)^2}\right)^2 + \left(\frac{\left(\frac{\omega}{\omega_c}\right)}{1 + \left(\frac{\omega}{\omega_c}\right)^2}\right)^2} \\ &= \sqrt{\frac{\left(\frac{\omega}{\omega_c}\right)^2 \left(1 + \left(\frac{\omega}{\omega_c}\right)^2\right)}{\left(1 + \left(\frac{\omega}{\omega_c}\right)^2\right)^2}} = \sqrt{\frac{\left(\frac{\omega}{\omega_c}\right)^2}{1 + \left(\frac{\omega}{\omega_c}\right)^2}} \end{aligned}$$

$$\frac{\omega}{\omega_c} \rightarrow 0, |H(\omega)| \rightarrow 0$$

$$\frac{\omega}{\omega_c} \rightarrow \infty, |H(\omega)| \rightarrow 1$$

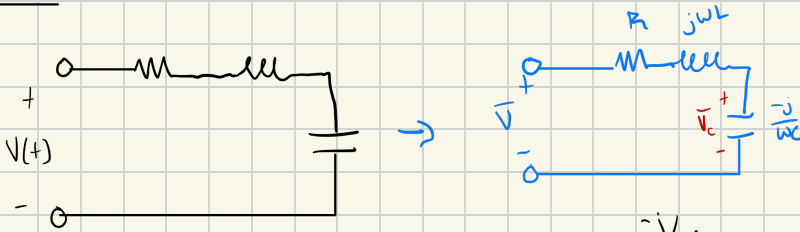


$$\theta(\omega) = \tan^{-1}\left(\frac{I_m}{R_c}\right) = \tan^{-1}\left(\frac{\omega/\omega_c}{(\omega/\omega_c)^2}\right) = \tan^{-1}\left(\frac{\omega_c}{\omega}\right)$$

$$\omega \rightarrow \infty ; \theta(\omega) \rightarrow 0$$

$$\omega \rightarrow 0 ; \theta(\omega) \rightarrow \frac{\pi}{2}$$

RLC



$$H(\omega) = \frac{-j/\omega_c}{R + j\omega L - \frac{j}{\omega c}}$$

* Band Pass Filter *

More Schuh lectures:

- LTI system response to cosinusoids & Multi-frequency inputs

Ex1

$$\frac{d^2 y}{dt^2} + 4 \frac{dy}{dt} + 4y = \frac{df}{dt}$$

Assuming $f(t) = F_p \cos(\omega t)$

$$\bar{F} = (F_p e^{j0}) e^{j\omega t}$$

phasors

$$\frac{d\bar{F}}{dt} = j\omega \bar{F} e^{j0} e^{j\omega t}$$

$$= j\omega \bar{F}$$

$$(j\omega)^2 \bar{Y} + j4\omega \bar{Y} + 4\bar{Y} = j\omega \bar{F}$$

$$\bar{Y}(4 - \omega^2 + j4\omega) = j\omega \bar{F}$$

$$\bar{Y} = \underbrace{\left(\frac{j\omega}{4 - \omega^2 + j4\omega} \right)}_{H(\omega)} \bar{F}$$

$$H(\omega) = \frac{j\omega}{4 - \omega^2 + j4\omega}$$

$$H(\omega) = \frac{j\omega}{4 - \omega^2 + j4\omega} \cdot \frac{(4 - \omega^2 - j4\omega)}{(4 - \omega^2 - j4\omega)} = \frac{4\omega^2 + j\omega(4 - \omega^2)}{(4 - \omega^2)^2 + 16\omega^2}$$

$$|H(\omega)| = \sqrt{\text{Re}^2 \cdot \text{Im}^2} = \sqrt{\frac{(4\omega^2)^2 + \omega^2(4 - \omega^2)^2}{((4 - \omega^2)^2 + 16\omega^2)^2}} = \sqrt{\frac{16\omega^4 + \omega^2(4 - \omega^2)^2}{((4 - \omega^2)^2 + 16\omega^2)^2}} = \sqrt{\frac{\omega^2(16\omega^2 + (4 - \omega^2)^2)}{(16\omega^2 + (4 - \omega^2)^2)^2}} = \sqrt{\frac{\omega^2}{16\omega^2 + (4 - \omega^2)^2}} = |H(\omega)|$$

$$\omega \rightarrow 0, |H(\omega)| \rightarrow 0$$

$$\omega \rightarrow \infty, |H(\omega)| \rightarrow 0$$

* Band Pass Filter *



Decibels (dB)

$$|H(\omega)|_{dB} = 20 \log_{10}(|H(\omega)|)$$

Low Pass Filter

$$|H(\omega)| = \frac{1}{1 + \omega^2}$$

$$|H(\omega)|_{dB} = 20 \log_{10}((1 + \omega^2)^{-1/2})$$

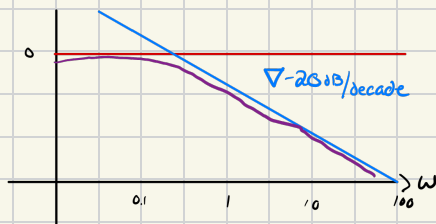
$$= -10 \log_{10}(1 + \omega^2)$$

$$\omega \rightarrow 0, |H(\omega)|_{dB} \rightarrow 0$$

$$\omega \rightarrow \infty, |H(\omega)|_{dB} \rightarrow -10 \log_{10}(\omega^2) \rightarrow -20 \log_{10}(\omega)$$

For any time ω increases by 10x

$|H(\omega)|$ decreases by 20dB



High Pass Filter

Assume $|H(\omega)| = \sqrt{\frac{\omega^2}{1+\omega^2}}$

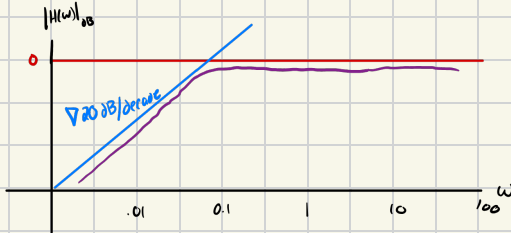
$$|H(\omega)|_{dB} = 20 \log_{10} \left(\left[\frac{\omega^2}{1+\omega^2} \right]^{1/2} \right)$$

$$= 10 \log_{10} \left(\frac{\omega^2}{1+\omega^2} \right)$$

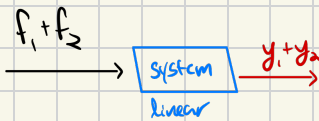
$$= 10 (\log_{10}(\omega^2) - \log_{10}(1+\omega^2))$$

$$\omega \rightarrow \infty ; |H(\omega)|_{dB} \rightarrow 10 (\log(\omega^2) - \log(\omega^2)) \rightarrow 0$$

$$\omega \rightarrow 0 ; |H(\omega)|_{dB} \rightarrow 10 (\log(\omega^2) - \log(1)) \rightarrow 10 \log(\omega^2) \rightarrow 20 \log_{10}(\omega)$$



Multiple Frequencies



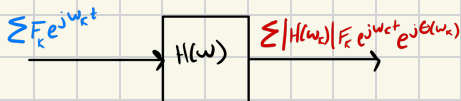
$$\bar{F}_1 = F_{p1} e^{j\omega_1 t}$$

$$\bar{Y}_1 = |H(\omega_1)| F_{p1} e^{j\omega_1 t} e^{j\theta(\omega_1)}$$

$$\bar{F}_2 = F_{p2} e^{j\omega_2 t}$$

$$\bar{Y}_2 = |H(\omega_2)| F_{p2} e^{j\omega_2 t} e^{j\theta(\omega_2)}$$

$$Y = Y_1 + Y_2$$



Ex) let $H(\omega) = \frac{1}{1+j\omega} = \frac{1-j\omega}{1+\omega^2} \rightarrow |H(\omega)| = \frac{1}{\sqrt{1+\omega^2}} \rightarrow \Theta(\omega) = \tan^{-1}(-\omega)$

let $f(t) = 1\cos(t) + 0.1\cos(10t) + 0.01\cos(100t)$

ω	F	$ H(\omega) $	$\Theta(\omega)$
1	1	$\frac{\sqrt{2}}{2} \approx 0.707$	$\tan^{-1}(-1) = -45^\circ = -\frac{\pi}{4}$
10	0.1	$\frac{1}{\sqrt{101}} \approx 0.1$	$\tan^{-1}(-10) = -84.29^\circ$
100	0.1	$\frac{1}{\sqrt{10001}} \approx 0.03$	$\tan^{-1}(-100) = -89.43^\circ$

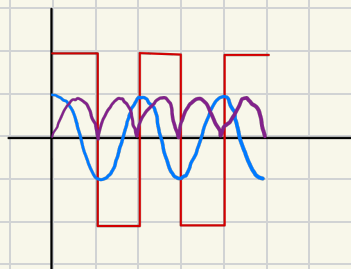
$$y(t) = 0.7(1)\cos(t - 45^\circ) + 0.1(0.1)\cos(10t - 84.29^\circ) + 0.03(0.01)\cos(100t - 89.43^\circ)$$

Periodic Signals

$\exists f(t) = f(t - t_0)$
 $t \neq 0$, $f(t)$ is periodic

$K \in \text{integers}$ *periodic functions repeat in time*

$f(t) = f(t - Kt_0)$



T : smallest t_0 for which a signal repeats

Ex) $\cos(t) \rightarrow T = 2\pi \text{ sec}$
 $\cos(3t) \rightarrow T = \frac{2\pi}{3} \rightarrow T = \frac{2\pi}{3} \text{ sec}$

$f(t) = \cos(2t) + \cos(3t)$

$T_1 = \frac{2\pi}{2} = \pi \text{ sec}$ $T_2 = \frac{2\pi}{3} \text{ sec}$

Overall: LCM T_1 & T_2

$T_{\text{tot}} = 2\pi$
 $T_1 \cdot (2) = 2\pi$
 $T_2 \cdot (3) = 2\pi$

Test for if sum of periodic signals is periodic

$$\frac{\omega_1}{\omega_2} = \text{rational Number (Fraction)} \rightarrow \text{will be periodic}$$

Ex) $\omega_1 = 2, \omega_2 = 3$

$$\frac{\omega_1}{\omega_2} = \frac{2}{3} \quad \text{periodic}$$

Ex) $f(t) = \cos(t) + \cos(\sqrt{2}t)$

$$\omega_1 = 1 \quad \omega_2 = \sqrt{2}$$

$$\frac{\omega_1}{\omega_2} = \frac{1}{\sqrt{2}} \quad \text{non periodic}$$

Fourier Series

* Periodic functions can be approximated by sums of sines + cosines *

Complex Exponential Form ($e^{j\theta} = \cos\theta + j\sin\theta$)

$$f(t) = \sum_{\substack{K=-\infty \\ K \in \text{integers}}}^{\infty} F_K e^{jk\omega_0 t}$$

$\nearrow$ complex #
 $\nwarrow$ fundamental frequency

$$\omega_0 = \frac{2\pi}{T}$$

$$K\omega_0 = K^{\text{th}} \text{ harmonic}$$

$$F_K \in \mathbb{C} \quad (F_K \in \text{complex \#s})$$

Trigonometric Form

$$F_K e^{jK\omega_0 t} = F_K \cos(K\omega_0 t) + jF_K \sin(K\omega_0 t)$$

$$f(t) = \sum_{K=-\infty}^{\infty} F_K \cos(K\omega_0 t) + jF_K \sin(K\omega_0 t)$$

$$K=0: F_0 \cos(0) + jF_0 \sin(0) \\ = F_0$$

$$f(t) = F_0 + \sum_{k=1}^{\infty} F_k \cos(k\omega_0 t) + jF_k \sin(k\omega_0 t) + F_k \cos(-k\omega_0 t) + jF_k \sin(-k\omega_0 t)$$

Since $\cos$ is an even function, positives and negatives are equal

and $\sin$ functions are odd: $\sin(-1) = -\sin(1)$

$$= F_0 + \sum_{k=1}^{\infty} (F_k + F_k) \cos(k\omega_0 t) + j(F_k - F_k) \sin(k\omega_0 t)$$

We can define:

$$a_0 = 2F_0$$

$$f(t) = \frac{a_0}{2} + \sum_{k=1}^{\infty} a_k \cos(k\omega_0 t) + b_k \sin(k\omega_0 t)$$

$$a_k = F_k + F_k$$

$$b_k = j(F_k - F_k)$$

Compact Form (non-complex functions only)

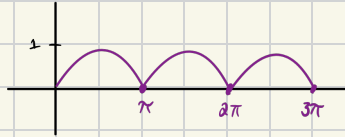
$$c_0 = a/2$$

$$f(t) = \frac{c_0}{2} + \sum_{k=1}^{\infty} c_k \cos(k\omega_0 t + \theta_k)$$

$$c_k = a/2$$

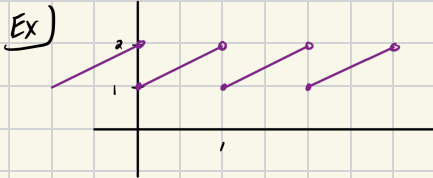
$$\theta_k = \tan^{-1} \left(\frac{\text{Im}(F_k)}{\text{Re}(F_k)} \right)$$

Ex) $f(t) = |\sin(t)|$



$$T = \pi$$

$$\omega_0 = \frac{2\pi}{T} = \frac{2\pi}{\pi} = 2 \frac{\text{rad}}{\text{sec}}$$



$$T = 1 \text{ sec}$$

$$\omega_0 = \frac{2\pi}{T} \Rightarrow \omega_0 = 2\pi \text{ rad/sec}$$

Fourier Series + its forms

1) Sinusoidal input (Frequency Response)

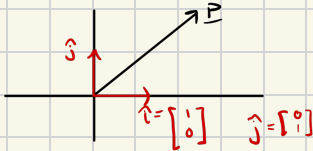
2) Multiple sinusoidal inputs (Frequency Response + Linearity)

3) Periodic signals

4) Fourier Series - periodic signal written as sines + cosines

Linear Algebra

Basis: $\{\hat{i}, \hat{j}\}$ ← orthogonal (no mixing of information)



$$a = \frac{P \cdot \hat{i}}{|\hat{i}|^2}$$

$$b = \frac{P \cdot \hat{j}}{|\hat{j}|^2}$$

$$\underline{P} = a\hat{i} + b\hat{j}$$

* functions are vectors in ∞ dimensional space

Inner Product

~ Extension of the dot product to ∞ -dimensional spaces

$$\langle f(t), g(t) \rangle = \int_0^T f(t) g^*(t) dt$$

inner product of $f(t)$ and $g(t)$

$\langle f(t), g(t) \rangle = 0 \rightarrow$ the functions are orthogonal

Ex1 $e^{j\omega_0 t}, e^{-j\omega_0 t} \rightarrow$ Find inner product

$$\begin{aligned} \langle e^{j\omega_0 t}, e^{-j\omega_0 t} \rangle &= \int_0^T e^{j\omega_0 t} e^{-j\omega_0 t} dt \\ &= \int_0^T e^{-j\omega_0 t} dt \\ &= \int_0^T \cos(\omega_0 t) - j \sin(\omega_0 t) dt \\ &= \left. \frac{1}{\omega_0} \sin(\omega_0 t) + j \frac{1}{\omega_0} \cos(\omega_0 t) \right|_0^T \end{aligned}$$

$$\omega_0 = \frac{2\pi}{T}$$

$$\omega_0 T = 2\pi$$

$$= \frac{1}{\omega_0} (\sin(\omega_0 T) - \sin(0) + j [\cos(\omega_0 T) - \cos(0)])$$

$$= \frac{1}{\omega_0} (\sin(2\pi) - \sin(0) + j [\cos(2\pi) - \cos(0)])$$

$$= \frac{1}{\omega_0} (0 + j(1-1)) = \frac{1}{\omega_0} (0 + j0) = 0$$

** Orthogonal **

$$f(t) = \sum_{n=-\infty}^{\infty} F_n e^{jn\omega_0 t}$$

$$\langle f(t), e^{jm\omega_0 t} \rangle = \int_0^T \sum_{n=-\infty}^{\infty} F_n e^{jn\omega_0 t} e^{-jm\omega_0 t} dt$$

← whichever F_n we care about

$$= \sum_{n=-\infty}^{\infty} F_n \int_0^T e^{j(n-m)\omega_0 t} dt$$

$$\int_0^T e^{j(n-m)\omega_0 t} dt = 0 \quad n \neq m$$

$$\int_0^T e^{j(n-m)\omega_0 t} dt = \int_0^T e^{j0} dt = \int_0^T 1 dt = T \quad n = m$$

$$\langle f(t), e^{jm\omega_0 t} \rangle = T F_m$$

$$\star F_m = \frac{1}{T} \int_0^T f(t) e^{-jm\omega_0 t} dt \star$$

Ex) $f(t) = \cos^2(t) = \frac{1}{2}(1 + \cos(2t))$
 $= \frac{1}{2} + \frac{1}{2}\cos(2t)$

① Start with finding F_0

$$F_0 = \frac{1}{T} \int_0^T f(t) e^{j0} dt = \frac{1}{T} \int_0^T f(t) dt$$

Average value of $f(t)$

$$T = \pi$$

$$= \frac{1}{\pi} \int_0^{\pi} \left(\frac{1}{2} + \frac{1}{2}\cos(2t) \right) dt = \frac{1}{\pi} \left[\frac{1}{2}t + \frac{1}{2} \left(\frac{1}{2}\sin(2t) \right) \right]_0^{\pi}$$

$$= \frac{1}{\pi} \left[\frac{1}{2}(\pi - 0) + \frac{1}{4}(\sin(2\pi) - \sin(0)) \right]$$

$$= \frac{1}{\pi} \left[\frac{\pi}{2} \right] \Rightarrow \boxed{F_0 = \frac{1}{2}}$$

② Find F_n ($n \neq 0$)

$$F_n = \frac{1}{\pi} \int_0^{\pi} \cos^2(t) e^{jn\omega t} dt \Rightarrow \frac{1}{\pi} \int_0^{\pi} \cos^2(t) e^{j2nt} dt \Rightarrow \frac{1}{\pi} \int_0^{\pi} \left(\frac{1}{2} + \frac{1}{2} \cos(2t) \right) (\cos(2nt) - j \sin(2nt)) dt$$

$$w_0 = \frac{2\pi}{T} = 2$$

$$= \frac{1}{\pi} \int_0^{\pi} \left(\frac{1}{2} \cos(2nt) - j \frac{1}{2} \sin(2nt) + \frac{1}{2} \cos(2t) \cos(2nt) - j \frac{1}{2} \cos(2t) \sin(2nt) \right) dt$$

$$\cos(A)\cos(B) = \frac{1}{2}(\cos(A+B) + \cos(A-B))$$

$$\cos(A)\sin(B) = \frac{1}{2}(\sin(A+B) - \sin(A-B))$$

$$= \frac{1}{\pi} \int_0^{\pi} \left(\frac{1}{4} (\cos(2(1+n)t) + \cos(2(1-n)t)) + \frac{1}{4} (\sin(2(1+n)t) + \sin(2(1-n)t)) \right) dt$$

only 2 values of n where

the integral $\neq 0$

$n = -1$

$n = 1$

$$\Rightarrow \frac{1}{\pi} \int_0^{\pi} \frac{1}{4} (1) dt \Rightarrow \frac{1}{\pi} \left(\frac{1}{4} t \right) \Big|_0^{\pi} = \frac{1}{4}$$

$$\Rightarrow \frac{1}{\pi} \int_0^{\pi} \frac{1}{4} (1) dt \Rightarrow \frac{1}{\pi} \left(\frac{1}{4} t \right) \Big|_0^{\pi} = \frac{1}{4}$$

In terms of complex exp.

$$F_{-1} = \frac{1}{4} \quad F_1 = \frac{1}{4}$$

$$f(t) = \frac{1}{2} + \frac{1}{4} e^{-j2t} + \frac{1}{4} e^{j2t}$$

Trig Form:

$$a_0 = 2F_0$$

$$a_n = F_n + F_{-n}$$

$$b_n = F_n - F_{-n}$$

$$a_0 = 2\left(\frac{1}{2}\right) = 1$$

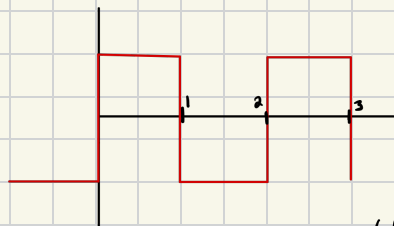
$$a_1 = \frac{1}{4} + \frac{1}{4} = \frac{1}{2}$$

$$b_1 = \frac{1}{4} - \frac{1}{4} = 0$$

$$f(t) = \frac{1}{2} + \frac{1}{2} \cos(2t)$$

✓

Running through examples of Fourier



$$T = 2s$$

$$\omega_0 = \frac{2\pi}{T} = \pi$$

$$F_0 = \frac{1}{T} \int_0^T f(t) dt \Rightarrow$$

$$\frac{1}{2} \int_0^2 f(t) dt$$

must break this up
because values are different
@ diff locations

$$= \frac{1}{2} \left(\int_0^1 1 dt + \int_1^2 -1 dt \right)$$

$$= \frac{1}{2} \left(+1 - 1 \right) = \frac{1}{2} (0) = 0 \quad \checkmark \quad F_0 = 0$$

$$F_n = \frac{1}{T} \int_0^T f(t) e^{-jn\omega_0 t} dt = \frac{1}{2} \int_0^2 f(t) e^{-jn\pi t} dt = \frac{1}{2} \left(\int_0^1 1 e^{-jn\pi t} dt + \int_1^2 -1 e^{-jn\pi t} dt \right) = \frac{1}{2} \left(\frac{1}{-jn\pi} e^{-jn\pi t} \Big|_0^1 + (-1) \frac{1}{-jn\pi} e^{-jn\pi t} \Big|_1^2 \right)$$

$$\frac{1}{2} \left(\frac{1}{-jn\pi} (e^{-jn\pi} - 1) - \frac{1}{jn\pi} (e^{-j2n\pi} - e^{-jn\pi}) \right) = \frac{1}{2} \left(\frac{1}{-jn\pi} (e^{-jn\pi} - 1) + \frac{1}{jn\pi} (e^{-jn\pi} - e^{-j2n\pi}) \right)$$

$$\frac{1}{2} \left(\frac{1}{jn\pi} (e^{-jn\pi} - 1) + \frac{1}{jn\pi} (e^{-jn\pi} - 1) \right) = \frac{1}{jn\pi} (e^{-jn\pi} - 1)$$

$$e^{-jn\pi} = \cos(n\pi) - j\sin(n\pi)$$

$$n \in \mathbb{Z}$$

$$\frac{1}{jn\pi} ((-1)^n - 1)$$

$$n: \text{even} \Rightarrow F_n = 0$$

$$\text{odd} \Rightarrow F_n = \frac{-2}{jn\pi} \cdot \frac{j}{2} = \frac{-j}{n\pi}$$

n	cos(nπ)
1	-1
2	1
3	-1

if n is odd: cos(nπ) = -1
if n is even: cos(nπ) = 1

$$\cos(n\pi) = (-1)^n$$

$$n: \text{even}, F_n = 0$$

$$n: \text{odd}, F_n = \frac{-j}{n\pi}$$

$$f(t) = 0 + \sum_{\substack{n=-\infty \\ n \neq 0 \\ n \text{ odd}}}^{\infty} \frac{-j}{n\pi} e^{jn\pi t}$$

Ex)



$$f(t) = \frac{t}{2} \quad 0 \leq t < 2$$

$$T = 2s$$

$$\omega_0 = \frac{2\pi}{2s} = \pi$$

① Find F_0

$$F_0 = \frac{1}{2} \int_0^2 \frac{t}{2} dt \Rightarrow \frac{1}{2} \left(\frac{t^2}{4} \Big|_0^2 \right) = \frac{1}{2} \left(\frac{4}{4} - 0 \right) = \frac{1}{2}$$

② Find F_n

$$F_n = \frac{1}{2} \int_0^2 \frac{t}{2} e^{-jn\pi t} dt = \frac{1}{4} \int_0^2 t e^{-jn\pi t} dt = \frac{1}{4} \left(\frac{t}{-jn\pi} e^{-jn\pi t} - \int_0^2 \frac{1}{-jn\pi} e^{-jn\pi t} dt \right) = \frac{1}{4} \left(\frac{2}{-jn\pi} e^{-jn\pi} - 0 \right) = \frac{1}{2} \left(\frac{1}{-jn\pi} \right) e^{-jn\pi}$$

$e^{-jn\pi} = 1$

$$= \frac{1}{2} \left(\frac{1}{-jn\pi} \right) \Rightarrow \frac{j}{2n\pi} = F_n$$

$u = t \quad v = \frac{1}{-jn\pi} e^{-jn\pi t}$
 $du = dt \quad dv = -e^{-jn\pi t}$

$$f(t) = \frac{1}{2} + \sum_{\substack{n=-\infty \\ n \neq 0}}^{\infty} \frac{j}{2n\pi} e^{jn\pi t}$$

Ex)

$$f(t) = |\sin(t)|$$



$$T = \pi s$$

$$\omega_0 = \frac{2\pi}{T} = \frac{2\pi}{\pi} = 2 \text{ rad/sec}$$

① Find F_0

$$\frac{1}{\pi} \int_0^{\pi} \sin(t) dt = \frac{1}{\pi} (-\cos(t)) \Big|_0^{\pi} = \frac{1}{\pi} (-(-1) + 1) = \frac{2}{\pi} = F_0$$

② Find F_n

$$F_n = \frac{1}{\pi} \int_0^{\pi} \sin(t) e^{-jn\omega_0 t} dt = \frac{1}{\pi} \int_0^{\pi} \left(\frac{e^{jt} - e^{-jt}}{j2} \right) e^{-j2nt} dt = \frac{1}{j2\pi} \int_0^{\pi} e^{jt} e^{-j2nt} - e^{-jt} e^{-j2nt} dt = \frac{1}{j2\pi} \int_0^{\pi} e^{j(1-2n)t} - e^{-j(1+2n)t} dt$$

$$F_n = \frac{2}{\pi} \left[\frac{1}{1-4n^2} \right]$$

$$f(t) = \frac{a}{\pi} + \sum_{\substack{n=-\infty \\ n \neq 0}}^{\infty} \frac{a}{\pi} \left(\frac{1}{1-4n^2} \right) e^{j2nt}$$

Exponential Fourier Series

- Let $f(t) = 1 + 2\sin(t) + \sin^2(\frac{\pi}{4}t)$ ↖ DC offset
- Determine its exponential Fourier Series

Find signal must look like $\sum_{n=-\infty}^{\infty} F_n e^{jn\omega_0 t}$

$$\sin^2(x) = \frac{1}{2}(1 - \cos(2x))$$

$$f(t) = 1 + 2\sin(t) + \frac{1}{2} - \frac{1}{2}\cos(\frac{\pi}{4}t) = \frac{3}{2} + 2\sin(t) - \frac{1}{2}\cos(\frac{\pi}{4}t)$$

$$\omega_0 = \text{GCD}(1, \frac{\pi}{4}) = \frac{1}{4} \text{ rad/s}$$

$$= \frac{3}{2} + 2 \left(\frac{e^{jt} - e^{-jt}}{2j} \right) - \frac{1}{2} \left(\frac{e^{j\frac{\pi}{4}t} + e^{-j\frac{\pi}{4}t}}{2} \right) =$$

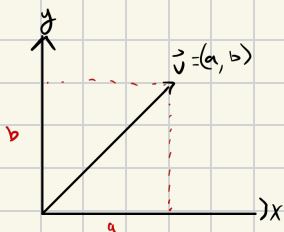
$$\frac{3}{2} + \frac{1}{j}e^{jt} - \frac{1}{j}e^{-jt} - \frac{1}{4}e^{j\frac{\pi}{4}t} - \frac{1}{4}e^{-j\frac{\pi}{4}t} = f(t)$$

$$f(t) = \sum_{n=-\infty}^{\infty} F_n e^{jn\omega_0 t} = F_0 + F_1 e^{j\frac{1}{4}t} + F_{-1} e^{-j\frac{1}{4}t} + F_2 e^{j\frac{1}{2}t} + F_{-2} e^{-j\frac{1}{2}t} + F_3 e^{j\frac{3}{4}t} + F_{-3} e^{-j\frac{3}{4}t} + \dots$$

$\downarrow \quad \downarrow \quad \downarrow \quad \downarrow \quad \downarrow \quad \downarrow \quad \downarrow$
 $\frac{3}{2} \quad 0 \quad 0 \quad 0 \quad 0 \quad \frac{1}{4} \quad \frac{1}{4}$

- What if $f(t)$ is sinusoidal or a complex exponential? Just match coefficients
- If not, but $f(t)$ is periodic, will use $\{e^{jn\omega_0 t}\}$ as a basis to project onto.

- a is a projection of $\vec{v}$ onto $\vec{x}$
- b is a projection of $\vec{v}$ onto $\vec{y}$.



$$F_n = \langle f(t), e^{jn\omega_0 t} \rangle = \frac{1}{T} \int_T f(t) e^{-jn\omega_0 t} dt$$

$\nwarrow$
 $0 \text{ to } T$
 or $-\frac{T}{2} \text{ to } \frac{T}{2}$

• $\{e^{jn\omega_0 t}\}$ is an orthonormal basis:

$$\langle e^{jn\omega_0 t}, e^{jm\omega_0 t} \rangle = \begin{cases} 1 & n=m \\ 0 & \text{else} \end{cases}$$

$$\begin{aligned} \langle e^{jn\omega_0 t}, e^{jm\omega_0 t} \rangle &= \frac{1}{T} \int_T e^{jn\omega_0 t} \cdot e^{-jm\omega_0 t} dt = \frac{1}{T} \int_T e^{j(n-m)\omega_0 t} dt = \\ &= \frac{e^{j(n-m)\omega_0 T} - 1}{j(n-m)\omega_0} \bigg|_0^T = \frac{1}{T} \left(\frac{e^{j(n-m)\omega_0 T} - 1}{j(n-m)\omega_0} \right) = 0 \end{aligned}$$

if $n \neq m$:

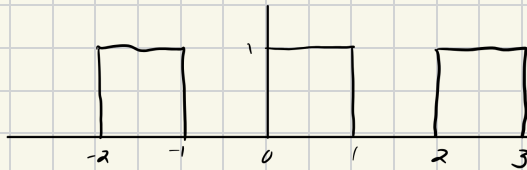
if $n = m$:

$$\langle e^{jn\omega_0 t}, e^{jn\omega_0 t} \rangle = \frac{1}{T} \int_T e^{jn\omega_0 t} \cdot e^{-jn\omega_0 t} dt = \frac{1}{T} \int_T 1 dt = 1$$

Ex:

$$\text{Let } f(t) = \begin{cases} 1 & t \in [0, 1) \\ 0 & t \in [1, 2) \end{cases}$$

have period = 2s



Determine exponential Fourier Series

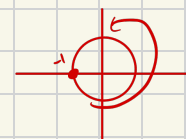
$$f(t) = \sum_{n=-\infty}^{\infty} F_n e^{jn\omega_0 t}$$

$$\begin{aligned} F_n &= \frac{1}{T} \int_T f(t) e^{-jn\omega_0 t} dt = \frac{1}{2} \left[\int_0^1 (1) e^{-jn\pi t} dt + \int_1^2 (0) e^{-jn\pi t} dt \right] \quad (n \text{ is an integer}) \\ &= \frac{1}{2} \left[\frac{e^{-jn\pi t}}{-jn\pi} \bigg|_0^1 \right] = \frac{-1}{2jn\pi} (e^{-jn\pi} - 1) \end{aligned}$$

$n \neq 0$

$$F_0 = \frac{1}{T} \int_T f(t) e^{j0\pi t} dt = \frac{1}{2} \int_T f(t) dt = \frac{1}{2} \leftarrow \text{average of } f(t)$$

DC Term



$$F_n = \begin{cases} \frac{-1}{jn2\pi} (1-1) = 0 & n \text{ even} \\ & n \neq 0 \\ \frac{-1}{jn2\pi} (-1-1) = \frac{1}{jn\pi} & n \text{ is odd} \\ \frac{1}{a} & n=0 \end{cases}$$

$$f(t) = \frac{1}{2} + \sum_{\substack{n=-\infty \\ n \text{ odd}}}^{\infty} \frac{1}{jn\pi} e^{jn\pi t}$$

Terminology:

F_0 is the DC component

F_1 corresponds to the fundamental frequency term

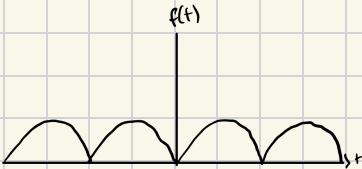
F_n corresponds to the n^{th} harmonic

- Existence of Fourier series representation

$$f(t) = \sum_{n=-\infty}^{\infty} F_n e^{jn\omega_0 t}$$

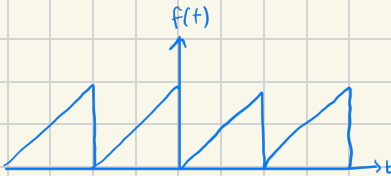
$$f(t) = F_0 + F_1 e^{j\omega_0 t} + F_{-1} e^{-j\omega_0 t} + \dots$$

① $f(t) = |\sin(t)|$



Note: With Fourier transform, the transform does not know where discontinuities exist. This is known as Gibbs phenomenon

②



- For existence of the Fourier series, we need:

① Absolute integrability of $f(t)$ over period T

$$\int_T |f(t)| dt < \infty \text{ has to be finite}$$

② Plottability

- over one period
- Finite # of maxima and minima
 - Finite number of finite discontinuities (series converges to midpoint at discontinuity)

• Fourier Series Forms

- Exponential Fourier series

$$f(t) = \sum_{n=-\infty}^{\infty} F_n e^{jn\omega_0 t}$$

- Trigonometric

$$f(t) = \frac{a_0}{2} + \sum_{n=1}^{\infty} (a_n \cos(n\omega_0 t) + b_n \sin(n\omega_0 t))$$

$$a_0 = 2F_0 \quad a_n = F_n + F_{-n} \quad b_n = j(F_n - F_{-n})$$

$$F_0 = \frac{a_0}{2} \quad F_n = \frac{a_n - jb_n}{2} \quad F_{-n} = \frac{a_n + jb_n}{2}$$

- Compact Fourier Series, for real valued functions only

$$f(t) = \frac{C_0}{2} + \sum_{n=1}^{\infty} C_n (\cos(n\omega_0 t + \theta_n))$$

$$C_0 = 2F_0 \quad C_n = 2|F_n| \quad \theta_n = \angle F_n$$

$$F_0 = \frac{C_0}{2} \quad F_n = \frac{C_n}{2}$$

$$f(t) = \left(\frac{1}{2} \right) + \sum_{n=-\infty}^{\infty} \frac{1}{jn\pi} e^{jn\pi t} \rightarrow \text{trig FS of } f(t)$$

$$f(t) = \frac{a_0}{2} + \sum_{n=1}^{\infty} a_n \cos(n\omega_0 t) + b_n \sin(n\omega_0 t)$$

$$= \frac{1}{2} + \sum_{n=1}^{\infty} \left(\frac{1}{jn\pi} e^{jn\pi t} + \frac{1}{j(-n)\pi} e^{j(-n)\pi t} \right) =$$

$$= \frac{1}{2} + \sum_{n=1}^{\infty} \frac{1}{n\pi} \left(\frac{e^{jn\pi t} - e^{-jn\pi t}}{j} \right) =$$

$$= \frac{1}{2} + \sum_{n=1}^{\infty} \frac{2}{n\pi} \left(\frac{e^{jn\pi t} - e^{-jn\pi t}}{j2} \right) =$$

$$= \frac{1}{2} + \sum_{n=1}^{\infty} \frac{2}{n\pi} \sin(n\pi t)$$

$$a_n = \begin{cases} 1 & n=0 \\ 0 & \text{else} \end{cases}$$

$$b_n = \begin{cases} 0 & n=\text{even} \\ \frac{2}{n\pi} & n=\text{odd} \end{cases}$$

Exponential F.S. $\rightarrow$ compact F.S.

$$F_n = \begin{cases} \frac{1}{2} & n=0 \\ \frac{1}{jn\pi} & n \text{ odd} \\ 0 & \text{else} \end{cases}$$

$$C_0 = 2F_0 = 1$$

$$C_n = 2|F_n| = 2\left|\frac{1}{jn\pi}\right|$$

$$= \begin{cases} \frac{2}{n\pi} & n \text{ odd} \\ 0 & \text{even, } n \neq 0 \end{cases}$$

$$\Theta_n = \angle F_n = \begin{cases} -\pi/2 & n \text{ odd} \\ 0 & \text{else} \end{cases}$$

$$f(t) = \frac{1}{2} + \sum_{\substack{n=1 \\ n \text{ odd}}}^{\infty} \frac{2}{n\pi} \cos(n\pi t - \frac{\pi}{2})$$

• Properties of Exp. F.S.

Consider

$$g(t) = \begin{cases} 2 & t \in [0, 1) \\ 0 & t \in [1, 2) \end{cases} \text{ with period } 2s, \text{ and } f(t) = \begin{cases} 1 & t \in [0, 1) \\ 0 & t \in [1, 2) \end{cases} = \frac{1}{2} + \sum_{\substack{n=-\infty \\ n \text{ odd}}}^{\infty} \frac{1}{jn\pi} e^{jn\pi t}$$

What are the exponential Fourier series coefficients G_n

$$g(t) = 2f(t)$$

$$2(f(t)) = 2\left(\frac{1}{2} + \sum_{\substack{n=-\infty \\ n \text{ odd}}}^{\infty} \frac{1}{jn\pi} e^{jn\pi t}\right)$$

(Amplitude scaling property)
only the amplitude is
affected

Consider:

$$f(t) = \begin{cases} 1 & t \in [0, 1) \\ 0 & t \in [1, 2) \end{cases} = \frac{1}{2} + \sum_{\substack{n=-\infty \\ n \text{ odd}}}^{\infty} \frac{1}{jn\pi} e^{jn\pi t}$$

and

$$h(t) = \begin{cases} 0 & t \in [0, 1) \\ 1 & t \in [1, 2) \end{cases}$$

$$h(t) = f(t-1) = \sum_{n=-\infty}^{\infty} F_n e^{jn\omega_0(t-1)} = \sum_{n=-\infty}^{\infty} F_n e^{jn\omega_0} \cdot e^{jn\omega_0 t}$$

$$h(t) = \sum_{n=-\infty}^{\infty} H_n e^{jn\omega_0 t}$$

$$h(t) = \sum_{n=-\infty}^{\infty} H_n e^{jn\omega_0 t} [v]$$

$$H_n = F_n e^{-jn\omega_0 t_0}$$

$$h(t) = f(t-1) \Rightarrow H_n = F_n e^{-jn\omega_0} = F_n e^{-jn\pi}$$

• Time shift property:

$$h(t) = f(t-t_0)$$

$$H_n = F_n e^{-jn\omega_0 t_0}$$

$$F_n = \begin{cases} \frac{1}{jn\pi} & n \text{ odd} \\ \frac{1}{2} & n = 0 \\ 0 & n \text{ even } n \neq 0 \end{cases}$$

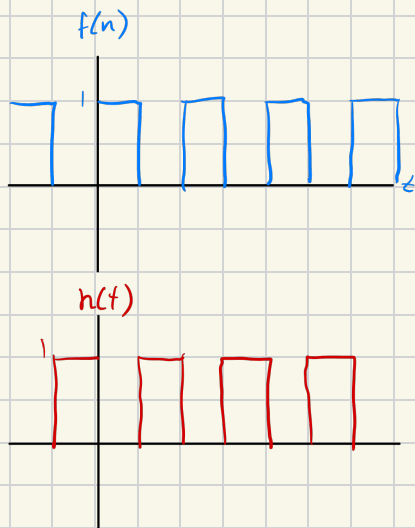
$$H_n = \begin{cases} \frac{1}{jn\pi} (-1) = \frac{-1}{jn\pi} & n \text{ odd} \\ \frac{1}{2} (-1) & n = 0 \\ 0 & n \text{ even } n \neq 0 \end{cases}$$

• Addition Property: If $f(t)$ and $h(t)$ have same ω_0 , then

$$X(t) = f(t) + h(t) ; X_n = F_n + H_n$$

Let:

$$x(t) = \begin{cases} 1 & t \in [0, 1) \\ -1 & t \in [1, 2) \end{cases} \quad T=2s$$



Recall:

$$g(t) = \begin{cases} 2 & t \in [0, 1) \\ 0 & t \in [1, 2) \end{cases} \quad G_n = \begin{cases} \frac{2}{jn\pi} & n \text{ odd} \\ 1 & n = 0 \\ 0 & n \text{ even} \neq 0 \end{cases}$$

$$X(t) = \begin{cases} 1 & t \in [0, 1) \\ -1 & t \in [1, 2) \end{cases} \quad T=2s$$

• Recall that in an LTI system

$$e^{j\omega t} \rightarrow \boxed{\text{LTI}}^{H(\omega)} \rightarrow H(\omega) e^{j\omega t}$$

$$\cos(\omega t + \theta) \rightarrow \boxed{\text{LTI}}^{H(\omega)} \rightarrow |H(\omega)| \cos(\omega t + \theta + \angle H(\omega))$$

so that

$$f(t) = \sum_{n=-\infty}^{\infty} F_n e^{jn\omega_0 t} \rightarrow \boxed{\text{LTI}}^{H(\omega)} \rightarrow y(t) = \sum_{n=-\infty}^{\infty} H(n\omega_0) F_n e^{jn\omega_0 t}$$

or

$$f(t) = \frac{C_0}{2} + \sum_{n=1}^{\infty} C_n \cos(n\omega_0 t + \theta_n) \rightarrow \boxed{\text{LTI}} \rightarrow y(t) = H(0) \frac{C_0}{2} + \sum_{n=1}^{\infty} |H(n\omega_0)| C_n \cos(n\omega_0 t + \theta_n + \angle H(n\omega_0))$$

Ex:

$$f(t) = \begin{cases} 1 & t \in [0, 1) \\ 0 & t \in [1, 2) \end{cases} = \frac{1}{2} + \sum_{\substack{n=-\infty \\ n \text{ odd}}}^{\infty} \frac{1}{jn\pi} e^{jn\pi t} \quad \omega_0 = \pi \text{ rad}$$

Let

$$H(\omega) = \frac{1}{2+j\omega} \quad |H(\omega)| = \frac{1}{\sqrt{4+\omega^2}} \quad \angle H(\omega) = -\tan^{-1}\left(\frac{\omega}{2}\right)$$

Determine the steady state output, $y(t)$

$$y(t) = \underline{\frac{1}{2} H(0)} + \sum_{\substack{n=-\infty \\ n \text{ odd}}}^{\infty} H(n\omega_0) \frac{1}{jn\pi} e^{jn\pi t} =$$

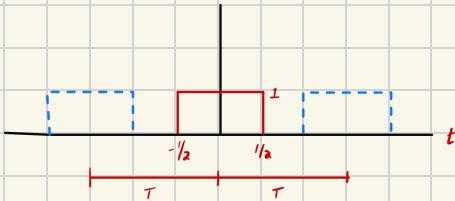
$$\frac{1}{2} \left(\frac{1}{2} \right) + \sum_{\substack{n=-\infty \\ n \text{ odd}}}^{\infty} \left(\frac{1}{2+jn\pi} \right) \frac{1}{jn\pi} e^{jn\pi t}$$

Chapter 7

Fourier Transform and LTI System Response to Energy Signals

Recall that in an LTI system, the output to a periodic input is also periodic

What if $f(t)$ is not periodic
aperiodic



• Fourier Transform

$$\begin{aligned} f_T(t) &= \sum_{n=-\infty}^{\infty} F_n e^{jn\omega_0 t} = \sum_{n=-\infty}^{\infty} \left(\frac{1}{T} \int_{-T/2}^{T/2} f(s) e^{-jn\omega_0 s} ds \right) e^{jn\omega_0 t} = \sum_{n=-\infty}^{\infty} \frac{\omega_0}{2\pi} \int_{-\pi/\omega_0}^{\pi/\omega_0} f(s) e^{-jn\omega_0 s} ds \cdot e^{jn\omega_0 t} = \\ &= \frac{1}{2\pi} \sum_{n=-\infty}^{\infty} \left(\int_{-\pi/\omega_0}^{\pi/\omega_0} f(s) e^{-jn\omega_0 s} ds \right) e^{jn\omega_0 t} \cdot \omega_0 = \\ &= \frac{1}{2\pi} \sum_{n=-\infty}^{\infty} F(n\omega_0) e^{jn\omega_0 t} \cdot \omega_0 \quad \text{define as } F(n\omega_0) \quad \rightarrow \omega_0 \rightarrow 0 \\ &\rightarrow \frac{1}{2\pi} \int_{-\infty}^{\infty} F(\omega) e^{j\omega t} d\omega = f(t) \end{aligned}$$

Fourier Transform Pairs

$$F(\omega) = \int_{-\infty}^{\infty} f(t) e^{-j\omega t} dt \quad \in \mathbb{C} \quad \text{Fourier Transform}$$

$$f(t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} F(\omega) e^{j\omega t} d\omega \quad \text{inverse Fourier Transform}$$

time domain

$$f(t) \longleftrightarrow F(\omega)$$

unique transform pair

$$f(t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} F(\omega) e^{j\omega t} d\omega \rightarrow \boxed{\frac{H(\omega)}{L\{f\}}}$$

$$g(t) = \frac{1}{2\pi} \dots$$

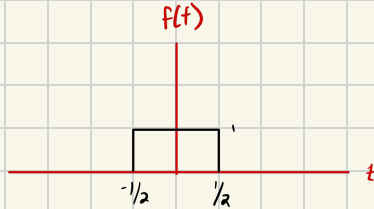
We can represent any function in terms of a Fourier Transform if $f(t)$ is absolutely integrable

i.e.

$$\int_{-\infty}^{\infty} |f(t)| dt < \infty$$

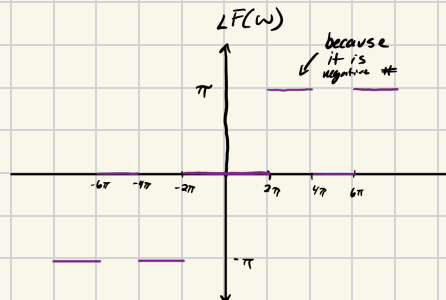
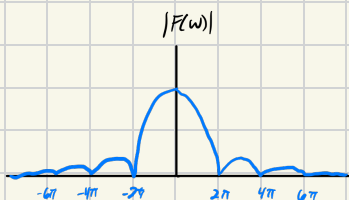
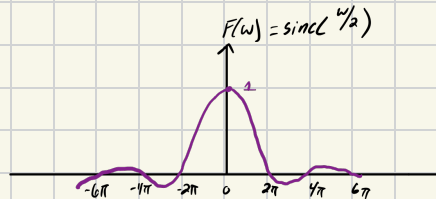
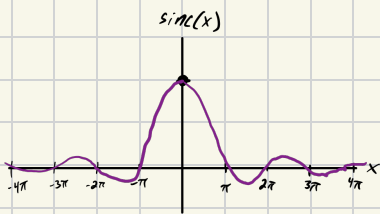
Ex)

$$f(t) = \begin{cases} 1 & |t| < 1/2 \\ 0 & \text{else} \end{cases} = \text{rect}(t)$$



$$\text{sinc}(x) = \frac{\sin(x)}{x}$$

$$\begin{aligned} F(\omega) &= \int_{-\infty}^{\infty} f(t) e^{-j\omega t} dt = \int_{-1/2}^{1/2} 1 e^{-j\omega t} dt = \\ &= \left. \frac{e^{-j\omega t}}{-j\omega} \right|_{-1/2}^{1/2} = \frac{e^{-j\omega(1/2)} - e^{-j\omega(-1/2)}}{-j\omega} = \left(\frac{e^{-j\frac{\omega}{2}} - e^{j\frac{\omega}{2}}}{-j\omega} \right) \frac{2}{2} = \frac{2 \sin(\frac{\omega}{2})}{\omega} = \frac{\sin(\frac{\omega}{2})}{\frac{\omega}{2}} = \text{sinc}\left(\frac{\omega}{2}\right) \end{aligned}$$



Doing Prof Schuh's lectures

$$P_{avg} = \frac{1}{T} \int_0^T |f(t)|^2 dt \quad \text{st. } |f(t)|^2 = f(t) \cdot f^*(t)$$

$$= \left(\sum_{n=-\infty}^{\infty} F_n e^{jn\omega_0 t} \right) \left(\sum_{m=-\infty}^{\infty} F_m^* e^{-jm\omega_0 t} \right)$$

$$= \sum_{n=-\infty}^{\infty} \sum_{m=-\infty}^{\infty} F_n F_m^* e^{j(n-m)\omega_0 t}$$

$$P_{avg} = \frac{1}{T} \int_0^T \sum_{n=-\infty}^{\infty} \sum_{m=-\infty}^{\infty} F_n F_m^* e^{j(n-m)\omega_0 t} dt$$

$$= \frac{1}{T} \sum_{n=-\infty}^{\infty} \sum_{m=-\infty}^{\infty} F_n F_m^* \int_0^T e^{j(n-m)\omega_0 t} dt \quad \leftarrow n \text{ must} = m, \text{ because otherwise you're integrating over sines + cosines which would be zero.}$$

$$= \frac{1}{T} \sum_{n=-\infty}^{\infty} F_n F_n^* (T)$$

$$= \sum_{n=-\infty}^{\infty} |F_n|^2$$

Real Valued f(t)

$$C_0 = 2|F_0| \Rightarrow |F_0| = \frac{C_0}{2}$$

$$C_n = 2|F_n| \Rightarrow |F_n| = \frac{C_n}{2}$$

↓ changing bounds

$$P_{avg} = |F_0|^2 + \sum_{n=1}^{\infty} |F_n|^2 + |F_{-n}|^2$$

$$= |F_0|^2 + 2 \sum_{n=1}^{\infty} |F_n|^2$$

$$= \left(\frac{C_0}{2}\right)^2 + 2 \sum_{n=1}^{\infty} \left(\frac{C_n}{2}\right)^2$$

$$P_{avg} = \frac{C_0^2}{4} + \sum_{n=1}^{\infty} \frac{C_n^2}{2}$$

↑ DC power ↑ similar to $P_{ac} = \frac{1}{2} V_p^2$

Distortion

Non-linear system: $y(t) = Af(t) + \epsilon f(t)^2$
 $\epsilon \ll 1$

Let's say $f(t) = \cos(\omega t)$

$$y(t) = A \cos(\omega t) + \epsilon \cos^2(\omega t)$$

$$= A \cos(\omega t) + \epsilon \left(\frac{1}{2} + \frac{1}{2} \cos(2\omega t) \right)$$

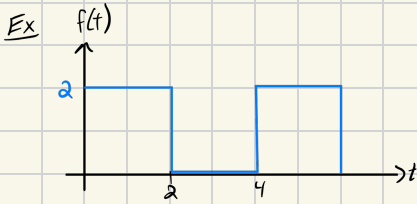
$$= \frac{1}{2} \epsilon + A \cos(\omega t) + \frac{\epsilon}{2} \cos(2\omega t)$$

1st Harmonic power: $\frac{1}{2} A^2$
 2nd Harmonic power: $\frac{\epsilon^2}{8}$

2nd Harmonic Distortion: $\frac{\frac{\epsilon^2}{8}}{\frac{1}{2} A^2} = \frac{\epsilon^2}{4 A^2}$

Total Harmonic Distortion

$$THD = \frac{\sum_{n=2}^{\infty} \frac{1}{2} C_n^2}{\frac{1}{2} C_1^2} = \frac{\sum_{n=2}^{\infty} C_n^2}{C_1^2}$$



$$\begin{aligned} P_{avg} &= \frac{1}{4} \int_0^4 f(t)^2 dt = \frac{1}{4} \left(\int_0^2 2^2 dt + \int_2^4 0^2 dt \right) \\ &= \frac{1}{4} \int_0^2 4 dt \\ &= t \Big|_0^2 \\ &= 2W \end{aligned}$$

$$f(t) = 1 + \sum_{n=1}^{\infty} \frac{4}{n\pi} \sin\left(\frac{n\pi t}{2}\right)$$

$$P_1 = \frac{1}{2} C_1^2 = \frac{1}{2} \left(\frac{4}{\pi}\right)^2 = \frac{16}{2\pi^2} = \frac{8}{\pi^2} = 0.8106W$$

$$P_{2-\infty} = \sum_{n=2}^{\infty} \frac{1}{2} C_n^2 \approx 0.1878W$$

$$THD = \frac{P_{2-\infty}}{P_1} = \frac{0.1878}{0.8106} = 23.17\%$$

$$H(w) = \frac{1}{1+jw} \Rightarrow |H(w)| = \frac{1}{\sqrt{1+w^2}}$$

$$y(t) = \underbrace{|H(0)|}_{Y_0} (1) + \sum_{n=1}^{\infty} |H(\frac{n\pi}{2})| \left| \frac{4}{n\pi} \sin\left(\frac{n\pi t}{2} + 0\right) \right|$$

$$Y_n = \frac{4}{n\pi} \left(\frac{1}{\sqrt{1+(\frac{n\pi}{2})^2}} \right) \rightarrow Y_0 = 2$$

$$P_{avg} = \frac{Y_0^2}{4} + \sum_{n=1}^{\infty} \frac{1}{2} Y_n^2 = 1.238W$$

$$P_1 = \frac{1}{2} Y_1^2 \approx 0.2538W$$

$$P_{2-\infty} = \sum_{n=2}^{\infty} \frac{1}{2} Y_n^2 = 0.00468W$$

$$THD = \frac{P_{2-\infty}}{P_1} \rightarrow 1.984\%$$

Review of periodic signals

$$f(t) = \sum_{n=-\infty}^{\infty} F_n e^{jn\omega_0 t}$$

$$\omega_0 = \frac{2\pi}{T}$$

$$F_n \rightarrow \boxed{H(\omega)} \rightarrow Y_n = H(n\omega_0) F_n$$

* What if we are no longer periodic *

* Fourier Transform *

Assume $f(t) = \sum_{n=-\infty}^{\infty} F_n e^{jn\omega_0 t} \Rightarrow F_n = F(n\omega_0)$ $\frac{1}{2\pi} \hat{F}(n\omega_0) = F(n\omega_0)$

$$f(t) = \sum_{n=-\infty}^{\infty} \frac{\omega_0}{2\pi} \hat{F}(n\omega_0) e^{jn\omega_0 t}$$

$$\int_{-T/2}^{T/2} f(t) e^{-jn\omega_0 t} dt = \sum_{n=-\infty}^{\infty} \frac{\omega_0}{2\pi} \hat{F}(n\omega_0) \int_{-T/2}^{T/2} e^{j(n-m)\omega_0 t} dt$$

n=m for $\int_{-T/2}^{T/2} e^{j(n-m)\omega_0 t} dt \neq 0$

$$= \frac{\omega_0}{2\pi} \hat{F}(n\omega_0) T \rightarrow T = \frac{2\pi}{\omega_0}$$

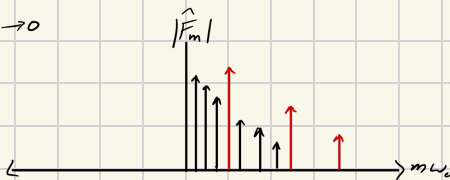
since the other $\int$ only non-zero

$$\hat{F}(n\omega_0) = \int_{-T/2}^{T/2} f(t) e^{-jn\omega_0 t} dt$$

For nonperiodic signals, $T \rightarrow \infty$, $\omega_0 \rightarrow 0$

$$m\omega_0 \Rightarrow m \dots -2, -1, 0, 1, 2, \dots$$

$$-\infty \leq m \leq \infty$$



$$\boxed{\hat{F}(\omega) = \int_{-\infty}^{\infty} f(t) e^{-j\omega t} dt} \quad \text{Fourier Transform} *$$

$\forall \omega$

$m\omega_0 \rightarrow \omega$
↑ discrete ↑ continuous

standard notation:

$$F(\omega) = \int_{-\infty}^{\infty} f(t) e^{-j\omega t} dt = \text{Forward Fourier Transform}$$

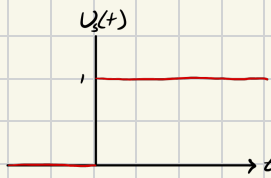
$$f(t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} F(\omega) e^{j\omega t} d\omega = \text{inverse Fourier Transform}$$

Fourier Transform
 is essentially converting
 from time domain to
 frequency domain

Fourier Transform is the
 combination of sines and cosines
 of all possible frequencies for
 aperiodic signals

Ex) Unit step function

$$u_s(t) = \begin{cases} 0 & t < 0 \\ 1 & t > 0 \end{cases}$$



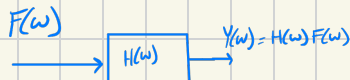
$$f(t) = e^{-t} u_s(t)$$

$$\begin{aligned} F(\omega) &= \int_{-\infty}^{\infty} f(t) e^{-j\omega t} dt = \int_{-\infty}^0 f(t) e^{-j\omega t} dt + \int_0^{\infty} f(t) e^{-j\omega t} dt \\ &= \int_0^{\infty} e^{-t} e^{-j\omega t} dt \\ &= \int_0^{\infty} e^{-(1+j\omega)t} dt \\ &= \left. \frac{e^{-(1+j\omega)t}}{-(1+j\omega)} \right|_0^{\infty} \\ F(\omega) &= \frac{1}{1+j\omega} \end{aligned}$$

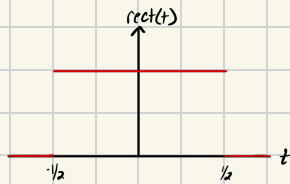
Ex) $f(t) = e^{-|t|}$



$$\begin{aligned} F(\omega) &= \int_{-\infty}^{\infty} f(t) e^{-j\omega t} dt \\ &= \int_{-\infty}^0 f(t) e^{-j\omega t} dt + \int_0^{\infty} f(t) e^{-j\omega t} dt \\ &= \int_{-\infty}^0 e^t e^{-j\omega t} dt + \int_0^{\infty} e^{-t} e^{-j\omega t} dt \\ &= \int_{-\infty}^0 e^{(1-j\omega)t} dt + \int_0^{\infty} e^{-(1+j\omega)t} dt \\ &= \left. \frac{e^{(1-j\omega)t}}{1-j\omega} \right|_{-\infty}^0 + \left. \frac{e^{-(1+j\omega)t}}{-(1+j\omega)} \right|_0^{\infty} \\ &= \frac{1}{1-j\omega} + \frac{1}{1+j\omega} \\ &= \frac{1+j\omega + 1-j\omega}{1+\omega^2} \\ F(\omega) &= \frac{2}{1+\omega^2} \end{aligned}$$



Ex) $\text{rect}(t) \rightarrow \begin{cases} 0 & |t| > 1/2 \\ 1 & |t| \leq 1/2 \end{cases}$



$$F(\omega) = \int_{-\infty}^{\infty} f(t) e^{-j\omega t} dt$$

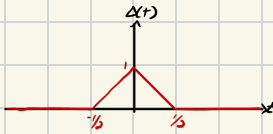
$$= \int_{-1/2}^{1/2} e^{-j\omega t} dt$$

$$\sin(x) = \frac{e^{jx} - e^{-jx}}{j2} \Rightarrow j2\sin(x) = e^{jx} - e^{-jx}$$

$$F(\omega) = \frac{e^{-j\omega t}}{-j\omega} \Big|_{-1/2}^{1/2} = \frac{1}{-j\omega} (e^{-j\frac{\omega}{2}} - e^{j\frac{\omega}{2}}) = \frac{1}{-j\omega} (-j2\sin(\frac{\omega}{2})) = \frac{2}{\omega} \sin(\frac{\omega}{2}) = \frac{\sin(\frac{\omega}{2})}{\frac{\omega}{2}} = \text{sinc}(\frac{\omega}{2})$$

$$\text{rect}(t) \longleftrightarrow \text{sinc}(\frac{\omega}{2})$$

Ex) $\Delta(t) = \begin{cases} 1-2|t| & |t| \leq 1/2 \\ 0 & |t| > 1/2 \end{cases}$



$$F(\omega) = \int_{-\infty}^{\infty} f(t) e^{-j\omega t} dt$$

$$= \int_{-1/2}^0 (1-2t) e^{-j\omega t} dt + \int_0^{1/2} (1-2t) e^{-j\omega t} dt$$

$$= \frac{2}{(-j\omega)^2} \left[2\cos(\frac{\omega}{2}) - 2 \right]$$

$$= \frac{4}{\omega^2} (\cos(\frac{\omega}{2}) - 1)$$

$$= \frac{-4}{\omega^2} (1 - \cos(\frac{\omega}{2}))$$

$$= \frac{8}{\omega^2} \sin^2(\frac{\omega}{4})$$

$$= \frac{1}{2} \left(\frac{16}{\omega^2} \right) \sin^2(\frac{\omega}{4})$$

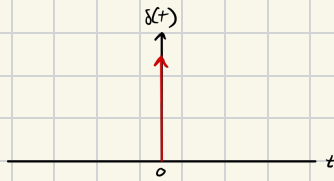
$$= \frac{1}{2} \left(\frac{\sin^2(\frac{\omega}{4})}{(\frac{\omega}{4})^2} \right)$$

$$= \frac{1}{2} \text{sinc}^2(\frac{\omega}{4})$$

$$\Delta(t) \longleftrightarrow \frac{1}{2} \text{sinc}^2(\frac{\omega}{4})$$

Ex) $\delta(t)$ (Dirac Delta function)

$$\delta(t) = \begin{cases} \infty & t=0 \\ 0 & \text{otherwise} \end{cases}$$



Properties

1) Linearity $f_1 + f_2 \leftrightarrow F_1(\omega) + F_2(\omega)$

2) Time-shift $f(t-t_0) \leftrightarrow e^{-j\omega t_0} F(\omega)$

3) Freq.-shift $F(\omega-\omega_0) \leftrightarrow e^{j\omega_0 t} f(t)$

4) Time scaling $f(ct) \leftrightarrow \frac{1}{|c|} F\left(\frac{\omega}{c}\right)$

5) Time derivative $\frac{df}{dt} \leftrightarrow j\omega F(\omega)$

Ex) $f(t) = \Delta(t - \frac{1}{2})$

$$\Delta(t) \leftrightarrow \frac{1}{\omega} \sin^2\left(\frac{\omega}{2}\right)$$

$$f(t) = \Delta(t - \frac{1}{2}) \leftrightarrow F(\omega) = \frac{1}{\omega} \sin^2\left(\frac{\omega}{2}\right) e^{-j\omega/2}$$

Ex) $f(t) = \cos(\omega_0 t)$

use inverse

$$f(t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} F(\omega) e^{j\omega t} d\omega$$

$$\cos(\omega_0 t) = \frac{e^{j\omega_0 t} + e^{-j\omega_0 t}}{2} = \frac{1}{2\pi} \int_{-\infty}^{\infty} F(\omega) e^{j\omega t} d\omega$$

$$e^{j\omega_0 t} + e^{-j\omega_0 t} = \frac{1}{\pi} \int_{-\infty}^{\infty} F(\omega) e^{j\omega t} d\omega$$

$$F(\omega) = \pi \delta(\omega - \omega_0) + \pi \delta(\omega + \omega_0)$$

Fourier Series

Periodic Signals $\Rightarrow f(t) \longleftrightarrow F_n$ used to describe a signal in Fourier domain
Discrete Frequencies, $n\omega_0$

Aperiodic Signals $\Rightarrow g(t) \longleftrightarrow G(\omega)$

All frequencies

How do we determine what freq. is important in Fourier Transform?

$$W = \int_{-\infty}^{\infty} |f(t)|^2 dt = \int_{-\infty}^{\infty} f(t) f^*(t) dt$$

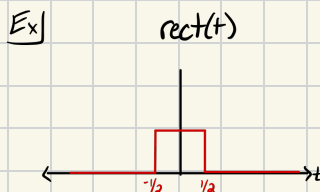
$$f(t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} F(\omega) e^{j\omega t} d\omega \quad f^*(t) = \left(\frac{1}{2\pi} \int_{-\infty}^{\infty} F(\omega) e^{j\omega t} d\omega \right)^* = \frac{1}{2\pi} \int_{-\infty}^{\infty} F^*(\omega) e^{-j\omega t} d\omega$$

$$W = \frac{1}{2\pi} \int_{-\infty}^{\infty} |F(\omega)|^2 d\omega \quad \text{Rayleigh's Theorem}$$

$$P = \sum_{n=-\infty}^{\infty} |F_n|^2 \quad \leftarrow \text{Parseval's Theorem}$$

$|F(\omega)|^2$ = energy spectrum

signal has finite $|F(\omega)|^2$, "energy signal"



$$f(t) = \text{rect}(t) \xrightarrow{F} \text{sinc}\left(\frac{\omega}{2}\right) = F(\omega)$$

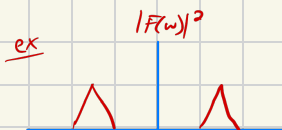
Since integrating $\text{sinc}(\frac{\omega}{2})$ may be difficult, we will use time domain

$$W = \int_{-\infty}^{\infty} |\text{rect}(t)|^2 dt = \int_{-\infty}^{\infty} \text{rect}^2(t) dt = \int_{-1/2}^{1/2} 1^2 dt = t \Big|_{-1/2}^{1/2} = 1 \text{ J}$$

Signal Classification

* $|F(\omega)|^2$ is concentrated around low frequencies
 $\Rightarrow$ low pass signal

* $|F(\omega)|^2$ is concentrated around a band of frequencies
 $=$ band pass signal



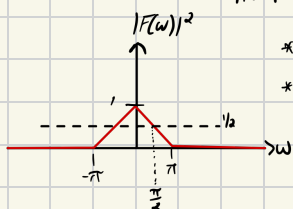
Signal Bandwidth - width of the energy spectrum

low pass bandwidth

$\Rightarrow \Omega = 2\pi B$
 Hz, Bandwidth

3dB bandwidth:

$$\frac{|F(\omega)|^2}{|F(0)|^2} = \frac{1}{2}$$



* Ω is positive

* total width is $2 \times \Omega$

$$\frac{|F(\omega)|^2}{|F(0)|^2} = \frac{1}{2} \Rightarrow |F(\omega)|^2 = \frac{1}{2}$$

$$\Omega = \frac{\pi}{2} \text{ rad/s} \Rightarrow \frac{\pi}{2} = 2\pi B \Rightarrow B = \frac{1}{4} \text{ Hz}$$

Percentage Bandwidth

$$r\omega = \frac{1}{2} \int_{-\infty}^{\infty} |F(\omega)|^2 d\omega$$

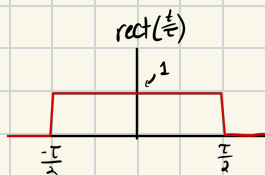
$$r \in [0, 1]$$

Ex] $f(t) = \text{rect}(\frac{t}{\tau})$

$$\frac{t}{\tau} = \frac{1}{2}$$

$$t = \frac{\tau}{2}$$

$$\omega = \int_{-\infty}^{\infty} f(t) dt = \int_{-\tau/2}^{\tau/2} 1 dt \Rightarrow \omega = \tau$$



Let's say our bandwidth is $\Omega = \frac{2\pi}{\tau}$

$$\text{rect}(\frac{t}{\tau}) \leftrightarrow \tau \text{sinc}(\frac{\omega\tau}{2}) = \tau \left(\frac{\sin(\frac{\omega\tau}{2})}{\frac{\omega\tau}{2}} \right)$$

$$r(\omega) = \frac{1}{2\pi} \int_{-\frac{\pi}{2}}^{\frac{\pi}{2}} r^2 \sin^2\left(\frac{\omega\tau}{2}\right) d\omega$$

$$r(\tau) = \frac{1}{2\pi} \int_{-\pi}^{\pi} r^2 \sin^2(x) \left(\frac{\pi}{\tau}\right) dx =$$

$$\text{let } x = \frac{\omega\tau}{2}$$

$$\frac{\pi}{\tau} dx = d\omega$$

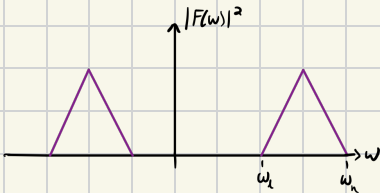
$$r(\tau) = \frac{\tau}{\pi} \int_{-\pi}^{\pi} \sin^2(x) dx$$

$$r = 0.903$$

$\Omega = \frac{2\pi}{\tau}$ is the 90.3% bandwidth

$$B = \frac{\Omega}{2\pi} \Rightarrow B = \frac{1}{\tau} \text{ Hz}$$

Bandpass Bandwidth



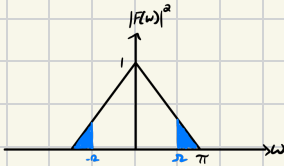
$$\Omega = \omega_{\text{upper}} - \omega_{\text{lower}} \quad (\text{positive values})$$

if $f(t)$ is real:

$$f(t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} F(\omega) e^{j\omega t} d\omega = \frac{1}{2\pi} \int_0^{\infty} |F(\omega)| \cos(\omega t + \theta) d\omega$$

the phase shift

Ex)



Ω is the 95% bandwidth

$$W = \frac{1}{2\pi} \int_{-\infty}^{\infty} |F(\omega)|^2 d\omega = \frac{1}{2\pi} \left(\frac{1}{2} (2\pi) (1) \right) \Rightarrow W = \frac{1}{2}$$

We need the area of our triangles to be 5% of W

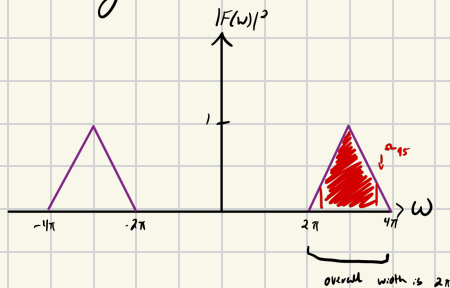
$$\frac{1}{2\pi} \left(\frac{1}{2} (\pi - \Omega) \left[\frac{\pi - \Omega}{2} \right] \right) = 0.025 \left(\frac{1}{2} \right)$$

$$\frac{1}{4\pi} (\pi - \Omega)^2 = 0.025 \left(\frac{1}{2} \right)$$

$$(\pi - \Omega)^2 = 0.05 \pi^2$$

$$\Omega = \pi (1 - \sqrt{0.05}) \text{ rad/sec}$$

Let's say now:

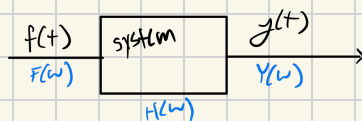


We want to find 95% bandwidth

We only shifted our bandwidth by 2, so our 95% bandwidth is twice our previous i.e.

$$\Sigma_{95\%} = 2(\Sigma_{95}) = 2\pi(1.5005)$$

$Y(\omega) = H(\omega)F(\omega)$ is the entire O state response not just steady state



Ex) $\frac{d^2 y}{dt^2} + 4\frac{dy}{dt} + 3y = u_s(t)$

$$(j\omega)^2 Y(\omega) + 4j\omega Y(\omega) + 3Y(\omega) = \frac{1}{j\omega} + \pi\delta(\omega)$$

$$\frac{dy}{dt} \leftrightarrow j\omega Y(\omega)$$

$$(3 - \omega^2 + j4\omega) Y(\omega) = \frac{1}{j\omega} [1 + j\omega\pi\delta(\omega)]$$

$$3 + j4\omega - \omega^2 = (1+j\omega)(3+j\omega)$$

$$Y(\omega) = \frac{1 + j\omega\pi\delta(\omega)}{j\omega(3 - \omega^2 + j4\omega)} \Rightarrow Y(\omega) = \frac{1 + j\omega\pi\delta(\omega)}{j\omega(1+j\omega)(3+j\omega)} = \frac{A}{j\omega} + \frac{B}{1+j\omega} + \frac{C}{3+j\omega} = \frac{1}{j\omega} + \frac{\pi\delta(\omega)}{1+j\omega} - \frac{1}{3+j\omega}$$

$$Y(\omega) = \frac{1}{j\omega} + \frac{\pi\delta(\omega)}{1+j\omega} - \frac{1}{3+j\omega} = \frac{1}{j\omega} + \frac{\pi\delta(\omega)}{1+j\omega} - \frac{1}{3+j\omega}$$

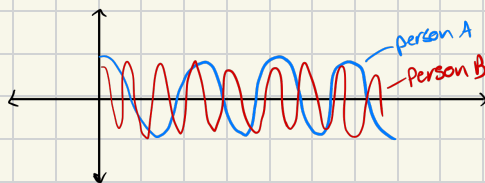
$$\frac{1}{j\omega} \leftrightarrow \frac{1}{s} \leftrightarrow \frac{1}{s} \leftrightarrow \frac{1}{s} \leftrightarrow \frac{1}{s}$$

$$y(t) = \frac{1}{6} \sin(t) - \frac{1}{2} e^{-t} u_s(t) + \frac{1}{6} e^{-3t} u_s(t) + \frac{1}{2\pi} \int_{-\infty}^{\infty} \left(\frac{\pi\delta(\omega)}{1+j\omega} - \frac{\pi\delta(\omega)}{3+j\omega} \right) e^{j\omega t} d\omega$$

$$y(t) = \frac{1}{6} \sin(t) + \frac{1}{6} - \frac{1}{2} e^{-t} u_s(t) + \frac{1}{6} e^{-3t} u_s(t) + \frac{1}{2\pi} \left(\frac{\pi}{1} e^{j0} - \frac{\pi}{3} e^{j0} \right) e^{j0}$$

$$y(t) = \frac{1}{3} u_s(t) + \frac{1}{6} e^{-3t} u_s(t) - \frac{1}{2} e^{-t} u_s(t) + \frac{1}{6}$$

Modulation property, AM signal, coherent demodulation



How do we get the information?

- occupy same frequency band + can't get information

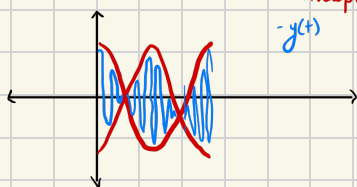
Amplitude Modulation

$$y = \underbrace{f(t)}_{\text{info}} \cos(\underbrace{\omega_c t}_{\text{carrier frequency}})$$

output

In the United States, AM radio stations use 540-1600 KHz for f_c at 10 KHz intervals

Ex) $y(t) = \underbrace{\cos(t)}_{\text{info}} \underbrace{\cos(10t)}_{\text{carrier wave}}$



Frequency Modulation

$$y(t) = f(t) \cos(\omega_c t) = \frac{1}{2} f(t) [e^{j\omega_c t} + e^{-j\omega_c t}]$$

$$y(t) = \frac{1}{2} (f(t) e^{j\omega_c t} + f(t) e^{-j\omega_c t})$$

$$Y(\omega) = \frac{1}{2} (F(\omega - \omega_c) + F(\omega + \omega_c))$$

* Modulation is not LT $\neq$ *

Ex) $f(t) = \cos(4\pi t)$

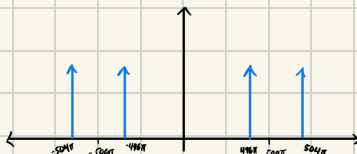
$$F(\omega) = \pi [\delta(\omega - 4\pi) + \delta(\omega + 4\pi)]$$



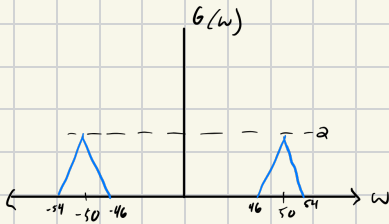
$$y(t) = f(t) \cos(500\pi t)$$

$$\omega_c = 500\pi$$

$$Y(\omega) = \frac{1}{2} [F(\omega - 500\pi) + F(\omega + 500\pi)]$$

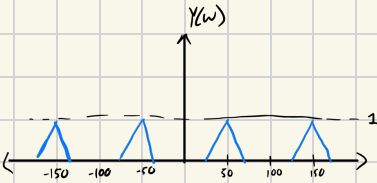


Ex)



$$y(t) = g(t) \cos(100t)$$

$$Y(\omega) = \frac{1}{2} [G(\omega - 100) + G(\omega + 100)]$$

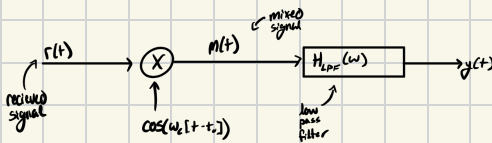


How to reconstruct a signal and get the information?

Coherent Demodulation

* Receiving many signals at once *

* An adjustable band-pass filter to "tune in" the correct station *



$f(t)$

$$\xleftrightarrow{F} F(\omega)$$

$$f(t) \cos(\omega_c t)$$

$$\xleftrightarrow[\text{Freq. Modulation}]{F} \frac{1}{2} [F(\omega - \omega_c) + F(\omega + \omega_c)]$$

$$r(t)$$

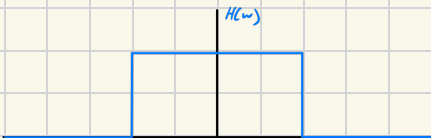
$$\xleftrightarrow[\text{time delay}]{F} \frac{1}{2} (F(\omega - \omega_c) e^{j\omega t_0} + F(\omega - \omega_c) e^{-j\omega t_0})$$

$$r(t) = f(t + t_0) \cos(\omega_c(t + t_0))$$

$$m(t) = f(t + t_0) \cos^2(\omega_c(t + t_0))$$

$$m(t) = f(t + t_0) \left[\frac{1}{2} + \frac{1}{2} \cos(2\omega_c(t + t_0)) \right]$$

$$\longleftrightarrow M(\omega) = \frac{1}{2} F(\omega) e^{j\omega t_0} + \frac{1}{4} [F(\omega - 2\omega_c) e^{j\omega t_0} + F(\omega + 2\omega_c) e^{j\omega t_0}]$$



$$Y(\omega) = M(\omega) H(\omega)$$

$$= \frac{1}{2} F(\omega) e^{j\omega t_0}$$

$$\uparrow$$

$$y(t) = \frac{1}{2} f(t + t_0)$$

* When implementing this, must

know ω_c AND at the receiving end

to use this *

Envelope Detection

Desired: $f(t)$

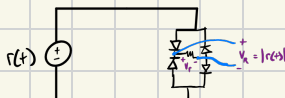
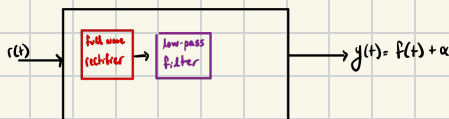
at send: $f(t) + \alpha \cos(\omega_c t)$
 $\alpha > 0$
 ω_c carrier frequency

Modulation: $S(t) = (f(t) + \alpha) \cos(\omega_c t)$

Receiving End: $r(t) = (f(t) + \alpha) \cos(\omega_c t)$ * there will be t -delay, but we are ignoring it for simplicity *

Envelope: $|f(t) + \alpha| = f(t) + \alpha$ because of init cond.

Envelope Detector



$$|r(t)| = |(f(t) + \alpha) \cos(\omega_c t)| = |f(t) + \alpha| |\cos(\omega_c t)|$$

$$= (f(t) + \alpha) |\cos(\omega_c t)|$$

$$T = \frac{1}{f_c} = \frac{2\pi}{\omega_c} = \frac{\pi}{\omega_c}$$

$$\rightarrow \omega_c = \frac{2\pi}{T} = 2\omega_c \rightarrow |\cos(\omega_c t)| = \frac{1}{\pi} \sum_{n=1}^{\infty} \frac{4}{n\pi} \cos(2n\omega_c t)$$

Design a filter that looks like this:

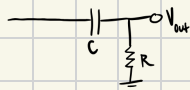


By designing the filter like this, we eliminate all higher frequencies of ω

$$y(t) = H(\omega) |r(t)|$$

$$= \left[\frac{1}{\pi} (f(t) + \alpha) \right] \left(\frac{\pi}{2} \right)$$

$$y(t) = f(t) + \alpha$$



* This requires a tunable low pass filter *

Superheterodyne

1) Mix $s(t) = (f(t) + \alpha) \cos(\omega_c t)$ with $\cos(\omega_{LO} t)$
Local Oscillator

$$m(t) = (f(t) + \alpha) \cos(\omega_c t) \cos(\omega_{LO} t)$$

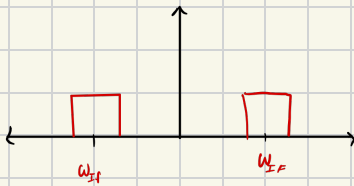
$$m(t) = \frac{(f(t) + \alpha)}{2} [\cos(\omega_c - \omega_{LO} t) + \cos(\omega_c + \omega_{LO} t)]$$

$$\omega_{LO} = \omega_c + \omega_{IF}$$

center frequency f_{IF} is fixed. f_{IF} tends to be = 455 kHz

$$m(t) = \frac{f(t) + \alpha}{2} [\cos(-\omega_{IF} t) + \cos(2\omega_c + \omega_{IF} t)]$$

2) Send through a fixed BPF



$$y(t) = \frac{f(t) + \alpha}{2} \cos(\omega_{IF} t)$$

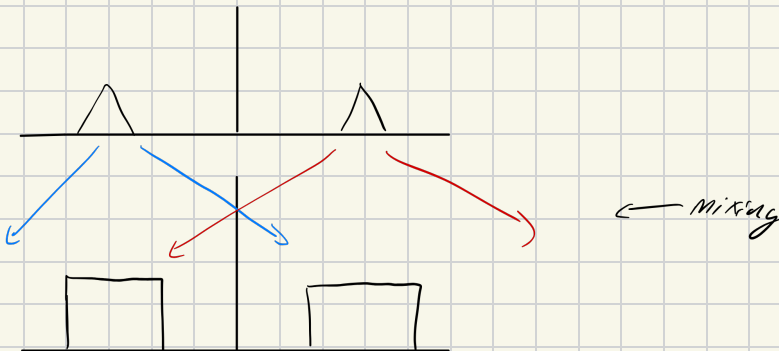
send through envelope detector

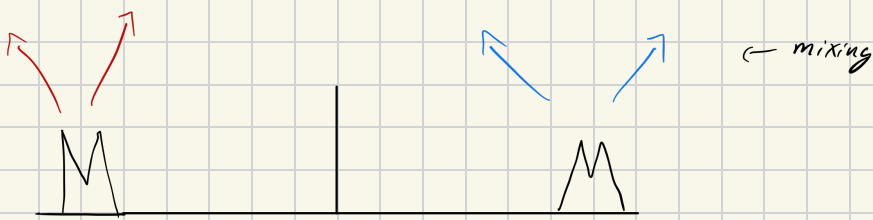
$$\frac{f(t) + \alpha}{2} = \text{output}$$

ω_{LO} : Local LC Circuit that we tune by adjusting the capacitance of the capacitor

$$\omega_{LO} = \frac{1}{\sqrt{LC}}$$

Image Station Problem





$$\omega_{ca} = \omega_{ci} + 2\omega_{IF}$$

Image
Station

$$m(t) = \frac{f(t) + a}{2} (\cos(\omega_c - \omega_i)t) + \cos(\omega_c + \omega_i)t)$$

$$\omega_{LO} = \omega_{ci} + \omega_{IF}$$

$$= \omega_{ca} - \omega_{LO}$$

$$= (\omega_{ci} + 2\omega_{IF}) - (\omega_{ci} + \omega_{IF})$$

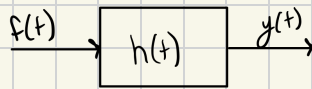
$$= \omega_{IF}$$

← Will interfere w actual desired freq.

We can use pre-selector p. 276 in textbook

Convolution & FT convolution properties

Convolution: how the shape of one function is modified by another



Convolution is commutative

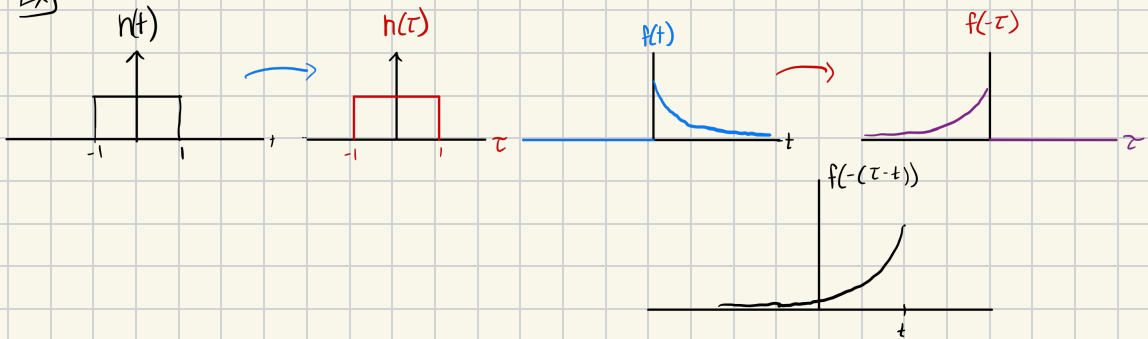
$$y(t) = f(t) * h(t)$$

↑ convolved with

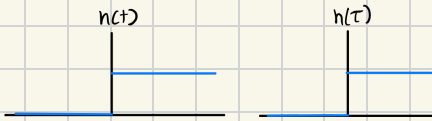
$$y(t) = \int_{-\infty}^{\infty} h(\tau) f(t-\tau) d\tau$$

↑
dummy variable

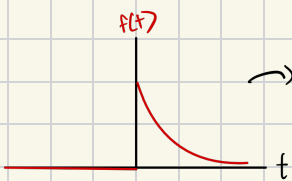
Ex)



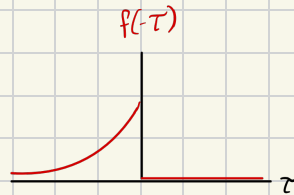
Ex) $h(t) = u_3(t)$



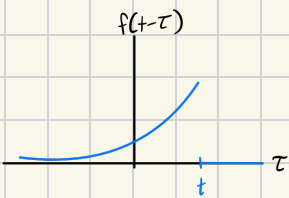
$f(t) = e^{-t} u_3(t)$



$f(\tau) = e^{-(t-\tau)} u_3(-\tau)$
 $= e^{\tau} u_3(-\tau)$



$f(t-\tau) = e^{-(t-\tau)} u_3(t-\tau) = e^{\tau-t} u_3(-(\tau-t))$



$y(t) = \int_{-\infty}^{\infty} h(\tau) f(t-\tau) d\tau$

look when the functions overlap
 $\rightarrow$



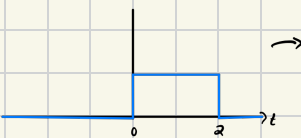
t can be any value.
 for what value of t do we see the functions begin to overlap?

$t - \tau = 0$: overlap

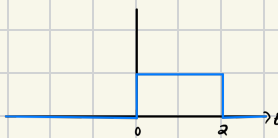
$y(t) = \int_0^t (1) e^{-(t-\tau)} d\tau = \int_0^t e^{-t+\tau} d\tau = \int_0^t e^{-t} e^{\tau} d\tau = e^{-t} \int_0^t e^{\tau} d\tau = e^{-t} (e^{\tau})_0^t = e^{-t} (e^t - 1) = (1 - e^{-t}) u_3(t)$

Ex)

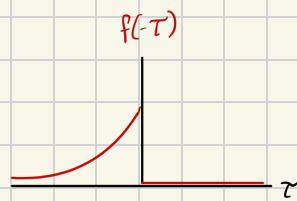
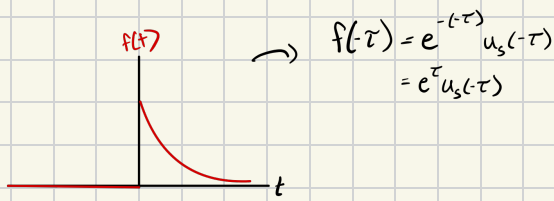
$h(t) = \text{rect}(\frac{t-1}{2})$



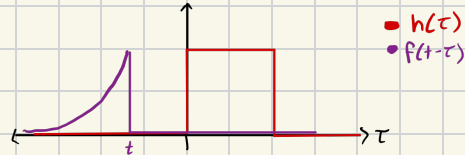
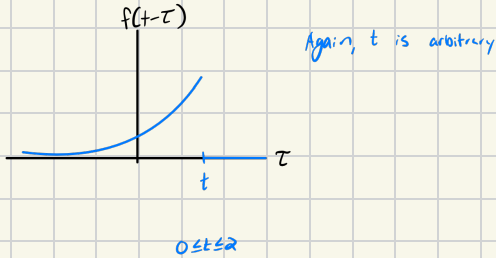
$h(t) = \text{rect}(\frac{\tau-1}{2})$



$f(t) = e^{-t} u_3(t)$

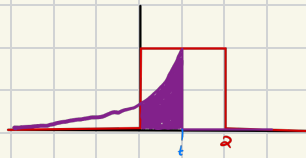


$$f(t-\tau) = e^{-(t-\tau)} u_3(t-\tau) = e^{\tau-t} u_3(t-\tau)$$

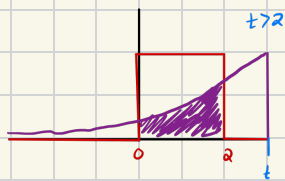


$t=0$: overlap

$t=2$: other consideration



$$\int_0^t e^{-(t-\tau)} d\tau = (1-e^{-t}) u_3(t)$$



$$y(t) = \int_0^2 e^{-(t-\tau)} d\tau = e^{-t} (e^{\tau}) \Big|_0^2 = e^{-t} (e^2 - 1) \Rightarrow (e^{-(t-2)} - e^{-t}) u(t-2)$$

$$y(t) = \begin{cases} 0 & t < 0 \\ (1-e^{-t}) u_3(t) & 0 \leq t < 2 \\ (e^{-(t-2)} - e^{-t}) u_3(t-2) & 2 \leq t \end{cases}$$

Properties of Convolution

1) $y(t) = f(t) * h(t) = h(t) * f(t)$

4) $y(t - (t_1 + t_2)) = h(t - t_1) * f(t - t_2)$

2) $y(t) = f(t) * h(t)$

$y(t - t_0) = f(t - t_0) * h(t) = f(t) * h(t - t_0)$

5) $(f_1 + f_2) * h(t) = f_1 * h(t) + f_2 * h(t)$

3) $y(t) = h(t) * f(t)$

$\frac{\partial y}{\partial t} = \frac{\partial h}{\partial t} * f(t)$

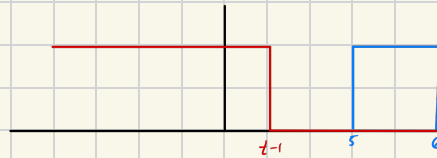
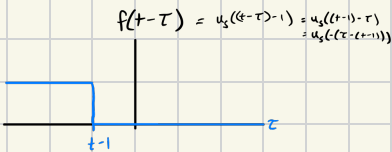
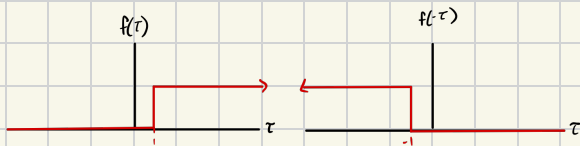
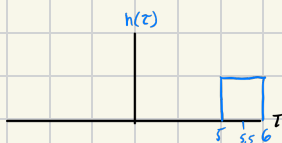
Graphical Convolution

Ex) $\text{rect}\left(\frac{t-1}{2}\right)$ $f(t) = e^{-t} u_3(t)$

$$\text{rect}\left(\frac{t-1}{2}\right) = u_3(t) - u_3(t-2)$$

$$\begin{aligned} y(t) &= \text{rect}\left(\frac{t-1}{2}\right) * e^{-t} u_3(t) \\ &= (u_3(t) - u_3(t-2)) * e^{-t} u_3(t) \\ &= u_3(t) * e^{-t} u_3(t) - u_3(t-2) * e^{-t} u_3(t) \\ &= u_3(t) * e^{-t} u_3(t) - u_3(t) * e^{-(t-2)} u_3(t-2) \\ &= (1 - e^{-t}) u_3(t) - (1 - e^{-(t-2)}) u_3(t-2) \end{aligned}$$

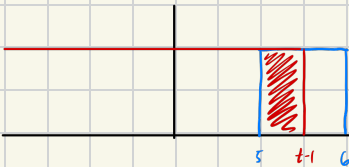
Ex) $y(t) = \underbrace{\text{rect}(t-5.5)}_{h(t)} * u_3(t-1)$



$$\begin{aligned} t-1 &= 5 \\ t &= 6 \end{aligned}$$

$$\begin{aligned} t-1 &= 6 \\ t &= 7 \end{aligned}$$

$$6 \leq t < 7$$

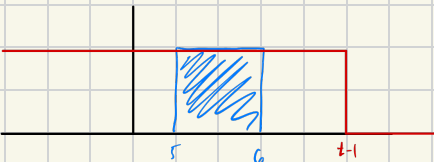


$$6 \leq t < 7$$

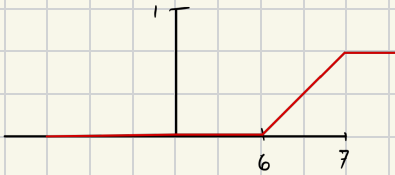
$$y(t) = \int_5^{t-1} (1) d\tau = \int_5^{t-1} d\tau = \tau \Big|_5^{t-1} = t-1-5 = \boxed{t-6 = y(t)}$$

$$y(t) = \begin{cases} 0 & t < 6 \\ t-6 & 6 \leq t < 7 \\ 1 & t \geq 7 \end{cases}$$

$$t \geq 7$$



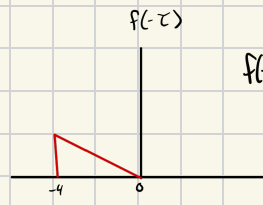
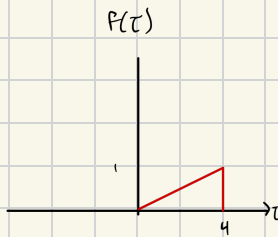
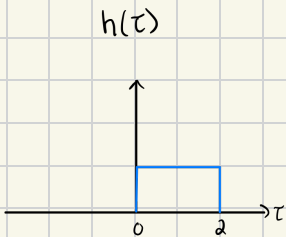
$$y(t) = 1$$



Convolution gives the Zero-state solution
so does solving a system in frequency domain.

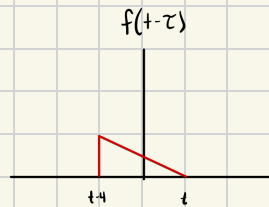
Convolution Examples

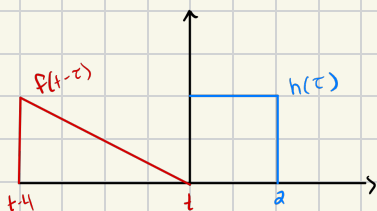
Ex) $\text{rect}\left(\frac{t-1}{2}\right) * f(t)$ st $f(t) = \begin{cases} \frac{1}{4}t & 0 \leq t \leq 4 \\ 0 & \text{otherwise} \end{cases}$



$$f(-\tau) = \begin{cases} -\frac{1}{4}\tau & -4 \leq \tau \leq 0 \\ 0 & \text{else} \end{cases}$$

$$\begin{aligned} f(t-\tau) &= \begin{cases} \frac{1}{4}(t-\tau) & 0 \leq t-\tau \leq 4 \\ 0 & \text{else} \end{cases} \\ &= \begin{cases} -\frac{1}{4}(\tau-t) & -t \leq -\tau \leq 4-t \\ 0 & \text{else} \end{cases} \\ &= \begin{cases} \frac{1}{4}(\tau-t) & t \geq \tau > t-4 \\ 0 & \text{else} \end{cases} \end{aligned}$$





$$t < 0$$

$$y(t) = 0$$

$t = 0$: overlap

$t = 2$: overlap 2

$t = 4$: end of overlap

$$0 \leq t \leq 2$$

$$y(t) = \int_0^t \left(\frac{1}{4}(\tau - t) \right) d\tau \Rightarrow \frac{1}{4} \left(\frac{1}{2} \tau^2 - \tau t \right) \Big|_0^t = \frac{t^2}{8}$$

$$2 \leq t \leq 4$$

$$y(t) = \int_0^2 \left(\frac{1}{4}(\tau - t) \right) d\tau \Rightarrow \frac{1}{4} \left(\frac{1}{2} \tau^2 - \tau t \right) \Big|_0^2 = \frac{1}{2}(t-1)$$

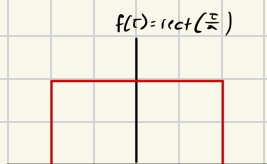
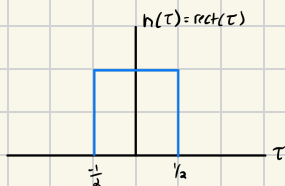
$$4 \leq t \leq 6$$

$$y(t) = \int_{t-4}^2 \left(\frac{1}{4}(\tau - t) \right) d\tau = \frac{1}{4} \left(\frac{1}{2} \tau^2 - \tau t \right) \Big|_{t-4}^2 \Rightarrow y(t) = \frac{1}{8}(t+2)(6-t)$$

$$y(t) = \begin{cases} \frac{1}{8}t^2 & 0 \leq t < 2 \\ \frac{1}{2}(t-1) & 2 \leq t < 4 \\ \frac{1}{8}(t+2)(6-t) & 4 \leq t < 6 \\ 0 & \text{else} \end{cases}$$

Ex

$$\text{rect}\left(\frac{t}{2}\right) * \text{rect}(t)$$



$$f(t-\tau)$$

$$f(t-\tau) = \text{rect}\left(\frac{t-\tau}{2}\right)$$

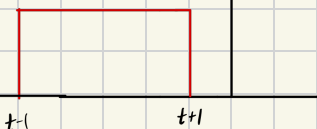
$$= \text{rect}\left(-\frac{\tau-t}{2}\right)$$

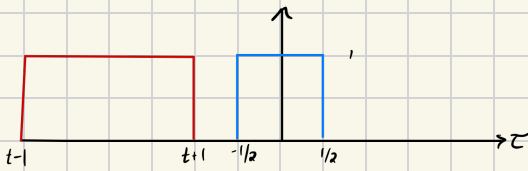
$$= \text{rect}\left(\frac{\tau-t}{2}\right)$$

$$\frac{\tau-t}{2} = \frac{1}{2} \Rightarrow \tau - t = 1$$

$$\tau = t+1$$

$$\tau = t-1$$





$$t-1 = \frac{-1}{-1} \Rightarrow t = \frac{-3}{2} \quad (\text{start of overlap})$$

$$t-1 = \frac{1}{2} \Rightarrow t = \frac{3}{2} \quad (\text{end of overlap})$$

$$t+1 = \frac{1}{2} \Rightarrow t = \frac{-1}{2} \quad (\text{blue fully enclosed by red})$$

$$t-1 = \frac{-1}{2} \Rightarrow t = \frac{1}{2} \quad (\text{blue no longer fully enclosed by red})$$

$$\frac{-3}{2} \leq t < \frac{-1}{2}$$

$$y(t) = \int_{-1/2}^{t+1} (1)(1) d\tau = \tau \Big|_{-1/2}^{t+1} = t+1 + \frac{1}{2} = t + \frac{3}{2}$$

$$\frac{-1}{2} \leq t < \frac{1}{2}$$

$$y(t) = \int_{-1/2}^{1/2} d\tau = \tau \Big|_{-1/2}^{1/2} = \frac{1}{2} + \frac{1}{2} = 1$$

$$\frac{1}{2} \leq t < \frac{3}{2}$$

$$y(t) = \int_{t-1}^{1/2} (1)(1) d\tau = \tau \Big|_{t-1}^{1/2} = \frac{1}{2} - t + 1 = \frac{3}{2} - t$$

$$y(t) = \begin{cases} t + \frac{3}{2} & \frac{-3}{2} \leq t < \frac{-1}{2} \\ 1 & \frac{-1}{2} \leq t < \frac{1}{2} \\ \frac{3}{2} - t & \frac{1}{2} \leq t < \frac{3}{2} \\ 0 & \text{else} \end{cases}$$

Properties

$$y(t) = \text{rect}\left(\frac{t}{2}\right) * \text{rect}(t) \Rightarrow (\text{rect}(t + \frac{1}{2}) + \text{rect}(t - \frac{1}{2})) * \text{rect}(t)$$

$$= \text{rect}(t + \frac{1}{2}) * \text{rect}(t) + \text{rect}(t - \frac{1}{2}) * \text{rect}(t)$$

$$y(t-t_0) = f(t-t_0) * h(t)$$

$$\text{rect}(t) * \text{rect}(t) = \Delta\left(\frac{t}{2}\right)$$

$$= \Delta\left(\frac{t + \frac{1}{2}}{2}\right) + \Delta\left(\frac{t - \frac{1}{2}}{2}\right)$$

$$\text{rect}\left(\frac{t}{B}\right) * \text{rect}\left(\frac{t}{B}\right) = B \cdot \Delta\left(\frac{t}{2B}\right)$$

Impulse and its properties

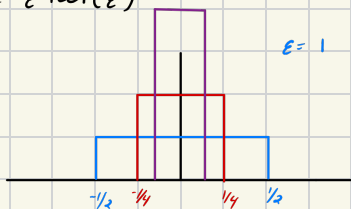
$$* a(1) = a \quad \leftarrow \text{scalar multiplication}$$

$$* M I = M \quad \leftarrow \text{matrix multiplication}$$

$$* f(t) * g(t) = f(t)$$

Approximate Function

$$p_\epsilon(t) = \frac{1}{\epsilon} \text{rect}\left(\frac{t}{\epsilon}\right)$$



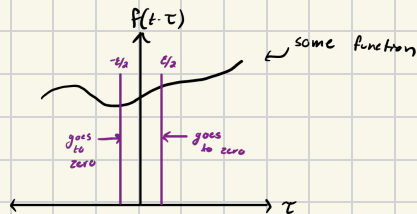
$$y(t) = f(t) * p_\epsilon(t)$$

$$= \int_{-\infty}^{\infty} \frac{1}{\epsilon} \text{rect}\left(\frac{\tau}{\epsilon}\right) f(t-\tau) d\tau$$

$$= \frac{1}{\epsilon} \int_{-\frac{\epsilon}{2}}^{\frac{\epsilon}{2}} (1) f(t-\tau) d\tau$$

$$= \frac{1}{\epsilon} \int_{-\frac{\epsilon}{2}}^{\frac{\epsilon}{2}} f(t-\tau) d\tau$$

$$\lim_{\epsilon \rightarrow 0} \frac{1}{\epsilon} \int_{-\frac{\epsilon}{2}}^{\frac{\epsilon}{2}} f(t-\tau) d\tau \rightarrow f(t)$$



Identity for convolution

$$f(t) * \delta(t) = f(t)$$

Properties of $\delta(t)$

$$1) \delta(t-t_0) * f(t) = f(t-t_0)$$

$$2) \delta(t) = \frac{du}{dt}$$

$$u(t) = \int_{-\infty}^t \delta(x) dx$$

$$3) \frac{\partial}{\partial t} (\delta(t)) * f(t) = \frac{\partial f}{\partial t}$$

$$4) \delta(t) \xrightarrow{F} 1$$

* Convolution in the time domain is the same as multiplication in the frequency domain *

$$5) \int_{-\infty}^{\infty} \delta(t-t_0) f(t) dt = f(t_0)$$

$$6) \int_{-\infty}^{\infty} \delta(t) dt = 1$$

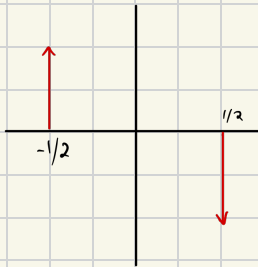
Ex) $f(t) = \text{rect}(t - \frac{1}{2})$ $h(t) = \delta(t-1) - \delta(t-3)$

$$y(t) = \text{rect}(t - \frac{1}{2}) * (\delta(t-1) - \delta(t-3))$$

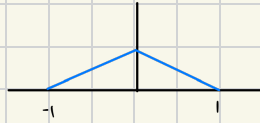
$$= \text{rect}(t - \frac{1}{2}) * \delta(t-1) - \text{rect}(t - \frac{1}{2}) * \delta(t-3)$$

$$= \text{rect}(t-1.5) - \text{rect}(t-3.5)$$

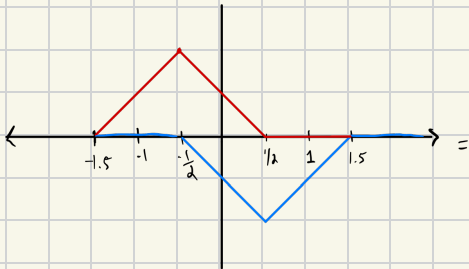
Ex)



*



=



Ex] $H(\omega) = \frac{j\omega}{1+j\omega}$

$f(t) = \text{rect}(t)$

$\mathcal{F} \updownarrow$

$F(\omega) = \text{sinc}(\frac{\omega}{2})$

$Y(\omega) = \frac{j\omega}{1+j\omega} \left(\text{sinc}(\frac{\omega}{2}) \right)$ ← Not useful
Not helpful

$f(t) = \text{rect}(t)$

$H(\omega) = \frac{j\omega}{1+j\omega} = \frac{j\omega+1-1}{1+j\omega} = \frac{1+j\omega}{1+j\omega} - \frac{1}{1+j\omega} = 1 - \frac{1}{1+j\omega}$

$h(t) = \delta(t) - e^{-t} u_s(t)$

$y(t) = (\delta(t) - e^{-t} u_s(t)) * (u_s(t+\frac{1}{2}) - u_s(t-\frac{1}{2}))$
 $= \delta(t) * u_s(t+\frac{1}{2}) - \delta(t) * u_s(t-\frac{1}{2}) - e^{-t} u_s(t) * u_s(t+\frac{1}{2}) + e^{-t} u_s(t) * u_s(t-\frac{1}{2})$
 $= u_s(t+\frac{1}{2}) - u_s(t-\frac{1}{2}) - (1 - e^{-(t+\frac{1}{2})}) u_s(t+\frac{1}{2}) + (1 - e^{-(t-\frac{1}{2})}) u_s(t-\frac{1}{2})$
 $= \text{rect}(t) - (1 - e^{-(t+\frac{1}{2})}) u_s(t+\frac{1}{2}) + (1 - e^{-(t-\frac{1}{2})}) u_s(t-\frac{1}{2})$

FT of power signals

What is a power signal?

Energy signals: $W = \int_{-\infty}^{\infty} |f(t)|^2 dt < \infty$

What about signals s.t.

$\underbrace{|f(t)|^2}_{\text{instantaneous power}} < \infty$, $W = \int_{-\infty}^{\infty} |f(t)|^2 dt \rightarrow \infty$

* Power signal: $|f(t)|^2 < \infty$, $W \rightarrow \infty$

Ex. $\cos(\omega_0 t)$, $\sin(\omega_0 t)$, $u_3(t)$

Fourier Transform of Power Signals

$$f(t) = \cos(\omega_0 t)$$

$$F(\omega) = \int_{-\infty}^{\infty} \cos(\omega_0 t) e^{-j\omega t} dt = \frac{1}{2} \int_{-\infty}^{\infty} (e^{j\omega_0 t} + e^{-j\omega_0 t}) e^{-j\omega t} dt = \frac{1}{2} \int_{-\infty}^{\infty} e^{j(\omega_0 - \omega)t} + e^{-j(\omega_0 + \omega)t} dt$$

Value is unhelpful since

$$\lim_{t \rightarrow \infty} e^{j\omega t} = \infty$$

Solve the inverse problem instead.

We know we want $f(t) = \cos(\omega_0 t) = \frac{1}{2} (e^{j\omega_0 t} + e^{-j\omega_0 t})$

$$f(t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} F(\omega) e^{j\omega t} d\omega$$

$$\frac{1}{2} [e^{j\omega_0 t} + e^{-j\omega_0 t}] = \frac{1}{2\pi} \int_{-\infty}^{\infty} F(\omega) e^{j\omega t} d\omega$$

$$\pi [e^{j\omega_0 t} + e^{-j\omega_0 t}] = \int_{-\infty}^{\infty} F(\omega) e^{j\omega t} d\omega$$

← By analyzing this, we see only two frequency values survive:

ω_0 and $-\omega_0$.

$$F(\omega) = \pi [\delta(\omega - \omega_0) + \delta(\omega + \omega_0)]$$

Ex) $f(t) = \sin(\omega_0 t) = \frac{j}{2} (e^{j\omega_0 t} - e^{-j\omega_0 t})$

$$f(t) = \frac{j}{2} (e^{j\omega_0 t} - e^{-j\omega_0 t}) = \frac{j}{2\pi} \int_{-\infty}^{\infty} F(\omega) e^{j\omega t} d\omega$$

$$j\pi (e^{j\omega_0 t} - e^{-j\omega_0 t}) = \int_{-\infty}^{\infty} F(\omega) e^{j\omega t} d\omega$$

$$F(\omega) = j\pi [\delta(\omega + \omega_0) - \delta(\omega - \omega_0)]$$

Ex) $f(t) = 1$

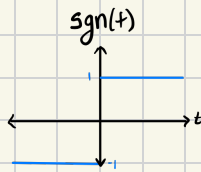
Ex) $f(t) = u_s(t) = \frac{1}{2} (\text{sgn}(t) + 1)$

$$1 = \frac{1}{2\pi} \int_{-\infty}^{\infty} F(\omega) e^{j\omega t} d\omega$$

$$2\pi = \int_{-\infty}^{\infty} F(\omega) e^{j\omega t} d\omega$$

$\omega = 0 \text{ rad/sec}$

$$F(\omega) = 2\pi \delta(\omega)$$



$1 \xleftrightarrow{F} 2\pi \delta(\omega)$

$\text{sgn}(t) \xleftrightarrow{F} \frac{2}{j\omega}$

$$f(t) = u_s(t) = \frac{1}{2} (1 + \text{sgn}(t)) \longleftrightarrow \pi \delta(\omega) + \frac{1}{j\omega}$$

Ex) Modulation

$$f(t)g(t) \xleftrightarrow{F} \frac{1}{2\pi} F(\omega) * G(\omega)$$

$$f(t) * g(t) \longleftrightarrow F(\omega) \cdot G(\omega)$$

let $g(t) = \cos(\omega_c t)$

$$f(t)\cos(\omega_c t) \xleftrightarrow{F} \frac{1}{2\pi} (F(\omega) * \pi [\delta(\omega - \omega_c) + \delta(\omega + \omega_c)])$$

$$\longleftrightarrow \frac{1}{2} (F(\omega) * \delta(\omega - \omega_c) + F(\omega) * \delta(\omega + \omega_c))$$

$$\longleftrightarrow \frac{1}{2} (F(\omega - \omega_c) + F(\omega + \omega_c))$$

Let's now try the Fourier Transform of a generic periodic function

periodic signal

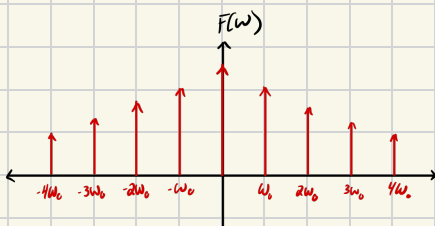
$$f(t) = \sum_{n=-\infty}^{\infty} F_n e^{jn\omega_0 t}$$

$$\omega_0 = \frac{2\pi}{T}$$

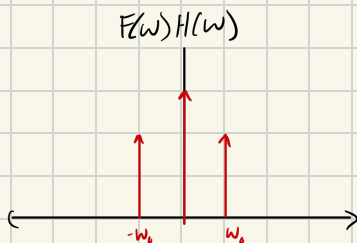
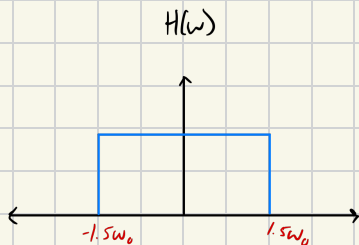
$$\sum_{n=-\infty}^{\infty} F_n e^{jn\omega_0 t} = \frac{1}{2\pi} \int_{-\infty}^{\infty} F(\omega) e^{j\omega t} d\omega$$

Integer
Multiples of
some base ω

$$F(\omega) = \sum_{n=-\infty}^{\infty} 2\pi F_n \delta(\omega - n\omega_0)$$



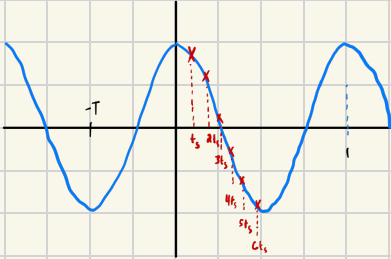
* Impulse Train: sum of delta functions
a fixed interval apart *



Sampling and analog signal reconstruction

$$f(t) = \cos(2\pi ft) \quad \leftarrow f \text{ is a frequency in Hz}$$

$$f = \frac{1}{T}$$



$f_s = \text{sampling rate}$
 $t_s = \text{sampling time}$

$$T = \frac{1}{f_s}$$

$$F[n] = f(nt_s) = \cos(2\pi f n t_s) = [f(0t_s), f(1t_s), f(2t_s), \dots]$$

↑
some integer

Reconstruction:

$$f_r(t) = \sum_n F[n] \phi_n(t)$$

basis function

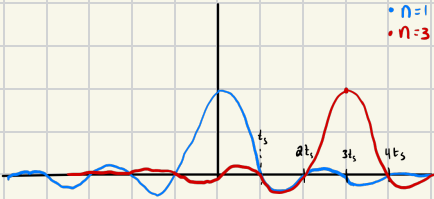
In this class, $\phi_n(t)$ will be $= \text{sinc}\left(\frac{\pi}{t_s}[t - nt_s]\right)$

$$\Rightarrow \sum_n F[n] \text{sinc}\left(\frac{\pi}{t_s}[t - nt_s]\right)$$

$$\text{sinc}(x) = \frac{\sin(x)}{x}$$

$$\phi_n = \begin{cases} 1 & t = nt_s \\ 0 & \text{all other vals of } t_s \end{cases}$$

• $n=1$
 • $n=3$



Now from continuous to discrete

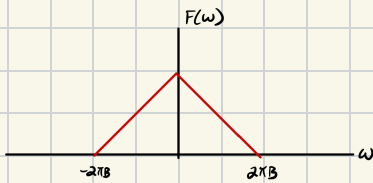
$$F[n] = \sum_t f(t) \delta(t - nt_s)$$



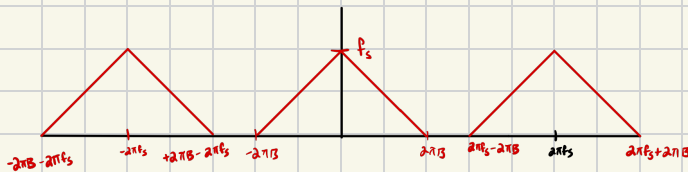
We can also take the Fourier Transform of a discrete signal

$$\begin{aligned}
 \sum_n f(t) \delta(t - nt_s) &\xrightarrow{F} \frac{1}{2\pi} \left(F(\omega) * \sum_{n=-\infty}^{\infty} \frac{2\pi}{t_s} \delta(\omega - n \frac{2\pi}{t_s}) \right) \\
 &= \frac{1}{2\pi} \sum_{n=-\infty}^{\infty} F(\omega) * \frac{2\pi}{t_s} \delta(\omega - n \frac{2\pi}{t_s}) \\
 &= \frac{1}{t_s} \sum_{n=-\infty}^{\infty} F(\omega - n \frac{2\pi}{t_s}) \\
 &= \frac{1}{t_s} \sum_{n=-\infty}^{\infty} F(\omega - n 2\pi f_s)
 \end{aligned}$$

Let's say $f(t) \rightarrow$ Bandwidth B
 $\omega = 2\pi B$



↓ Sampling



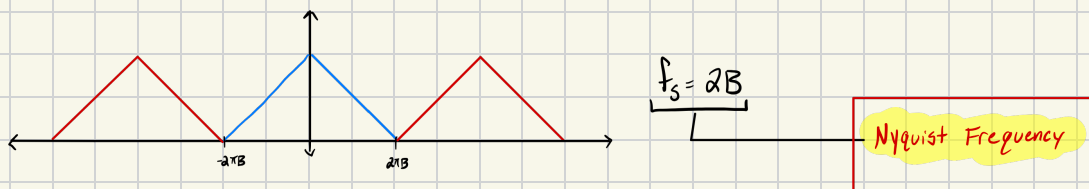
for some sampling rate:



this overlap will cause noise.

$\therefore$ the minimum: $2\pi f_s - 2\pi B = 2\pi B$

↓
 what this means



Nyquist's Sampling Theorem:

$f_s > 2B$ to reconstruct $f(t)$ from sampled signal

If $f_s < 2B$: aliasing (projecting higher frequency signal onto a lower frequency)

DAC: Digital to analog converter

$$f(n t_s) \rightarrow \left(\sum_n \delta(t - n t_s) \right) \rightarrow m(t)$$

$$\rightarrow p(t - n t_s) = \text{rect}\left(\frac{t - n t_s}{t_s}\right)$$

