

# Optimization Stories from the Field (3<sup>rd</sup> in a Series)

Marvin Gnagy, P.E., President



PMG Consulting, Inc.

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# Agenda

- Optimization practices used in the field
  - Short synopsis
- Optimization stories
  - Evaluations made
  - Technical solutions developed
  - Implementation and verification
  - Results achieved
- Questions



# Optimization Practices Used in Field

- **Define objectives/goals**
  - Why should this project be initiated
- **Develop baseline characteristics**
  - Current operations and metrics
- **Benchmark industry standards or best practices**
  - Compare where things are to where you believe they should be
- **Conduct gap analysis**
  - How do I get to the goals?
  - Tools, capital, training, operating adjustments that might be needed to achieve the goals

# Optimization Practices Used in Field

- **Establish Implementation strategy**
  - Capital needs
  - Tools, modeling, etc.
  - Operational changes
  - Adjustment protocols
  - Verification procedures
- **Track progress against objectives/goals**
  - Did you meet the objectives and goals?
  - Did you exceed the objectives and goals?
  - Did you improve water quality?
  - Did you improve performance?

# Attica, Ohio



# Attica, Ohio

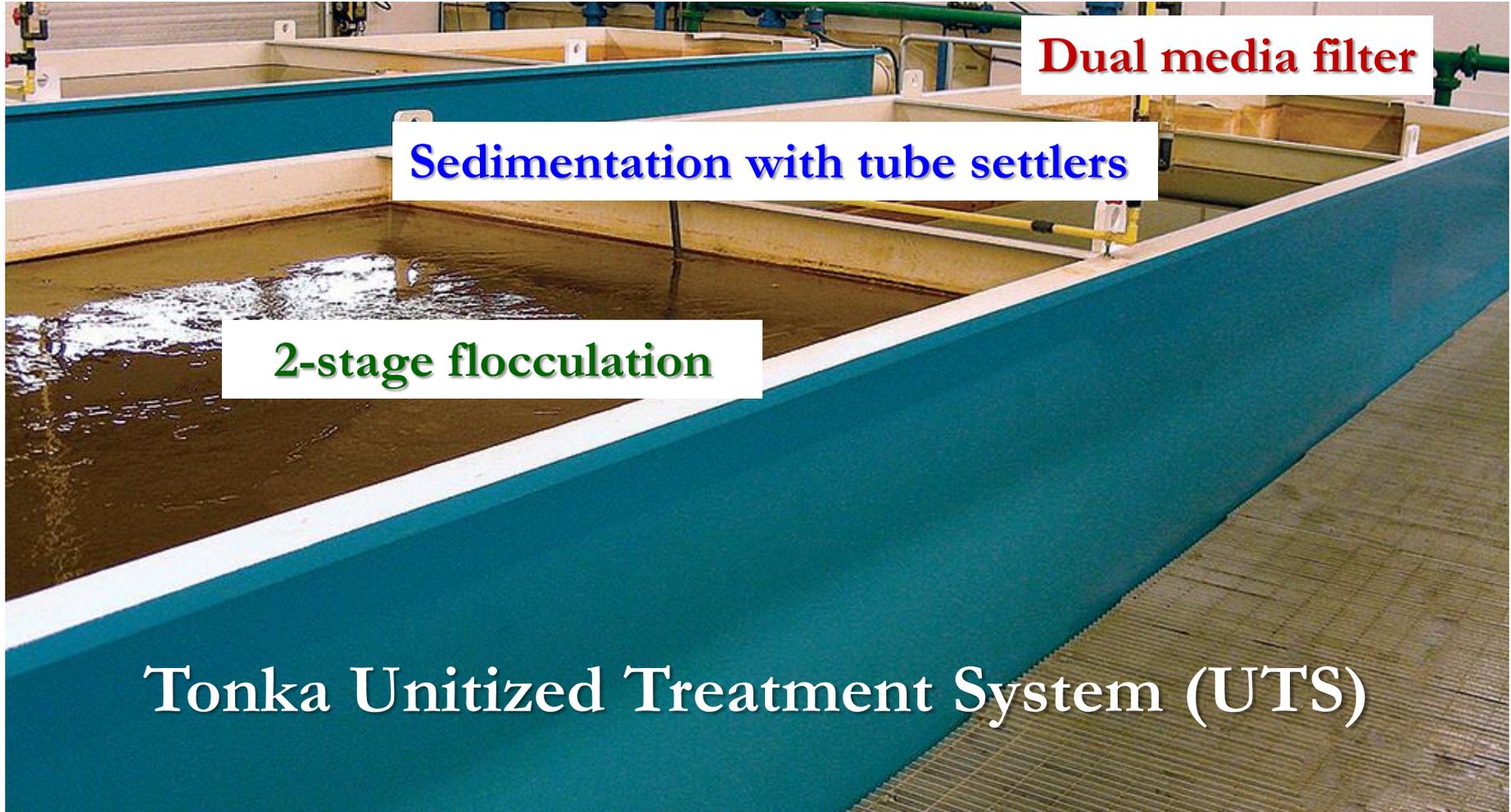
- 0.5 mgd surface water softening plant
  - Average daily production 0.105 mgd (5 hours per day)
- Small reservoir just north of plant
  - Moderate TOC, high hardness, seasonal algae
- Coagulation/pH adjustment/filtration
  - Chemical treatment
  - Solids handling
  - Disinfection and storage
- Finished water pumping to distribution system
  - 900 people

# Attica, Ohio



**Floc Speed Adjustment Initiative**

# Attica Floc Speed Adjustment



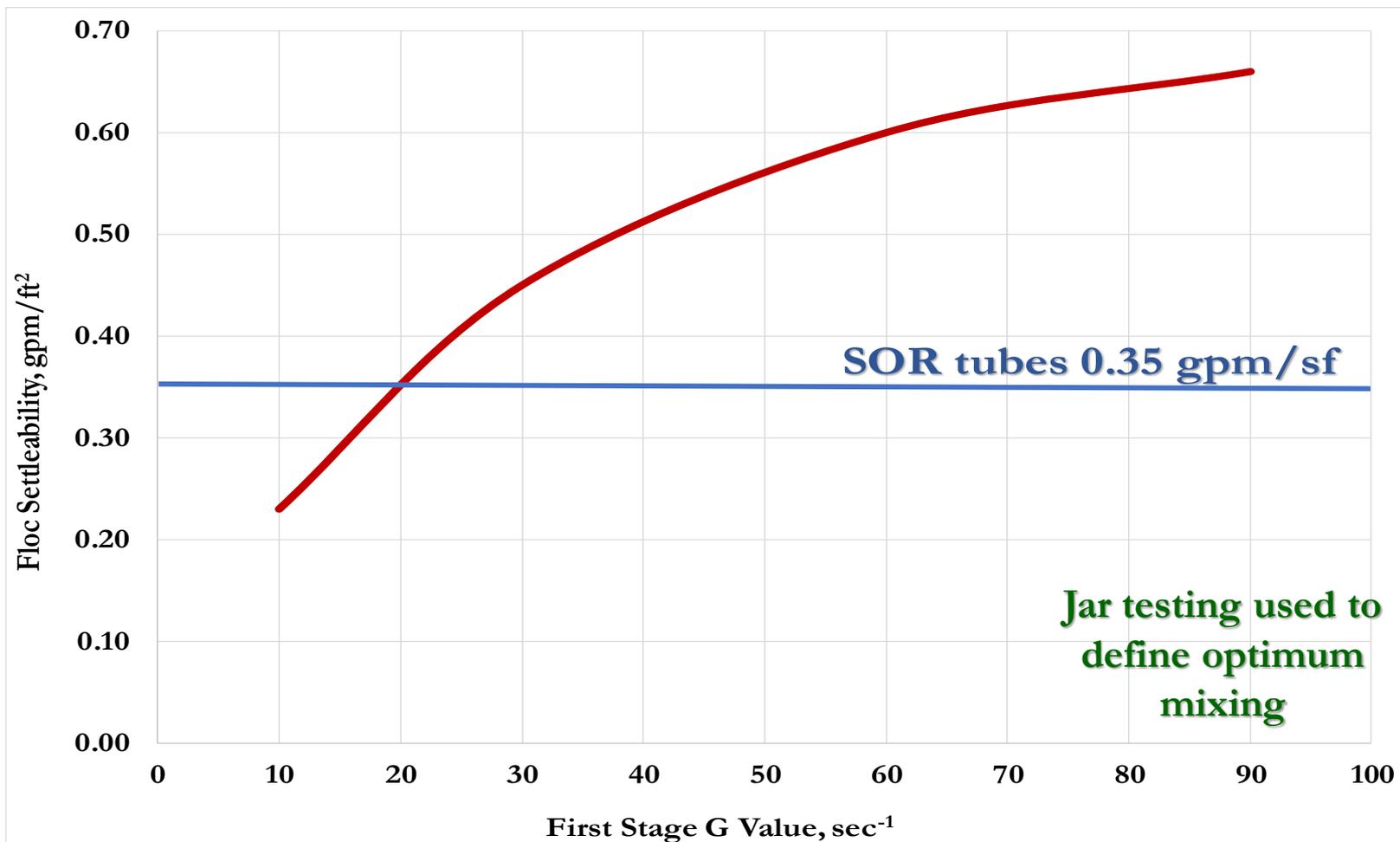
# Attica Floc Speed Adjustment

- **Initial floc mixer operation**
  - 20% speed
  - G value stage 1 -  $10 \text{ sec}^{-1}$
  - G value stage 2 -  $7 \text{ sec}^{-1}$
- **Floc characteristics**
  - 0.6 mm diameter
  - Settleability 0.22 gpm/sf
- **Settled water turbidity**
  - 8 NTU
  - Poor water clarity
  - High filter solids loading

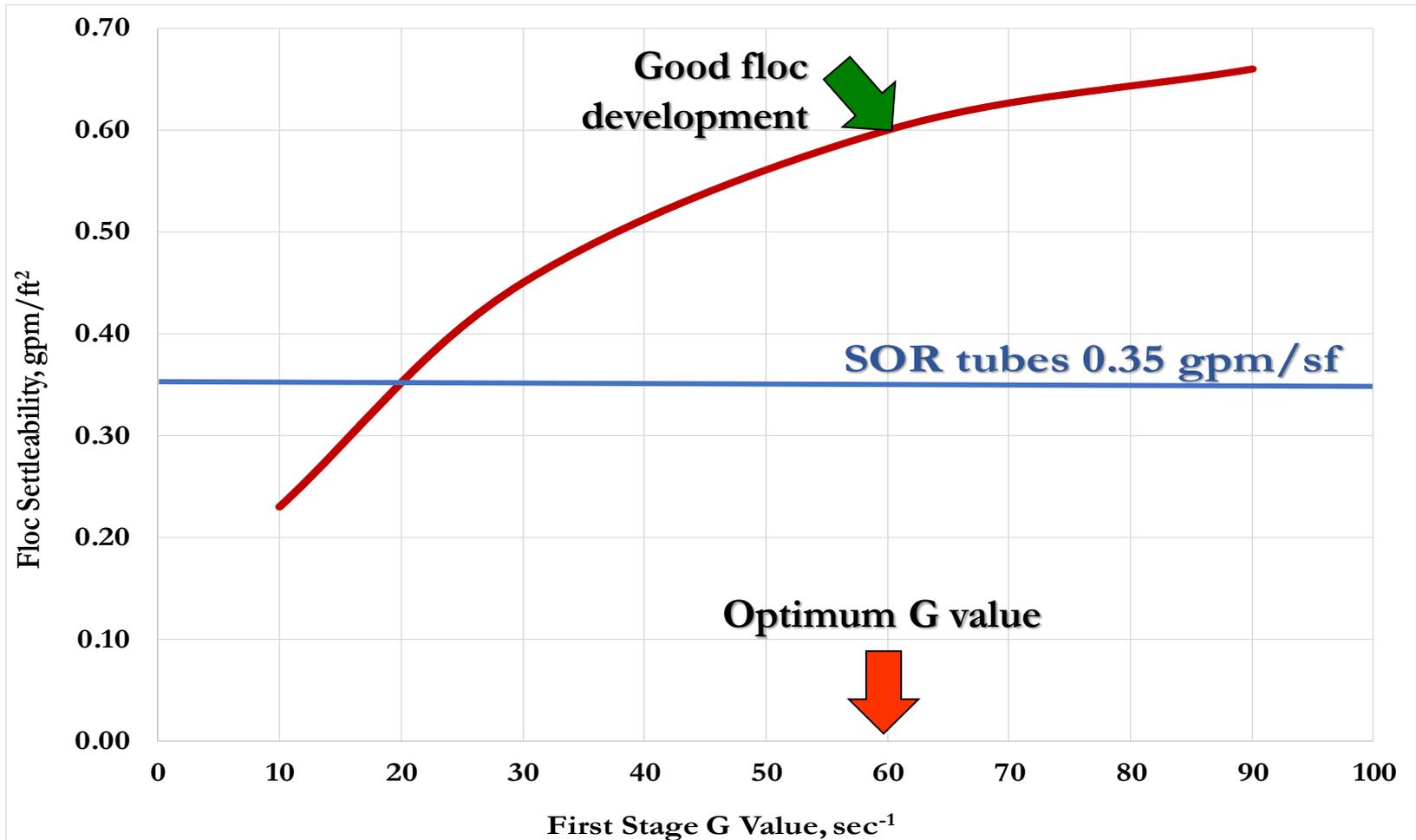
SOR tubes 0.35 gpm/sf

Cannot see tube  
settlers due to high  
settled turbidity (yes  
this is an actual  
picture)

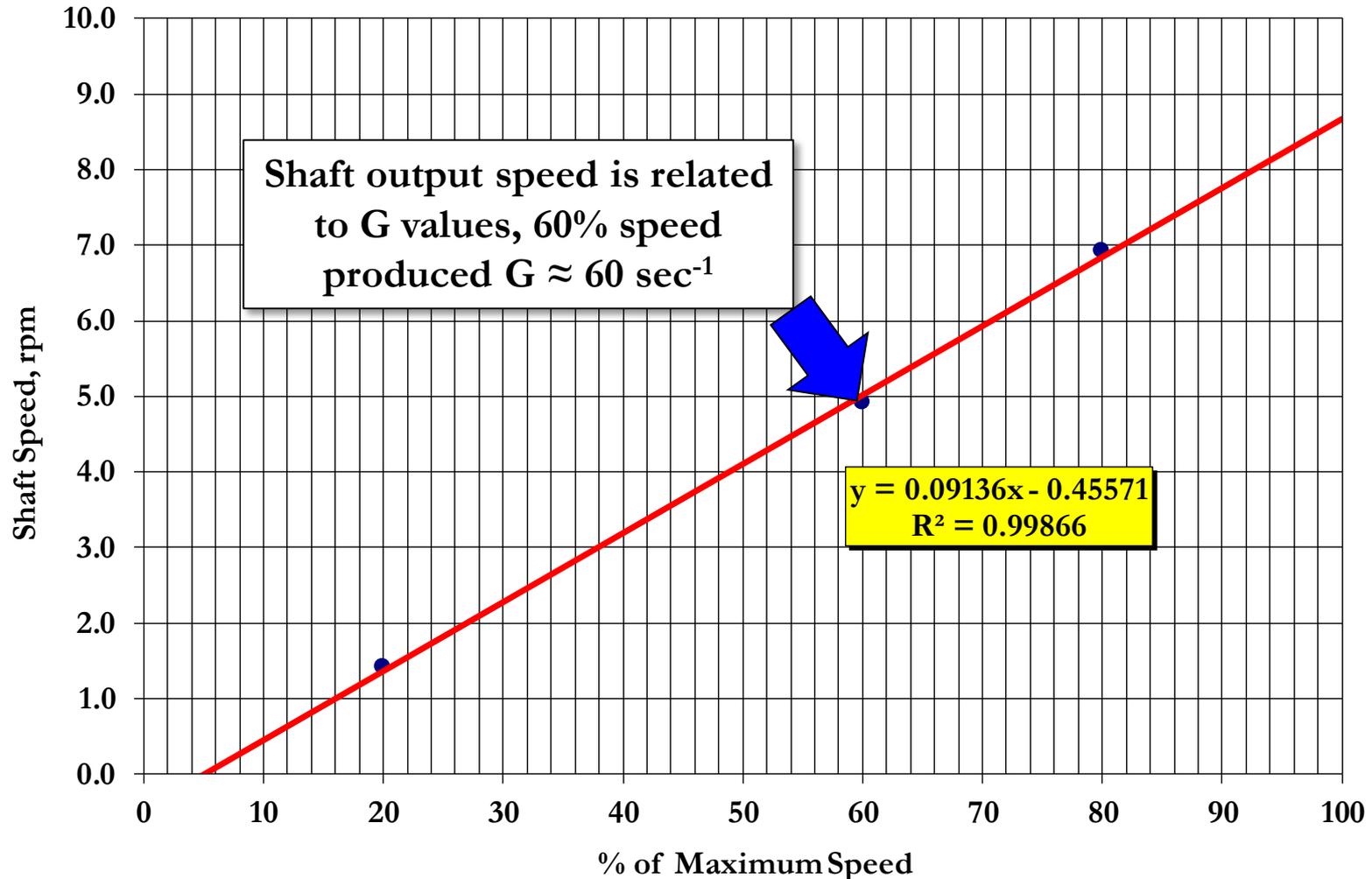
# Attica Floc Speed Adjustment



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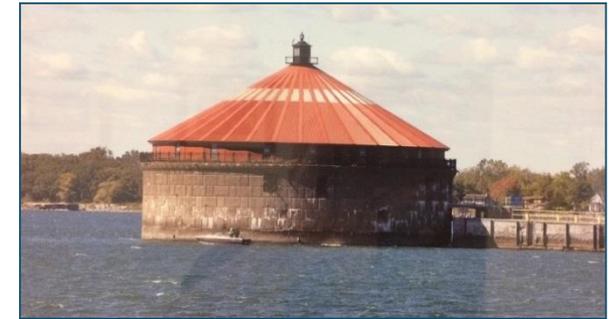
# Attica Floc Speed Adjustment

- Adjusted floc speed to 60%
  - G values
    - Stage 1 - 61 sec<sup>-1</sup>
    - Stage 2 - 43 sec<sup>-1</sup>
  - Floc size increase to 1.2 mm diameter
  - Floc settleability increased to 0.6 gpm/sf
  - Settled water turbidity decreased to 0.63 NTU
  - Extended filter run times



# Buffalo Water

- 120 mgd surface water plant, originally 1922
  - Average daily production 71 mgd
- Direct draw from eastern basin Lake Erie
  - Just upstream of Niagara River
- Coagulation/filtration plant
  - Chemical treatment
  - Solids handling
  - Disinfection and storage
- Finished water pumping to distribution system
  - 257,00 people



Lake Intake Structure

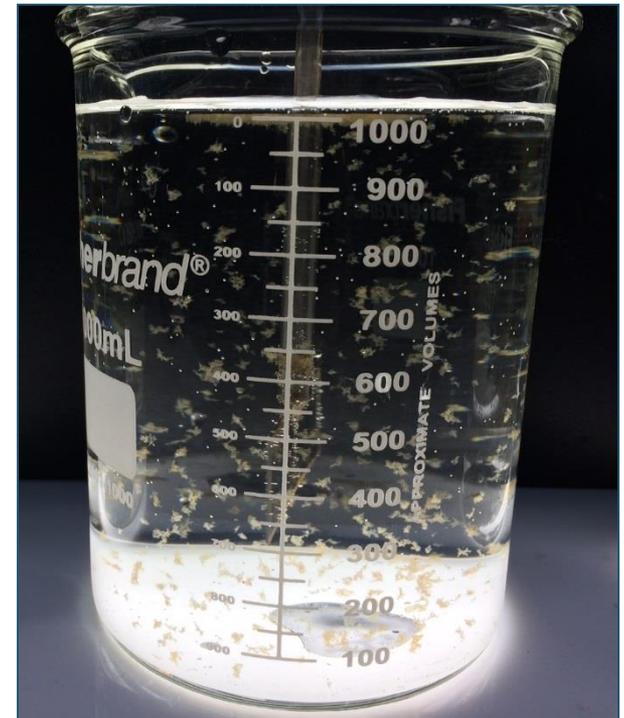
# Buffalo Water

## Floc Speed Adjustment Initiative

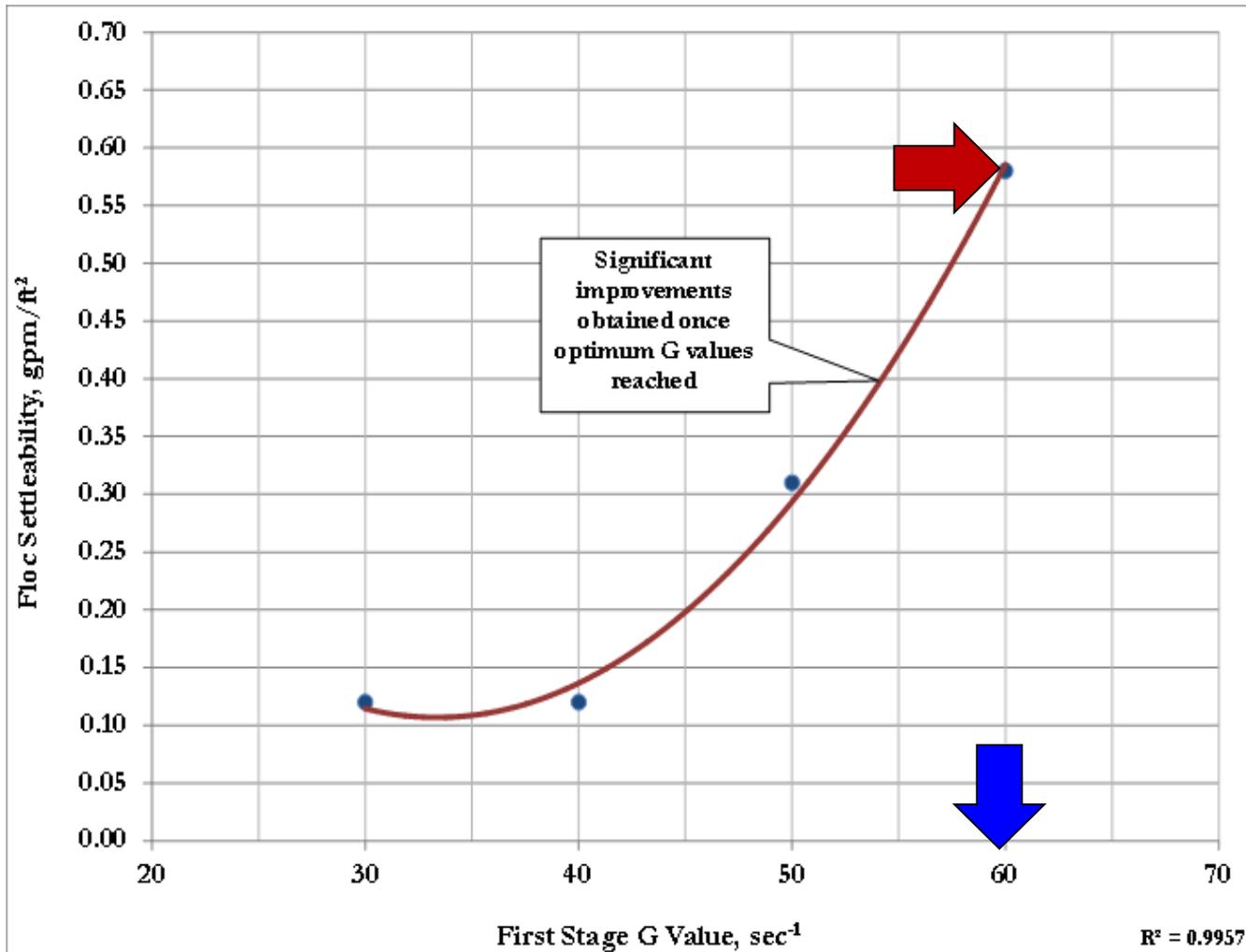


# Buffalo Floc Speed Adjustments

- **SternPac coagulant used since 1990's**
  - Raw water turbidity averages 2 NTU
  - 2016 Settled water turbidity averaged 0.28 NTU
    - Previous coagulant mixing improvements
  - Filter run times 72 hours
    - Low head loss
- **Initial floc drive operations**
  - 4 stages, VFDs
    - Stage 1 - 18 Hz, 30 G
    - Stage 2 - 12 Hz, 16 G
    - Stage 3 - 10 Hz, 14 G
    - Stage 4 - 8 Hz, 12 G



# Buffalo Floc Speed Adjustments

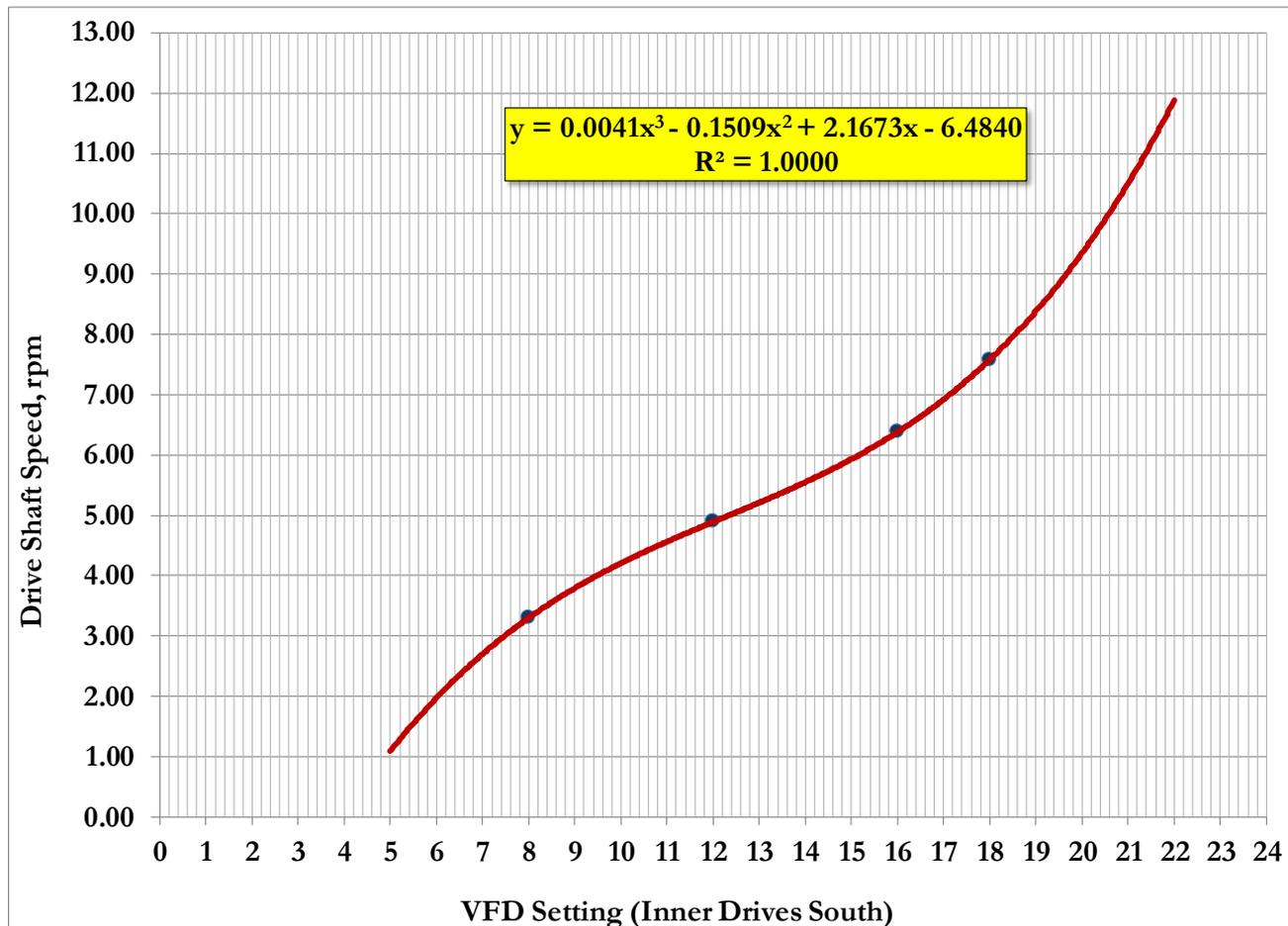


Jar testing suggested that higher G values in flocculation could improve floc development and settleability

Floc size improvement from 0.3 mm to 0.6 mm

# Buffalo Floc Speed Adjustments

- Floc drive settings and rotational speeds verified in field



# Buffalo Floc Speed Adjustments

- Floc speed adjustments suggested from G values calculations based on temperature variations
  - Stage 1 - 20.2 Hz, 60 G
  - Stage 2 - 19.4 Hz, 50 G
  - Stage 3 - 18.4 Hz, 40 G
  - Stage 4 - 16.6 Hz, 30 G
- Implemented floc speed adjustments late in 2016
  - Adjust floc drive speeds twice per year (temperature-based)
- Verified target settled water turbidity
  - 0.7 NTU to 1.0 NTU

# Buffalo Floc Speed Adjustments

- Floc speed adjustments immediately led to 13% average reduction in coagulant dosage
  - 8.5 mg/L 2016
  - 7.4 mg/L 2017
    - Settled water turbidity averaged 0.83 NTU
    - Target turbidity 0.7 NTU to 1.0 NTU
- Coagulant reduction also impacted
  - Sludge dewatering
  - Polymer conditioning
  - Cake disposal
  - Operating costs

# Buffalo Floc Speed Adjustments



# Buffalo Floc Speed Adjustments

2016 Operating Metrics	
SternPac, mg/L	8.5
Dewatering polymer, lbs/ton	11.9
Cake production, dry tons/yr	173
Cake solids, %	31.8

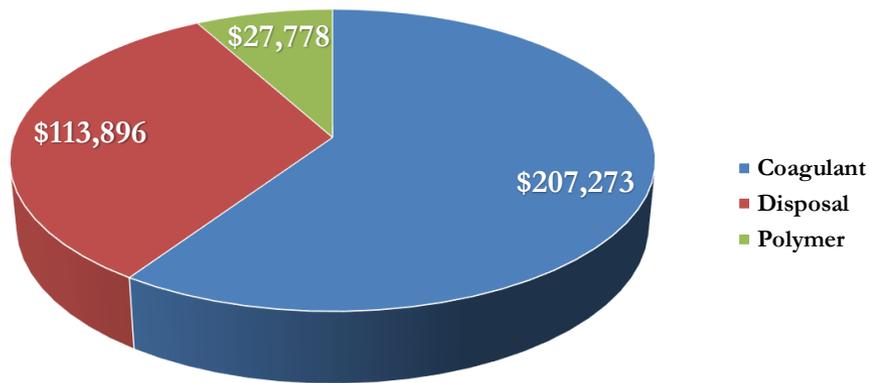


# Buffalo Floc Speed Adjustments

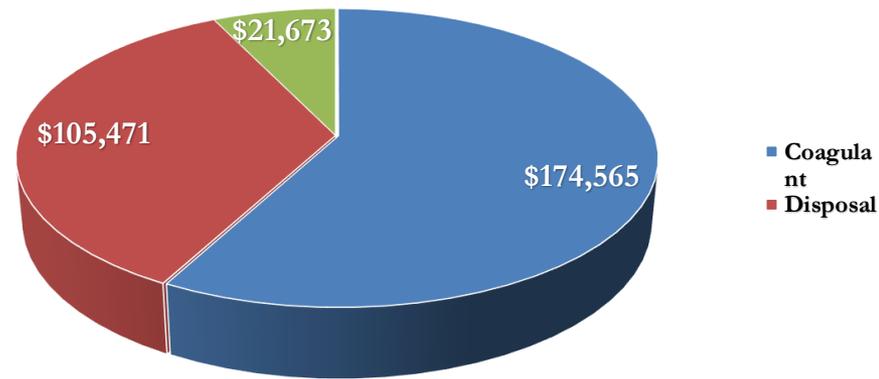
2016 Operating Metrics		2017 Operating Metrics	
SternPac, mg/L	8.5	SternPac, mg/L	7.4
Dewatering polymer, lbs/ton	11.9	Dewatering polymer, lbs/ton	10.5
Cake production, dry tons/yr	173	Cake production, dry tons/yr	154
Cake solids, %	31.8	Cake solids, %	32.7

# Buffalo Floc Speed Adjustments

2016 Annual Operating Costs  
**\$348,947**



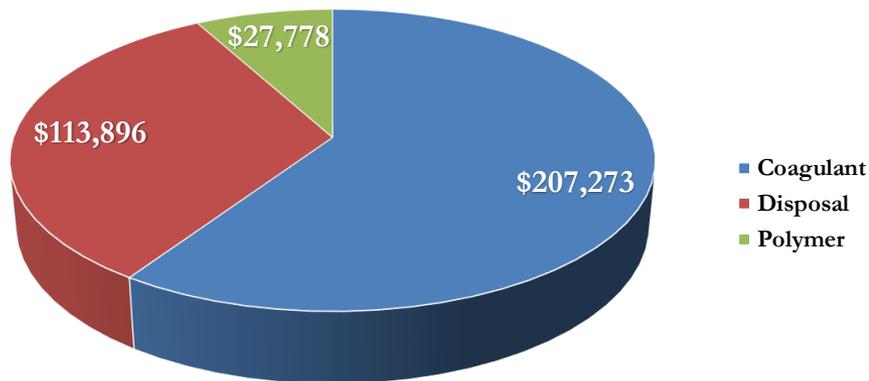
2017 Annual Operating Costs  
**\$301,709**



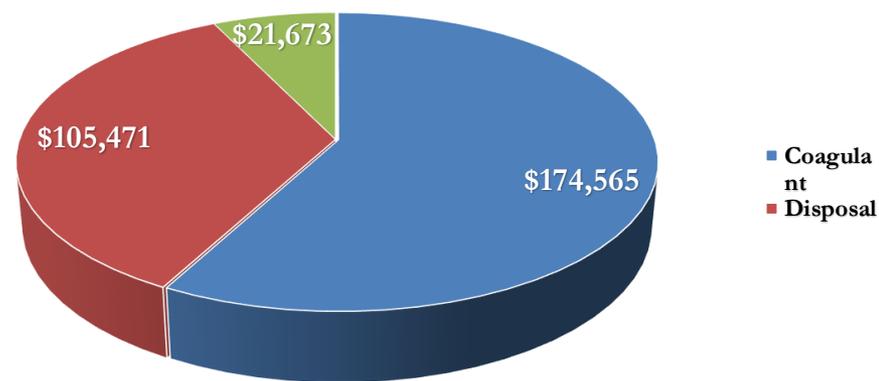
**Actual 13.5% reduction realized in annual costs**

# Buffalo Floc Speed Adjustments

2016 Annual Operating Costs  
**\$348,947**



2017 Annual Operating Costs  
**\$301,709**



**Actual 13.5% reduction realized in annual costs**

**Annual cost savings \$47,238**

# Fort Recovery, Ohio



# Fort Recovery

- 0.5 mgd ground water softening plant
  - Average daily production 0.11 mgd (7 hours per day)
- Two wells around treatment plant
  - 400 gpm, 370 gpm
- Aeration/lime-soda softening/recarbonation/filtration
  - Chemical treatment
  - Solids handling
  - Disinfection and storage
- Finished water pumping to distribution system
  - 1,400 people

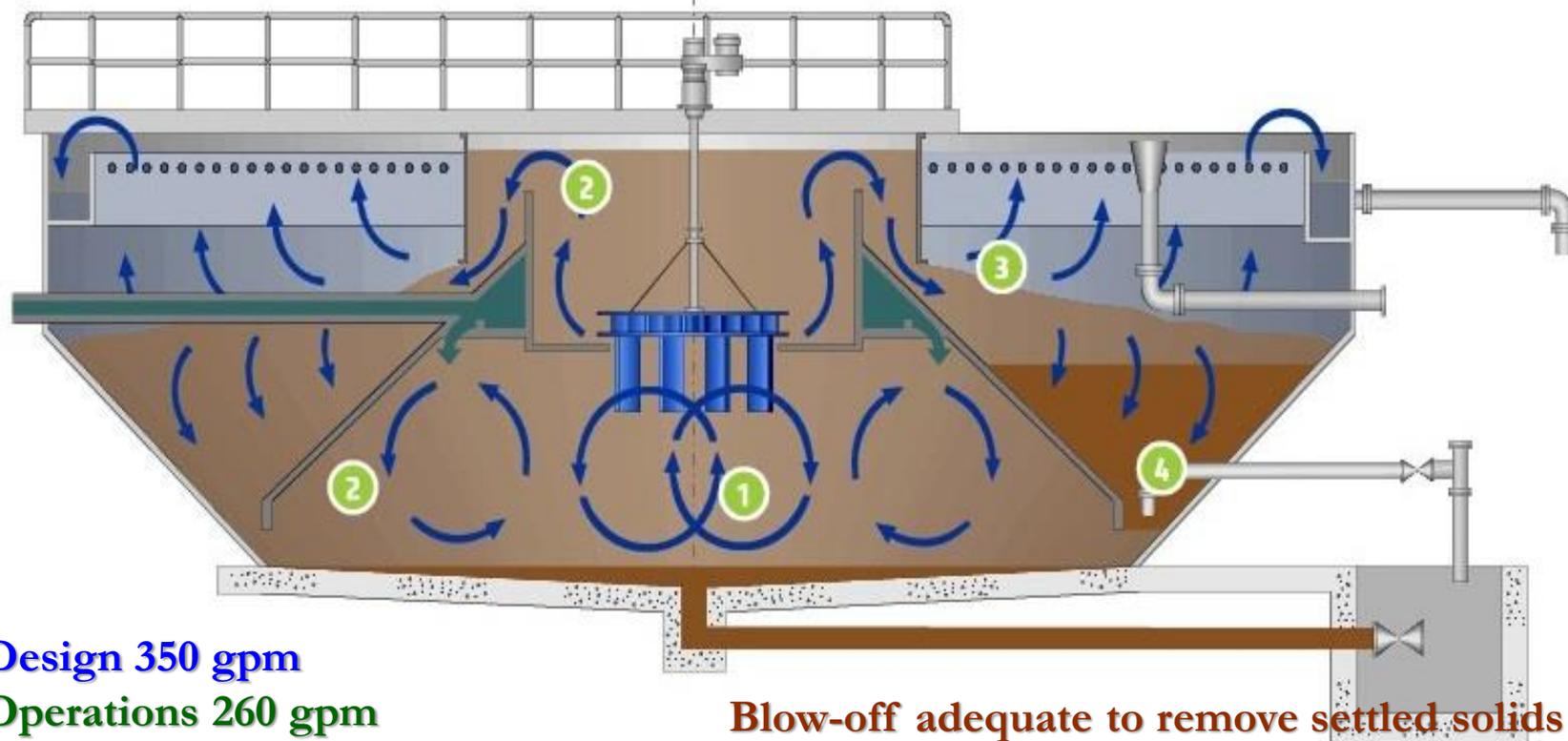
# Fort Recovery

## Clarifier Optimization Initiative



# Fort Recovery Clarifier Optimization

## Infilco (Suez) Accelerator



Design 350 gpm  
Operations 260 gpm

Blow-off adequate to remove settled solids

# Fort Recovery Clarifier Optimization

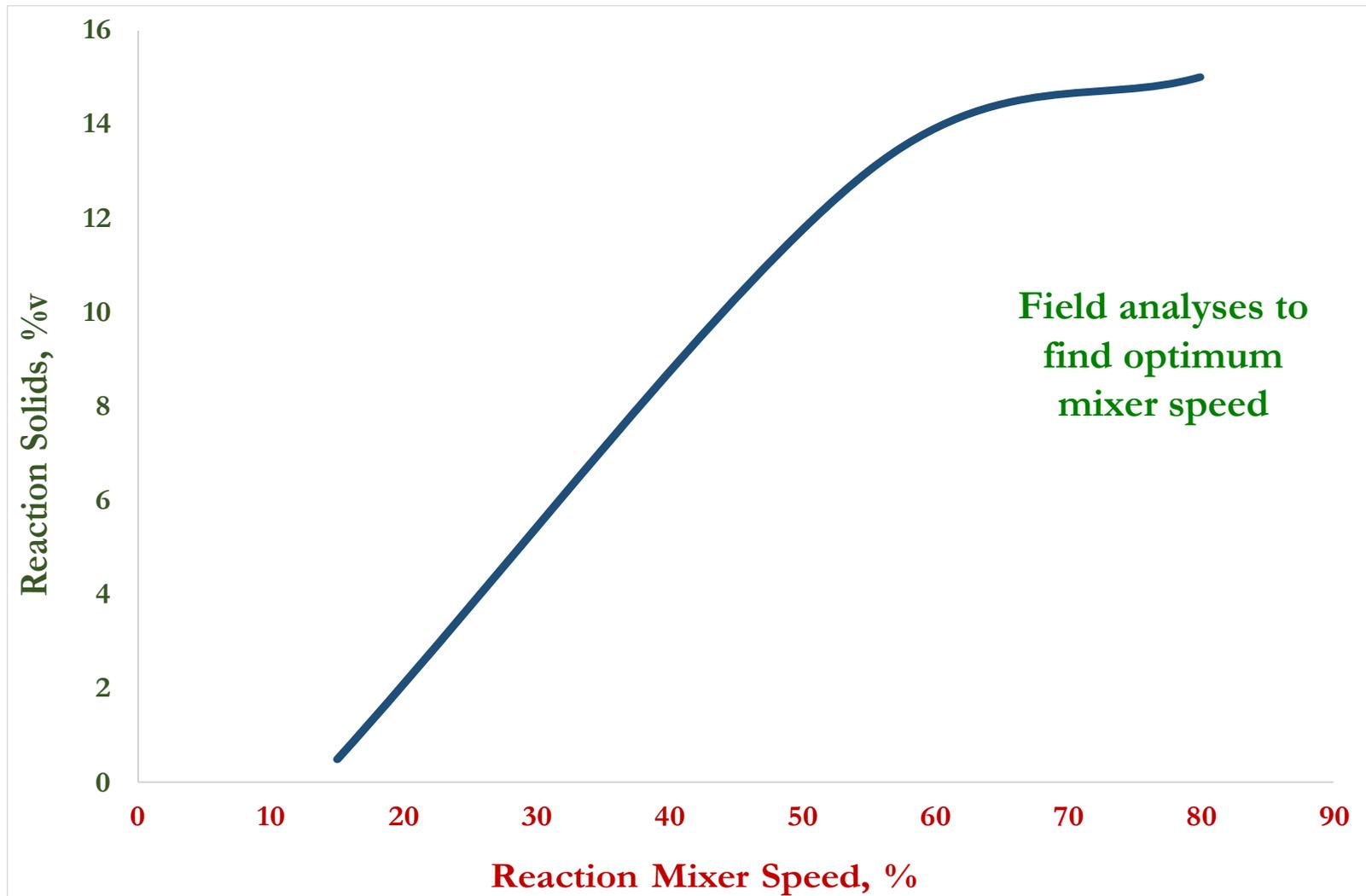
## ■ Clarifier Optimization Initiative

- Poor water clarity ( $\text{CaCO}_3$  and OH carryover)
  - 4-inches clear water at sidewall
  - Previously tried ferric chloride and anionic polymers to improve clarity
- No reaction solids observed
  - Mixer set at 15% speed since 1992 plant start up
- Excessive OH alkalinity
  - 105 mg/L average
- Likely need softening improvements as well
  - Average lime dosage 61 mg/L
  - Average NaOH dosage 313 mg/L

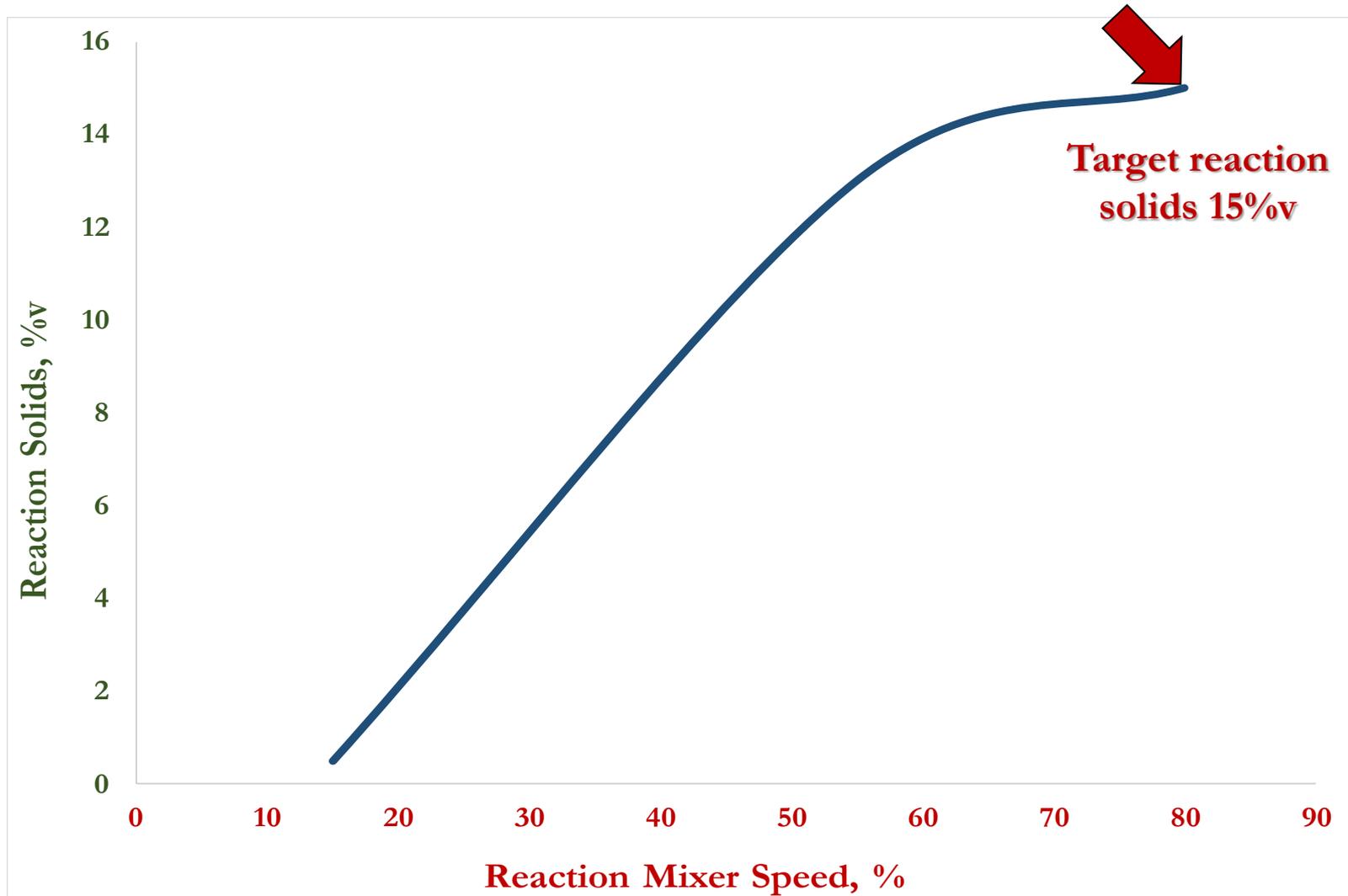
# Fort Recovery Clarifier Optimization



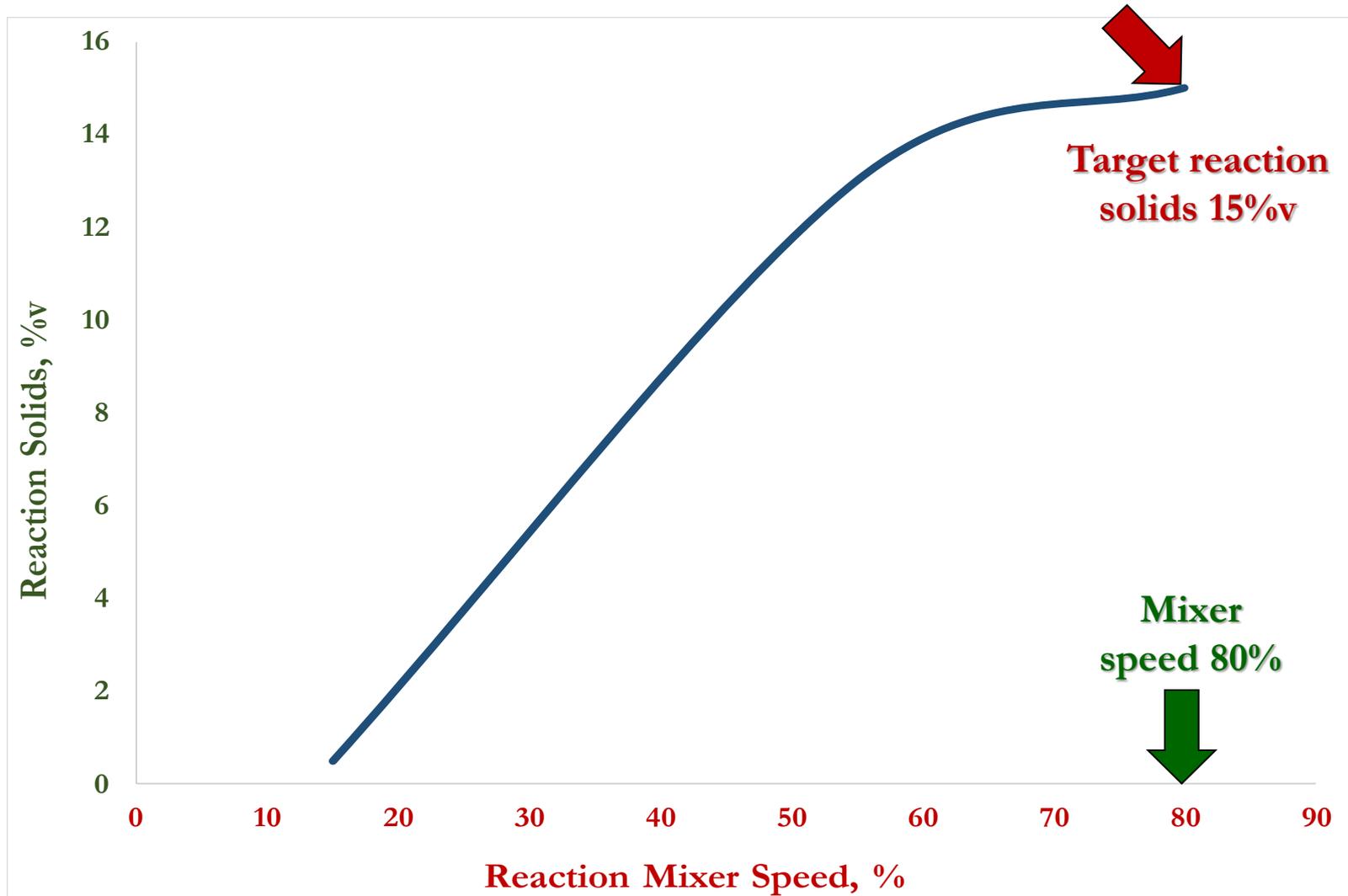
# Fort Recovery Clarifier Optimization



# Fort Recovery Clarifier Optimization

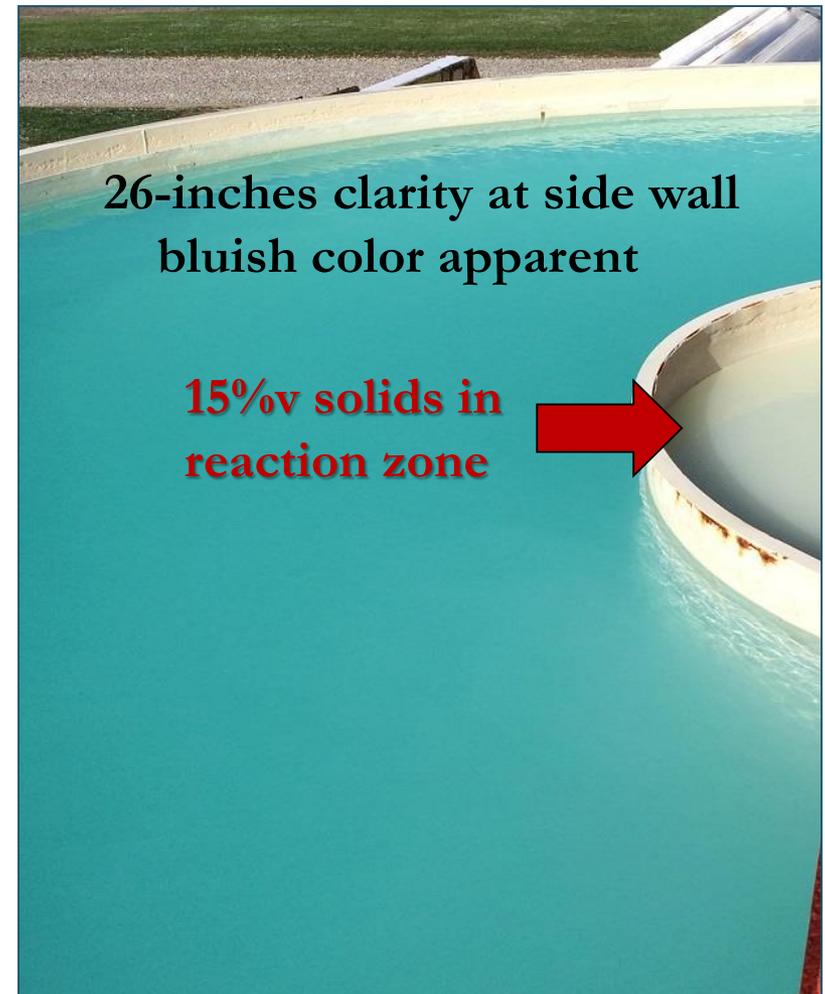


# Fort Recovery Clarifier Optimization



# Fort Recovery Clarifier Optimization

- Water clarity improved within 2 hours
- Reaction solids observed
- Mixer speed maintained 80%
- Review softening operations
  - Improve stability



# Fort Recovery Clarifier Optimization

Parameter	Raw Water	Clarified Water
Water pH, s.u.	7.31	11.27
CO <sub>2</sub> , mg/L	16	0
Hardness, mg/L	705	258
Total alkalinity, mg/L	163	109
Phenol alkalinity, mg/L	0	107
CO <sub>3</sub> alkalinity, mg/L	0	4
OH alkalinity, mg/L	0	105
Calcium, mg/L	405	172
Magnesium, mg/L	300	86

Lime 61 mg/L  
NaOH 313 mg/L

# Fort Recovery Clarifier Optimization

- **Computer modeling to simulate softening and recarbonation**
  - Significant noncarbonate hardness (540 mg/L)
  - Review Lime/NaOH
  - Investigate Lime/soda ash
- **Target hardness 240 mg/L**
  - Too expensive to reduce hardness further
  - Finished water stability adjustments (excessive media growth)
    - Bi-annual filter rebuilding



# Fort Recovery Clarifier Optimization

**Fort Recovery Water Treatment Plant**

SETTLED WATER QUALITY		
Remaining Compounds	After softening, meq/L	Predicted Water Quality
Carbon dioxide	0.00	<b>Calcium - as CaCO<sub>3</sub></b> 181 mg/L
Calcium carbonate	0.47	
Magnesium hydroxide	0.46	<b>Magnesium - as CaCO<sub>3</sub></b> 79 mg/L
Calcium bicarbonate	0.00	
Magnesium bicarbonate	0.00	<b>Hardness - as CaCO<sub>3</sub></b> 259 mg/L
Magnesium carbonate	0.00	
Calcium sulfate	2.77	<b>Total alkalinity - as CaCO<sub>3</sub></b> 64 mg/L
Calcium chloride	0.00	
Magnesium sulfate	0.37	<b>Phenol alkalinity - as CaCO<sub>3</sub></b> 60 mg/L
Magnesium chloride	0.75	
Calcium hydroxide (Excess)	0.37	<b>Water pH</b> 11.19
TA/PA ratio	1.07	
CO <sub>3</sub> /OH Ratio	<b>0.15</b>	<b>Bicarbonate alkalinity - as CaCO<sub>3</sub></b> 0 mg/L
		<b>Carbonate alkalinity - as CaCO<sub>3</sub></b> 8 mg/L
		<b>Hydroxide alkalinity - as CaCO<sub>3</sub></b> 56 mg/L

Lime dosage	62 mg/L
Caustic soda dosage	316 mg/L

**Model matched current dosages and water quality relatively close to existing treatment on plant visits**

# Fort Recovery Clarifier Optimization

**Fort Recovery Water Treatment Plant**

SETTLED WATER QUALITY		
Remaining Compounds	After softening, meq/L	Predicted Water Quality
Carbon dioxide	0.00	Calcium - as CaCO <sub>3</sub> 173 mg/L
Calcium carbonate	0.47	
Magnesium hydroxide	0.23	Magnesium - as CaCO <sub>3</sub> 67.3 mg/L
Calcium bicarbonate	0.00	
Magnesium bicarbonate	0.00	Hardness - as CaCO <sub>3</sub> 240 mg/L
Magnesium carbonate	0.00	
Calcium sulfate	2.99	Total alkalinity - as CaCO <sub>3</sub> 35 mg/L
Calcium chloride	0.00	
Magnesium sulfate	0.47	Phenol alkalinity - as CaCO <sub>3</sub> 23 mg/L
Magnesium chloride	0.65	
Calcium hydroxide (Excess)	0.00	Water pH 10.75
TA/PA ratio	1.51	
CO <sub>3</sub> /OH Ratio	<b>2.04</b>	Bicarbonate alkalinity - as CaCO <sub>3</sub> 0 mg/L
		Carbonate alkalinity - as CaCO <sub>3</sub> 24 mg/L
		Hydroxide alkalinity - as CaCO <sub>3</sub> 12 mg/L

Lime dosage	431 mg/L
Soda ash dosage	416 mg/L

**Lime/soda ash dosages quite high to meet target hardness, increased operating costs**

# Fort Recovery Clarifier Optimization

**Fort Recovery Water Treatment Plant**

SETTLED WATER QUALITY		
Remaining Compounds	After softening, meq/L	Predicted Water Quality
Carbon dioxide	0.00	<b>Calcium - as CaCO<sub>3</sub></b> 175 mg/L
Calcium carbonate	0.47	
Magnesium hydroxide	0.46	<b>Magnesium - as CaCO<sub>3</sub></b> 66 mg/L
Calcium bicarbonate	0.00	
Magnesium bicarbonate	0.00	<b>Hardness - as CaCO<sub>3</sub></b> 240 mg/L
Magnesium carbonate	0.00	
Calcium sulfate	3.02	<b>Total alkalinity - as CaCO<sub>3</sub></b> 39 mg/L
Calcium chloride	0.00	
Magnesium sulfate	0.00	<b>Phenol alkalinity - as CaCO<sub>3</sub></b> 35 mg/L
Magnesium chloride	0.86	
Calcium hydroxide (Excess)	0.00	<b>Water pH</b> 11.14
TA/PA ratio	1.12	
CO <sub>3</sub> /OH Ratio	<b>0.26</b>	<b>Bicarbonate alkalinity - as CaCO<sub>3</sub></b> 0 mg/L
		<b>Carbonate alkalinity - as CaCO<sub>3</sub></b> 8 mg/L
		<b>Hydroxide alkalinity - as CaCO<sub>3</sub></b> 31 mg/L

Lime dosage	159 mg/L
Caustic soda dosage	293 mg/L

**Increase in lime and decrease in NaOH met target hardness, reduced OH alkalinity to about 30 mg/L**

# NEMRWSD - Tupelo, MS



# NEMRWD - Tupelo, MS

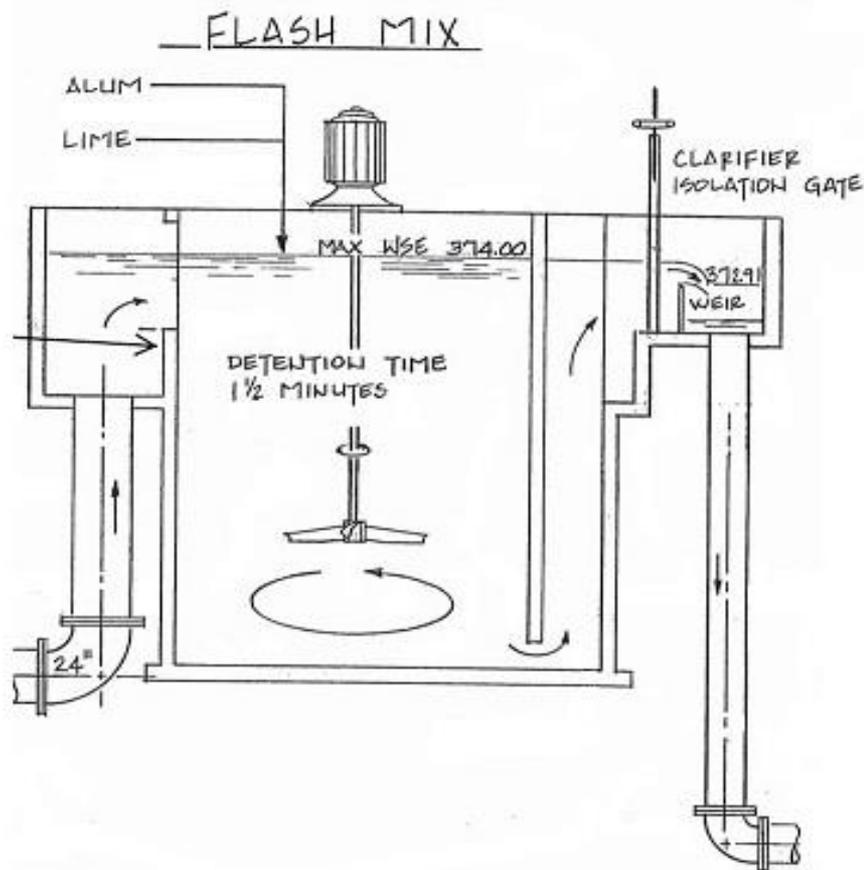


# NEMRWD - Tupelo, MS

- 18 mgd surface water plant drawing from Tombigbee River
  - Average daily production 12 mgd
- Coagulation/pH adjustment/filtration plant
  - Chemical treatment
  - Solids handling
  - Disinfection and storage
    - Final chloramination
- Finished water pumping to four wholesale distribution systems
  - $\approx 70,000$  people

# NEMRWD - Tupelo, MS

## LACR and TOC Removal Initiative



# Tupelo LACR and TOC Removal

- **Low alkalinity source water inhibits TOC removals**
  - Average annual alkalinity 45 mg/L
  - TOC varies 5 mg/L to 22 mg/L
- **Alum coagulation**
  - 58 mg/L average dosage
  - 150 mg/L during rain events
    - Due to high color and high TOC
    - Maximum dosage under NSF
    - Often results in elevated turbidity levels
    - Typically insufficient alkalinity to foster coagulation reactions

# Tupelo LACR and TOC Removal

- **LACR (pr: lacker)**
  - **L**ime to **A**lkalinity **C**onsumed **R**atio
    - Lime most common alkalinity supplement
  - Replacement of alkalinity reacted during coagulation to foster optimum metal hydroxide formation
    - Low alkalinity source water <60 mg/L
    - Metal hydroxides adsorb organic contaminants (TOC)
    - Alkalinity control needed for optimum coagulation, corrosion control, and stability control
- **LACR maintains control of alkalinity levels and TOC reduction**
  - Alkalinity replacement common using lime or other chemicals

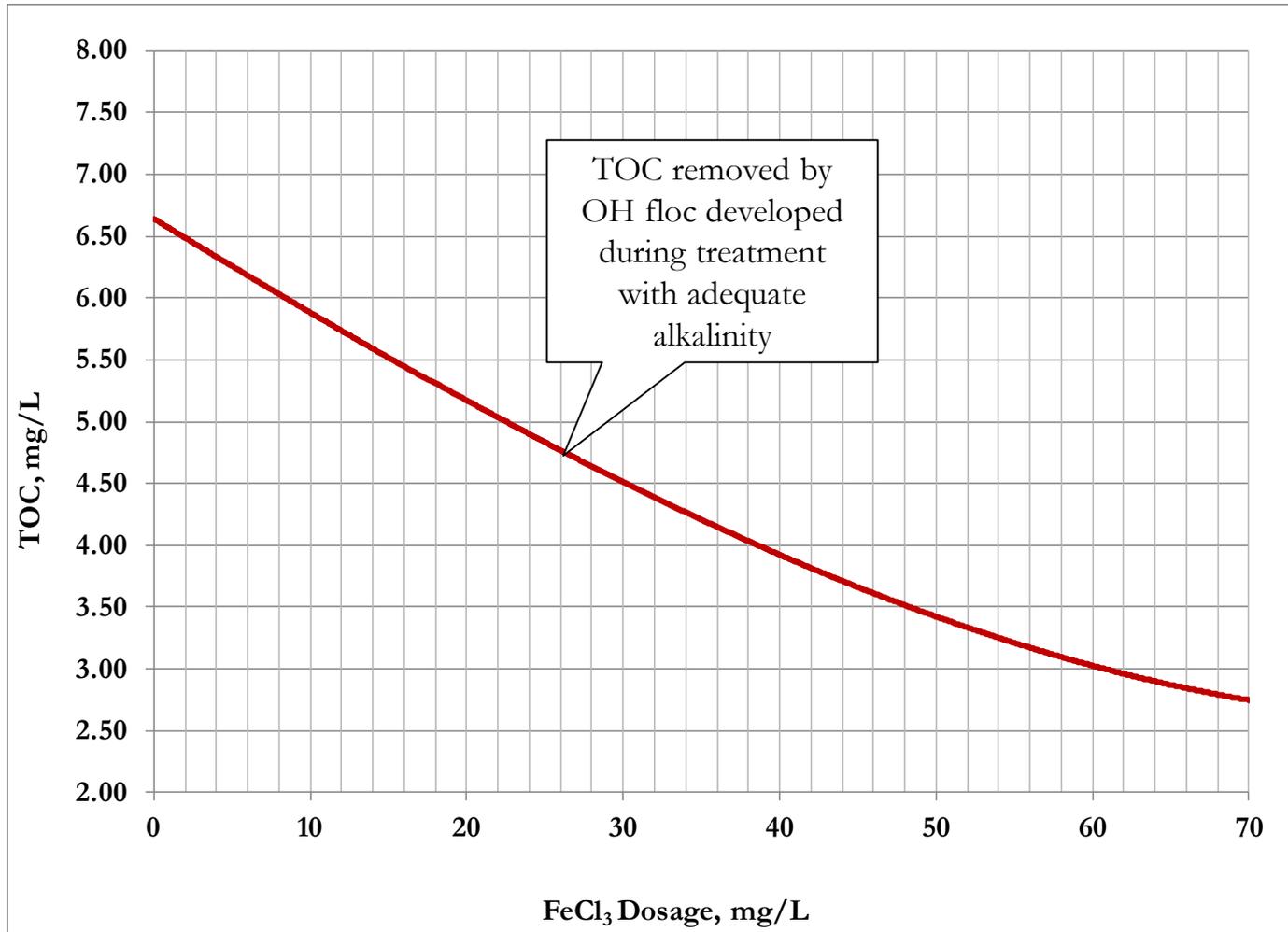
# Tupelo LACR and TOC Removal

$$LACR = \frac{\textit{alkalinity dosage, mg / L}}{k * \textit{coagulant dosage, mg / L}}$$

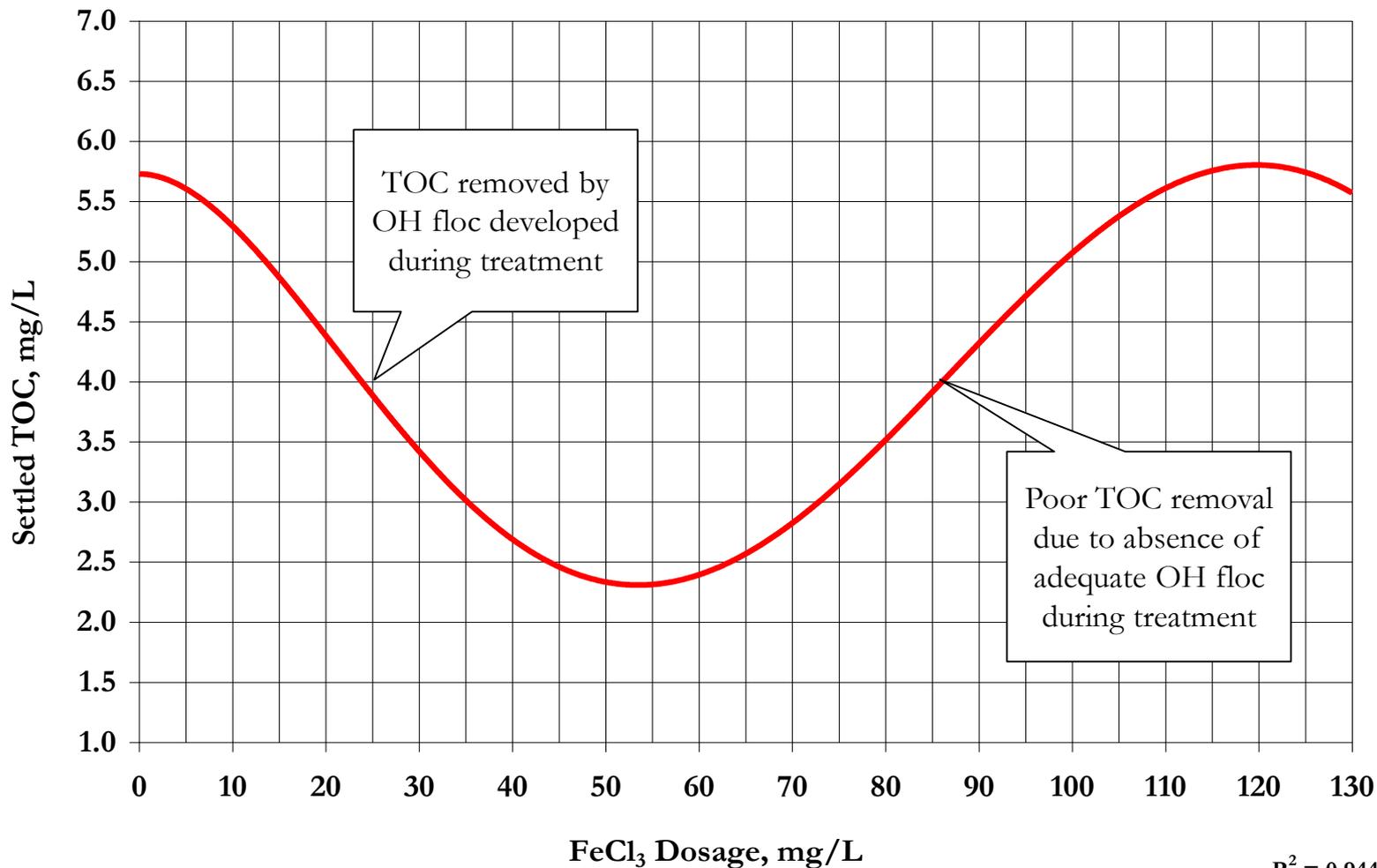
$k = \textit{alkalinity consumption coefficient}$

$$LACR * k * \textit{coagulant dosage, mg / L} = \textit{alkalinity dosage, mg / L}$$

# Tupelo LACR and TOC Removal

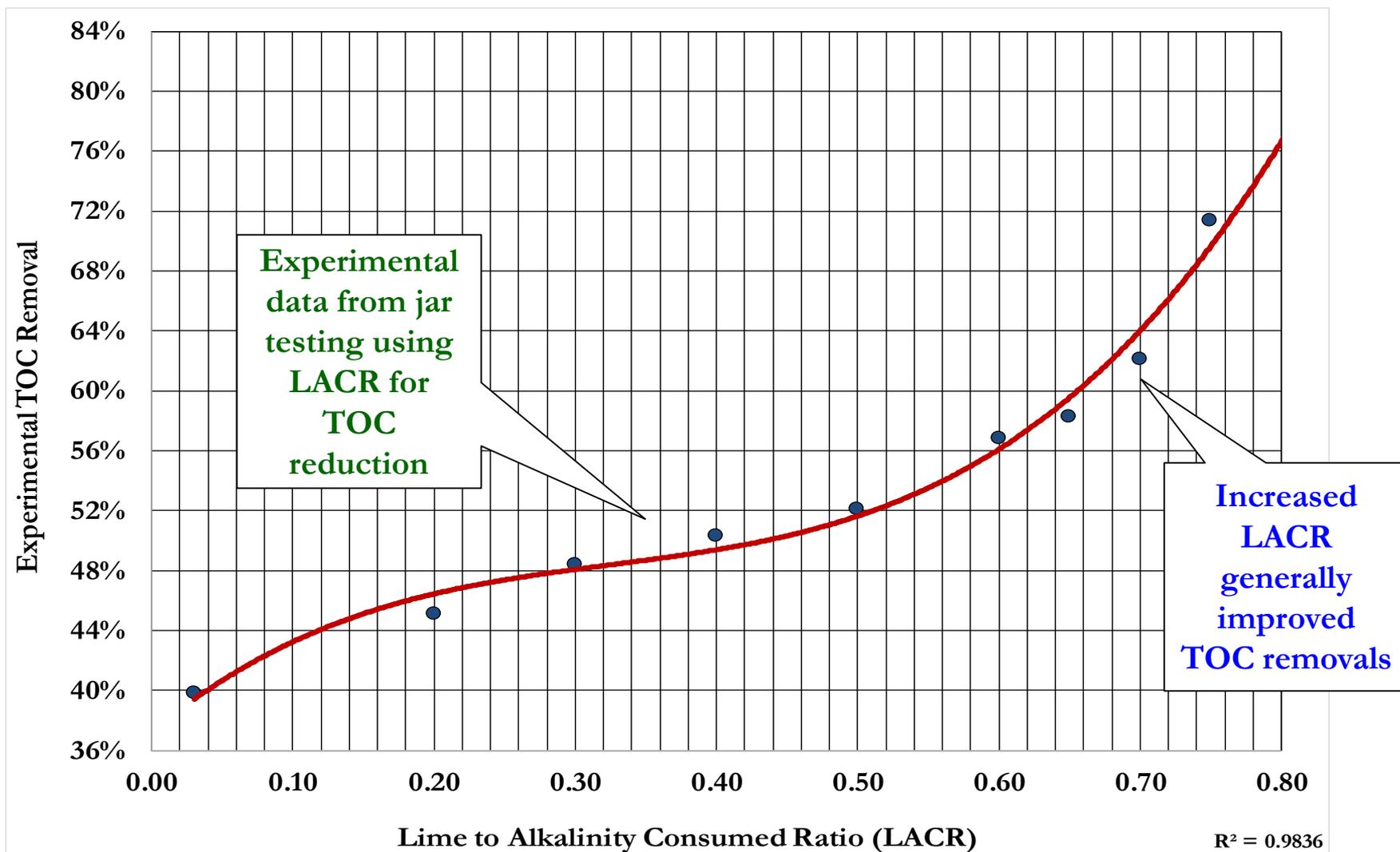


# Tupelo LACR and TOC Removal

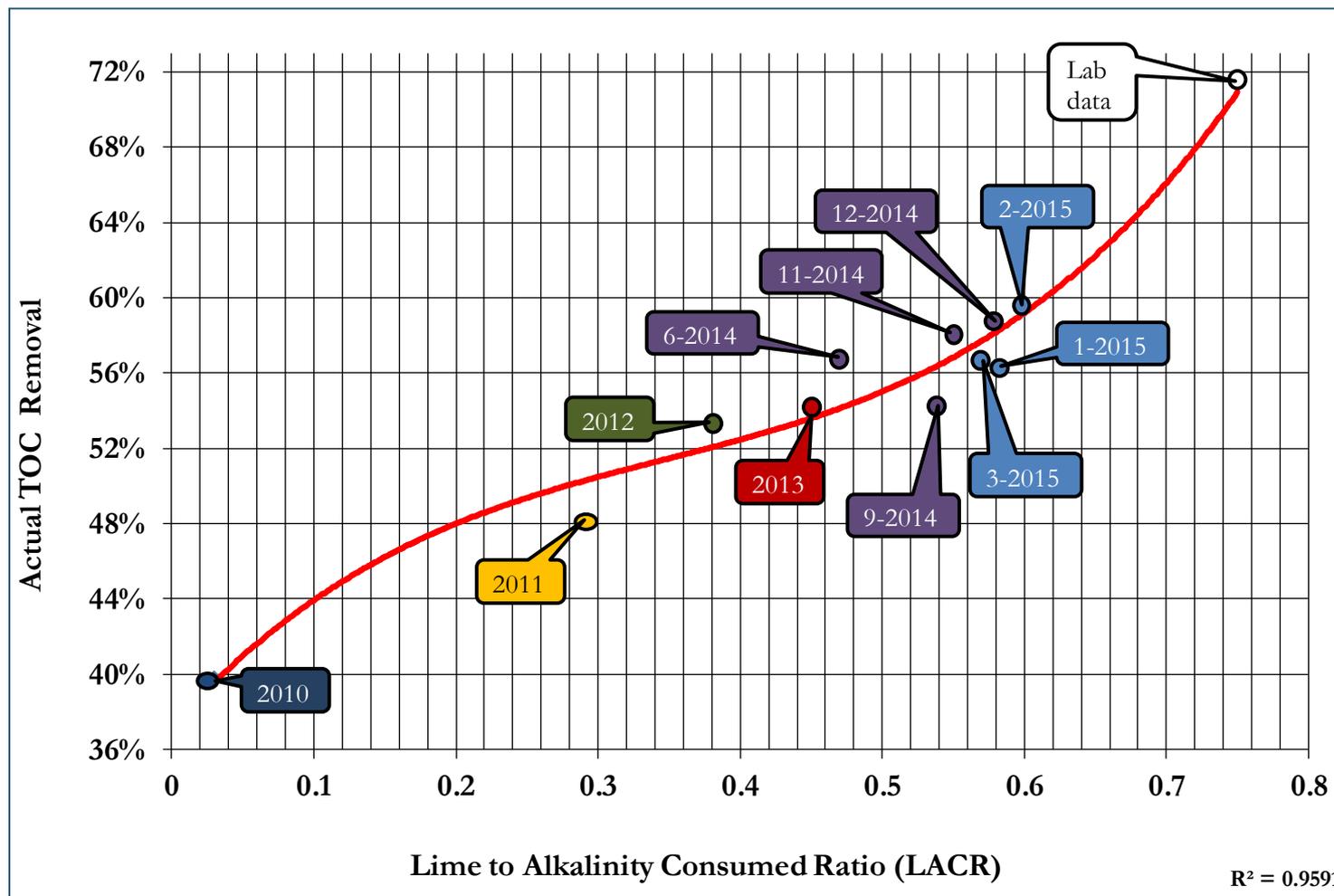


R<sup>2</sup> = 0.9442

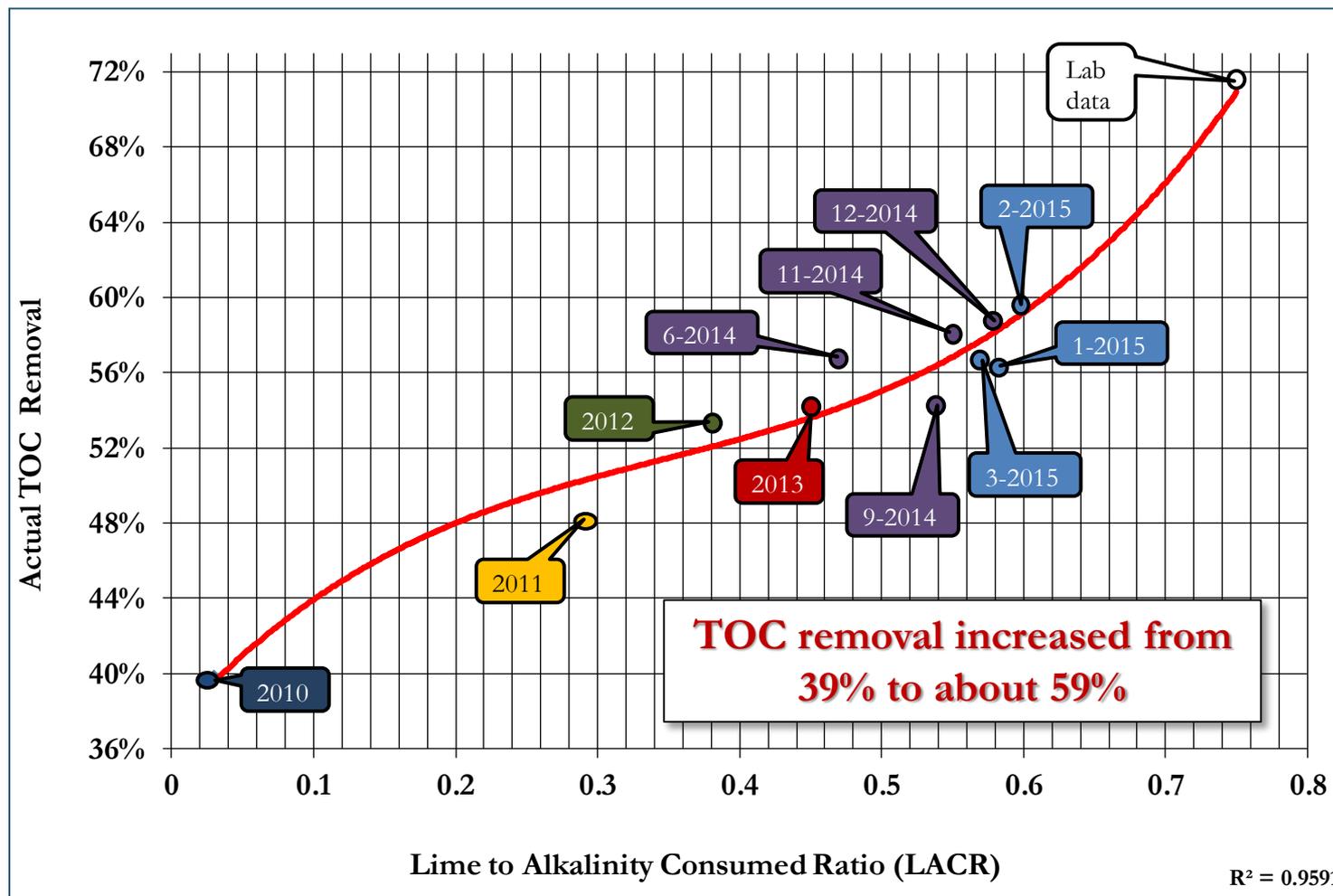
# Tupelo LACR and TOC Removal



# Tupelo LACR and TOC Removal



# Tupelo LACR and TOC Removal



# Conclusions

- **Optimization can produce excellent results**
  - Better performance in many applications
  - Follow scientific principles and established procedures
  - Document findings and projections
  - Verify with first-year field data
  - Often improves water quality and can produce cost savings
- **Start making you own stories**

# *Questions*

**Marvin Gnagy**

**[pmgconsulting710@gmail.com](mailto:pmgconsulting710@gmail.com)**

**419.450.2931**