## OPTIMIZATION OF LIME－SOFTENING PROCESS AT WADSWORTH WTP

OPERATOR TRAINING COMMITTEE OF OHIO，INC． PROCRASTINATORS WORKSHOP

December 11， 2014


## Agenda

- Plant Overview
- Plant Process Description
- Water Quality Data
- Hardness Removal Chemistry
- Recarbonation Systems
- Chemical Optimization Study
- Recommended Improvement Plan
- Alternatives
- Lessons Learned
- Questions


## Wadsworth Water Quality Data 2013



## Water Well Information

| Well \# | 2 | 3 | 4 | $7 A$ | 9 | $10 A$ | 11 | 12 | 13 | 14 | 15 | 19 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Depth, <br> Feet | 275 | 275 | 275 | 275 | 275 | 275 | 275 | 275 | 275 | 275 | 275 | 275 |
| Capacity, <br> GPM | 300 | 250 | 360 | 195 | 390 | 245 | 335 | 250 | 300 | 240 | 300 | 700 |

Notes:

1. \#16 used as monitoring well.
2. Wells \#7A \& \#9 cannot run at the same time.
3. Wells \#11 \& \#12 cannot run at the same time unless it is an emergency.

## Average Annual Daily Flow Rates



## Peak Day Factor

Max Flow: Avg. Flow = 1.3
—Annual Average Daily Flow, MGD
-Annual Max Daily Flow, MGD

## Process Flowsheet



High Service Pumps Low Service Pumps


Chlorine Contract/ Clearwell
547,000 Gal.


## INDUCED DRAFT AERATOR

- Oxidation of Iron and Manganese
- Reaction Basin: 64,000 gallons
- Detention Time: 20 Min. @4.6 MGD
- Plant Design Capacity; 3 MGD
- Peak Hourly Flow 3.3 MGD
- Peak Day Capacity 4.5 MGD
- Treatment to Reduce Hardness
- Lime Feed to Precipitate Ca++ and Mn++ at pH 8.9
- No pH Re-adjustment
- Chlorination
- Flouridation


## Flash Mix

- Two (2) units each:
- 2 HP Mixer
$-5.5^{\prime} \times 5.5^{\prime} \times 5.5^{\prime}$ SWD
- 166.4 CF 1,244 Gallons
- Detention Time:
- 60 sec Min Required
- 72 sec @ 3.0 MGD



## FLoculation

- Four (4) tanks each:
- 2 HP Mixer
- $33.0^{\prime} \times 9.42^{\prime} \times 12^{\prime}$ SWD
- 3730.3 CF
- 27,903 Gallons Each
- 111,611 Gallons Total

- Detention Time:
- 53.6 Minutes (4 in service)


## Settling Basins

- Two (2) tanks each:
$-88.5^{\prime} \times 20.0^{\prime} \times 12^{\prime}$ SWD
- 21,240 CF
- 158,875 Gallons Each
- 317,750 Gallons Total
- Detention Time:
- 2.54 Hours (2 @ 3 MGD)



## Existing Recarb \& Post Settling Basinn win

- Post Settling Basin (1 Each):
$-76.0^{\prime} \times 14.83^{\prime} \times 12^{\prime}$ SWD
- 13,525 CF
- 101,167 Gallons Each
- 418,917 Gallons Total
- Detention Time:

- 0.81 Hours (Post Settling Tank only)
- 3.35 Hours (2 Settling \& 1 Post Settling Tanks in Service)


## Chemical Feed:

 WATER \& WASTE WATERDIGTRIGUTIGN

- Zinc Orthophosphate
- Chlorine Feed



## Sand Filters

- 4 Filters each:
$-16.5^{\prime} \times 16^{\prime}$
- Dual Media
- 268 SF Each (Typical 4)
- Loadings w/1 Filter Out of Service
- 804 SF
- 3.48 MGD @ 3 gpm/sf
- 4.63 MGD @ 4 gpm/sf

- Filters Rebuilt in 2013-14


## High Service Pump Station

- High Service Pumps:
- 3 @ 1,400 gpm
- 1 @ 2,000 gpm
- Max. Hydraulic Pumping Rate:
- 2,800 GPM
- 4.00 MGD
- Low Service Pumps:
- 3 @ 1,500 gpm
- 1 @ 2,000 gpm


CLEARWELL CAPACITY $=0.547 \mathrm{MG}$

- Max. Hydraulic Pumping Rate :
- 1,800 GPM
- 1.87 MGD


## Hardness Classification

- Hardness Classification Scale:
- $0-75 \mathrm{mg} / \mathrm{L}$ as $\mathrm{CaCO}_{3}$ : Soft
- $75-150 \mathrm{mg} / \mathrm{L}$ as $\mathrm{CaCO}_{3}$ :
- $150-300 \mathrm{mg} / \mathrm{L}$ as $\mathrm{CaCO}_{3}$ :
- > $300 \mathrm{mg} / \mathrm{L}$ as $\mathrm{CaCO}_{3}$ :

Moderately Hard Goal Hard current Condition
Very Hard

## Wadsworth Water Quality Data 2013

|  | Plant Tap |  |  |  |  |  |  |  |  |  | Distribution System |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | pH | $\begin{aligned} & \text { P } \\ & \text { Alk } \end{aligned}$ | Tot Alk | Total Hardness | Ca | Mg | $\begin{aligned} & \mathrm{CaCO}_{3} \\ & \text { Stablikity } \end{aligned}$ | $\begin{aligned} & \text { Free } \\ & \mathrm{Cl}_{2} \end{aligned}$ | Total $\mathrm{CL}_{2}$ | FI | Free <br> Cl | Tot <br> Cl | FI |
| Max. | 8.1 | 0 | 88 | 223 | 127 | 96 | 0 | 1.2 | 1.4 | 1.03 | 0.9 | 1.1 | 1.00 |
| Min. | 7.9 | 0 | 69 | 186 | 117 | 91 | 0 | 1.0 | 1.1 | 0.91 | 0.7 | 0.8 | 0.90 |
| AVG. | 8.0 | 0 | 79 | 216 | 122 | 94 |  | 1.1 | 1.2 | 0.97 | 0.8 | 0.9 | 0.95 |

## Hardness of Tap Water

- Total Hardness:
- Calcium + Magnesium
$=122 \mathrm{mg} / \mathrm{l}+94 \mathrm{mg} / \mathrm{l}=216 \mathrm{mg} / \mathrm{l}$

Goals:
Calcium $\quad 80 \mathrm{mg} / \mathrm{l}$ Magnesium 40 mg/l

Total Hardness 150 mg/l

- Carbonate Hardness:
- Alkalinity

$$
\text { = } 79 \mathrm{mg} / \mathrm{l}
$$

- Non-Carbonate Hardness:
- Total Hardness - Carbonate Hardness
$=216 \mathrm{mg} / \mathrm{l}-79 \mathrm{mg} / \mathrm{l}=137 \mathrm{mg} / \mathrm{l}$

Non-Carbonate Hardness can only be removed: by lime \& soda ash

- Calcium Sulfate: $\mathrm{CaSO}_{4}$
- Calcium Chloride: $\mathrm{CaCl}_{2}$
- Magnesium Sulfate: $\mathrm{MgSO}_{4}$
- Magnesium Chloride: $\mathrm{MgCl}_{2}$


## Influent Water Quality

Composite Wells Raw and Post-Aerator

|  | Wells \# | Total Alk | Total Hardness | Non-Carb Hardness | Calcium Hardness | Mag Hardness | Iron | Mn | TDS | pH | CO2 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Raw 10/1/14 | 15-19 | 196 | 336 | 140 | 230 | 106 | 7.76 | 0.56 | 430 | 7.2 | 28.62 |
| $\begin{aligned} & \text { Aerator } \\ & 10 / 1 / 14 \end{aligned}$ | 15-19 | 176 | 338 | 162 | 230 | 108 | 5.70 | 0.56 | 430 | 7.3 | 25.7 |
| Raw 10/2/14 | 3-10-12-14-19 | 209 | 310 | 101 | 204 | 106 | 4.20 | 0.34 | 340 | 7.3 | 30.51 |
| Aerator 10/2/14 | 3-10-12-14-19 | 194 | 330 | 136 | 208 | 122 | 3.30 | 0.33 | 500 | 7.6 | 11.25 |
| Raw 10/9/14 | 4-11-13-15 | 192 | 302 | 110 | 200 | 102 | 8.30 | 0.67 | 440 | 7.2 | 28.02 |
| Aerator 10/9/14 | 4-11-13-15 | 170 | 318 | 148 | 224 | 94 | 6.70 | 0.63 | 430 | 6.9 | 39.44 |

Secondary Limits:

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- Iron = 0.30 mg/l (99.65% Removal)
- Manganese = 0.05 mg/l (99.25% Removal)
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## Secondary OEPA Standards

- Aesthetic
- Standards related to color:
- Aluminum, Color, Copper,

Foaming Agents, Iron, Manganese, Total Dissolved Solids

- Standards related to odor and taste:
- Chloride, Copper, Foaming Agents, Iron, Manganese pH, Sulfate, Threshold Odor Number (TON), Total Dissolved Solids, Zinc
- Technical
- Standards related to corrosion and staining:
- Chloride, Copper, Corrosivity, Iron, Manganese, pH, Total Dissolved Solids, Zinc
- Standards related to scale and sediments:
- Iron, pH, Total Dissolved Solids, Aluminum.
- Cosmetic
- Silver and Fluoride


## Secondary Drinking Water Regulations:

| Contaminant | Secondary MCL | Noticeable Effects above the Secondary MCL |  |
| :---: | :---: | :---: | :---: |
| Aluminum | $0.05-0.2 \mathrm{mg} / \mathrm{L}^{*}$ |  | colored water |
| Chloride | $250 \mathrm{mg} / \mathrm{L}$ |  | salty taste |
| Corrosivity | Non-corrosive | metallic taste; corroded pipes/ fixtures staining |  |
| Fluoride | $2.0 \mathrm{mg} / \mathrm{L}$ |  | tooth discoloration |
| Iron | $0.3 \mathrm{mg} / \mathrm{L}$ | rusty color; sediment; metallic taste; reddish or orange staining |  |
| Manganese | $0.05 \mathrm{mg} / \mathrm{L}$ | black to brown color; black staining; bitter metallic taste |  |

## Hardness Removal

- Most chemical forms of hardness are water soluble, except:
- Exceptions: Calcium Carbonate \& Magnesium Hydroxide removed by precipitation
- Lime softening removes only carbonate hardness

Hardness due to
Anions:

- Bicarbonate $\left(\mathrm{HCO}_{3}{ }^{-}\right)$
- Carbonate $\left(\mathrm{CO}_{3}{ }^{2-}\right)$
- Sulfate $\left(\mathrm{SO}_{4}{ }^{2-}\right)$
- Chloride ( $\mathrm{Cl}^{-}$)
- Nitrate $\left(\mathrm{NO}_{3}{ }^{-}\right)$
- Silica $\left(\mathrm{SiO}_{3}{ }^{2-}\right)$
- Calcium Carbonates $\left[\mathrm{CaCO}_{3]}\right.$ \& Calcium Bicarbonates $\left[\mathrm{Ca}\left(\mathrm{HCO}_{3}\right)_{2]}\right.$
- Magnesium Carbonates $\left[\mathrm{CaCO}_{3]}\right.$ and Mg Bicarbonates $\mathrm{Mg}\left(\mathrm{HCO}_{3}\right)_{2}$
- Lime \& Soda Ash softening required to remove non-carbonate hardness
- Chloride: $\mathrm{MgCl}_{2}$
- Calcium Sulfate: $\mathrm{CaSO}_{4}$
- Calcium Chloride: $\mathrm{CaCl}_{2}$
- Magnesium Sulfate: $\mathrm{MgSO}_{4}$
- Magnesium Chloride: $\mathrm{MgCl}_{2}$


## Alkalinity and pH

- Alkalinity = Measure of the acid neutralizing capacity of water
- Forms:
- Bicarbonate
- Carbonate
- Hydroxide
- Total Alkalinity = [Bicarbonate] + [Carbonate] + [Hydroxide] expressed in $\mathrm{mg} / \mathrm{L}$ as calcium carbonate


## Lime Required for Removal of <br> Carbonate Hardness and Magnesium

- $\mathrm{CaO}(\mathrm{lb} / \mathrm{mil}$ gal $)=$
$=10.6 \mathrm{lbs} . / \mathrm{MG} \mathrm{x} \mathrm{CO}_{2}\left(\mathrm{mg} / \mathrm{Las} \mathrm{CO}_{2}\right)$
+4.7 [Alkalinity $\left(\mathrm{mg} / \mathrm{L}\right.$ as $\left.\mathrm{CaCO}_{3}\right)$
+Mg hardness ( $\mathrm{mg} / \mathrm{L}^{2 s} \mathrm{CaCO}_{3}$ )
+ required excess hydroxide alkalinity as $\mathrm{CaCO}_{3}$ (typically $30-70 \mathrm{mg} / \mathrm{I}$ )]

- $\mathrm{CaO} \times \mathrm{MGD}=\mathrm{CaO} /$ divided by 0.88 to 0.95 (actual chemical purity of CaO )
- $\mathrm{CaO}_{\text {Total/MGD }}$ Required $\left.\times 3 \mathrm{MGD}\right)=$
- $\mathrm{CaO}_{\text {Total/MGD }} \times 3 \mathrm{MGD} / .90$ purity $=$ Required Daily Usage


## Acid Feed for Neutralization

- CO2 offers safer and more robust system over acids as shown in Table 1:
- Final pH should be selected by looking at scaling indices:
- Langlier index
- CCPP (Calcium Carbonate Precipitation Potential)
- Ryznar index
- Lead solubility

| $l$ |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Table 1: Comparison of chemicals for pH control <br> at water treatment plant $\mathrm{CO}_{2}$ |  |  |  | $\mathrm{H}_{2} \mathrm{SO}_{4}$ | HCl |
| Safety |  |  |  |  |  |
| Permit for use |  |  |  |  |  |
| Availability |  |  |  |  |  |
| Price Variability |  |  |  |  |  |
| Ease of Storage |  |  |  |  |  |
| System Maintenance |  |  |  |  |  |
| Environment-friendliness |  |  |  |  |  |
| Process Control |  |  |  |  |  |
| Effect of Overdosing |  |  |  |  |  |
| Cost of Implementation |  |  |  |  |  |
| Limitations for Use |  |  |  |  |  |

## Recarbonation Chemistry

 WATER \& WASTE WATER DISTRIGUTIION- The effluent from lime softening process is supersaturated with carbonates at high pHs ( 10 or greater) and it is necessary to stabilize the water to prevent deposition of a hard carbonate scale on the piping and filters.
- Lime Softening

$$
\begin{aligned}
& \mathrm{Ca}(\mathrm{HCO} 3) 2+\mathrm{Ca}(\mathrm{OH}) 2 \square 2 \mathrm{CaCO} 3+2 \mathrm{H} 2 \mathrm{O} \\
& \mathrm{Mg}(\mathrm{HCO} 3) 2+2 \mathrm{Ca}(\mathrm{OH}) 2 \rightleftarrows \mathrm{Mg}(\mathrm{OH}) 2+\mathrm{CaCO} 3+2 \mathrm{H} 2 \mathrm{O}
\end{aligned}
$$

- Recarbonation

$$
\begin{aligned}
& \mathrm{CaCO} 3+\mathrm{CO} 2+\mathrm{H} 2 \mathrm{O} \\
& \mathrm{Mg}(\mathrm{OH}) 2+\mathrm{CO} 2 \square \mathrm{Ca}(\mathrm{HCO} 3)^{2} \\
& \\
& \mathrm{MgCO} 3+\mathrm{H} 2 \mathrm{O}
\end{aligned}
$$

## Process Flowsheet Soda Ash \& Recarbonation with $\mathrm{CO}_{2}$



## Carbonate Forms vs. pH

- The effluent from lime softening process is supersaturated with carbonates at high pHs (10 or greater) and it is necessary to stabilize the water to prevent deposition of a hard carbonate scale on the piping and filters.
- pH lowered to below pH of 9.5 and dissolve the CaCO 3 into bicarbonate form.
- CO2 Usage

- Theoretical 330 lbs /MG
- Finished Water pH = 8.8-9.2 (Adjustable)


## CO2 Recarbonation Schematic

## Gas Feed Systems Recommended Design Parameters

- Contact basins shall provide a minimum detention time 30 minutes, and
- Tank water depths greater than 15 feet to achieve 60-85\% transfer efficiency.



## Pressurized CO2 Feed System

- $99.9 \%$ of the chemical reaction has taken place within 3 minutes of the carbonic acid injection.
- pH is controlled and the water is stabilized within this 3 minute period.
- Recarb Basin Basis of Design = 4.5 MGD x 1.33
- Flow $\quad=6 \mathrm{MGD}$
- Detention Time $=5$ minutes (min.)
- Existing Recarb Basin (11.5' x 14.83' x 12' SWD)
- Capacity = 15,300 gallons
- Detention Time (Ex. Recarb Tank) $=3.67 \mathrm{~min}$.
- Add Mix Chamber in Influent Channel
- $14.83^{\prime} \times 5^{\prime} \times 12^{\prime}$ SWD $=890$ CF
- Capacity = 6,655 gallon
- Detention Time = @ 1.6 minutes


CO2 Storage Tank \& Feed System

## Process Flowsheet Soda Ash \& Recarbonation with $\mathrm{CO}_{2}$




New Pressurized Recarb Basin

## Optimization for Hardness Removal



## Sludge Production for Alternates

| Parameter |  | Lime w/o <br> Recarb | Lime w/ <br> Recarb | Lime \& Soda <br> Ash /w <br> Recarb |
| :--- | :--- | ---: | ---: | ---: |
| pH | 8.8 | 10.97 | 11.16 |  |
| Magnesium Hydroxide | $\mathrm{mg} / \mathrm{l}$ | 0 | 0 | 38 |
|  | Lbs./MG | 0 | 0 | 321 |
| Calcium Carbonate | $\mathrm{mg} / \mathrm{I}$ | 284 | 338 | 442 |
|  | $\mathrm{Ibs./MG}$ | 2,380 | 2,831 | 3,685 |

## Blending or Split Treatment W/O Soda Ash

 WATER \& WASTE WATER DISTRIDUTION

## Pressure Filters and Softeners



FILTER SECTION

## Water Softeners

# Res-Kem <br> GENERAL WATER 

## FEATURES AND SPECIFICATIONS

| Model Prefix | Vessel Diameter inches | Flow Rate <br> Rangegpm | Resin Quantity <br> cubic feet | Capacity Range <br> grains |  | Inlet/Outlet Pipe Size Range inches | Brine Tank Diameter x Height inches | Approximate Dimensions xDxH inches |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ZSO-20 | 20 | 26-54 | 5-7 | 150,000 | 210,000 | 1 to $11 / 2$ | 24x54 | $56 \times 32 \times 94$ |
| ZSO-24 | 24 | 37-75 | 7-10 | 210,000 | 300,000 | $11 / 2$ to 2 | $24 \times 54$ | $60 \times 36 \times 94$ |
| ZSO-30 | 30 | 59-118 | 11-16 | 330,000 | 480,000 | 2 to $21 / 2$ | $30 \times 60$ | $72 \times 42 \times 98$ |
| ZSO-36 | 36 | 85-170 | 16-24 | 480,000 | 720,000 | 2 to 3 | $39 \times 48$ | 87x48x98 |
| ZSO-42 | 42 | 115-230 | 21-32 | 630,000 | 960,000 | $21 / 2$ to 3 | $50 \times 60$ | $104 \times 54 \times 101$ |
| ZSO-48 | 48 | 150-225 | 28-42 | 840,000 | 1,260,000 | $21 / 2$ to 4 | 50x60 | $110 \times 60 \times 101$ |
| ZSO-54 | 54 | 190-380 | 36-53 | 1,080,000 | 1,590,000 | 3 to 4 | 60x46 | $126 \times 66 \times 110$ |
| ZSO-60 | 60 | 235-470 | 44-65 | 1,320,000 | 1,950,000 | 3 to 4 | $72 \times 46$ | $144 \times 72 \times 110$ |
| ZSO-66 | 66 | 285-570 | 53-79 | 1,590,000 | 2,370,000 | 3 to 4 | $72 \times 46$ | $150 \times 78 \times 110$ |
| ZSO-72 | 72 | 340-680 | 64-94 | 1,920,000 | 2,820,000 | 4 to 6 | 84×46 | $168 \times 84 \times 110$ |
| ZSO-78 | 78 | 400-795 | 75-111 | 2,250,000 | 3,330,000 | 4 to 6 | Not Included | $174 \times 90 \times 110$ |
| ZSO-84 | 84 | 460-925 | 87-128 | 2,610,000 | 3,840,000 | 4 to 6 | Not Included | 180×96x110 |

Specification Bases: (For your specific water source, contact Res-Kem for estimates)
Flow Rate Range: Minimum Flow $12 \mathrm{gpm} / \mathrm{ft} 2$ to Maximum Flow $24 \mathrm{gpm} / \mathrm{ft} 2$
Resin Quantity: Bed Depth 27-40 inches
Capacity Range: Regeneration Level is $15 \mathrm{lbs} \mathrm{NaCl} / \mathrm{ft} 3$

Area $=700$ GPM $/ 2$ units $=350 \mathrm{gpm} / 12 \mathrm{gpm} / \mathrm{sf}=29.2 \mathrm{sf}$ Provide 3-72" Dia. (1 standby)

## Water Softener Regeneration

$$
\begin{aligned}
\text { Regeneration } & =84^{\prime \prime} \text { Dia. Bed Capacity/ Loading } \\
& =\frac{2,400,000 \text { Grains Hardness }}{360 \mathrm{mg} / \mathrm{l} / 17.1 \mathrm{mg} / \mathrm{l} / \text { grain }}
\end{aligned}
$$

$=\frac{2,400,000 \mathrm{gr} \times 3 \mathrm{beds}}{700 \mathrm{gpm} \times 21.05 \mathrm{gr} / \mathrm{gallon}}$
= 8.4 hours / bed @ 1 MGD flow

## Stabilization for Corrosion Control

- Increasing Ca hardness, alkalinity or pH:
- Increase scaling and decrease corrosive tendency
- Increasing temperature:
- Increase scaling and corrosive tendency
- TDS can affect scaling and corrosivity

STABILIZATION<br>Process of<br>making water<br>less corrosive and less<br>depositing

- Caustic soda is commonly used as an acidity buffer
- Unstable water: red water, lead and copper corrosion problems
- Orthophosphates, silicates used to prevent lead \& copper corrosion, sequester Ca \& carbonate
- CCPP: Calcium Carbonate Precipitation Potential


## Conclusions

- Assess variability in raw water quality analysis and water demand.
- Assess impact of process improvements for aeration, mixing, settling, recarb, filters, chemical feed, and solids handling.
- Establish effluent water quality goals.
- Establish EPA rules and water quality standards.
- Evaluate options and improvements needed to meet goals.
- Estimate any additional O\&M costs or savings.
- Prepare Capital Improvement Plan with prioritized improvement plan, budgetary costs, impact on rates, and funding sources.


## Thank You!

 WATER \& WASTE WATER DISTRIIUTIIAN
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## Any Questions?

