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STRUCTURAL CALCULATION REPORT

CITY OF PLACENTIA

STRUCTURAL ANALYSIS

FOR PROJECT

(E) RESIDENTIAL TYPE (VB) CONSTRUCTION WALL REMOVAL

PROJECT ADDRESS

1914 Brookhaven Ave, Placentia, CA 92870



PER

 ${\it ASCE 7-22~MINIMUM~DESIGN~LOADS~FOR~BUILDINGS~\&~OTHER~STRUCTURES} \label{eq:ascellation} (E)~LOAD~BEARING~WALL~REMOVAL~\&~INSTALLATION~OF~NEW~STEEL~SUPPORT~BEAM.$











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Address:

1914 Brookhaven Ave Placentia, California

92870

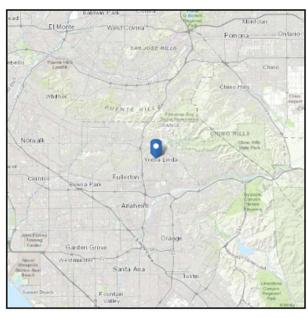
ASCE Hazards Report

Standard: ASCE/SEI 7-22 Latitude: 33.896943
Risk Category: || Longitude: -117.859032

Soil Class: Default Elevation: 335.79396899343817 ft

(88 **DVAM**)





Wind

Results:

Wind Speed 95 Vmph 10-year MRI 66 Vmph 25-year MRI 72 Vmph 50-year MRI 76 Vmph 100-year MRI 81 Vmph 300-year MRI 89 Vmph 700-year MRI 95 Vmph 1,700-year MRI 102 Vmph 3,000-year MRI 106 Vmph 10,000-year MRI 115 Vmph 100,000-year MRI 133 Vmph 1,000,000-year MRI 151 Vmph

Data Source: ASCE/SEI 7-22, Fig. 26.5-1B and Figs. CC.2-1–CC.2-4, and Section 26.5.2

Date Accessed: Tue May 28 2024









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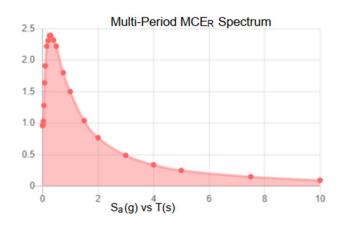


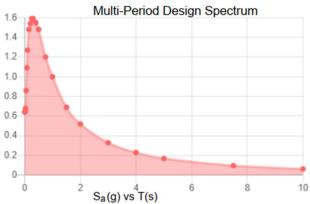


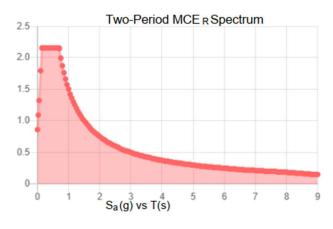
Seismic

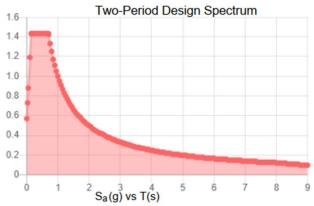
Site Soil Class: Results:	Default			
PGA _M :	0.86	T _L :	8	
S _{MS} :	2.15	S _s :	2.01	
S _{M1} :	1.5	S ₁ :	0.7	
S _{DS} :	1.43	V _{S30} :	260	
S _{D1} :	1			

Seismic Design Category: D









MCE_R Vertical Response Spectrum Vertical ground motion data has not yet been made available by USGS. Design Vertical Response Spectrum Vertical ground motion data has not yet been made available by USGS.

AFFILIATIONS









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BUILDING LO	BUILDING LOAD CALCULATION (ROOF)								
LOAD TPYE	DEAD LOAD								
LOAD LEVEL	ROOF								
LEVEL AREA (SQ.FT)	1,460.0								
LOUD SOURCE	LOAD (P.S.F)	TOTAL LOAD (LBS)							
ROOFING MATERIALS (SHINGLES)	2.5	3,650.0							
SHEATHING	1.8								
RAFTER AND TRUSSES	4.0								
INSULATION	1.0								
UNDERLAYMENT	0.5								
CEILING FINISHES	2.2								
MICELLANEOUS LOAD									
STRUCTURAL MEMBERS	2.0								
TOTAL DEAD LOAD (15 MIN)	15.0	3,650.0							
ATTIC DEAD LOAD (IF EXIST)	15.0								
DESIGN LOAD:	30.0								









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BUI	LDING LOAD CALCULATION (FLO	OOR)
LOAD TPYE	DEAD LOAD	
LOAD LEVEL	1ST FLOOR	
LEVEL AREA (SQ.FT)	1,460.0	
LOUD SOURCE	LOAD (P.S.F)	TOTAL LOAD (LBS)
CONCRETE SLAB	12.5	18,250.0
FLOOR FINISH (CARPET)	1.0	1,460.0
FLOOR FINISH (TILE)	7.0	10,220.0
HARWOOKD FLOORING	3.5	5,110.0
SUBFLOOR (PLYWOOD)	2.2	3,212.0
JOISTS & BEAMS	2.0	2,920.0
UTILITIES & DUCT WORK	2.1	3,066.0
GYPSUM BOARD	2.2	3,212.0
TOTAL DEAD LOAD	20.0	47,450.0
DESIGN LOAD :	20.0	









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	SEISMIC DESIGN CRITERIA & PARAMETERS PER ASCE 7-22										
Site Classification= (Default)		D	ASCE 7-22 Section 11.4.2								
Risk Category=		II	ASCE 7-22 Table 1.5-1								
Seismic Design Category=		D	ASCE 7-22 Section 11.6								
Importance Factor=	I=	1	ASCE 7-22 Section 11.5 Table 1.5-2								
Response Modification Factor	R=	6.5	ASCE 7-22 Table 12.2-1 (light frame wood shear walls)								
System Overstrength Factor	Ω_0 =	3	ASCE 7-22 Table 12.2-1								
Deflection Amplification Factor	C _d =	4	ASCE 7-22 Table 12.2-1								
Rho Factor (ρ)	ρ=	1.3	ASCE 7-22 Section 12.3.4.2 Reliability Redundancy Factor								
Approximate Fundamental Period	T =	0.4	ASCE 7-22 Section 12.8-2								
Long Period	$T_L =$	8	ASCE 7-22 Figure 22-14 to 22-17 ASCE 7 Hazard Report								
Spectral Response Short Period	S _s =	2.01	ASCE 7-22 Chapter 22 ASCE 7 Hazard Report								
Spectral Response Long Period	$S_1 =$	0.7	ASCE 7-22 Chapter 22 ASCE 7 Hazard Report								
Short Period Site Coefficien Fa=	t	1. 1	ASCE 7-22 Section 11.4.4 Site Coefficients MCER								
Long Period Site Coefficient	$F_{V}=$	2.5	ASCE 7-22 Section 11.4.4 Site Coefficients MCER								
Spectral Response Accelerations Short	S _{MS} =FaS _s =	2.15	ASCE 7-22 Section 11.4.4 Site Coefficients MCE _R								
Spectral Response Accelerations Long	$S_{M1}=FvS_1=$	1.5	ASCE 7-22 Section 11.4.4 Site Coefficients MCER								
Spectral Response Short Period	S _{DS} =	1.43	ASCE 7-22 Section 11.4.5 Design Spectral Acceleration.								
Spectral Response Long Period	$S_{D1}=$	1	ASCE 7-16 Section 11.4.5 Design Spectral Acceleration								
$T_s = (S_{D1} / S_{DS})$	$T_s=$	0.76	ASCE 7-22 Section 11.4.6 .095<1.5xTs=0.830*								
Coefficient as determined from table 12.8-2	C _t =	0.02	ASCE 7-22 table 12.8-2								
Structural Height as defined in section 11.2	h _n =	14.5	ASCE 7-22 table 12.8-2								
Coefficient as determined from table 12.8-2	x =	0.75	ASCE 7-22 Section 12.8-2								
Approximate Fundamental Period	$T_a = (Ct * h_n^X) =$	0.148	ASCE 7-22 Section 12.8-8								
Seismic Response Coefficient	CS =	0.17875	ASCE 7-22 Eq. 12.8-2 Seismic Response Coefficient								
Maximum Seismic Response Coefficient	Cs _{max} =	0.17875	ASCE 7-22 Eq. 12.8-3 Maximum								
Minimum Seismic Response Coef	ficient	.00793	ASCE 7-22 Eq. 12.8-5 or 12.8-6 Minimum								
*Site specific ground motion analysis is a	not required per ASC	E 7-22 Section 11.4.8 Exce	eption 2 Seismic Design Category specified from Table 11.4-2								
			·								

• Minimum C_s :

$$C_s \geq rac{0.044 imes S_{DS} imes I}{R} \ C_s \geq rac{0.044 imes 1.43 imes 1.0}{8} = 0.00793$$

• Maximum
$$C_s$$
:

$$C_s \leq rac{S_{DS}}{R} \ C_s \leq rac{1.43}{8} = 0.17875$$

<u>AFFILIATIONS</u>







$C_s = rac{S_{DS}}{R/I}$

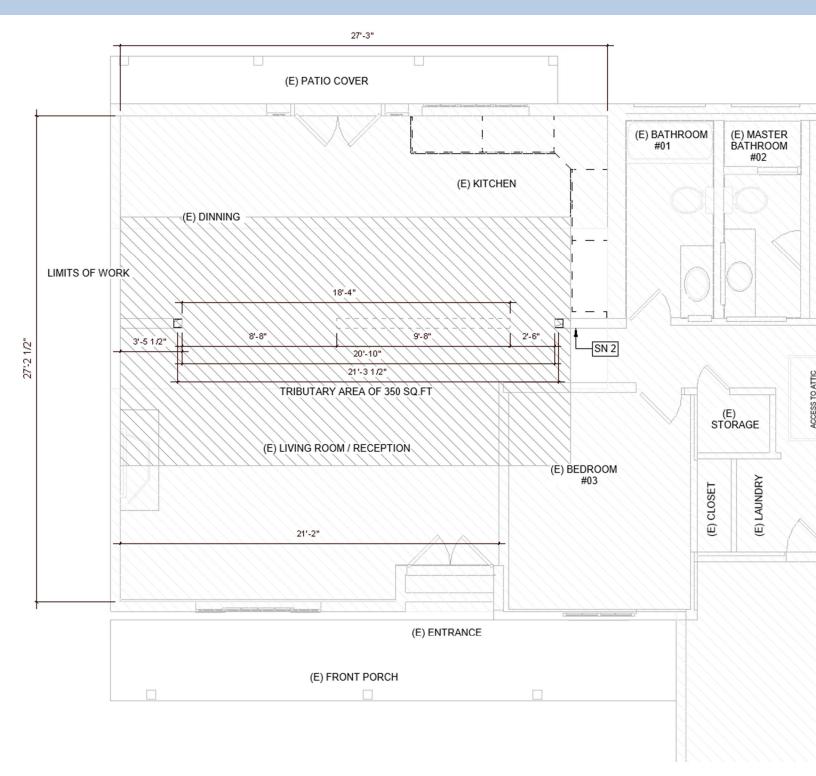
Substituting the values:

$$C_s = \frac{1.43}{8/1.0} = 0.17875$$



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MEMBERS TRIBUTARY AREAS & LOAD CALCULATION













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MEMBER LOAD CALCULATION			
MEMBER TAG	BM-1		
MATERIALS	STEEL		
TRIBUTARY AREA (SQ.FT)	350.0		
LEGNTH	21.3		
LOUD SOURCE	LOAD (P.S.F)	TOTAL LOAD (LBS)	LOAD P.L.F (LB/F)
DEAD LOAD (FLOOR)	0.0	0.0	0.0
DEAD LOAD (ROOF)	30.0	10,500.0	494.1
LIVE LOAD (ROOF)	15.0	5,250.0	247.1
LIVE LOAD (ATTIC)		0.0	0.0
LIVE LOAD (FLOOR)		0.0	0.0
SEISMIC LOAD		0.0	0.0
WIND LOAD		0.0	0.0
SNOW LOAD		0.0	0.0
TOTAL LOAD	45.0	15,750.0	741.2
	P.S.F	LBS	LBS PER LINEAR FOOT
DESIGN LOAD (K/L.F)	0.7	LOAD PER SUPPORT	7,875.0









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Project File: KEVIN CHANG PLACENTIA.ec6 **Steel Beam**

LIC#: KW-06018864, Build:20.24.01.31 ACC & Engineering (c) ENERCALC INC 1983-2023

DESCRIPTION: BM-1 LOAD CHECK

CODE REFERENCES

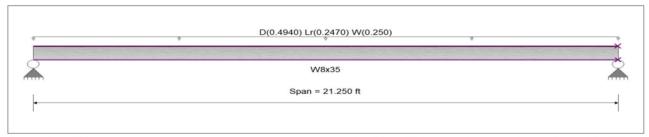
Calculations per AISC 360-16, IBC 2018, CBC 2019, ASCE 7-16

Load Combination Set: IBC 2021

Material Properties

Analysis Method Load Resistance Factor Design Fy: Steel Yield: 50.0 ksi Beam Bracing: Beam is Fully Braced against lateral-torsional buckling E: Modulus: 29,000.0 ksi

Bending Axis: Major Axis Bending



Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Beam self weight calculated and added to loading
Uniform Load: D = 0.4940, Lr = 0.2470, W = 0.250 k/ft, Tributary Width = 1.0 ft, (UNIFORM DL & Lr @T.A OF 350 SQ.FT) D=45 P.S.F)

DESIGN SUMMARY				Design OK
Maximum Bending Stress Ratio =	0.501:1	0.501 : 1 Maximum Shear Stress Ratio =		
Section used for this span	W8x35	Section used for this span		W8x35
Mu : Applied	65.194 k-ft		Vu : Applied	12.272 k
Mn * Phi : Allowable	130.125 k-ft		Vn * Phi : Allowable	75.516 k
Load Combination	+1.20D+1.60Lr+0.50W		Combination tion of maximum on span	+1.20D+1.60Lr+0.50W 0.000 ft
Span # where maximum occurs	Span # 1	Span	# where maximum occurs	Span # 1
Maximum Deflection				
Max Downward Transient Deflection	0.313 in Ratio =	815 >=360.	Span: 1: W Only	
Max Upward Transient Deflection	0 in Ratio =	0 <360.0	n/a	
Max Downward Total Deflection	1.035 in Ratio =	246 >=240.	Span: 1: +D+0.750Lr+0.450	OW .
Max Upward Total Deflection	0 in Ratio =	0 <240.0	n/a	

Maximum Forces & Stresses for Load Combinations

Load Combination		Max Stres	s Ratios	Su	mmary of Mo	ment Va	lues			Summar	y of She	ar Values
Segment Length	Span #	M	V	nax Mu + max Mu -	Mu Max	Mnx	Phi*Mnx	Cb	Rm	VuMax	Vnx	Phi*Vnx
+1.40D												
Dsgn. L = 21.25 ft	1	0.321	0.104	41.80	41.80	144.58	130.13	1.00	1.00	7.87	75.52	75.5
+1.20D+0.50Lr												
Dsgn. L = 21.25 ft	1	0.329	0.107	42.80	42.80	144.58	130.13	1.00	1.00	8.06	75.52	75.5
+1.20D												
Dsgn. L = 21.25 ft	1	0.275	0.089	35.83	35.83	144.58	130.13	1.00	1.00	6.74	75.52	75.5
+1.20D+1.60Lr												
Dsgn. L = 21.25 ft	1	0.447	0.145	58.14	58.14	144.58	130.13	1.00	1.00	10.94	75.52	75.5
+1.20D+1.60Lr+0.50W												
Dsgn. L = 21.25 ft	1	0.501	0.163	65.19	65.19	144.58	130.13	1.00	1.00	12.27	75.52	75.5
+1.20D+0.50W												
Dsgn. L = 21.25 ft	1	0.330	0.107	42.89	42.89	144.58	130.13	1.00	1.00	8.07	75.52	75.5
+1.20D+0.50Lr+W												
Dsgn. L = 21.25 ft	1	0.437	0.142	56.91	56.91	144.58	130.13	1.00	1.00	10.71	75.52	75.5
+1.20D+W												
Dsgn. L = 21.25 ft	1	0.384	0.124	49.94	49.94	144.58	130.13	1.00	1.00	9.40	75.52	75.5
+0.90D+W												
Dsgn. L = 21.25 ft	1	0.315	0.102	40.98	40.98	144.58	130.13	1.00	1.00	7.71	75.52	75.5
+0.90D												
Dsgn. L = 21.25 ft	1	0.207	0.067	26.87	26.87	144.58	130.13	1.00	1.00	5.06	75.52	75.5









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Steel Beam Project File: KEVIN CHANG PLACENTIA.ec6

LIC#: KW-06018864, Build:20.24.01.31 ACC & Engineering (c) ENERCALC INC 1983-2023

DESCRIPTION: BM-1 LOAD CHECK

Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl Lo	ocation in Span	Load Combination	Max. "+" Defl	Location in Spar
+D+0.750Lr+0.450W	1	1.0346	10.686		0.0000	0.000
/ertical Reactions			Suppor	t notation : Far left is #1	Values in KIPS	
Load Combination		Support 1	Support 2			
Max Upward from all Load	Conditions	8.784	8.784			
Max Upward from Load Cor	mbinations	8.784	8.784			
Max Upward from Load Cas	ses	5.621	5.621			
D Only		5.621	5.621			
+D+Lr		8.245	8.245			
+D+0.750Lr		7.589	7.589			
+D+0.60W		7.214	7.214			
+D+0.750Lr+0.450W		8.784	8.784			
+D+0.450W		6.816	6.816			
+0.60D+0.60W		4.966	4.966			
+0.60D		3.372	3.372			
Lr Only		2.624	2.624			
W Only		2.656	2.656			









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Project File: KEVIN CHANG PLACENTIA.ec6 **Wood Column**

LIC#: KW-06018864, Build:20.24.01.31 (c) ENERCALC INC 1983-2023 ACC & Engineering

DESCRIPTION: 6X6 WOOD POST LAOD CHECK

Code References

Calculations per NDS 2018, IBC 2018, CBC 2019, ASCE 7-16

Load Combinations Used: IBC 2021

General Information

Analysis Method	Load Resi	stance Factor	Design	Wood Section Name	6x6		
End Fixities	Top Fixed	, Bottom Fixed	I	Wood Grading/Manu	f. Graded Lu	ımber	
Overall Column I	Height on-slender calculat	tions)	8 ft	Wood Member Type	Sawn		
				Exact Width	5.50 in Al	low Stress Modification Factor	ors
Wood Species	Douglas Fir-L	arch		Exact Depth	5.50 in	Cf or Cv for Bending	1.0
Wood Grade	No.2			Area	30.250 in^2	Cf or Cv for Compression	1.0
Fb +	900.0 psi	Fv	180.0 psi	lx	76.255 in^4	Cf or Cv for Tension	1.0
Fb -	900.0 psi	Ft	575.0 psi	ly	76.255 in 4	Cm : Wet Use Factor	1.0
Fc - Prll	1,350.0 psi	,	31.210 pcf	,	70.255 111 4	Ct : Temperature Fact	1.0
Fc - Perp	625.0 psi					Cfu : Flat Use Factor	1.0
E: Modulus of E	lasticity	x-x Bending	y-y Bending	Axial		Kf : Built-up columns	1.0
	Basic	1,600.0	1,600.0	1,600.0 ksi		Use Cr : Repetitive ?	No
	Minimum	580.0	580.0	Column Buckling Condition:		-	

Fully braced against buckling ABOUT X-X Axis

Fully braced against buckling ABOUT Y-Y Axis

Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Column self weight included : 52.450 lbs * Dead Load Factor

AXIAL LOADS

BEAM REACTIONS: Axial Load at 8.0 ft, D = 7.70, Lr = 7.70 k

BENDING LOADS

CONSERVATIVE: Lat. Uniform Load creating My-y, E = 0.20 k/ft

DESIGN SUMMARY

Bending & Shear Check Results	
PASS Max. Axial+Bending Stress Ratio =	0.5240 : 1
Load Combination	+1.20D+E
Governing NDS Forumla Comp + Myy	, NDS Eq. 3.9-3
Location of max.above base	0.0 ft
At maximum location values are .	
Applied Axial	9.303 k
Applied Mx	0.0 k-ft
Applied My	-1.067 k-ft
Fc : Allowable	2,916.0 psi
PASS Maximum Shear Stress Ratio =	0.06802 : 1
Load Combination	+0.90D+E
Location of max.above base	0.0 ft

Maximum SERVICE Lateral Load Reactions . .

Top along Y-Y Bottom along Y-Y 0.0 k 0.0 k Top along X-X 0.80 k Bottom along X-X 0.80 k

Maximum SERVICE Load Lateral Deflections . . .

Along Y-Y 0.0 in at 0.0 ft above base

for load combination: n/a

0.03022 in at Along X-X 4.027 ft above base

for load combination: E Only

Other Factors used to calculate allowable stresses . . .

<u>Be</u>	naing	Compression	Tension
LRFD - Format Conversion factor	2.541	2.400	2.700
LRFD - Resistance factor	0.850	0.900	0.800

Load Combination Results

Applied Design Shear Allowable Shear

			Maximum Axial	+ Bending	Stress Ratios	Maximu	Maximum Shear Ratios				
Load Combination	Lambda	CP	Stress Ratio	Status	Location	Stress Ratio	Status	Location			
+1.40D	1.000	1.000	0.1230	PASS	0.0 ft	0.0	PASS	0.0 ft			
+1.20D+0.50Lr	1.000	1.000	0.1491	PASS	0.0 ft	0.0	PASS	0.0 ft			
+1.20D	1.000	1.000	0.1055	PASS	0.0 ft	0.0	PASS	0.0 ft			
+1.20D+1.60Lr	1.000	1.000	0.2451	PASS	0.0 ft	0.0	PASS	0.0 ft			
+1.20D+E	1.000	1.000	0.5240	PASS	0.0 ft	0.06802	PASS	0.0 ft			
+0.90D	1.000	1.000	0.07910	PASS	0.0 ft	0.0	PASS	0.0 ft			
+0.90D+E	1.000	1.000	0.5192	PASS	0.0 ft	0.06802	PASS	0.0 ft			

59.504 psi

388.80 psi









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Wood Column		Project File: KEVIN CHANG PLACENTIA.ec6
LIC#: KW-06018864, Build:20.24.01.31	ACC & Engineering	(c) ENERCALC INC 1983-2023

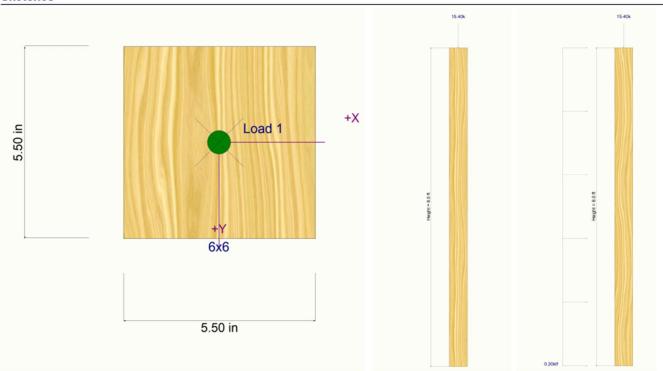
DESCRIPTION: 6X6 WOOD POST LAOD CHECK

Maximum Reactions							Note: O	nly non-zero	reactions a	re listed.
	X-X Axis R	eaction k	Y-Y	Axis	Reaction	Axial Reaction	My - End Mo	oments k-ft	Mx - End	Moments
Load Combination	@ Base	@ Top	@	Base	@ Top	@ Base	@ Base	@ Top	@ Base	@ Top
D Only						7.752				
+D+Lr						15.452				
+D+0.750Lr						13.527				
+D+0.70E	0.560	0.560				7.752	0.747	-0.747		
+D+0.5250E	0.420	0.420				7.752	0.560	-0.560		
+0.60D						4.651				
+0.60D+0.70E	0.560	0.560				4.651	0.747	-0.747		
Lr Only						7.700				
E Only	0.800	0.800					1.067	-1.067		

Maximum Deflections for Load Combinations

Load Combination	Max. X-X Deflection	Distance	Max. Y-Y Deflection	Distance
D Only	0.0000 in	0.000ft	0.000 in	0.000 ft
+D+Lr	0.0000 in	0.000ft	0.000 in	0.000 ft
+D+0.750Lr	0.0000 in	0.000ft	0.000 in	0.000 ft
+D+0.70E	0.0212 in	4.027ft	0.000 in	0.000ft
+D+0.5250E	0.0159 in	4.027ft	0.000 in	0.000 ft
+0.60D	0.0000 in	0.000ft	0.000 in	0.000ft
+0.60D+0.70E	0.0212 in	4.027ft	0.000 in	0.000 ft
Lr Only	0.0000 in	0.000ft	0.000 in	0.000 ft
E Only	0.0302 in	4.027ft	0.000 in	0.000 ft

Sketches



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Project File: KEVIN CHANG PLACENTIA.ec6

General Footing (c) ENERCALC INC 1983-2023 LIC#: KW-06018864, Build:20.24.01.31 ACC & Engineering

DESCRIPTION: FOUNDATION LOAD CHECK

Code References

Calculations per ACI 318-14, IBC 2018, CBC 2019, ASCE 7-16

Load Combinations Used: IBC 2021

General Information

fc : Concrete 28 day strength fy : Rebar Yield Ec : Concrete Elastic Modulus Concrete Density φ Values Flexure	= = =	2,85 14	2.50 ksi 60.0 ksi 60.0 ksi 55.0 pcf 0.90	Allowable Soil Bearing Soil Density Increase Bearing By Footing Weight Soil Passive Resistance (for Sliding) Soil/Concrete Friction Coeff.	= = = =	1.50 ksf 110.0 pcf No 100.0 pcf 0.30
Shear Analysis Settings Min Steel % Bending Reinf. Min Allow % Temp Reinf. Min. Overturning Safety Factor	=	0.° = = =	0.00180 1.0 : 1	Increases based on footing Depth Footing base depth below soil surface Allow press. increase per foot of depth when footing base is below	= = =	2.0 ft ksf ft
Min. Sliding Safety Factor Add Ftg Wt for Soil Pressure Use ftg wt for stability, moments & s Add Pedestal Wt for Soil Pressure Use Pedestal wt for stability, mom 8		: :	1.0:1 Yes Yes No Yes	Increases based on footing plan dimensional Allowable pressure increase per foot of de when max. length or width is greater than	epth =	ksf ft

Dimensions

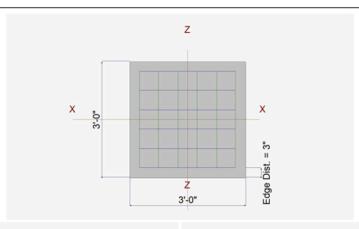
Width parallel to X-X Axis	=	3.0 ft
Length parallel to Z-Z Axis	=	3.0 ft
Footing Thickness	=	24.0 in

Pedestal dimensions.. px: parallel to X-X Axis pz : parallel to Z-Z Axis in Height Rebar Centerline to Edge of Concrete... at Bottom of footing = 3.50 in

Reinforcing

Bars parallel to X-X Axis Number of Bars Reinforcing Bar Size 5 Bars parallel to Z-Z Axis Number of Bars 6 5 Reinforcing Bar Size Bandwidth Distribution Check (ACI 15.4.4.2) Direction Requiring Closer Separation n/a # Bars required within zone n/a

Bars required on each side of zone







Applied Loads

		D	Lr	L	S	W	E	H
P : Column Load OB : Overburden	= _	3.950	6.80 0.0					k ksf
M-xx M-zz	= =						0.0 0.0	k-ft k-ft
V-x V-z	= -						0.0 0.0	k k

n/a









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Project File: KEVIN CHANG PLACENTIA.ec6

+1.20D+1.60Lr

Stability Ratio

DIR | PW-LR-1000801097 DPELSG | 39074 CSLB | 1073807

General Footing

LIC#: KW-06018864, Build:20.24.01.31

DESCRIPTION: FOUNDATION LOAD CHECK

2-way Punching

ACC & Engineering

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DESIGN SUMMARY Design OK Capacity Min. Ratio Item **Applied Governing Load Combination PASS** 0.9893 Soil Bearing 1.484 ksf 1.50 ksf +D+Lr about Z-Z axis **PASS** n/a Overturning - X-X 0.0 k-ft 0.0 k-ft No Overturning Overturning - Z-Z PASS n/a 0.0 k-ft 0.0 k-ft No Overturning PASS n/a Sliding - X-X 0.0 k 0.0 k No Sliding PASS n/a Sliding - Z-Z 0.0 k 0.0 k No Sliding **PASS** n/a Uplift 0.0 k 0.0 k No Uplift 0.03540 Z Flexure (+X) +1.20D+1.60Lr **PASS** 1.953 k-ft/ft 55.160 k-ft/ft Z Flexure (-X) 0.03540 1.953 k-ft/ft 55.160 k-ft/ft +1.20D+1.60Lr PASS **PASS** 0.03540 X Flexure (+Z) 1.953 k-ft/ft 55.160 k-ft/ft +1.20D+1.60Lr PASS 0.03540 X Flexure (-Z) 1.953 k-ft/ft 55.160 k-ft/ft +1.20D+1.60Lr **PASS** n/a 1-way Shear (+X) 0.0 psi 75.0 psi n/a PASS 0.0 1-way Shear (-X) 0.0 psi 0.0 psi n/a PASS n/a 1-way Shear (+Z) 0.0 psi 75.0 psi n/a **PASS** n/a 1-way Shear (-Z) 0.0 psi 75.0 psi n/a

PASS Detailed Results

Soil Bearing Rotation Axis &		Xecc	Zecc	Actual	Soil Bearing S	Stress @ Loc	ation	Actual / Allow
Load Combination	Gross Allowable	(ir		Bottom, -Z	Top, +Z	Left, -X	Right, +X	Ratio
X-X, D Only	1.50	n/a	0.0	0.7289	0.7289	n/a	n/a	0.486
X-X, +D+Lr	1.50	n/a	0.0	1.484	1.484	n/a	n/a	0.989
X-X, +D+0.750Lr	1.50	n/a	0.0	1.296	1.296	n/a	n/a	0.864
X-X, +0.60D	1.50	n/a	0.0	0.4373	0.4373	n/a	n/a	0.292
Z-Z, D Only	1.50	0.0	n/a	n/a	n/a	0.7289	0.7289	0.486
Z-Z, +D+Lr	1.50	0.0	n/a	n/a	n/a	1.484	1.484	0.989
Z-Z, +D+0.750Lr	1.50	0.0	n/a	n/a	n/a	1.296	1.296	0.864
Z-Z, +0.60D	1.50	0.0	n/a	n/a	n/a	0.4373	0.4373	0.292

75.0 psi

Resisting Force

6.378 psi

Overturning Stability

Rotation Axis & Load Combination	Overturning Moment	Resisting Moment	Stability Ratio	Status	
Footing Has NO Overturning					_

Sliding Stability

Sliding Force

Force Application Axis Load Combination...

Footing Has NO Sliding

Footing Flexure

Flexure Axis & Load Combination	Mu k-ft	Side	Tension Surface	As Req'd in^2	Gvrn. As in^2	Actual As in^2	Phi*Mn k-ft	Status
X-X, +1.40D	0.6913	+Z	Bottom	0.5184	ACI 7.6.1.1	0.620	55.160	ок
X-X, +1.40D	0.6913	-Z	Bottom	0.5184	ACI 7.6.1.1	0.620	55.160	OK
X-X, +1.20D+0.50Lr	1.018	+Z	Bottom	0.5184	ACI 7.6.1.1	0.620	55.160	OK
X-X, +1.20D+0.50Lr	1.018	-Z	Bottom	0.5184	ACI 7.6.1.1	0.620	55.160	OK
X-X, +1.20D	0.5925	+Z	Bottom	0.5184	ACI 7.6.1.1	0.620	55.160	OK
X-X, +1.20D	0.5925	-Z	Bottom	0.5184	ACI 7.6.1.1	0.620	55.160	OK
X-X, +1.20D+1.60Lr	1.953	+Z	Bottom	0.5184	ACI 7.6.1.1	0.620	55.160	OK
X-X, +1.20D+1.60Lr	1.953	-Z	Bottom	0.5184	ACI 7.6.1.1	0.620	55.160	OK
X-X, +0.90D	0.4444	+Z	Bottom	0.5184	ACI 7.6.1.1	0.620	55.160	OK
X-X, +0.90D	0.4444	-Z	Bottom	0.5184	ACI 7.6.1.1	0.620	55.160	OK
Z-Z, +1.40D	0.6913	-X	Bottom	0.5184	ACI 7.6.1.1	0.620	55.160	OK
Z-Z, +1.40D	0.6913	+X	Bottom	0.5184	ACI 7.6.1.1	0.620	55.160	OK
Z-Z, +1.20D+0.50Lr	1.018	-X	Bottom	0.5184	ACI 7.6.1.1	0.620	55,160	OK
Z-Z, +1.20D+0.50Lr	1.018	+X	Bottom	0.5184	ACI 7.6.1.1	0.620	55,160	OK
Z-Z, +1,20D	0.5925	-X	Bottom	0.5184	ACI 7.6.1.1	0.620	55.160	OK
Z-Z, +1,20D	0.5925	+X	Bottom	0.5184	ACI 7.6.1.1	0.620	55,160	OK
Z-Z, +1.20D+1.60Lr	1.953	-X	Bottom	0.5184	ACI 7.6.1.1	0.620	55.160	OK







All units k

Status



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General Footing		Project File: KEVIN CHANG PLACENTIA.ec6
LIC#: KW-06018864, Build:20.24.01.31	ACC & Engineering	(c) ENERCALC INC 1983-2023
DESCRIPTION: FOUNDATION LOAD CHECK		

Footing Flexure

Flexure Axis & Load Combination	Mu k-ft	Side	Tension Surface	As Req'd in^2	Gvrn. As in^2	Actual As in^2	Phi*Mn k-ft	Status
Z-Z, +1.20D+1.60Lr	1.953	+X	Bottom	0.5184	ACI 7.6.1.1	0.620	55.160	oĸ
Z-Z, +0.90D	0.4444	-X	Bottom	0.5184	ACI 7.6.1.1	0.620	55.160	OK
Z-Z, +0.90D	0.4444	+X	Bottom	0.5184	ACI 7.6.1.1	0.620	55.160	OK
One Way Shear X								

Load Combination	Vu @ -X	Vu @ +X	Vu:Max	Phi Vn	/u / Phi*Vn	Status
+1.40D	0.00 p	si 0.00 ps	si 0.00 psi	75.00 ps	i 0.00	OK
+1.20D+0.50Lr	0.00 ps	si 0.00 ps	si 0.00 psi	75.00 ps	i 0.00	OK
+1.20D	0.00 p	si 0.00 ps	si 0.00 psi	75.00 ps	i 0.00	OK
+1.20D+1.60Lr	0.00 p	si 0.00 ps	si 0.00 psi	75.00 ps	i 0.00	OK
+0.90D	0.00 p	si 0.00 ps	0.00 psi	75.00 ps	i 0.00	OK

One Way Shear Z

Load Combination	Vu @ -Z	Vu @ +Z	Vu:Max	Phi Vn Vu	/ Phi*Vn	Status
+1.40D	0.00	osi 0.00 ps	i 0.00 psi	75.00 psi	0.00	ок
+1.20D+0.50Lr	0.00	osi 0.00 ps	i 0.00 psi	75.00 psi	0.00	OK
+1.20D	0.00	osi 0.00 ps	i 0.00 psi	75.00 psi	0.00	OK
+1.20D+1.60Lr	0.00	osi 0.00 ps	i 0.00 psi	75.00 psi	0.00	OK
+0.90D	0.00	osi 0.00 ps	i 0.00 psi	75.00 psi	0.00	OK
Two-Way "Punching" Shear			•		All units	k

Load Combination	Vu	Phi*Vn	Vu / Phi*Vn	Status
+1.40D	2.26 psi	150.00 psi	0.01505	OK
+1.20D+0.50Lr	3.32 psi	150.00 psi	0.02216	OK
+1.20D	1.94 psi	150.00 psi	0.0129	OK
+1.20D+1.60Lr	6.38 psi	150.00 psi	0.04252	OK
+0.90D	1.45 psi	150.00 psi	0.009677	OK

END OF REPORT

REGARDS,

ACC & Engineering Structural Desing Department

Design & Calculations by : BEN HAMED, A.M.ASCE, AIA Principal Engineer

Review & Stamp by : M.BAYOUMI, P.E., ASCE. Civil Engineer Of Record



AFFILIATIONS





