

# YTLA Project

## Prototype Down Converter Plate Characterization

### Timeline:

2015-Feb-12 Down Converter removed from telescope platform and brought down to Hilo

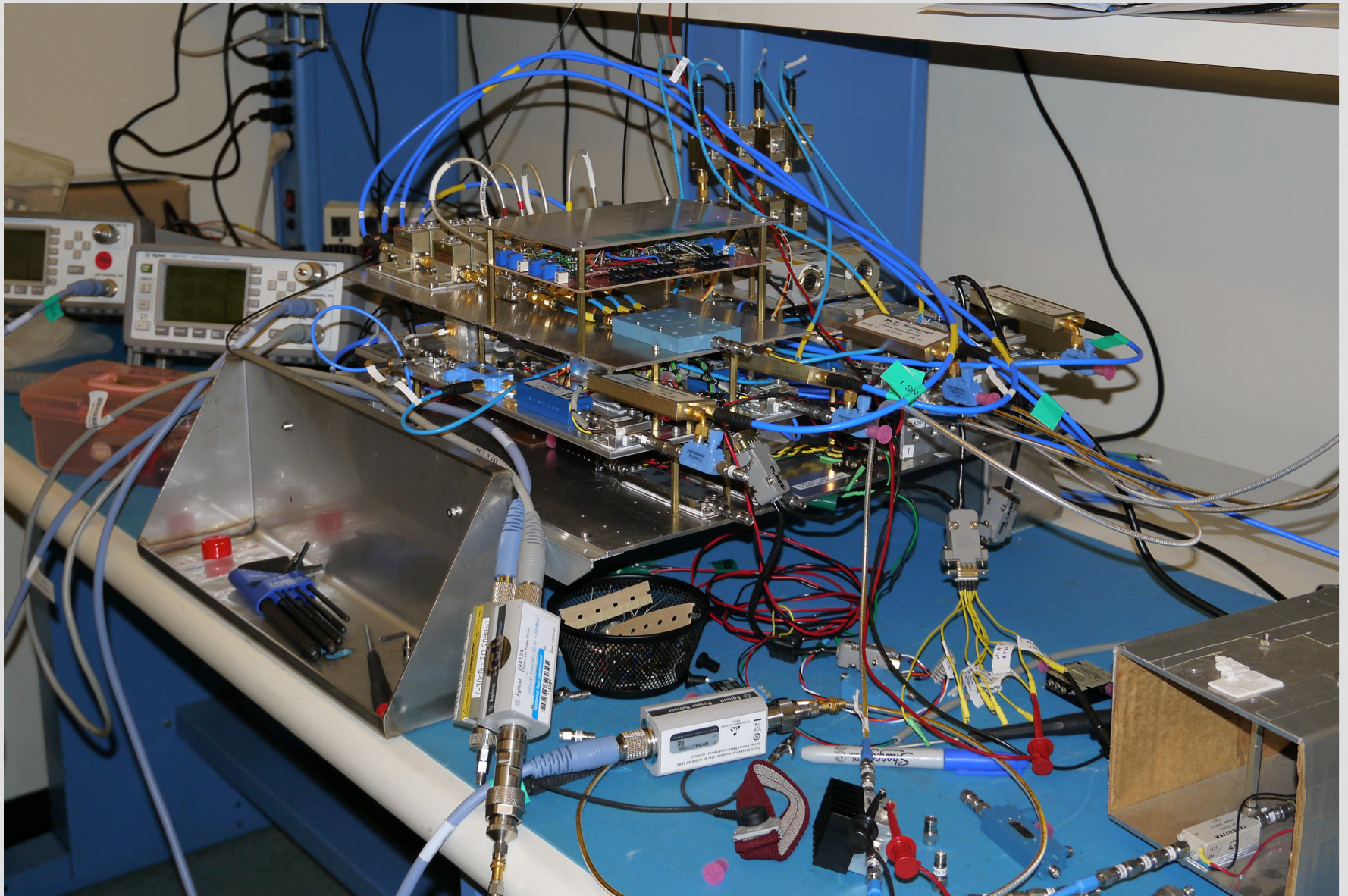
2015-Feb-25 Down Converter reinstalled on telescope platform

Filename = DC\_Plate\_Tests

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2015-Mar-4

Prototype Down Converter Plate Characterization

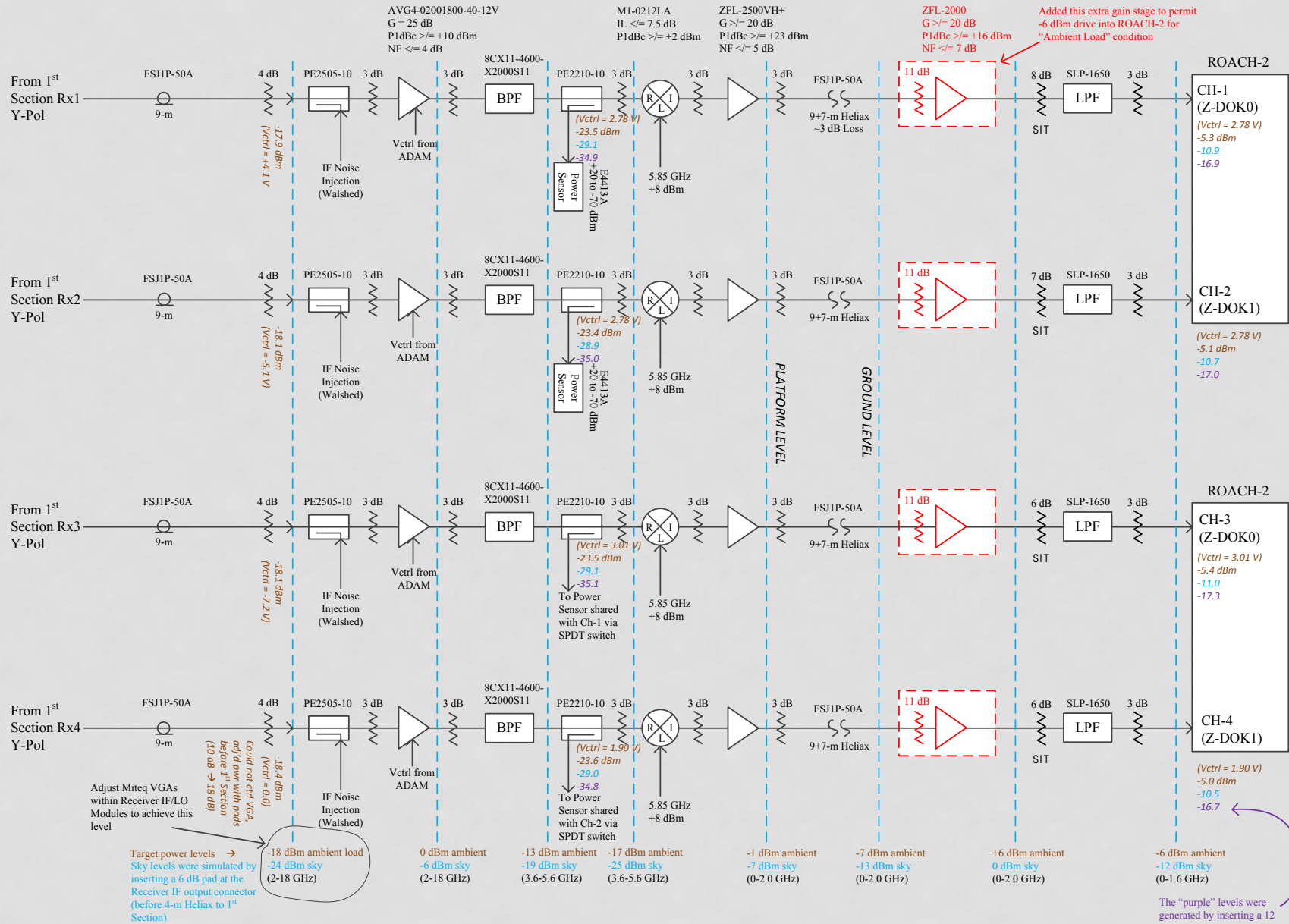


2015-Mar-4

Prototype Down Converter Plate Characterization



# "As Built Configuration" Down Converter Plate Schematic (cal noise source not shown)



# Baseband Output SNR Measurements

2-18 GHz noise source  
@ -24 dBm connected  
to down converter input

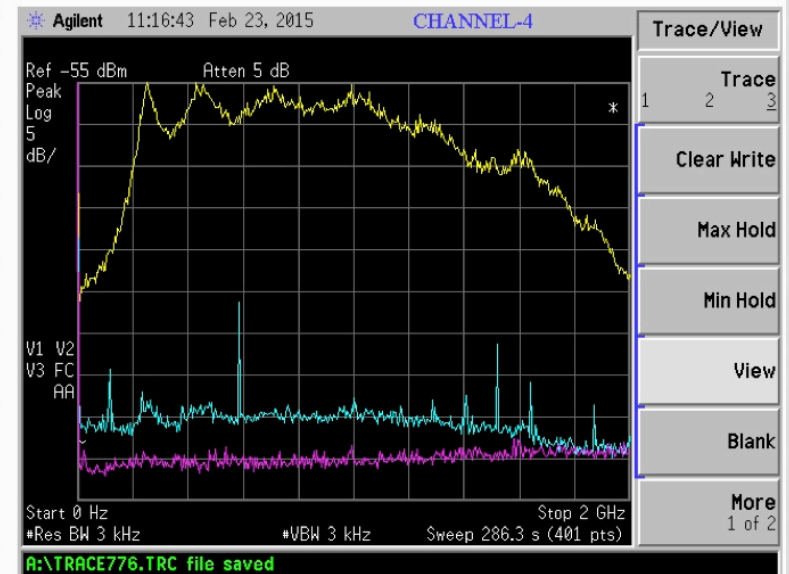
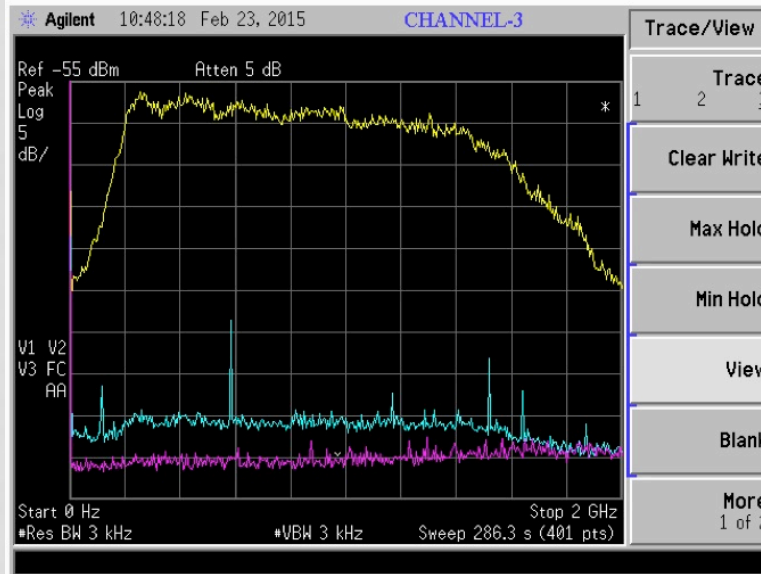
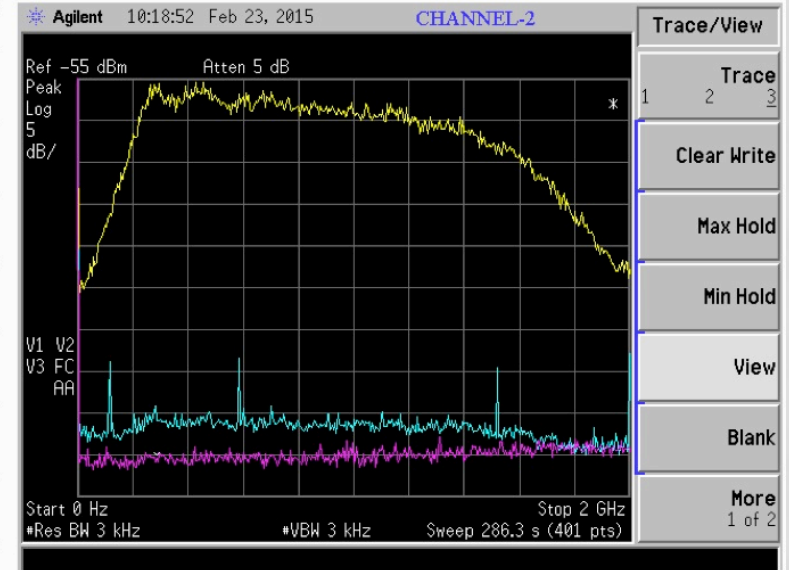
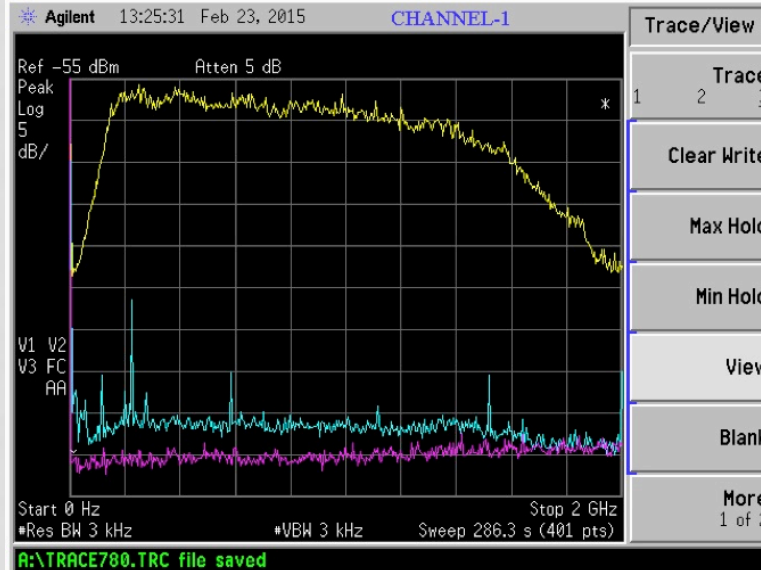
Yellow – VGAs set to  
produce -12 dBm at  
baseband output

Blue – Noise source  
removed from down  
converter input and  
terminated to 50 Ohms

Purple – Spectrum  
analyzer noise floor

Approximate spot SNRs  
at 1 GHz:

- CH1  $\geq 40$  dB
- CH2  $\geq 38$  dB
- CH3  $\geq 36$  dB
- CH4  $\geq 38$  dB





# Noise Figure Measurement and Analysis

With -24 dBm broadband noise (2-18 GHz) presented at the inputs, fine adjusted the VGA gains to produce -12 dBm at the outputs of the 4 channels.

Terminated the inputs with 50 Ohms and measured the baseband noise power level outputs for the 4 channels\*:

- CH1 = -46 dBm → SNR = 34 dB
- CH2 = -52 dBm → SNR = 40 dB
- CH3 = -51 dBm → SNR = 39 dB
- CH4 = -49 dBm → SNR = 37 dB

Noise Figure analysis to right shows equivalent noise power output of -49.5 dBm, fairly close to the measured values.

## Reduction in Y-factor due to down converter noise:

300K → -8.0 dBm → 1.585e-1 mW

LN2 → -12.0 dBm → 6.310e-2 mW

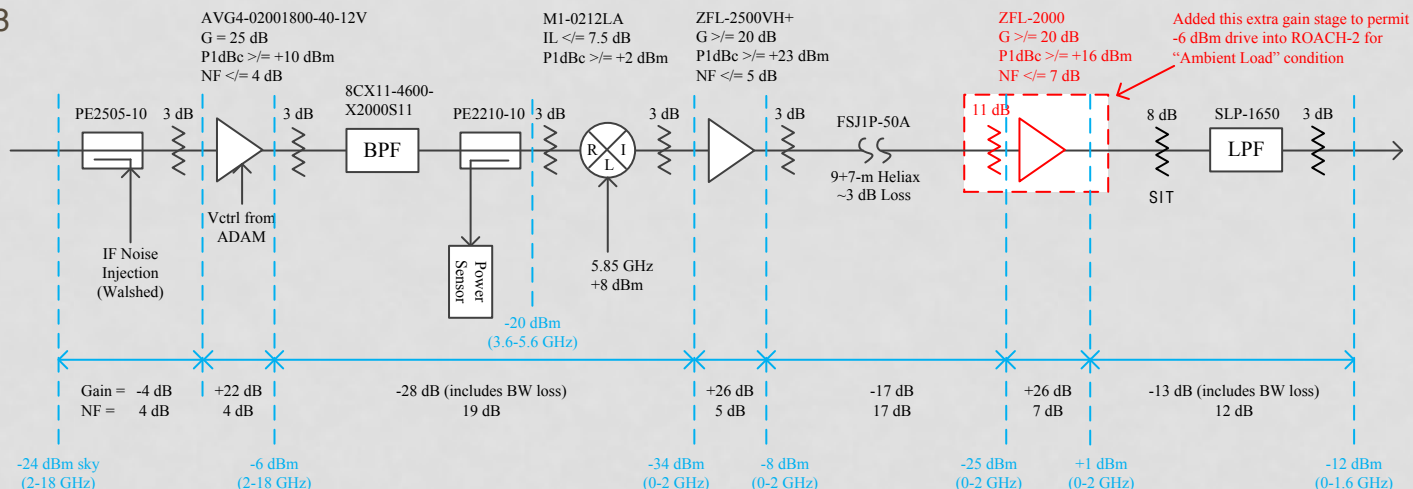
300K/LN2 = 2.5119 → **4.0000 dB**

-49 dBm → 1.259e-5 mW

(1.585e-1 + 1.259e-5)/(6.310e-2 + 1.259e-5)

= 2.5116 → **3.9995 dB**

\*Measurements may have been affected by spurs



NOISE FIGURE CALCULATOR

2015mar3

Enter values in yellow columns, if you have less than 10 items then enter in a gain of 0 dB and NF of 0 dB. Read final values shaded in green in lower right.

This spreadsheet is based on the following relationship for 2 cascaded devices:  
 $N_{Fab} = N_{Fa} + [(N_{Fb} - 1)/G_a]$



Item #	Gain (dB)	NF (dB)	gain	nf	cascaded gain	cascaded nf	Final Gain (dB)	Final NF (dB)
1	-4	4	0.40	2.51	0.40	2.51	-4.00	4.00
2	22	4	158.49	2.51	63.10	6.31	18.00	8.00
3	-19	19	0.01	79.43	0.79	7.55	-1.00	8.78
4	26	5	398.11	3.16	316.23	10.27	25.00	10.12
5	-17	17	0.02	50.12	6.31	10.43	8.00	10.18
6	26	7	398.11	5.01	2511.89	11.07	34.00	10.44
7	-12	12	0.06	15.85	158.49	11.07	22.00	10.44
8	0	0	1.00	1.00	158.49	11.07	22.00	10.44
9	0	0	1.00	1.00	158.49	11.07	22.00	10.44
10	0	0	1.00	1.00	158.49	11.07	22.00	10.44

The formula below calculates the equivalent noise output of the circuit with the input port terminated to 50 Ohms. It uses the values of G and NF determined above. Enter the bw in Hz in the yellow box below:

$P_{out} = (k \cdot T \cdot bw) \cdot g \cdot nf$  in Watts  
 $P_{out} = -174 \text{ dBm/Hz} + 10 \cdot \log(bw) + G + NF$  in dBm

bandwidth  
1.60E+09 Hz

Pout (dBm)  
-49.52

# Baseband Magnitude Response vs. VGA Gain Measurements

Broadband noise source (2-18 GHz) used as stimulus, -24 dBm

VGAs adjusted to produce +/-5 dB variations from nominal -12 dBm baseband outputs.

Blue – High output power of -7 dBm:

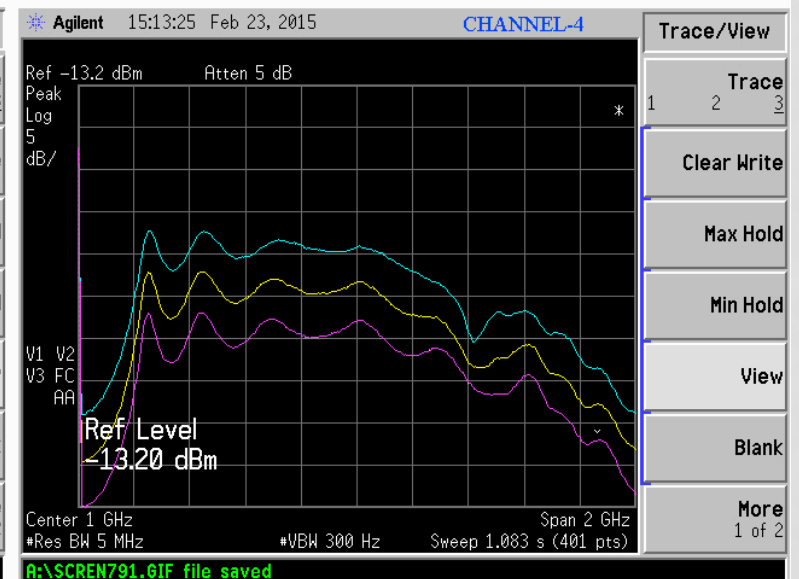
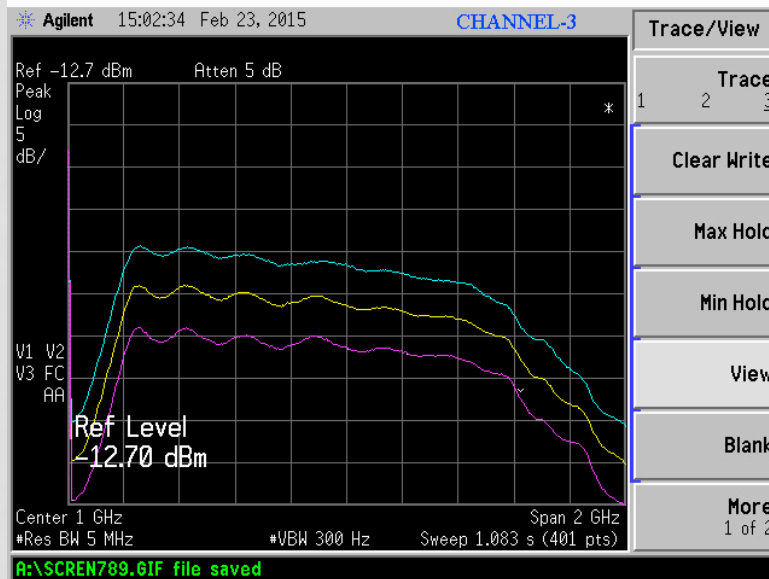
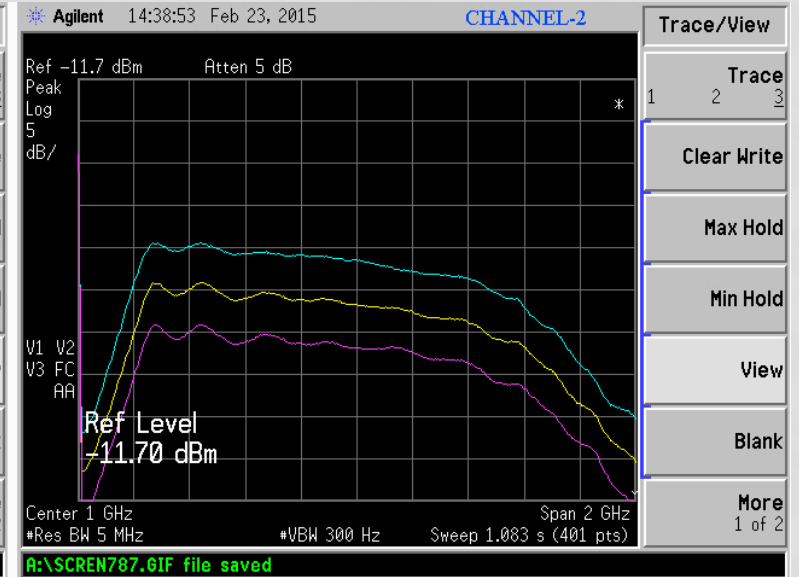
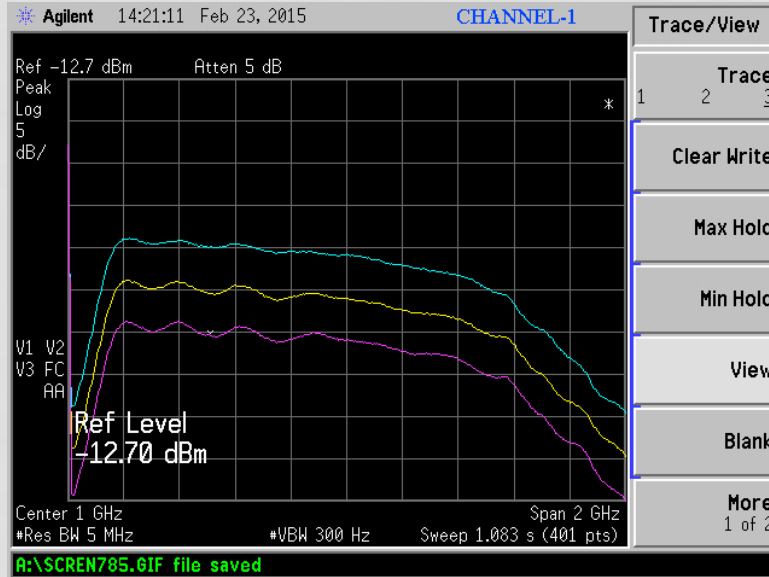
- CH1 (2.69V) = -6.6 dBm
- CH2 (2.69V) = -6.4 dBm
- CH3 (2.78V) = -7.4 dBm
- CH4 (2.68V) = -6.7 dBm

Yellow – Nominal output power of -12 dBm:

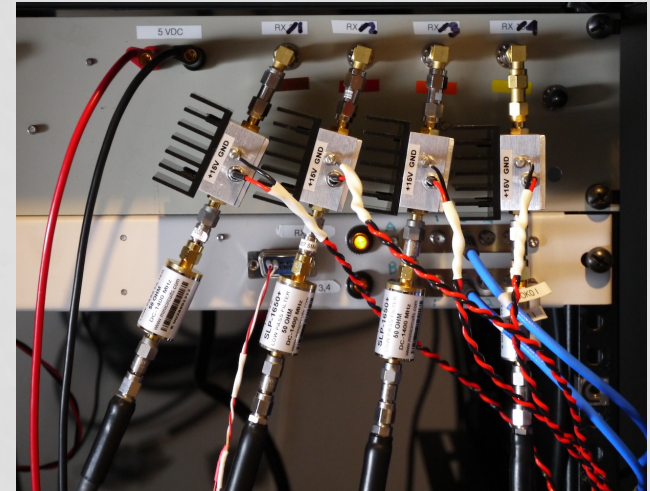
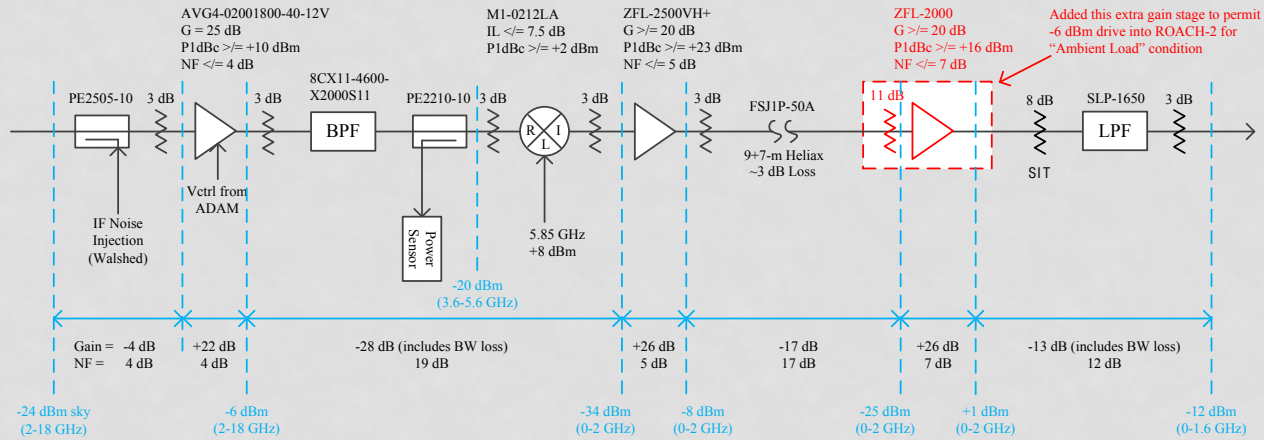
- CH1 (3.75V) = -11.8 dBm
- CH2 (3.75V) = -11.5 dBm
- CH3 (3.75V) = -12.0 dBm
- CH4 (3.75V) = -11.7 dBm

Purple – Nominal output power of -17 dBm:

- CH1 (5.61V) = -17.0 dBm
- CH2 (5.61V) = -16.7 dBm
- CH3 (5.60V) = -17.3 dBm
- CH4 (5.70V) = -16.7 dBm



# Signal Linearity Measurements (performed at Mauna Loa)



Characterized linearity shortly after plate was brought down to Hilo but results have been invalidated since the addition of the 2<sup>nd</sup> baseband amplifier (ZFL-2000)

Ran out of time so conducted a simulated Y-factor test using pads (0, 6 and 12 dB) at the receiver IF output after we installed the plate back onto the telescope platform

Changing 12 dB pad to 6 dB results in 6 dB\* change at baseband outputs and implies linear operation in this regime

Changing 6 dB pad to 0 dB results in results in 5.6 dB change at baseband outputs and implies signal compression

\*Some channels showed larger than 6 dB deltas and may be attributed to VSWR mismatch errors

Rx #	Simulated Condition	Pad at Rx Out (dB)	Coupler Pwr (dBm)	Delta Pwr (dB)	Pwr before cable (dBm)	Pwr at R2 (dBm)	Delta Pwr (dB)
1	Low	12	-34.9	0.0	-16.9	-17.6	0.0
1	Nom	6	-29.1	5.8	-10.9	-11.6	6.0
1	High	0	-23.5	11.4	-5.3	-6.0	5.6
2	Low	12	-35.0	0.0	-17.0	-17.7	0.0
2	Nom	6	-28.9	6.0	-10.7	-11.4	6.3
2	High	0	-23.5	11.4	-5.1	-5.8	5.6
3	Low	12	-35.1	0.0	-17.3	-18.0	0.0
3	Nom	6	-29.1	6.0	-11.0	-11.7	6.3
3	High	0	-23.5	11.6	-5.4	-6.1	5.6
4	Low	12	-34.8	0.0	-16.7	-17.4	0.0
4	Nom	6	-29.0	5.8	-10.5	-11.2	6.2
4	High	0	-23.6	11.2	-5.0	-5.7	5.5