_	1	2	3	4	5		6	7	8	
ſ										
	<u>GENERAL NOTES</u>									
	1. THE FOLLOWING NOT	TES ARE APPLICABLE TO ALL CO	NTRACT DOCUMENTS	PROTECTIVE SHE	TERS - GRENAD	F FAMILIARIZATION F	RANGE			
G	DISCREPANCY NOTI	EX THE CONTRACTING OFFICER	FOR CLARIFICATION		MU	NITION N	MINIMUM			
	2. UNLESS MORE STRIN	IGENT CRITERIA IS SPECIFIED IN	THE PROJECT			D				
	DOCUMENTS, ALL DE	SIGN, MATERIAL AND WORKMAN	ISHIP SHALL CONFORM TO			MET				
	THE MINIMUM REQUI	REMENTS FOUND IN THE GOVER	RNING CODES AND	FRAGMENTATION GRE	ENADE	M67	10 [33]			
	REFERENCED STAND	JARDS. JWN ON DESIGN DRAWINGS ARE								
	FLOOR ELEVATION 10	00'-0" CORRESPONDING TO A US	GS DATUM ELEVATION THAT							
	WILL VARY WITH THE	SITE ADAPTATIONS.								
	4. THE STRUCTURE SHO	OWN ON THESE DRAWINGS IS ST	FRUCTURALLY SOUND ONLY	DESI	GN EXPLOSIVE WE					
	IN THE COMPLETED F	-ORM. THE CONTRACTOR SHALL	BE RESPONSIBLE FOR THE							
	CONTRACTOR SHALL	PROVIDE TEMPORARY SUPPOR	RTS, SHORING, BRACING		E	XPLOSIVE	DISTANCE			
	AND ANY OTHER STR	RUCTURAL SYSTEMS AS REQUIR	ED TO RESIST ALL FORCES		W	/EIGHT (LB. TNT)	METERS [FEET]			
			NUNTIL THE STRUCTURE IS	WIRE/FENCE CLEA	RING	7	100 [328]			
	FULLY COMPLETED.		NG AND OTHER	WIRE/EENCE CLEARING W/		65	200 [656]			
	CONTRACTOR'S PRO	PERTY AFTER THEIR USE.				00				
	5. THE CONTRACTOR S	HALL VERIFY THE LOCATIONS O	F ALL EXISTING UTILITIES IN		G	166	100 [328]			
	THE AREA OF PROPC	SED CONSTRUCTION, BY HAND	DIGGING IF NECESSARY.	MINE CLEARING W/ LIVE	M15 MINES	166	314 [1030]			
	6. CONTRACTOR SHALL	VERIFY ALL DIMENSIONS AND E	XISTING CONDITIONS	STEEL CUTTING	G	10	100 [328]			
	DRAWINGS. ANY DISC	CREPANCIES BETWEEN FIELD CO	ONDITIONS AND THE	TIMBER CUTTIN	IG	70	100 [328]			
	CONTRACT DOCUME	NTS SHALL BE BROUGHT TO THE	E IMMEDIATE ATTENTION OF	CONCRETE OBSTA	ACLE	40	100 [328]			
	THE ENGINEER.					220	250 [924]			
	7. IT IS THE CONTRACT	OR'S RESPONSIBILITY TO FOLLO	W OSHA REQUIREMENTS			320	250 [821]			
	PHASES OF CONSTRI	UCTION	ATIONS DORING ALL		CRATER)	48	150 [492]			
Е										
				NOTE:						
				1. THE SECONDARY	FRAGMENTS FRO	OM THE INDIVIDUAL (CONCRETE			
	<u>CONCRETE NOTES</u>				L CUTTING, AND T	IMBER CUTTING STA	TIONS MUST BE			
				2 SHELTER NOT DE	SIGNED FOR LIVE	MINE CLEARING OP	FRATIONS AND			
	1. DESIGN, DETAILING		DRCED CONCRETE SHALL	BLAST RESISTAN	T GLAZING IS INAE	DEQUATE FOR M15 M	INES WITHIN THE			
	- BUILDING CODE RE	EQUIREMENTS FOR REINFORCE	D CONCRETE (ACI 318) LATEST	HAZARDOUS FRA	GMENT DISTANCE					
	EDITION			3. IF A BANGALORE	TORPEDO IS USEI		N THEN MINIMUM			
	- DETAILS AND DETA	AILING OF CONCRETE REINFORC	EMENT (ACI 315) LATEST		NOT ENCOMPASSI	ED BY THE TABLE AP	SOVE MUST BE			
				SITE ADAPTED AN	ND ACCOUNTED F	OR BY THE DESIGNE	R OF RECORD			
		CTURES (ACL 315R) LATEST EDITIO	ON	AND CHECKED B	Y CEHNC.					
	- SPECIFICATIONS F	FOR STRUCTURAL CONCRETE FC	OR BUILDINGS (ACI 301) LATEST							
D	EDITION									
	- GUIDE FOR CONCE	RETE FLOOR AND SLAB CONSTR	UCTION (ACI 302.1 R) LATEST							
			NORMAL WEIGHT AND SHALL	DESIGN LOADS						
	DEVELOP 28 DAY CO	OMPRESSIVE STRENGTH AS FOL	LOWS:							
	SLABS ON GRADE=	4000 PSI		1. BUILDING RISK CATE	GORY:	II				
	FOOTINGS, WALLS A	ND MISCELLANEOUS INSTALLATI	IONS= 4000 PSI	A. FLOOR LIVE LOADS	:	UFC 3-301-01				
			UNFIRMING TO ASTM A615,	OTHER AREAS:		100 PS	F			
	4. CONCRETE EXPOSE	ED TO WEATHER OR FREEZING S	HALL BE AIR-ENTRAINED.	B. ROOF LIVE LOADS:		UFC 3-3	301-01			
	EXTERIOR FOOTING	S, PEDESTALS, WALLS, SLABS A	ND ANY CONCRETE CAST			20 PSF	301 01			
	DURING COLD WEAT	THER SHALL BE CONSIDERED AS	CONCRETE EXPOSED TO	GROUND SNOW LOADS.	S:					
		EZING. E SHOWN PROVIDE FOLLOWING		D. WIND LOADS:		UFC 3-3	301-01			
С	STEEL:			(SITE ADAPT)			004.04			
	UNFORMED SURFAC	CES IN CONTACT WITH EARTH	3 IN.	E. EARTHQUAKE DESI	GN DATA: ICE FACTOR:	UFC 3-3	301-01			
		CES OVER MOISTURE BARRIERS.		(SITE ADAPT)		1.0				
		1 1/2 IN	K, OR WATERPROOFING/DAMP	BASIC SEISMIC-FORCE	E RESISTING SYST	EM:				
	6. PROVIDE SMOOTH F	FORMED FINISH ON ALL EXPOSE	D VERTICAL CONCRETE		RCED CONCRETE	SHEAR WALLS				
	SURFACES.			κ=4.0 (SITE ΔΠΔΡΤ)						
				ANALYSIS PROCED	URE:	ASCE 7	7-10			
	FOUNDATION NOTES			EQUIVALENT LATER	RAL FORCE PROCE	DURE				
				F. GEOTECHNICAL RE	PORT:	SITE ADAPT	05			
	1. THE DESIGN OF THE	E FOUNDATIONS IS BASED UPON	ITHE	ASSUMED ALLOWAN	BLE BEARING PRE R LIFC 3-340-02	550RE: 2000 P	5F			
	FOLLOWING ASSUM	IPTION FOR THE PURPOSE OF SI	TE		$\sqrt{1}$ $\sqrt{1}$ $\sqrt{1}$ $\sqrt{1}$ $\sqrt{1}$ $\sqrt{1}$ $\sqrt{1}$ $\sqrt{1}$ $\sqrt{1}$					
			DQE							
ט		ESS THAN 2000 PSF AT SITE SPI	ECIFIC	NOTE:						
	LOCATION THEN D	ESIGN FOR THE ALLOWABLE BE	ARING			דםוורדו ופר רחם מידי				
	PRESSURE OF TH	E SITE ADAPTATION.		I. INE DESIGNER SHOU		INUCIUKE FUK SIII				
	2. NO FOOTING SHALL	BEAR DIRECTLY ON ROCK. WHE		2. FOUNDATIONS SHALL	L BE REVISED TO I	REFLECT SPECIFIC S	SITE SOIL			
			E BOTTOM	CONDITIONS INCLUD	ING LOCAL SITING	, TOPOGRAPHIC CO	NDITIONS,			
	OF THE FOOTING A	ND TWO FEET WIDER THAN THE	FOOTING.	AND FROST PENETRA	ATION DEPTHS.					
	BACKFILL WITH APP	PROVED STRUCTURAL FILL.								
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ELEV = 108'-2 1/2"		ELEV = 108'-0"
		F.F.E. = 100'-0"
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GEN NOTES

- 1. WALL TYPE INDICATED WITH , REFER TO SHEET
- A5XX FOR WALL TYPE.
 2. WINDOW TYPE INDICATED WITH A, REFER TO SHEET A5XX FOR WINDOW TYPE.

FLOOR PLAN TAG NOTES

- CONCRETE FLOOR SLAB, REFER TO STRUCTURAL DRAWINGS.
- BRACKET MOUNTED FIRE EXTENGUISHER. MOUNT BOTTOM OF UNIT AT 27" A.F.F.
- (3) ALUMINUM FRAME WINDOW WITH BULLET RESISTANT GLAZING.





ANY DEVIATION FROM THICKNESS OF GLAZING ABOVE MUST MEET UL PROTECTION REQUIRED BY DA PAM 385-63 CHAPTER 5

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US ARMY CORPS OF ENGINEERS Engineering and Support Center, Huntsville



MISSILE PROOF SHELTER & OBSERVATION BUNKER

RANGE AND TRAINING LAND PROGRAM

HNC-EDC-S-18-07 02 APRIL 2018

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MISSILE PROOF SHELTER & OBSERVATION BUNKER

Prepared by

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02 April 2018

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2018 122

Date

Executive Summary

A standard design for a Missile Proof Shelter (MPS) and Observation Bunker was requested by the Range and Training Land Program (RTLP) of USACE in coordination with the Reachback Operations Center of USACE for training operations.

Conventional structural design criteria was used to develop the standard using RAM Elements Software, and the guidelines of DoD 6055.09-M, DA-PAM 385-63 and DA-PAM 385-64 were followed to determine adequate safe distances for essential personnel inside of the three-sided bunker. Previous designs of the MPS operated with a minimum safe distance of 100 meters (m). For this reason, the standard design was approached with the intent of maintaining this distance for the purpose of maximizing the usage of land resources while providing proper protection for personnel. The requirement for the MPS to be kept outside of Earth Throw Distance based on a DDESB Technical Paper 16 analysis forced the operation distances to increase higher than the 100 m safe distance. (Reference (D))

The operations being performed by the personnel requiring protection include wire obstacles, mines, steel cutting, timber cutting and road craters.

The governing explosives safety criteria for these operations is found in DoD 6055.09-M which states, "Essential Personnel Minimum Safe Distance (MSD) must be the same as the non-essential personnel MSD in accordance with paragraph V5.E3.2.6., or must provide personnel protection from fragment, thermal, overpressure, noise, and other hazards in accordance with paragraph V1. E9.3.2."

This requires that all fragments be contained or defeated, hearing protection be provided if noise levels exceed limits established in MIL-STD-1474D, thermal flux limited, and blast overpressures limited to less than or equal to 2.3 psi. Using the buried explosive module from DDESB Technical Paper 16 it was found that the distances of Table 1 were required due to the Soil Ejecta Distances of the cratering charges. Using UFC 3-340-02 Figure 2-15, it was determined that the overpressure from the Net Explosive Weights (NEWs) at the distances of Table 1 were sufficiently less than 2.3 psi to conform with this. The requirements of MIL-STD-1474D are met by requiring hearing protection within the MPS at all times of training operations. Spall can be assumed to be negligible at a standoff of 328 feet out in the open with blast pressures significantly less than 2.3 psi. Regarding thermal effects, the fireball diameter for the maximum NEW under consideration is significantly less than the MSD, so thermal effects can be neglected as well.

Table of Contents

Execu	xecutive Summary 2						
1.0	Introduction	4					
2.0	References	4					
3.0	Design Approach	5					
4.0	MPS Requirements and Concerns	5					
4.1	MPS Requirements	5					
4.2	MPS Concerns	6					
5.0	Design Results	6					
5.1	Window Design	7					
6.0	Conclusion	8					

1.0 Introduction

A standard design for a Missile Proof Shelter (MPS) and Observation Bunker (OB) was requested by the Range and Training Land Program (RTLP) of USACE in coordination with the Reachback Operations Center of USACE in support of Explosive Ordinance Disposal (EOD) training operations for use on standard light demo and hand grenade familiarization. The intent of the design is to develop a standard that can be replicated with minimal site adaptations to ease the implementation of the MPS/OB at various locations.

2.0 References

- a) DoD 6055.09-M "DoD Ammunition and Explosives Safety Standards: General Explosives Safety Information and Requirements," Volumes 1 through 8, Department of Defense, date varies by volume.
- b) Department of Defense, DA PAM 385-64 "Ammunition and Explosives Safety Standards," Department of the Army, 10 October 2013
- c) UFC 3-340-02 "Structures to Resist the Effects of Accidental Explosions," Department of Defense, 5 December 2008, Incorporating Change 2, 1 September 2014.
- d) Technical Paper No. 16 "Methodologies for Calculating Primary Fragment Characteristics," Department of Defense Explosive Safety Board, 19 December 2016.
- e) Department of Defense, DA PAM 385-63 "Range Safety," Department of the Army, 30 January 2012.

3.0 Design Approach

Conventional design criteria was used to develop the standard using RAM Elements Software, and the guidelines of DoD 6055.09-M (Reference (A)), DA-PAM 385-63 (Reference (B)) and DA-PAM 385-64 (Reference (E)) were followed to determine adequate safe distances for essential personnel inside of the three-sided bunker. Previous designs of the MPS operated with a safe distance of 100 meters (m). For this reason, the standard design was approached with the intent of maintaining this distance for the purpose of maximizing the usage of land resources while providing proper protection for personnel.

Overpressures on the structure due to the detonation of the maximum allowable charge weight by Reference (E) of 320 lbs NEW were calculated assuming the previously used 100m safe distance as the minimum standoff, and the structural response was determined using the methodologies found in Reference (C). Due to the low blast pressures at this distance, all structural components remain elastic under blast loading, and conventional loads controlled the structural design.

Earth throw distance calculated from the Buried Explosion Module Version 7.1 of Reference (D) controlled the distance from the bunker to the largest charges analyzed. Any MPS installed must be beyond these distances; therefore, these revised standoffs were assumed for the structural blast analysis.

Fragments were considered using the TP 16 Database Fragment Data Review Forms, and to ensure fragmentation hazards are defeated, the minimum thickness to prevent perforation for both concrete and bullet resistant glass were confirmed to be less than the thickness required by conventional loads and minimum ballistic glazing requirements of Reference (E), respectively. Only the two known munitions, Bangalore Torpedo M1A2 and M67 Fragmentation grenade, were considered and anything outside of the set listed on the drawings must be reviewed using a TP 16 analysis in the future.

4.0 MPS/OB Requirements and Concerns

4.1 MPS/OB Requirements

MPS must provide adequate protection to personnel per Reference (A) and Reference (B). This requires that all fragments be contained or defeated, hearing protection be provided if noise levels exceed limits established in MIL-STD-1474D, thermal flux be limited, and blast overpressures be limited to 2.3 psi or less. Table 1 shows the permitted operations for which the MPS is to be used along with each operation's respective charge weight at standoff limits.

DESIGN EXPLOSIVE WEIGHTS AND DISTANCES								
FOR MISSILE PROTECTIVE SHELTERS & OBSERVATION BUNKERS								
OPERATION	MAXIMUM	MINIMUM						
	EXPLOSIVE	DISTANCE (M[ft])						
	WEIGHT (LB.							
	TNT)							
Wire Fence Clearing	7	100 [328]						
Wire Fence Clearing w/ Bangalore	65	200 [656]						
Mine Clearing	166	100 [328]						
Mine Clearing w/ Live M15 Mines	166	314 [1030]						
Steel Cutting	10	100 [328]						
Timber Cutting	70	100 [328]						
Concrete Obstacle	40	100 [328]						
Cratering (Multiple Craters)	320	250 [821]						
Cratering (Single Crater)	48	150 [492]						
M67 Fragmentation Grenade	0.41	10 [32.8]						

Table 1

*Note: Any Operations using a Bangalore Torpedo must be done at 200 m [656 ft]

4.2 MPS/OB Design Criteria & Site Specific Adaptation

Site adaptations must acknowledge and adjust several MPS characteristics to validate the design for site specific parameters. For example, freeze-thaw cycles may require lowering the footings to provide adequate frost depth cover, and seismic values must be checked along with design wind speeds based on site specific locations to determine adequate structural integrity is achieved. Such checks should be performed by a qualified engineer. Any modification to the roof, walls, or windows should be reviewed and approved by CEHNC prior to implementation.

The NEWs shown on the drawings and listed above (Table 1) are the maximums considered for each training operation for the design. These NEWs can not be increased nor the distances from the NEWs reduced for any operation. From Table 1 the worst case blast load was induced by the Mine Clearing operation with a maximum explosive wt of 166 lbs at a distance of 328 ft.

5.0 Design Results

As the MPS will always be well beyond K40 overpressure distances, the design was generally controlled by conventional loads. The structure was designed to have eight inch walls and roof consisting of 4000 psi concrete reinforced with grade 60 #5 bars spaced at 12 inches center-to-center (C/C) in each direction on each face. The ground slab was designed to have a half inch

expansion joint between the concrete walls and ground slab. The ground slab is six inches deep and reinforced with #4 bars at 12 inches C/C. A three foot wide continuous footing lines the perimeter of three sides of the structure that ties into the walls with #5 rebar at 12 inches C/C. Openings are reinforced with additional #5 rebar, with the layout of rebar shown on Drawing S1XX to give additional capacity for stress concentration areas.

Due to the exposure of repeated detonation, it is recommended that Range Safety Standard Operation Procedures address periodic visual structural inspections of the shelter.

5.1 Window Design

The MPS/OB is designed to have three viewing windows in the front wall facing the training operations. As such, these windows must be shown to provide adequate protection from all hazards associated with such operations, including overpressure, fragmentation, and thermal hazards.

Section 5-1.b(7(a)) of Reference (E) contains viewing port construction requirements; this criteria has been assumed for blast analysis and consists of six alternating layers of polycarbonate and glass. From the outer/blast face and progressing inward toward the occupied/safe face of the window, these layers are 10mm glass, 7mm polycarbonate, 6mm glass, 6mm polycarbonate, 6mm glass, and 6mm polycarbonate. Using this layup with standard polyvinyl butyral (PVB) laminate, the software program WINGARD PE was used to analyze the 3 foot wide by 1 foot tall windows subjected to the worst case blast pressures assumed for the structural analysis. Results show that the window does not fail and has a maximum displacement of 0.00 inches. Results further show the requirement for a minimum frame bite of 0.50 inches, which is shown on the drawings.

Conservatively assuming the worst-case edge shear reaction load calculated by WINGARD for all edges of the window, minimum framing and anchorage requirements were determined. Using 6063 T6 Aluminum or stronger, a framing member must have a minimum elastic section modulus of 0.09 in³, which is far less than most conventional framing members for a window of this thickness. The $2x2x^{1}/_{4}$ angle on which the window frame bears has both a higher flexural strength and a higher elastic section modulus. Regarding the anchorage of the window frame into the surrounding structure, ¼" steel bolts spaced at 12" has been shown to be sufficient. The portion of the wall supporting the windows has been shown to be sufficient in the wall structural analysis.

As mentioned in Section 3.0 above, per the various Fragmentation Data Review Forms, the minimum thickness to prevent glass breakage due to fragmentation has been surpassed for all

munitions considered. CEHNC should be consulted prior to the use of any munition not listed on the general notes page of the design drawings for the MPS.

Any deviation from the approved window design shown in the design drawings should be analyzed by a competent blast engineer and reviewed by CEHNC prior to installation.

6.0 Conclusion

As demonstrated in the sections above, the MPS/Observation Bunker design described in this report will support the RTLP missions described while providing sufficient protection to personnel from overpressure, fragmentation, debris and thermal hazards in accordance with References (A) (B) & (E). Any deviations to the design described in this report should be reviewed by CEHNC prior to implementation.