

## Simplified RCC Column Design: An International Version

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### ABSTRACT

*1<sup>st</sup> time in the history of engineering a revolutionary idea for RCC column design is unearthed made so easy even on Android, Designing a column conventionally is a challenge to many structural engineers because it is cumbersome, complicated and time consuming in nature. The design method has also changed from time to time. The working stress method used in early 1970s. was improved with the introduction of ultimate design, which remained in vogue from early 1970's until 1980's. Now the limit state approach is being used. In these methods, curves and charts are given in different RCC Hand Books apart from these methods there are so many software are also available. Now, based on fundamental principles, A simple Program which simplify the arduous column design procedure, have been developed. The procedure adopted is applicable to all countries' codes.*

**Keywords:** column design, structure, RCC, International Version

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### INTRODUCTION

Every structural engineer knows the importance of columns' role in the structure.

Column as a main structural member which transfers all possible loads including earth quake loads and wind loads resulting the generation of axial loads and moments from beams above supporting Floors and Roofs. The safety and stability of structure mainly depends on columns. This paper presents new research and development for RCC column design based on basic concept and fundamentals in a very simplified method. This method is not only applicable for Indian code but also to all country codes. The design engineers will definitely get rid of the tardy, tedious, error in reading and time-consuming method by using various charts prepared

based on trials and experiments with so many approximations from time immemorial.

### THEORY AND METHOD

The initial work is based on first principal i.e., "moment is nothing but multiple of, force and eccentricity, due to these eccentricities, the increase in area of concrete section with no eccentricity, is again calculated then this area of concrete is converted in proportion to the area of steel. The summation of both these areas of steel, i.e., one due to pure axial compression and other due to converted area of steel due to the eccentricities. The theory for this research is explained for Indian, British and ACI Code similarly may be derived for other Country Codes. This simple Excel computer program may

be made developed With minimum calculations requiring less than 10 KB storage even on Android .Columns are the most common vertical load-bearing elements in reinforced concrete structures. The primary role of a column in a typical building is to support floor structures such as slabs , beams and girders and transmit the load to the lower levels and then to the foundation. Columns are mainly subjected to axial compression loads and are often called compression member. In reality however, few reinforced concrete columns are subjected to purely axial compression loads. More often, bending moments are also present due to eccentricity of applied loads, applied end moments, and lateral loading on the column. The moment in column may be due to gravity loads, wind loads or earthquake loads. Even the internal columns of a symmetrically framed building carry some amount of moments due to gravity loads when different types of live loads arrangement are applied. For wind and earthquake loads, all columns may carry some moments. So in effect, columns are subjected to combined axial load and flexure.

Here RCC columns are divided in 2 parts where Part A deals with column without Slenderness, i.e., Short column having axial load, uni-axial and bi-axial bending ,Part B deals with slender column having axial load, uni-axial and bi-axial moments are considered ,if the column is slender use Part B first then Part A otherwise wise versa

**PART A** (When the RCC column is Short with Axial load, Uni-axial and Bi-Axial Moments.)

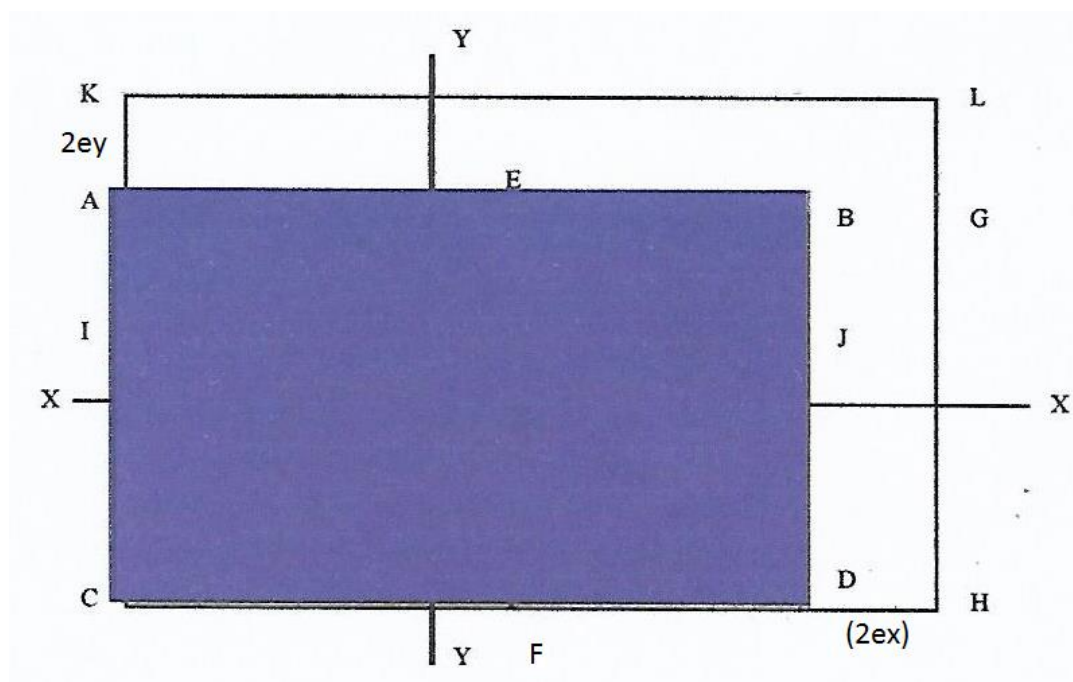
Basic concept of proposed simplified method for a sample design of short RCC columns is explained as under:

As the moment are  $M_x$  and  $M_y$ , hence eccentricity  $e_x$  and  $e_y$  will be governing.

Due to this eccentricity of load in x-direction and y-direction, the load  $P$  or  $P_{uz}$  will be at the junction of EF and IJ.

Where AB or CD is the width of section and AC or BD is the depth of section.

Consider CG of the section is at the origin of x-axis and y-axis



**Fig. 1.** Concrete section.

Eccentricity  $e_x = M_x/P$ , i.e., Position of load due to moment  $M_x$  from CG, Hence distance of CG from line AC =  $B_x/2$

Eccentricity  $e_y = M_y/P$ , i.e., Position of load due to moment  $M_y$  from CG, Hence distance of CG from line CD =  $D_y/2$

To neutralize the effect of eccentricity load has to be placed at CG(new), i.e.,

by a distance  $e_x$  away from y-axis and  $e_y$  away from x-axis at junction of line EF and IJ.

The revised width of the concrete core block shall be double of CF, i.e., CH

Hence revised half width  $CF = B_x/2 + e_x$

Therefore revised full width CH or  $B_{x1} = 2 \times (B_x/2 + e_x)$ , i.e.,  $(B_x + 2e_x)$

The revised depth of the concrete core block shall be double of CI, i.e., CK

Hence revised half depth  $CI = D_y/2 + e_y$

Therefore revised full depth CK or  $D_{y1} = 2 \times (D_y/2 + e_y)$ , i.e.,  $(D_y + 2e_y)$

Hence equivalent core section without the effect of eccentricity shall be area

AREA enclosed by KLCH or  $A_2 = AK \times CH$  or  $B_{x1} \times D_{y1}$ , i.e.,  $(D_y + 2e_y) \times (B_x + 2e_x)$

This equivalent area of concrete is divided in to two parts, i.e.,

First part, i.e., AREA enclosed by ABCD or  $A_1 = (D_y) \times (B_x)$

Second part i.e. Difference of AREAS between  $A_2$  and  $A_1$ , i.e.,  $(A_2 - A_1)$  as enclosed Blank Area in Figure 1.

As maximum stresses in concrete and steel at axial strain of 0.002 i/c factor of safety

As per Indian Code IS 456-1978 vide clause 38.6, Equation for ultimate Axial Load without any eccentricity

$$P_{uz} = (0.45) \times (f_{ck}) \times (A_c) + (0.75) \times (f_y) \times (A_{sc})$$

Factor for concrete  $a = (0.45) \times (f_{ck})$  and Factor for steel  $b = (0.75) \times (f_y)$  respectively.

$$P_{uz} = (0.450) \times (f_{ck}) \times (A_1 - A_{sc}) + (0.75) \times (f_y) \times (A_{sc})$$

$$A_{s1} \text{ or } A_{sc} = (P_{uz} - (0.450) \times (f_{ck})) \times (A_1) / (0.75 \times (f_y) - 0.450 \times (f_{ck}))$$

$A_{s2}$  = equivalent area of steel in proportion to concrete area in excess of original core area

$$\text{Excessive area of concrete} = (A_2 - A_1)$$

Conversion factor for equivalent concrete to steel  $a/b = (0.45) \times (f_{ck}) / (0.75) \times (f_y)$

$$A_{s2} = 0.450 \times f_{ck} / 0.75 \times (f_y) \times [A_2 - A_1]$$

$$A_s = A_{s1} + A_{s2}$$

If the value of  $A_{s1}$  or  $A_{sc}$  comes out to be less than zero than put it, i.e.,  $A_{s1}$  or  $A_{sc}$  as zero.

Replace the value of  $F_{ck}$  proportionally as  $F_{ck}' = (P_{uz}) \times 1000 / (0.45 \times A_1)$

Revise the calculations of accordingly.

**PART B** (when the RCC column is Slender with axial load, uni-axial and Bi-axial moments)

When Slender Ratio  $L_{ex}/B_x$  or  $L_{ey}/D_y > 12$ , the RCC column is supposed to be Slender

Where  $L_{ex}$  is effective length of the column parallel to  $B_x$  direction

Where  $L_{ey}$  is effective length of the column parallel to Bx direction

And L is unsupported length of RCC column

$$SR_x = L_{ex}/B_x \text{ and } SR_y = L_{ey}/D_y$$

Factor for revised Bx =  $SR_x/12 > 1$  or 1  
And Factor for revised Dy =  $SR_y/12 > 1$  or 1

Revised Bx' =  $(SR_x/12) \times (B_x)$  And  
Revised Dy' =  $(SR_y/12) \times D_y$

Increase eccentricity due to Bx', i.e.,  
 $ex_1 = (B_x' - B_x)/2$  and increase eccentricity due to Dy', i.e.,  $ey_1 = (D_y' - D_y)/2$

Total Eccentricity parallel to Bx, i.e.,  
 $ex'' = ex + ex'$  And Total Eccentricity parallel to Dy, i.e.,  $ey'' = ey + ey'$

Replace Bx' with Bx and Dy' with Dy  
And Replace  $ex''$  with ex and  $ey''$  with ey

Now replace these revised values of PART B to PART A and repeat the calculate to get the final results.

### ILLUSTRATIVE CALCULATION

Example of RCC rectangular column (Dr S.R.CARVE and Dr V.L.SHAH Ex.9.8-2 on P-899) [1]:

Design a short R.C. column of rectangular section for the following data:

Size of column 230 mm × 530 mm

Factored load  $P_u$ , i.e., 1200 kN

$M_{ux}$ , i.e.,  $M_x$  50 kNm

$M_{uy}$ , i.e.,  $M_y$  10 kNm

Concrete Mix, i.e.,  $F_{ck}$  M20

Characteristic strength of reinforcement  $F_e$   
i.e.,  $F_y$  250 N/mm<sup>2</sup>

$B_x$  = 530.00 mm

$D_y$  = 230.00 mm

$e_x$ , i.e.,  $M_x/P = 50 \times 1000/1200 = 41.67$  mm

$e_y$ , i.e.,  $M_y/P = 10 \times 1000/1200 = 8.33$  mm  
but < 20 mm hence 20 mm taken

$$\text{Area } A_1 = 230 \times 530 = 121900 \text{ mm}^2$$

Area

$$A_2 = (530 + 2 \times 41.67) \times (230 + 2 \times 20) = 165600 \text{ mm}^2$$

$$A_{s1} = (1000 \times 1200 - 0.45 \times 20 \times 121900) / (0.75 \times 250 - 0.45 \times 20) = 576.47 \text{ mm}^2$$

$$A_{s2} = 0.45 \times 20 / (0.75 \times 250) \times (165600 - 121900) = 2097.60 \text{ mm}^2$$

$$A_{s1} + A_{s2} = (576.47 + 2097.60)$$

$$A_s = 2674.07 \text{ mm}^2 \text{ as against } 2560.00 \text{ mm}^2$$

### RCC CIRCULAR COLUMN

**PART A** (When the RCC column is Short with Axial load, Uni-axial and Bi-Axial Moments.)

Basic Concept of Proposed simplified method for a sample design of Short RCC columns Is explained as under:

As the moment are  $M_x$  and  $M_y$ , hence eccentricity  $e_x$  and  $e_y$  will be governing.

As the RCC Column section is square hence resultant of  $M_x$  and  $M_y$  will be  $M = \sqrt{(M_x^2 + M_y^2)}$

Due to eccentricity of load in x-direction and y-direction, the load P or  $P_{uz}$  will be at the junction of O', i.e.,  $AB'/2$

Where AB is the diameter of circular section, i.e., DIA And Area of original section of column, i.e.,  $A_1 = (\pi/4) \times (DIA)^2$

Where, AB' is the diameter of circular section after considering moment, i.e., DIA1

Consider CG of the original section is at the junction of x-axis and y-axis, i.e., at O

Hence, distance of CG from A, i.e.,  $AO = DIA/2$ , and Hence, distance of CG from A, i.e.,  $AO' = DIA1/2$

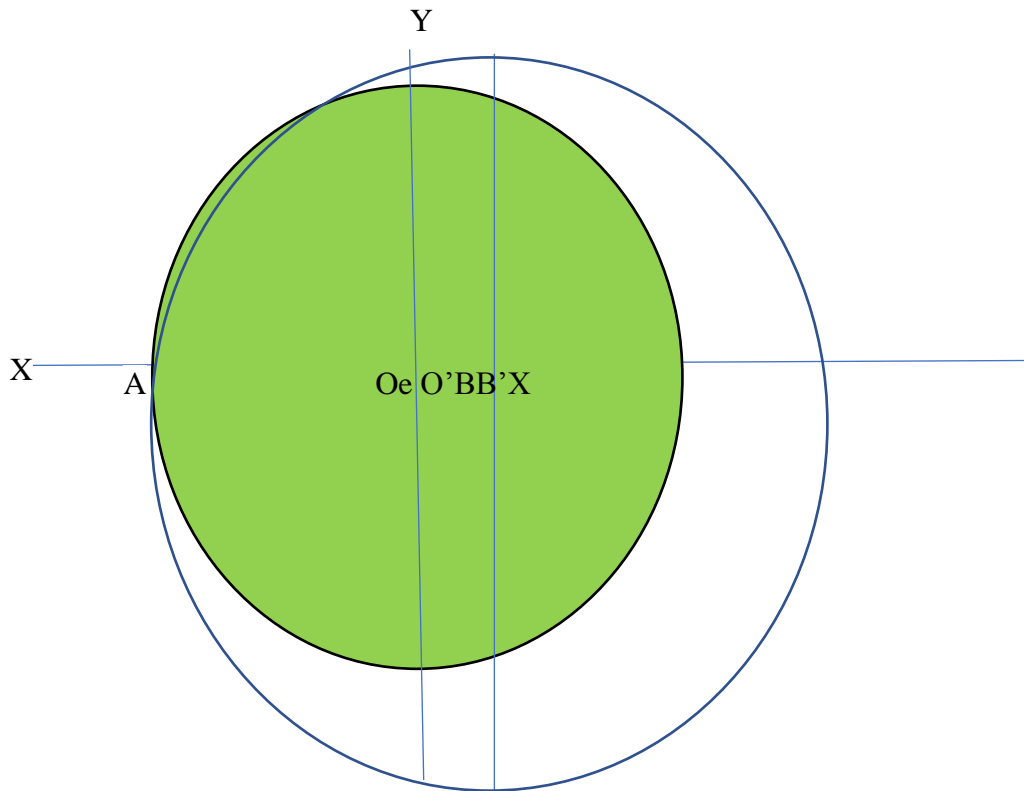


Fig. 2. Concrete Section.

Eccentricity  $e = M/P$ , i.e., Position of load due to moment  $M$  from CG, i.e.,  $O$

Hence, eccentricity  $e = AO' - AO = (DIA1/2 - DIA/2)$

To neutralize the effect of eccentricity load has to be placed at CG(new), i.e.,  $O'$  by a distance  $e$  away from  $x$ -axis at junction of line  $AO$  and  $AO'$ .

Hence equivalent core section without the effect of eccentricity shall be area  $A2 = (\pi/4) \times (DIA1)^2$

This equivalent area of concrete is divided in to two parts, i.e.,

Second part, i.e., Difference of AREAS between  $A2$  and  $A1$ , i.e.,  $(A2 - A1)$  as enclosed Blank Area in Figure 2.

As maximum stresses in concrete and steel at strain of 0.002 including factor of safety

As per Indian Code IS 456 -1978 vide clause 38.6 ,Equation for ultimate Axial Load without eccentricity  $Puz = (0.45) \times (fck) \times (Ac) + (0.75) \times (fy) \times (Asc)$

Factor for concrete  $a = (0.45) \times (fck)$  And Factor for steel  $b = (0.75) \times (fy)$  respectively.

$Puz = (0.450) \times (fck) \times (A1 - Asc) + (0.75) \times (fy) \times (Asc)$

$As1$  or  $Asc = (Puz - (0.450) \times (fck)) \times (A1) / (0.75 \times (fy) - 0.450 \times (fck))$

$As2 =$  equivalent area of steel in proportion to concrete area in excess of original core Area.

Excessive area of concrete  $= (A2 - A1)$   
Conversion factor for equivalent concrete to steel  $a/b = (0.45) \times (fck) / (0.75) \times (fy)$

$As2 = 0.450 \times fck / 0.75 \times (fy) \times [A2 - A1]$

$$A_s = A_{s1} + A_{s2}$$

If the value of  $A_{s1}$  or  $A_{s2}$  comes out to be less than zero than put it, i.e.,  $A_{s1}$  or  $A_{s2}$  as zero.

Replace the value of  $F_{ck}$  proportionally as  $F_{ck}' = (P_{uz}) \times 1000 / (0.45 \times A_1)$  And Revise the calculations

**PART B** (when the RCC column is Slender with axial load, uni-axial and Bi-axial moments)

When Slender Ratio  $L_e/DIA > 12$ , the RCC column is supposed to be Slender

Where  $L_e$  is effective length of the column And  $L$  is unsupported length of RCC column

$$SR = L_e/DIA$$

Factor for revised  $DIA' = SR/12 > 1$  or 1

$$\text{Revised } DIA' = SR/12 \times DIA$$

Hence increase in eccentricity due to slenderness, i.e.,  $e' = (DIA' - DIA)/2$

Total eccentricity to slenderness, i.e.,  $e'' = e + e'$

Replace  $DIA'$  with  $DIA$  and Replace  $e''$  with  $e$

Now replace these revised values of PART B to PART A and calculate to get the final results.

### ILLUSTRATIVE CALCULATION

Example of RCC Circular Column (RCC by ASHOK K JAIN vide Example 16.9 on P-494) [2]:

Design a Slender Braced Circular Column under uni-axial bending with the following data:

Size of column, i.e.,  $DIA$       40cm  
Concrete grade, i.e.,  $F_{ck}$       M20

Steel grade, i.e.,  $F_y$       415 N/mm<sup>2</sup>

Effective length, i.e.,  $L_e$  6.0 m

Unsupported length, i.e.,  $L$  7.0 m

Factored load, i.e.,  $P$       1200 kN

Factored moment 750 kNm at top 50 kNm at bottom

Design Moment  $M = 0.6 \times 75 + 0.4 \times 50 = 65$  kNm

As the RCC column is slender use PART B

$e$ , i.e.,  $M/P = 65 \times 1000 / 1200 = 54.17$  mm

$$SF = 6000/400 = 15$$

$$DIA' = 15/12 \times 400 = 500 \text{ mm}$$

$$e' = (500 - 400)/2 = 50 \text{ mm and } e'' = 54.17 + 50 = 104.17 \text{ mm}$$

Now use Part A

$$DIA = 500 \text{ mm}$$

$$e = 104.17 \text{ mm}$$

$$Area A_1 = (\pi/4) \times 500^2 = 196349.54 \text{ mm}^2$$

$$Area A_2 = (\pi/4) \times (500 + 2 \times 104.17) \times (500 + 2 \times 104.17) = 394062.62$$

$$A_{s1} = (1200 \times 1000 - 0.45 \times 20 \times 196349.54) / (0.75 \times 415 - 0.45 \times 20) = -1878.77 \text{ mm}^2 < 0$$

Hence  $A_{s1} = 0$ . Therefore, Revise the value  $f_{ck}$

$$F_{ck}' = 1200 \times 1000 / (0.45 \times 196349.54) = 13.58 \text{ N/mm}^2$$

$$A_{s2} = 0.45 \times 13.58 / (0.75 \times 415) \times (394062.62 - 196349.54) = 3882.20$$

$$A_{s1} + A_{s2} = (0 + 3882.20), \text{ i.e., } A_s = 3882.20 \text{ mm}^2 \text{ as against } 3800.00 \text{ mm}^2$$

### RCC L-SHAPE COLUMN

**PART A** (When the RCC column is Short with Axial load, Uni-axial and Bi-Axial Moments.)

Basic Concept of Proposed simplified method for a sample design of Short RCC columns is

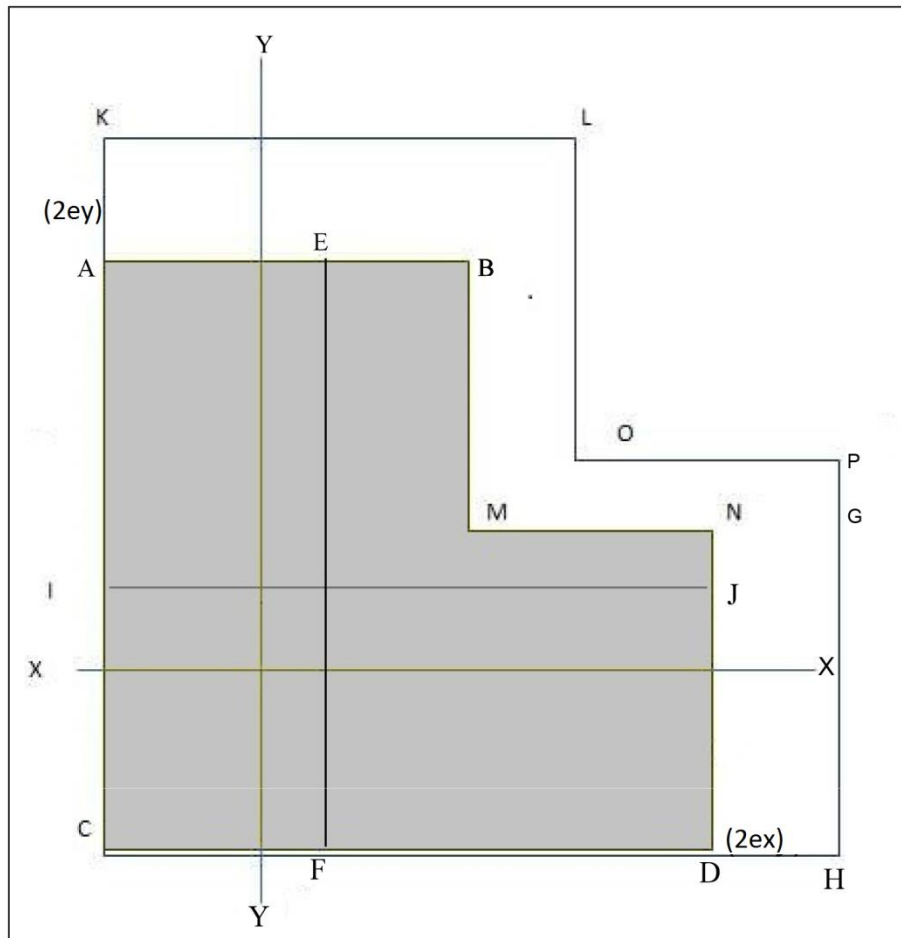


Fig.3. Concrete Section.

As the moment are  $M_x$  and  $M_y$ , hence eccentricity  $e_x$  and  $e_y$  will be governing.

Due to this eccentricity of load in  $x$ -direction and  $y$ -direction, the load  $P$  or  $P_{uz}$  will be at the junction of  $EF$  and  $IJ$ .

Where  $CD$  is the width of section, i.e.,  $B_x$  and  $AC$  is the depth of section i.e.  $D_y$

Thickness of leg in  $X$ -direction, i.e.,  $AB = T_x$  and Thickness of leg in  $Y$ -direction i.e.  $ND = T_y$

Consider  $CG$  of the section is at the origin of  $x$ -axis and  $y$ -axis

Eccentricity  $e_x = M_x/P$ , i.e., Position of load due to moment  $M_x$  from  $CG$

Eccentricity  $e_y = M_y/P$ , i.e., Position of load due to moment  $M_y$  from  $CG$

To neutralize the effect of eccentricity load has to be placed at  $CG(\text{new})$ , i.e., by a distance  $e_x$  away from  $y$ -axis and  $e_y$  away from  $x$ -axis at junction of line  $EF$  and  $IJ$ .

The revised width shown for the concrete core block shall be extended by a value of 2times  $e_x$  in  $X$ -direction

The revised depth shown for the concrete core block shall be extended by a value of 2 times  $e_y$  in  $Y$ -direction

Hence original area of concrete, i.e.,  $A_1 = (B_x) \times (T_y) + (D_y - T_y) \times (T_x)$

Hence, equivalent core section without the effect of eccentricity shall be area, i.e.,

$$A_2 = (B_x + 2e_x) \times (T_y + 2e_y) + (D_y - T_y) \times (T_x + 2e_x)$$

This equivalent area of concrete is divided in to two parts, i.e.,

First part, i.e., AREA of original L-section =  $A_1$

Second part, i.e., Difference of AREAS between  $A_2$  and  $A_1$ , i.e.,  $(A_2 - A_1)$  as enclosed Area in Figure 3.

As per Indian Code IS 456 -1978 vide clause 38.6, And Equation for ultimate Axial Load without eccentricity

$$P_{uz} = (0.45) \times (f_{ck}) \times (A_c) + (0.75) \times (f_y) \times (A_{sc})$$

Factor for concrete  $a = (0.45) \times (f_{ck})$  And Factor for steel  $b = (0.75) \times (f_y)$  respectively.

$$P_{uz} = (0.45) \times (f_{ck}) \times (A_1 - A_{sc}) + (0.75) \times (f_y) \times (A_{sc})$$

$$A_{s1} \text{ or } A_{sc} = (P_{uz} - (0.45) \times (f_{ck}) \times (A_1)) / (0.75 \times (f_y) - 0.45 \times (f_{ck}))$$

$A_{s2}$  = equivalent area of steel in proportion to concrete area in excess of original core area.

Excessive area of concrete =  $(A_2 - A_1)$  as enclosed Blank in Figure 3.

Conversion factor for equivalent concrete to steel  $a/b = (0.45) \times (f_{ck}) / (0.75) \times (f_y)$

$$A_{s2} = 0.45 \times f_{ck} / 0.75 \times (f_y) \times [A_2 - A_1] \text{ And } A_s = A_{s1} + A_{s2}$$

If the value of  $A_{s1}$  or  $A_{sc}$  comes out to be less than zero than put it, i.e.,  $A_{s1}$  or  $A_{sc}$  as zero.

Replace the value of  $F_{ck}$  proportionally as  $F_{ck}' = (P_{uz}) \times 1000 / (0.45 \times A_1)$ , i.e., Revise the calculations accordingly.

PART B (when the RCC column is Slender with axial load, uni-axial and Bi-axial moments)

When Slender Ratio  $L_{ex}/B_x$  or  $L_{ey}/D_y > 12$ , the RCC column is supposed to be Slender

Where  $L_{ex}$  is effective length of the column parallel to  $B_x$  direction

Where  $L_{ey}$  is effective length of the column parallel to  $D_y$  direction

And  $L$  is unsupported length of RCC column

$$SR_x = L_{ex}/B_x \text{ and } SR_y = L_{ey}/D_y$$

Factor for revised  $B_x = SR_x/12 > 1$  or 1 And Factor for revised  $D_y = SR_y/12 > 1$  or 1

$$\text{Revised } B_x' = (SR_x/12) \times B_x \text{ And Revised } D_y' = (SR_y/12) \times D_y$$

increase in eccentricity due to  $B_x'$ , i.e.,  $e_{x1} = (B_x' - B_x)/2$  and increase in eccentricity due to  $D_y'$ , i.e.,  $e_{y1} = (D_y' - D_y)/2$

Total Eccentricity parallel to  $B_x$ , i.e.,  $e_x'' = e_x + e_{x1}$  And Total Eccentricity parallel to  $D_y$ , i.e.,  $e_y'' = e_y + e_{y1}$

Replace  $B_x'$  with  $B_x$  and  $D_y'$  with  $D_y$  And Replace  $e_x''$  with  $e_x$  and  $e_y''$  with  $e_x$

Now replace these revised values of PART B to PART A and repeat the calculate to get the final results.

### ILLUSTRATIVE CALCULATION

Example of RCC L-Shape Column (Ramamurthy and Shah using method 1 and method 2 [3]).



Design a Short Column under bi-axial bending with dimension 400 mm × 300 mm × 200 mm nominal cover of 50 mm and subjected to an axial load of 890.8 kN and a factored moments of 90.4 and 56.5 kNm about x- and y-axis, respectively. compressive strength of concrete Fck is 25 N/mm<sup>2</sup> and yield strength of steel Fy is 415 N/mm<sup>2</sup>:

Size of column 400mm × 300mm × 200mm  
 Factored load P 890.8 kN  
 Mux, i.e., Mx 90.4kNm  
 Muy, i.e., My 56.5kNm  
 Concrete Mix, i.e., Fck M20  
 Characteristic strength of reinforcement Fy = 415 N/mm<sup>2</sup>  
 Bx = 400.00 mm  
 Dy = 300.00 mm  
 Tx = 200 mm and Ty = 200 mm  
 Ex, i.e., Mx/P=90.4× 1000/890.8=101.48 mm  
 ey, i.e., My/P = 56.5× 1000/890.8=63.43 mm  
 Area A1 =400× 200 + (300-200)× 200 = 100000 mm<sup>2</sup>  
 Area A2 = (400+2× 101.48) × (200+2× 63.43) + (300-200)× (200+2× 101.48) =237376.39 mm<sup>2</sup>

As (890.8× 1000-0.45× 25× 100000) < 0.0So As1= 0.0  
 So Fck<sup>2</sup> = 890.8× 1000/(0.45× 100000)=19.80 mm<sup>2</sup>  
 As2= 0.45× 19.80/(0.75× 415)× (237376.39-100000)= 3931.72 mm<sup>2</sup>  
 As1+ As2 = (0.0+3931.72)and As = 3931.72 mm<sup>2</sup>as against 3920 mm<sup>2</sup>

**BRITISH CODE**

The ultimate axial load of column is derived partially from concrete section and partially from quantity of steel as per British Code-8111 as per Ultimate Axial load, i.e.,

Puz = 0.45 Fck. Ac + 0.95 Fy. Asc” (worked out by Author, but it may vary)

Factor for concrete a = (0.45)× (fck) And Factor for steel b = (0.95)× (fy) respectively.

**ACI CODE**

The ultimate axial load of column is derived partially from concrete section and partially from quantity of steel as per ACI-CODE 318 as per Ultimate Axial load, i.e.,

Puz = 0.442Fck.Ac + 0.52Fy.Asc” (worked out by Author, but it may vary)  
 Factor for concrete a = (0.45)× (fck) And Factor for steel b = (0.95)× (fy) respectively.

Similarly theory and Procedure for the Design of RCC Column as per BRITISH CODE And as per ACI are same as in the case of INDIAN CODE except the Values of ‘a’ and ‘b’ in the above equation for ultimate axial load.

**RESULTS AND CONCLUSION**

The examples’ results will be so surprising to all Engineer’s community that so complicated and time consuming process to design All RCC Columns with axial Load and bi-Axial moments having slenderness of any shape and size particularly L-Shape and Irregular Shape RCC Columns with different dimensions and thicknesses in Both the directions as well ,are made so easy even on Android Phone. It is most simplified method ever attempted before as it requires minimum calculations. The results obtained are very authentic as being based on first principles of Force and Moment and Relationship with Eccentricity and The Results reasonably comparable to all the existing methods of design and software available for the design of RCC Columns.

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## AUTHORS' BIOGRAPHY

R.G. Gupta, a structural engineer and structural consultant graduated from Government Engineering College Jabalpur (India) completed BE (Hons) in Civil Engineering in year 1967 and joined Delhi Development Authority (India) worked as Structural Engineer in Central Design Organization of DDA retired as Superintending Engineer in year April 2005. Since a Firm was launched Namely 'Pitambara Structural Consultant' got empaneled as Structural Consultant From DDA has provided Consultancy to number of major civil projects in India.

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