# Run-on and Run-off Control System Plan – 2021 Update

## Rosebud Power Plant Landfill



# Rosebud County, MT

Originally Submitted: October 16, 2016 Revised: October 17, 2021

Presented by:



## Allied Engineering Services, Inc.

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#### 1. INTRODUCTION

This run-on and run-off control plan presents the hydrology and hydraulics of the stormwater system for the Coal Combustion Residuals (CCR) landfill of the Rosebud Power Plant in Rosebud County, Montana owned by Colstrip Energy Limited Partnership (CELP) in order to fulfill the requirements of the CCR rule as published in the Federal Register on April 17, 2015 and July 2, 2015 and its effective date of October 17, 2016. This document fulfills the requirements of 40 CFR § 257.81(c). The landfill in this report holds hydrated ash, which is solid and practically impermeable to water, similar to concrete. This 2021 update fulfills the requirement of 40 CFR 257.81(4) that an update be prepared every 5 years.

The project site is located approximately seven miles north of the town of Colstrip, Montana in the southwest quarter of Section 29 and the northwest quarter of Section 32 Township 3 North, Range 41 East (Latitude 45.978859°, Longitude -106.663772° (WGS 84)). A vicinity map is included on Sheet C0-1 of the plan set included in Appendix A. The landfill serves an on-site Power Plant owned by the Colstrip Energy Limited Partnership. The Power Plant and the landfill is operated by Rosebud Operating Services, Inc.

The landfill areas covered by this report are an active and closed landfill located on the subject property. The closed landfill, last used in October, 2005, has since been reclaimed in general accordance with applicable permits and regulations at closure. In accordance with 40 CFR § 257.50(d), this closed landfill is not subject to regulation by the above referenced rules. The active landfill includes Phase I and Phase II of a contiguous landfill permitted in 1997 and placed in service in October, 2005. This active landfill is subject to regulation by the above referenced CCR rules.

The information contained herein is based on an investigation and analysis of the property's topographical and subsurface conditions, a review of existing permits, regulatory requirements, and maps and literature for the project area as related to the landfilling operations of combusted coal residuals (CCR), more commonly referred to as fly ash and bottom ash. The purpose of this report is to quantify, mitigate and convey stormwater run-off and run-on for the project site.

In general, the CCR rules define run-on as water that drains overland onto the active landfill (§257.53). For this project, run-on will generally come from the west and flowing west to east across the project site to Armells Creek. Armells Creek flows generally north to the Yellowstone River. As demonstrated in this report, the specified run-on controls are adequate for the required 24-hour, 25 year storm event. Run-off refers to water that drains from the CCR landfill directly and includes the soil cap and containment berms. No rainfall that falls directly on the active CCR placement area will be allowed to flow from the confines of the landfill. This is accomplished with containment berms completely surrounding the active ash placement areas. During the active life of the landfill, incipient precipitation onto the ash placement area is consumed by ash hydration of the on-going ash placement. This configuration will change upon final closure when ash placement ceases and more runoff will be generated from the landfill cap area. For clarity, excess rainfall refers to all water that is not infiltrated, retained or otherwise held in place for a given area during a storm event.

## 2. DRAINAGE BASIN DELINEATION

The delineation of the drainage basins resulted in eleven drainage basins for the active life of the landfill and eight drainage basins for the post-closure time period. All areas with a portion draining a soil covered CCR landfill were included for both the active and closed landfill. No excess rainfall with direct contact to placed CCR will leave the site. For the operational life of the landfill, the drainage pipes will convey runoff and run-on under the landfills to existing drainages downstream. The active drainage basins are

numbered 1 through 11 (see sheet C2-1 in Appendix A).

To avoid reliance upon the buried pipelines and any problems they might otherwise present, once ash placement is complete, the drainage basins will change with the construction of surface drainage ways to replace the underground conveyance systems. All underground piping will be plugged and abandoned inplace. For specifics on abandonment of piping see the Rosebud Power Plant CCR Landfill Closure Plan. In general, the piping will be blocked at the inlet to stop any flow from entering the pipe. The post-closure drainage basins will be numbered 1 through 9 (see sheet C2-2 in Appendix A).

## **Active Drainage Basins**

Active Drainage Basin 1 will contribute the majority of run-on onto the active landfill and into Pipe 2 with an area of 103 acres. For reference, Pipe 2 is the 36-inch Duromaxx pipe located on the west end of Phase 2 of the active landfill. Pipe 2 drains directly to Pipe 1. Pipe 1 is the original 48-inch, High Density Polyethylene (HDPE) pipe, which accepts run-off from both Active Drainage Basins 1 and 2. The area in this basin is mostly undisturbed grasslands with sagebrush and snowberry. A small area near the inlet to Pipe 2 will contribute run-off from the side slopes created by the containment berms. This run-off will not be in direct contact with the CCR, but will come from the established final cover system that makes up the side slopes. The topsoil and seeding will be included for the berms as they are constructed, thereby reducing the amount of excess rainfall and expediting the reclamation process.

Active Drainage Basin 2 is a smaller basin receiving run-on from 14.6 acres of mostly off-site area, and a small amount of run-off from the containment berms near the Pipe 3 inlet. This area has similar land cover to Active Drainage Basin 1 and flows into Pipe 3. Pipe 3 is a 30-inch Duromaxx pipe that tees into Pipe 2, which in turn connects to the existing Pipe 1.

Active Drainage Basin 3 is the top of the active CCR landfill surface that is contained on all sides by a berm. This area will not contribute any run-off as all precipitation will be used to hydrate the ash or will evaporate over the course of the water year. The basin size will change over the lifetime of the power plant as ash placement moves vertically. Enough freeboard will be present within the contained area to hold all rain events by maintaining a minimum of two-feet of freeboard on the containment berms. Once ash placement is complete, this area will be capped with a subtle concave sub-soil and vegetated topsoil cap directing run-off to an armored channel as described below. This sequence will provide opportunity to establish, observe and if necessary maintain the reclaimed side slopes during the active life of the landfill, without the risk of suddenly adding considerably more drainage area to them upon closure.

The Active Drainage Basin 4, 5, and 6 will all drain run-off from the active landfill's side slopes. These slope areas are fairly small to start with and will grow as the landfill grows vertically, but will not receive run-off from the capped top even during post closure conditions. Run-off from these drainage basins will flow into existing swales and drainage pathways once they reach the bottom of the engineered slope.

The Active Drainage Basin 7 accepts run-on from the area west of the existing closed landfill into a 42-inch corrugated metal pipe (CMP). Some run-off coming from the west side of the existing landfill will flow off of the side slopes to the existing drainage pipe. All areas on the existing closed landfill are vegetated and protected with a soil cap. The drainage area for this basin is 67.4 acres of mostly undeveloped grass lands with some home sites. A small existing stock pond near the outlet of the basin is typically full and does not affect the peak flows of the drainage basin. The CMP has an obtuse angle in the middle of the pile that directs run-off to the north and into the historic drainage swale of the underlying basin that flows to Armells Creek.

Currently the existing closed landfill has a concave top that retains rainfall. This area is referred to as Active

Drainage Basin 8. As part of the post-closure plan, this area will be graded to drain to an armored channel that will direct flow off of the top of the existing landfill. During the operation of the power plant, this area was used periodically to store plant process wastewater that would have been used to hydrate ash. When fly ash sales reached their peak, ash was no longer being placed on the landfill and all the wastewater had to be retained on-site and allowed to evaporate or infiltrate. All plant process wastewater was stored in this area during that time. This function can now be achieved in the bermed active ash placement area.

The remaining Active Drainage Basins are 9, 10, and 11. They consist of smaller areas draining the side slopes of the existing closed landfill. The existing closed landfill drainage basins have stabilized conditions with good to excellent vegetation cover. Table 1 and Table 2 provide drainage basin information. The time to concentration is the most amount of time it takes the farthest hydraulic point of a watershed to reach the outlet. The Soil Conservation Service (SCS) Curve number is a parameter used for predicting run off or infiltration from a storm event that takes into account several variables including soil type and vegetation.

Active Drainage Basin	Total Area	Time to Concentration	SCS* Curve Number
1	103 acres	52 min.	72
2	14.6 acres	42 min.	72
3	4.3 acres	28 min.	72
4	13.6 acres	81 min.	72
5	16.3 acres	16.3 acres 56 min.	
6	4 acres	4 acres 12 min.	
7	67.4 acres	42 min.	72
8	3.2 acres	38 min.	72
9	10.5 acres	36 min.	72
10	5.6 acres	25 min.	72
11	5.8 acres	17 min.	72

Table 1 – Active Landfill Drainage Basin General Information

## **Post-Closure Drainage Basins**

Post Drainage Basin 1 is resultant of the filling/grading of the Pipe 2 inlet area and directing all excess rainfall into Drainage Way 1. Drainage Way 1 is a swale that will be constructed to flow from the inlet area of Pipe 2 around the southern border of the active landfill to the existing outlet swale. This drainage way accepts excess rainfall directly from 118 acres and indirectly from 23 acres. The indirect excess rainfall comes from Drainage Ways 2 and 3 which will be constructed to flow into the inlet of Drainage Way 1. This was intentionally done in order to reduce the amount of cut needed to convey flow around the north side of the active landfill. These swales will have 12-foot wide bottoms, which can be used as access roads if needed. Any run-off coming from the southern half of the landfill will be intercepted by Drainage Way 1.

As noted above, Post Drainage Basin 2 drains to the inlet of Drainage Way 1. The inlet of Drainage Way 2 is the inlet area to existing Pipe 3. The inlet area to existing Pipe 3 will be filled in order to raise the inlet elevation of the existing drainage up to the elevation needed for the drainage way to be constructed. All excess rainfall into the Post Drainage Basin 2 will flow down Drainage Way 2 and enter the Drainage Way 1 inlet fill area. The run-off from the top of the landfill will flow into the Pipe 3 fill area and out the drainage way. By allowing the majority of the excess rainfall to flow into the swale through the filled inlet areas, the

filled inlet areas effectively act as stilling basins to help remove any accumulated sediment from upstream drainage. These filled inlet areas also slow velocities of excess rainfall before entering the constructed drainage ways.

Post Drainage Basin 7 will be the Phase 2 landfill run-off that doesn't drain to Drainage Way 1 or 2. The majority of run-off from this drainage basin will sheet flow to an existing swale running along the northern side of the landfill. This swale will route any excess rainfall back toward the historic discharge point of the watershed near the outlet of Pipe 1. This area is similar to the Active Drainage Basin 5 during the active portion of the project.

Once ash storage is completed, a soil cap will be constructed over the hydrated ash top surface. This cap will utilize a concave geometry to direct run-off toward the north and into Drainage Way 3, an armored channel outfall. Run-off will exit the channel into an armored plunge pool that will drain out via a gentle vegetated swale to Drainage Basin 2.

Post Drainage Basin 3 will drain an area of 71.2 acres of approximately the same area as Active Drainage Basin 7. In order for this swale to be feasible, the inlet area to the existing CMP pipe will need to be filled and a drainage way cut into the existing ground. Drainage Way 4 will be constructed using a trapezoidal channel with 3H:1V side slopes and a 4-foot bottom width. Excess rainfall will flow in Drainage Way 4 and under the existing haul road in a proposed 36-inch diameter by 72 feet long Duromaxx culvert. Below the culvert, all excess rainfall from the landfill will flow from Post Drainage Basin 4. This lower area drains the northern slope of the existing closed landfill into Drainage Way 4. Drainage Way 4's discharge point will be near the outlet of the original drainage pipe under the existing closed landfill.

The top of the existing closed landfill will be filled and graded to drain to an armored channel, thus eliminating any retained excess rainfall in the existing depression. Active Drainage Basin 8 will become Post Drainage Basin 9 that drains into Drainage Way 5 (a rock armored channel). No changes are proposed to Active Drainage Basin 10 except that it becomes Post Drainage Basin 6.

Post Drainage Basin	Total Area	Time to Concentration	SCS* Curve Number
1	118 acres	54 min.	72
2	18.6 acres	44 min.	72
3	70.2 acres	48 min.	72
4	2.9 acres	26 min.	72
5	13 acres	74 min.	72
6	8.6 acres	29 min.	72
7	16.3 acres	38 min.	72
8	4.3 acres	38 min.	72
9	3 acres	32 min.	72

Table 2 – Post-Closure Landfill Drainage Basin General Information

#### 3. DRAINAGE BASIN STORM FLOW CALCULATION

Following the delineation of the drainage basins, the Soil Conservation Service (SCS) curve number method was utilized to calculate volumes and flow rates for the basins. The curve number used for the native ground was estimated at 72. This curve number assumed a land use type of sagebrush with grass understory rangeland for all existing and reclaimed areas. The hydrologic condition was estimated between fair and good with a Hydrologic Soil Group of mostly D. All areas were assumed to have this curve number, which should be considered conservative given that better vegetation and more porous soil areas exist within the reclaimed drainage basins. Soil porosity outside the project area was estimated using the Web Soil Survey.

The CCR rules require all stormwater conveyance systems be designed to handle the 25-year 24-hour event. The conveyance system for this site was modeled using the 25-year, 100-year and 500-year events. Precipitation for the 25-year and 100-year events was taken from the NOAA Atlas 2, Volume 1-Montana. The 500-year event was extrapolated from higher frequency storms.

Design Storm	Precipitation (inches)
25-Year, 24-Hour	2.90
100-Year, 24-Hour	3.82
500-Year, 24-Hour	4.66

**Table 3 – Precipitation Depths Summary** 

	Peak D	Peak Discharge During Event		
Active Drainage	25-Year, 24-Hour	100-Year, 24-Hour	500-Year, 24-Hour	Units
Basin				
1	40.9	79.4	119.1	cfs
2	6.7	13	19.5	cfs
3	0	0	0	cfs
4	3.9	7.5	11.3	cfs
5	6.13	11.9	17.9	cfs
6	3.7	7.0	10.3	cfs
7	22.4	43.5	65.1	cfs
8	1.6	3.0	4.6	cfs
9	5.4	10.4	15.5	cfs
10	3.7	7.0	10.4	cfs
11	4.7	9.0	13.2	cfs

Table 4 - Active Landfill Basins Peak Discharge

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	Peak D	Peak Discharge During Event		
Post Drainage Basin	25-Year, 24-Hour	100-Year, 24-Hour	500-Year, 24-Hour	Units
1	45.0	87.6	131.5	cfs
2	8.3	16.2	24.3	cfs
3	29.8	57.0	85.6	cfs
4	2.0	3.6	5.4	cfs
5	5.2	8.6	14.9	cfs
6	4.1	8.0	12	cfs
7	8.1	15.8	23.6	cfs
8	2.1	4.2	6.2	cfs
9	1.7	3.3	4.9	cfs

**Table 5 - Post-Closure Basins Peak Discharge** 

## 5. PIPE CONVEYANCE SYSTEM DESIGN

The drainage pipe system under the landfills was modeled using the program AutoCAD Storm and Sanitary Analysis 2016 (SSA). The main pipes for this project are as follows:

Pipe 1 - 48" HDPE Pipe (Phase 1)

Pipe 2 - 36" Duromaxx Pipe (Phase 2)

Pipe 3 - 30" Duromaxx Pipe (Phase 2)

Pipe 4 - 42" CMP (Existing Landfill)

Pipe 5 - 18" CMP (Existing Haul Road Culvert)

Pipe 6 - 36" Duromaxx Pipe (Haul Road Culvert Replacement)

SSA allows for modeling of any storm event routed through swales, reservoirs, pipes, culverts, and junctions. Using the 25-year event as the minimum standard for the performance of the pipes, the larger storms were routed through the system to identify long term adequacy of the system. During the 25-year 24-hour event, the existing and newly constructed piping under the landfills was found to be more than adequate to handle the design storm event.

Conveyance	Peak Flow (cfs)	Peak Flow (cfs)	Peak Flow (cfs)	<b>Design Flow</b>
Element	25-YR 24-HR	100-YR 24-HR	500-YR 24-HR	Capacity (cfs)
	Event	Event	Event	
Pipe 1	47.6	92.4	138.6	197.2
Pipe 2	40.9	79.4	119.1	115.1
Pipe 3	6.7	13.0	19.5	97.1
Pipe 4	22.4	55.7	83.8	150.8
Pipe 5	4.7	9.0	13.3	9.5
Pipe 6	30.3	54.5	88.6	60.2*
*This is for the pipe only. During larger flows water will overtop the road which is acceptable				

**Table 6 - Peak Flows in Piping** 

During less frequent, larger storms, the piping system will work well with some ponding at the inlets. Ponding is not an issue as pipe dams have been constructed downstream of the inlets to stop ponded water from entering the ash storage areas. Also, ponding will help slow velocities near the inlet and minimize erosion. Under these larger flows, the system will experience high velocities, which will aid in flushing out any accumulated sediment.

The proposed Pipe 6 (a 36 inch culvert) to replace the existing haul road culvert for Drainage Way 4 will pass a 100 year event and is intended for the active life of the landfill. After closure, this culvert can either be removed and regraded as a ford or left in place realizing it may not pass extreme events above 100 years without overtopping the road, which we consider acceptable because it is well over the 25 year design event standard, should not cause significant damage, and this area is away from CCR storage and thus there is no threat of exposing hydrated fly ash.

#### 6. DRAINAGE WAY FACILITIES

As stated above, the piping conveyance under the landfills will be plugged and abandoned and the inlet areas filled during the post-closure process in order to avoid potential long-term issues related to eventual pipe deterioration/failure. To facilitate surface drainage around the ash landfills, the drainage ways will need to be excavated into the existing ground. The drainage ways will be located outside of the fly ash footprint and placed so as to not pose a risk of future exposure of fly ash. All drainage ways will be excavated at 3H:1V side slopes. All channels will be reclaimed, and managed with appropriate BMPs to mitigate sediment run-off and sediment transport. Rock grade controls will be placed in the channels where slopes exceed 2%. A rock grade control will consist of a 2-feet wide by 4-feet deep strip of rock riprap excavated into the channel bottom and partially into the side slopes (See Sheet C3-2). The grade controls are designed to create an equilibrium slope of 2% between the grade controls by allowing for 3-feet of drop between structures. The equilibrium slope is defined in the National Engineering Handbook as "the channel slope that is required to transport the bed material supplied through the reach, without significant aggradation or degradation of the channel". Equilibrium slope was estimated by comparing existing drainage swale grades on and around the project site. A 2% slope was used as it is less than most of the natural drainage way slopes currently on or around the site. Additional protection will be available given that the grade control structures are 4-feet deep that provides an additional 1-foot of buried rock to help equalize the slope and prevent undermining.

For Drainage Way 1, eleven rock grade-control structures will be needed for a total of approximately 66 cubic yards of rock. Drainage Way 4 will require 12 rock grade-control structures with an estimated volume of 43.7 cubic yards of rock. The rock used in the drop structures should have a median diameter or D50 of 8 inches. The steeper drainage ways 3 and 4 will require the use of rock riprap with a D50 of 12-inches and a riprap thickness of 2-feet. The bottom of the channel and 6-feet on either side will be armored to protect against erosion.

The drainage ways were evaluated using the 25-, 100-, and 500-year 24-hour storm events (the same parameters that were used for the piping conveyance system). All drainage ways were found to be more than adequate for all storm events. Slopes for the drainage ways were mostly averaged and the peak design flow capacity is given for the most constrictive portion of the channel. The bottom widths and descriptions of the drainage ways are as follows:

Drainage Way 1 - 12' bottom width, vegetated swale with rock grade controls

Drainage Way 2 - 12' bottom width, vegetated swale

Drainage Way 3 – 4' bottom width into V-ditch, armored channel into plunge pool and vegetated swale

Drainage Way 4 – 4' bottom width, vegetated swale with rock grade control

Drainage Way 5 – 4' bottom width, armored channel into plunge pool and vegetated swale

Drainage Way 1 will run from its inlet fill area to the existing outlet swale of Pipe 1. Drainage Way 2 drains the Drainage Way 2 Inlet Fill Area to the Drainage Way 1 Inlet Fill Area. Drainage Way 3 is the armored channel from the top of the completed Phase 2 landfill to the Drainage Way 2 Inlet Fill Area. For drainage at the existing closed landfill, Drainage Way 4 will convey drainage from the existing pipe inlet to the existing drainage swale on the northern side of the existing landfill. Once the existing closed landfill top has been graded and filled to direct run-off to the west, Drainage Way 5 will convey the water to the Drainage Way 4 Inlet Fill Area.

Conveyance Element	Peak Flow (cfs) 25-YR 24-HR	Peak Flow (cfs) 100-YR 24-HR	Peak Flow (cfs) 500-YR 24-HR	Design Flow Capacity (cfs)
Brement	Event	Event	Event	cupacity (cis)
Drainage Way 1	42	86.2	119.7	152
Drainage Way 2	8.8	18.1	28.1	201
Drainage Way 3	2.1	4.1	6.2	563
Drainage Way 4	30.3	54.5	88.6	186
Drainage Way 5	1.7	3.2	4.8	540

**Table 7 - Peak Flows in Drainage Ways** 

As outlined in Table 7, the design capacity of the surface drainage ways greatly exceeds the calculated peak flows during the 25-year event. The reason that the drainage ways are so large on the Phase 2 Landfill is because of the anticipated use as access roads during the post-closure period. This use is assumed to be light and/or occasional enough in post closure to prevent significant damage to vegetation.

### 7. SURFACE RUN-OFF

In order to control any surface run-off at the project site, BMPs will be used on disturbed ground. Shallow slopes of 3H:1V or flatter have been used on all landfill features and channel side walls. These shallow slopes are used to limit erosion from higher velocities and promote sheet flow on vegetated slopes. The design of the landfill itself utilizes a 10-foot bench located at the 3170-foot elevation or roughly halfway up the Phase 2 slope. This bench helps to slow run-off velocities on the side slope of the landfill and encourages vegetation uptake. The top of the landfill will have a soil cap that will be seeded for vegetative cover.

## 8. CONCLUSION

All requirements of CCR 257.81 have been meet as shown below:

- (a) The owner or operator of an existing or new CCR landfill or any lateral expansion of a CCR landfill must design, construct, operate and maintain:
  - (1) A run-on control system to prevent flow onto the active portion of the CCR unit during the peak discharge from a 24-hour, 25-year storm; and

As discussed above, the landfill will have two systems for controlling run-on. During the active life of the landfill, internal piping will carry run-on under the landfill. For post-closure a series of drainage ways will be created that will direct flow around the CCR unit.

(2) A run-off control system from the active portion of the CCR unit to collect and control at least the water volume resulting from a 24-hour, 25-year storm.

As discussed above, the excess rainfall created by the active portion of the landfill will be controlled using shallow slopes, benching, and vegetative cover. The flows of water created in the design event will be conveyed in existing and constructed swales or piping to stabilized outlets.

(b) Run-off from the active portion of the CCR unit must be handled in accordance with the surface water requirements under §257.3-3.

In accordance with the surface water section of the Federal Register, no discharge of pollutants is expected to waters of the United States. All disturbed ground is to be vegetated and surface roughened as necessary to reduce run-off from excess rainfall, thus reducing sediment transport. Additional BMPs such as rock riprap, erosion control blankets, and grade controls will be used in areas of concentrated flow to reduce velocities, pond excess rainfall, and settle out sediment. BMPs such as this are already in-place at the inlets to Pipe 2 and Pipe 3.

(c) Run-on and run-off control system plan—(1) Content of the Plan. The owner or operator must prepare initial and periodic run-on and run-off control system plans for the CCR unit according to the timeframes specified... These plans must document how the run-on and run-off control systems has been designed and constructed to meet the applicable requirements of this section. Each plan must be supported by appropriate engineering calculations.

This document constitutes the control systems needed to handle all run-on and run-off for the active and post-closure lifecycles of the CCR landfills. This plan will be updated every 5 years. In each update, the plan will be modified to address the current state of the control system.

(5) The owner or operator must obtain a certification from a qualified professional engineer stating that the initial and periodic run-on and run-off control system plans meet the requirements of this section.

This plan was created by a qualified professional engineer and meets all requirements of the CCR rule 257.81.

Any expected run-on and run-off will be either mitigated using existing vegetation or directed to protected swales and/or piping. Most of the run-on will be handled at the property boundary through inlet areas that direct flow into either the existing piping or into the proposed surface drainage ways. This report shows that the stormwater conveyance systems for the project are more than adequate to handle the required storm event and also larger, less frequent storms that may occur during the active and post-closure time period of the landfill areas.

## 9. CERTIFICATION

This report was prepared by Allied Engineering Services, Inc., under the direction of Douglas S. Chandler, PhD, PE, with assistance from Andrew Graham, PE, and Ronald Orton, Environmental Scientist, and QC review by Brock Athman, PE.

## ALLIED ENGINEERING SERVICES, INC

Douglas S. Chandler, PhD, PE

Andrew S. Graham, PE

Ron Orton

QC Approval: Brock D. Athman, PE

rev. October 17, 2021

## 10. REFERENCES

AASHTO Model Drainage Manual. "Chapter 7, Hydrology." October 3, 1995

Autodesk, Storm and Sanitary Analysis 2016. Version 10.1.53.1

- National Oceanic and Atmospheric Administration. "NOAA Atlas 2 Precipitation Frequency Atlas of the Western United States-Volume I Montana." 1973
- National Engineering Handbook Part 654, "Technical Supplement 14- Grade Stabilization Techniques". 2007
- Urban Drainage And Flood Control District Criteria Manual, "Volume 2 Structures, Storage and Recreation". 2016
- Natural Resources Conservation Service. Web Soil Survey <a href="http://websoilsurvey.nrcs.usda.gov/app/WebSoilSurvey.aspx">http://websoilsurvey.nrcs.usda.gov/app/WebSoilSurvey.aspx</a>. 2016

# **APPENDIX A**

Rosebud Power Plant Fly Ash Landfill Post-Closure Design

# ROSEBUD POWER PLANT

# FLY ASH LANDFILL POST-CLOSURE DESIGN

PROJECT LOCATION: 6.5 MILES NORTH OF COLSTRIP, MT ON HIGHWAY 39

LEGAL DESCRIPTION: NW \(\frac{1}{4}\), SECTION 32, TOWNSHIP 3N, RANGE 41E, P.M.M., ROSEBUD COUNTY, MT

OWNER: COLSTRIP ENERGY LIMITED PARTNERSHIP (CELP) CLIENT: ROSEBUD OPERATING SERVICES, INC.

1087 W. RIVER STREET, SUITE 200

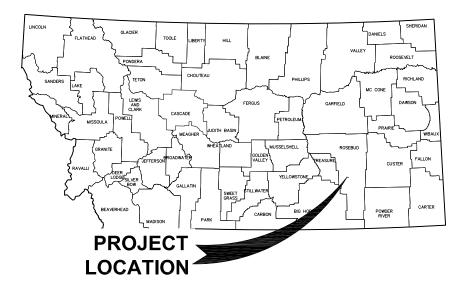
BOISE, ID 83702

1087 W. RIVER STREET, SUITE 200

BOISE, ID 83702

**SEPTEMBER 15, 2016** 

SET NO.



PRINCIPAL-IN-CHARGE: DOUG CHANDLER, PE, Ph.D

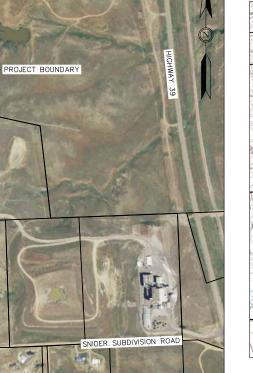
PROJECT ENGINEER: ANDREW S. GRAHAM, PE

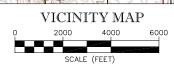
BROCK D. ATHMAN, PE QC REVIEW:

PROJECT SURVEYOR: KYLE THOMPSON, PLS

GREG FINCK, PLS







PROJECT SITE

32 DISCOVERY DRIVE BOZEMAN, MT 59718 PHONE (406) 582-0221 FAX (406) 582-5770 www.alliedengineering.com

Civil Engineering Geotechnical Engineering Land Surveying



ROSEBUD POWER PLANT CO-1 COVER SHEET

ROSEBUD POWER PLANT

## SHEET INDEX

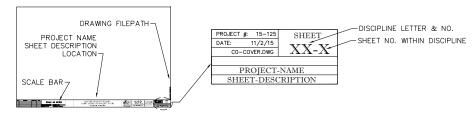
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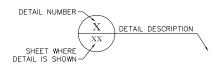
## GENERAL NOTES:

- THESE PLANS PRESENT FIELD AND DESIGN CHANGES TO THE ORIGINAL PLAN SET, ROSEBUD FLYASH DISPOSAL DATED MAY, 1996. THESE ORIGINAL PLANS WERE CREATED BY CHANDLER GEOTECHNICAL, INC. FOR THE DESIGN OF PHASE 1 AND PHASE 2 OF THE FLYASH LANDFILL. ASH PLACEMENT IN PHASE 1 BEGAN IN 2005 AND CONSTRUCTION OF PHASE 2 BEGAN IN AUGUST, 2015. THESE PLANS ARE A CONTINUATION TO THE ROSEBUD POWER PLANT, FLY ASH LANDFILL DESIGN MODIFICATIONS DATED JANUARY 7, 2016.
- 2. THIS PROJECT SHALL BE CONSTRUCTED IN ACCORDANCE WITH ALLIED ENGINEERING'S PLAN SET; ALONG WITH THE MONTANA PUBLIC WORKS STANDARD SPECIFICATIONS (MPWSS), SIXTH EDITION.
- 3. ALL DUROMOXX PIPE IS TO BE INSTALLED PER ALLIED ENGINEERING'S PLANS AND SPECIFICATIONS; ALONG WITH CONTECH'S DuroMaxx STEEL REINFORCED PE TECHNOLOGY INSTALLATION GUIDE.

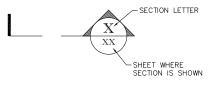
## AESI STANDARD BORDER FORMAT



## PLAN SHEET DETAIL CALLOUTS



## PLAN SHEET SECTION CALLOUTS



## LEGEND

4770	MAJOR CONTOUR - FG	s	SEWER MAIN
4771	MINOR CONTOUR - FG	s	SEWER MAIN - EXISTING
4770	MAJOR CONTOUR - EG	—ss——ss——ss—	SEWER SERVICE
4771	MINOR CONTOUR - EG	<b>S</b>	SANITARY SEWER MANHOLE
•	FOUND MONUMENT AS NOTED	<b>©</b>	SEWER CLEANOUT
0	SET MONUMENT	w	WATER MAIN
◬	CONTROL POINT	w	WATER MAIN - EXISTING
x x	FENCE - EXISTING		WATER SERVICE
OHP	OVERHEAD POWER - EXISTING	Ä	FIRE HYDRANT
— G — G —	UTILITY GAS - EXISTING	60	BLOW-OFF HYDRANT
TEL	UTILITY PHONE - EXISTING	₩V	WATER VALVE
— Е — Е —	UTILITY ELECTRIC - EXISTING	©	WELL
P	UTILITY POWER POLE - EXISTING	<b>@</b>	MONITORING WELL
*	LIGHT POLE - EXISTING	SD	STORM MAIN
E	ELECTRICAL PEDESTAL - EXISTING	=======	CULVERT - EXISTING
EM	ELECTRICAL METER - EXISTING		DITCH-CENTERLINE - EXISTING
EL	TELEPHONE PEDESTAL - EXISTING	(D)	STORM MAIN JOINT, BEND, OR STRUCTURE
GM	GAS METER - EXISTING	<u> </u>	
ov ⊠	GAS VALVE - EXISTING		
0-	GUY ANCHOR - EXISTING		
	EASEMENT LINE		
	BOUNDARY/ LOT LINE		

ROAD CENTERLINE ROAD - CURB

CONCRETE SIDEWALK

IVII	ABBREVIATIONS
SI ) /E	ALLIED ENGINEERING SERVICES, IN ACRE AVENUE
1	BUILDING BENCHMARK BACK OF GRATE (GUTTER)
MP ) )B	CAST IRON CENTERLINE CORRUGATED METAL PIPE CLEAN OUT CITY OF BOZEMAN CONCRETE CUBIC YARD
	DUCTILE IRON DIAMETER DRAWING
EV	EAST EACH EXISTING GRADE ELEVATION EDGE OF GRAVEL EDGE OF PAVEMENT EXISTING
	FLARED END TERMINAL SECTION FINISHED GRADE FIRE HYDRANT

FET FG FH' FL FM FT FLANGE FLOWLINE SEWER FORCE MAIN FEET

GALLONS PER MINUTE GATE VALVE

HDPF HIGH DENSITY POLYETHYLENE HORZ HP HWY HIGHWAY

INVERT ELEVATION INVERT INV

LF LP LT LOW POINT MAXIMUM

MANHOLE MINIMUM MECHANICAL JOINT MID POINT

MONTANA PUBLIC WORKS STANDARD SPECIFICATIONS MONTANA STATE UNIVERSITY

POINT OF CURVATURE
PLAIN END
POLYETHYLENE
POINT OF INTERSECTION
PROPERTY LINE
POUNDS PER SQUARE INCH

POINT OF TANGENCY POLYVINYL CHLORIDE RADIUS POINT

REINFORCED CONCRETE PIPE RIGHT-OF-WAY SOUTH SCHEDULE STORM DRAIN

SECTION SUBGRADE SANITARY SEWER MAIN SANITARY SEWER SERVICE

STANDARD SQUARE YARD

TEMPORARY BENCH MARK TOP BACK OF CURB TOTAL DYNAMIC HEAD TYPICAL TBC TDH TYP

UG UNDERGROUND VC VERT VITRIFIED CLAY

VERTICAL WATER MAIN WEST W/ W/O WS WITH WATER SERVICE

REVISIONS DRAWN BY DATE PROJECT ENGINEER: DSC DRAWN BY: ASG REVIEWED BY: DSC, BDA

ROSEBUD POST-CLOSURE DESIGN SHEET INDEX, LEGEND, & GENERAL NOTES ROSEBUD COUNTY, MT

32 DISCOVERY DRIVE BOZEMAN, MT 59718 PHONE (406) 582-0221 FAX (406) 582-5770 www.allledengineering.com

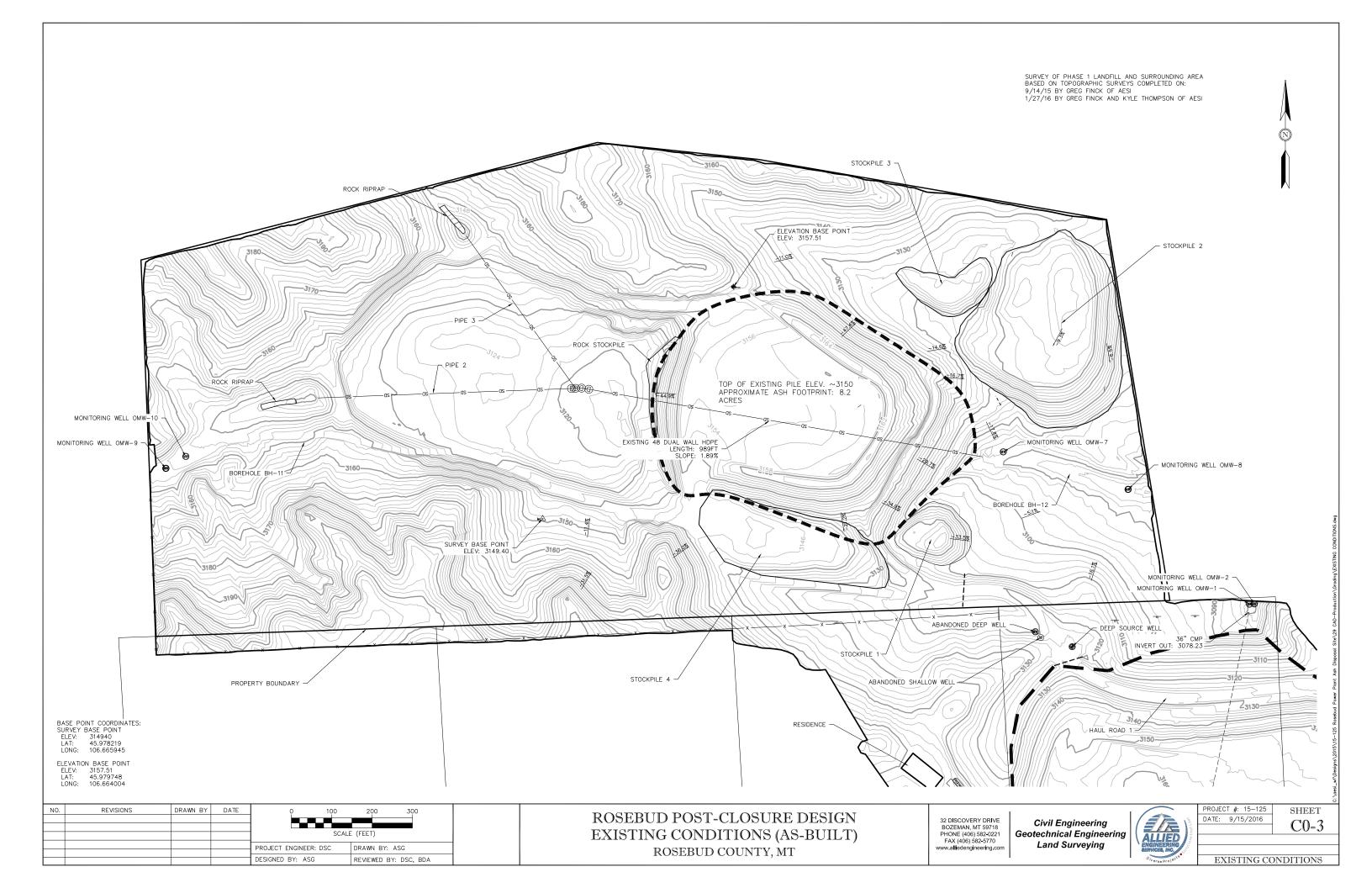
Civil Engineering Geotechnical Engineering Land Surveying

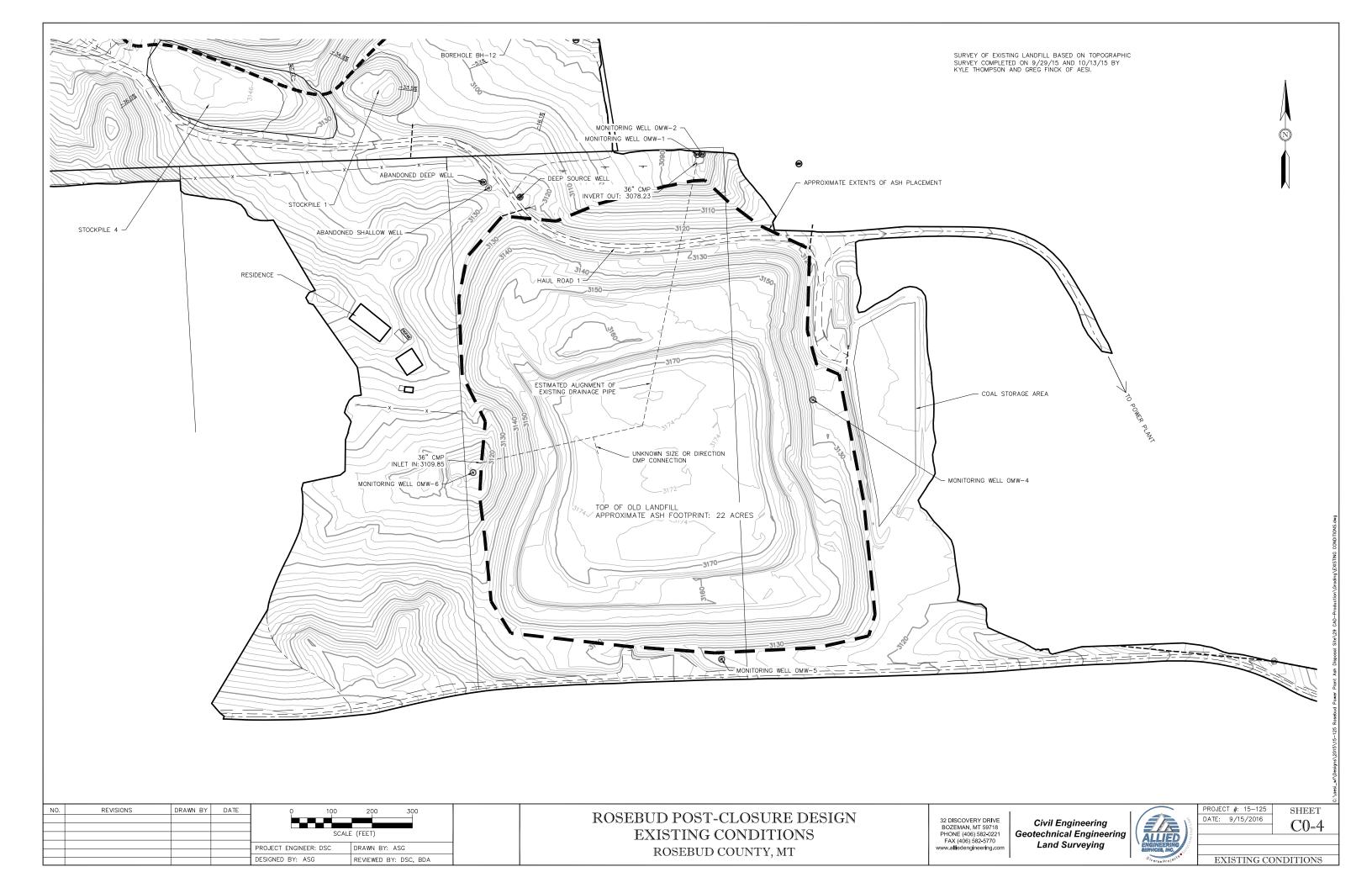


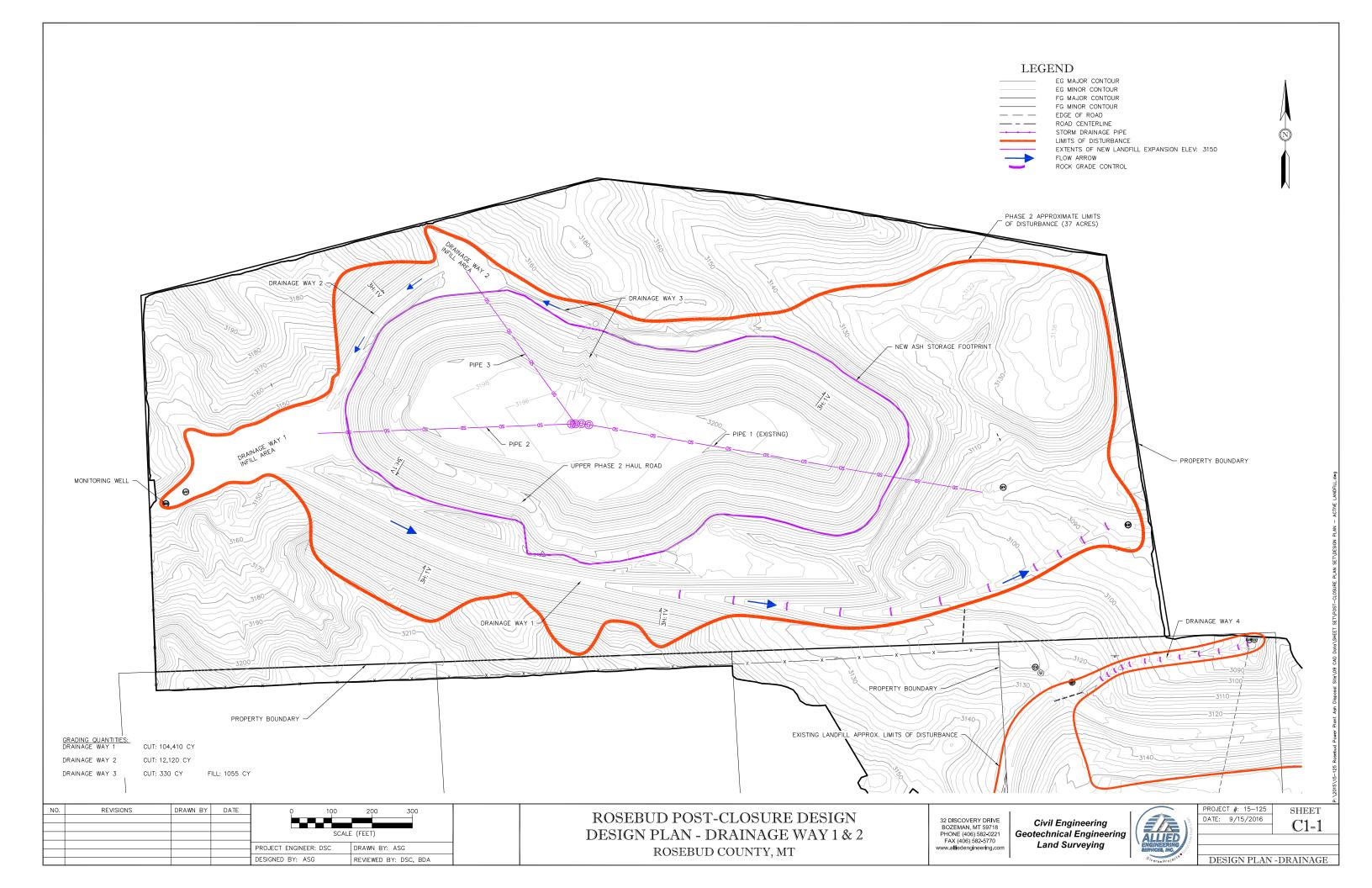
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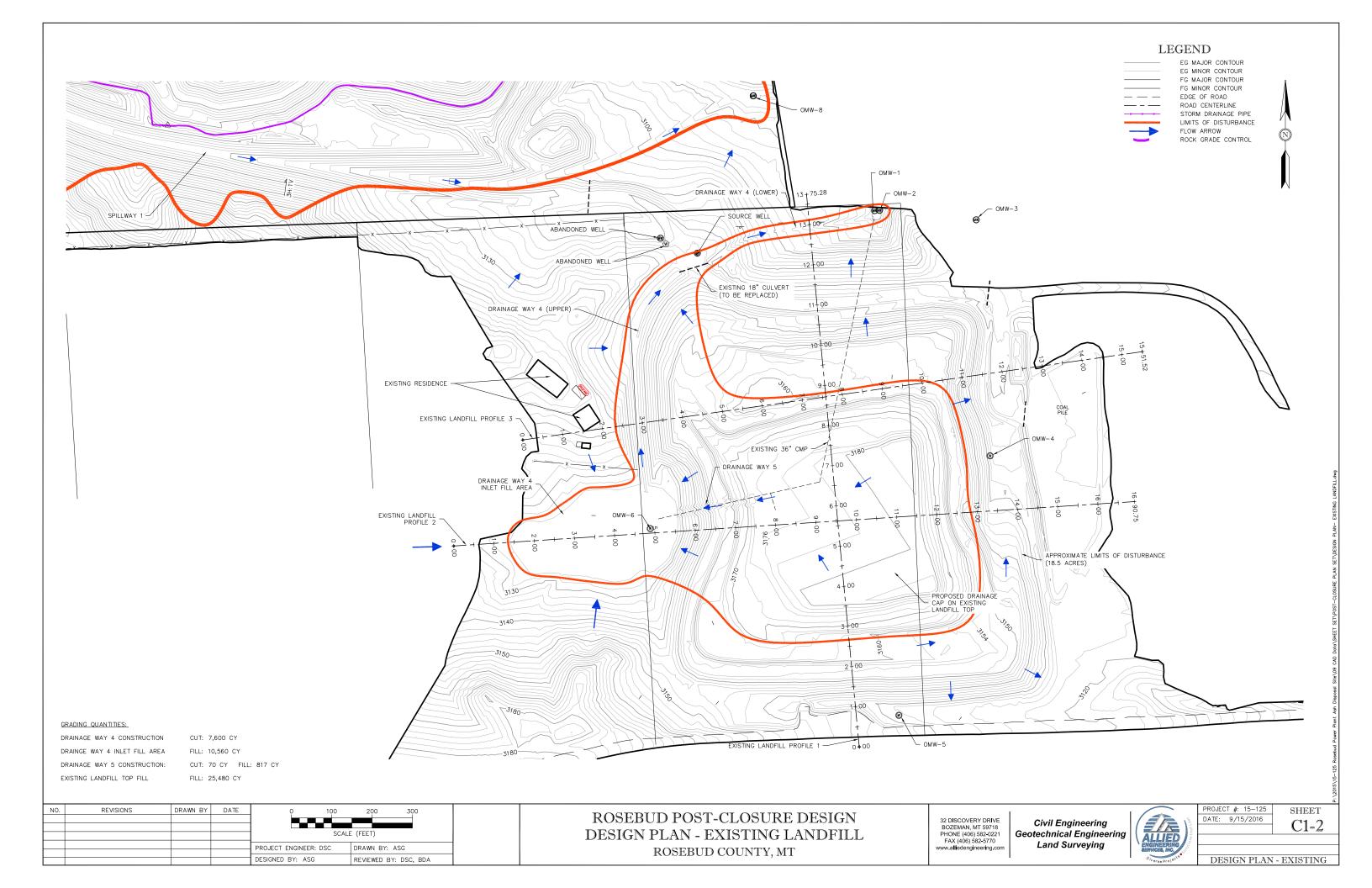
JECT #: 15-125 SHEET E: 9/15/2016 C0-2

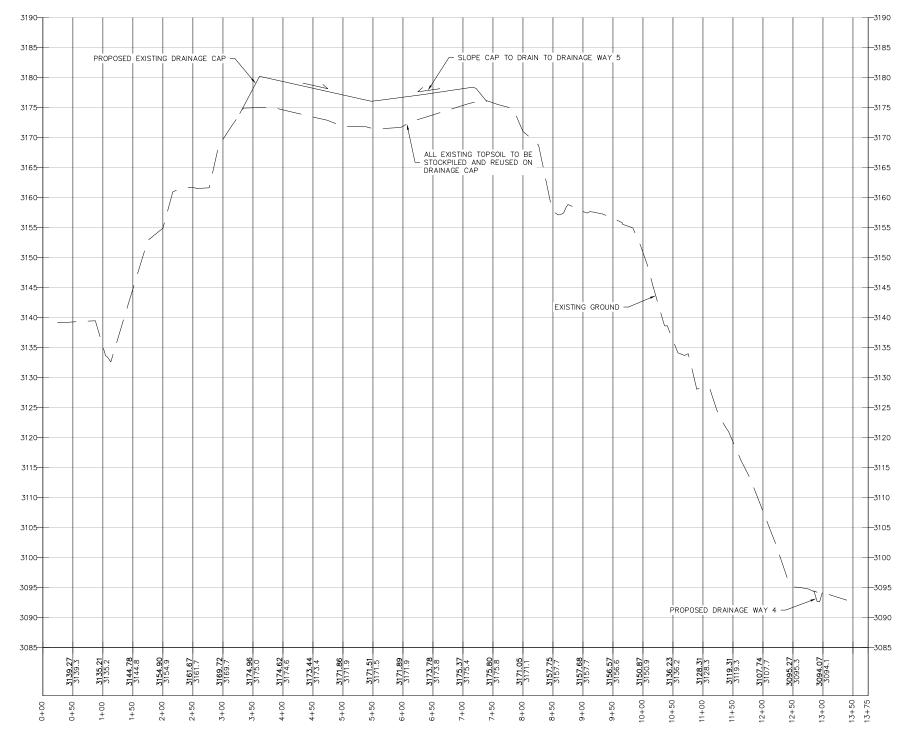
INDEX, LEGEND, & NOTES











PROFILE VIEW - EXISTING LANDFILL PROFILE 1

NO.	REVISIONS	DRAWN BY	DATE	HORIZONTAL SCALE FEET	VERTICAL SCALE FEET
				0 80 160	0 8 16
				PROJECT ENGINEER: DSC	DRAWN BY: ASG
				DESIGNED BY: ASG	REVIEWED BY: DSC, BDA

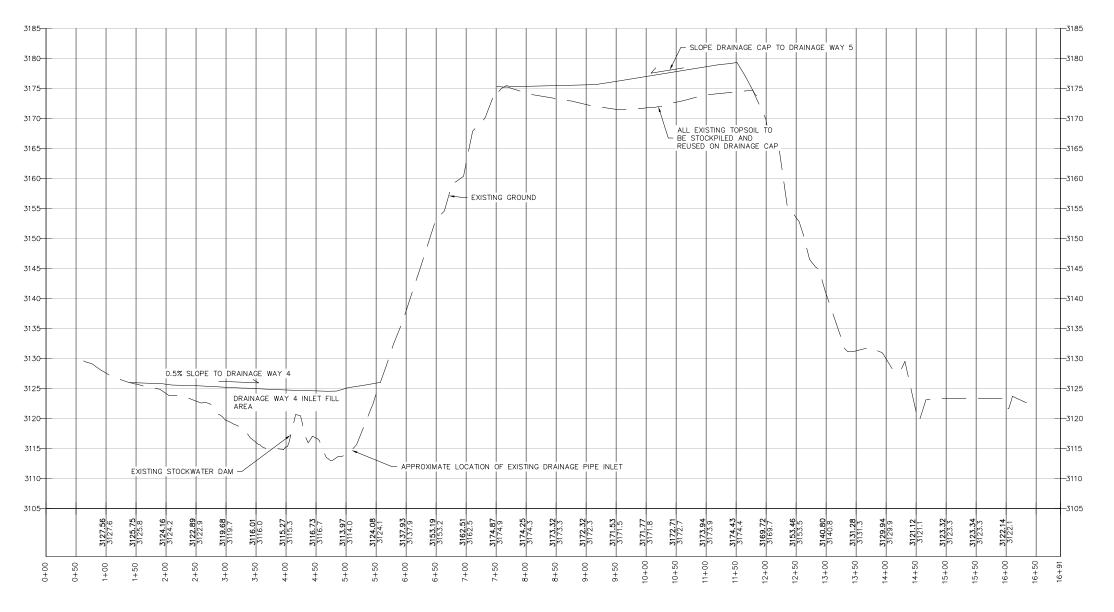
ROSEBUD POST-CLOSURE DESIGN PROFILE VIEW - EXISTING LANDFILL PROFILE 1 ROSEBUD COUNTY, MT

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PROJECT #: 15-125	SHEET
DATE: 9/15/2016	C1-3



PROFILE VIEW - PROFILE 2

NO.	REVISIONS	DRAWN BY	DATE	HORIZONTAL SCALE FEET	VERTICAL SCALE FEET
				0 80 160	0 8 16
					· · · · · · · · · · · · · · · · · · ·
				PROJECT ENGINEER: DSC	DRAWN BY: ASG
				DECIONED BY 100	
				DESIGNED BY: ASG	REVIEWED BY: DSC, BDA

ROSEBUD POST-CLOSURE DESIGN PROFILE VIEW - EXISTING LANDFILL PROFILE 2 ROSEBUD COUNTY, MT

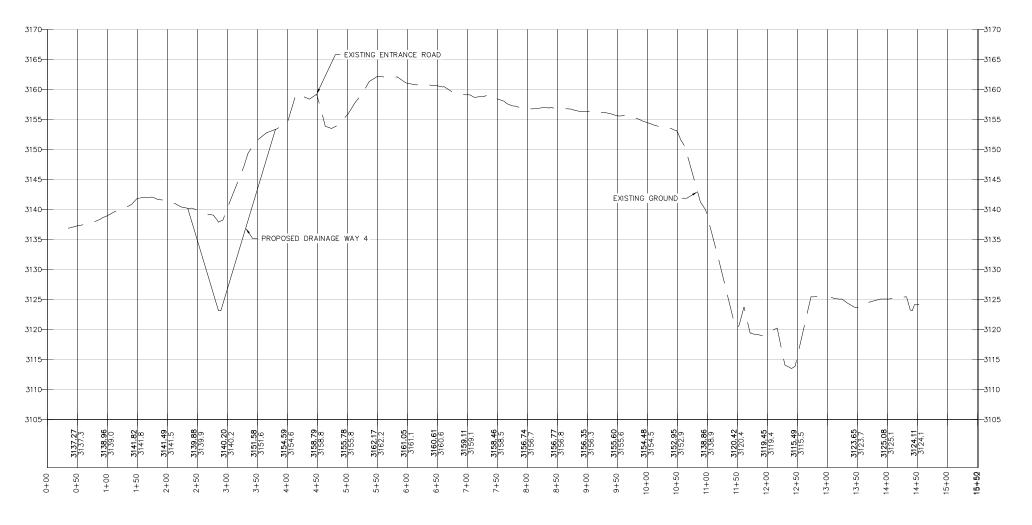
32 DISCOVERY DRIVE BOZEMAN, MT 59718 PHONE (406) 582-0221 FAX (406) 582-5770 www.alliedengineering.com

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C1-4

PROJECT #: 15-125 DATE: 9/15/2016



PROFILE VIEW - PROFILE 3

NO.	REVISIONS	DRAWN BY	DATE	HORIZONTAL SCALE FEET	VERTICAL SCALE FEET
				0 80 160	0 8 16
				PROJECT ENGINEER: DSC	DRAWN BY: ASG
				DESIGNED BY: ASG	REVIEWED BY: DSC, BDA

ROSEBUD POST-CLOSURE DESIGN PROFILE VIEW - EXISTING LANDFILL PROFILE 3 ROSEBUD COUNTY, MT

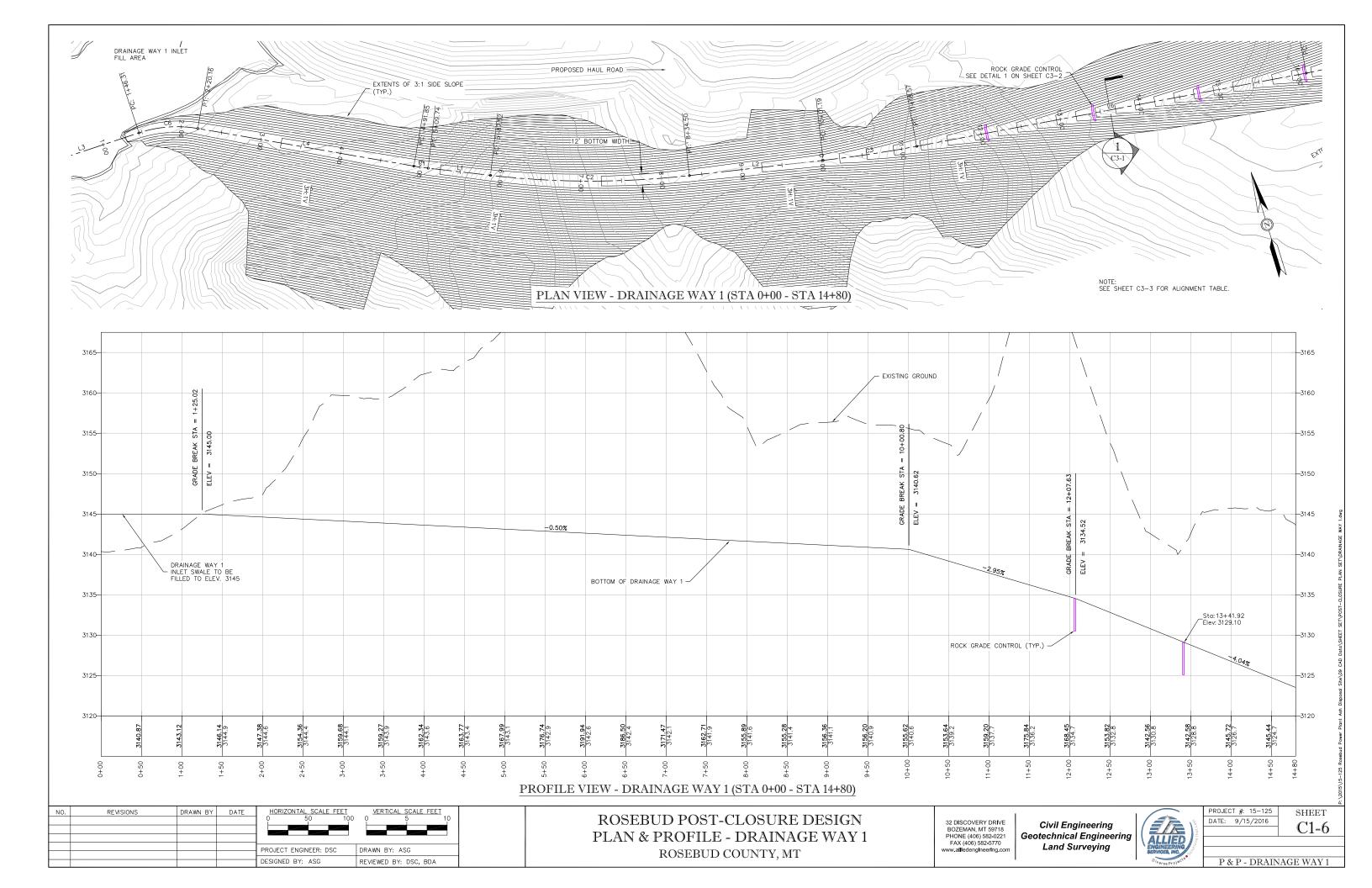
32 DISCOVERY DRIVE BOZEMAN, MT 59718 PHONE (406) 582-0221 FAX (406) 582-5770 www.alliedengineering.com

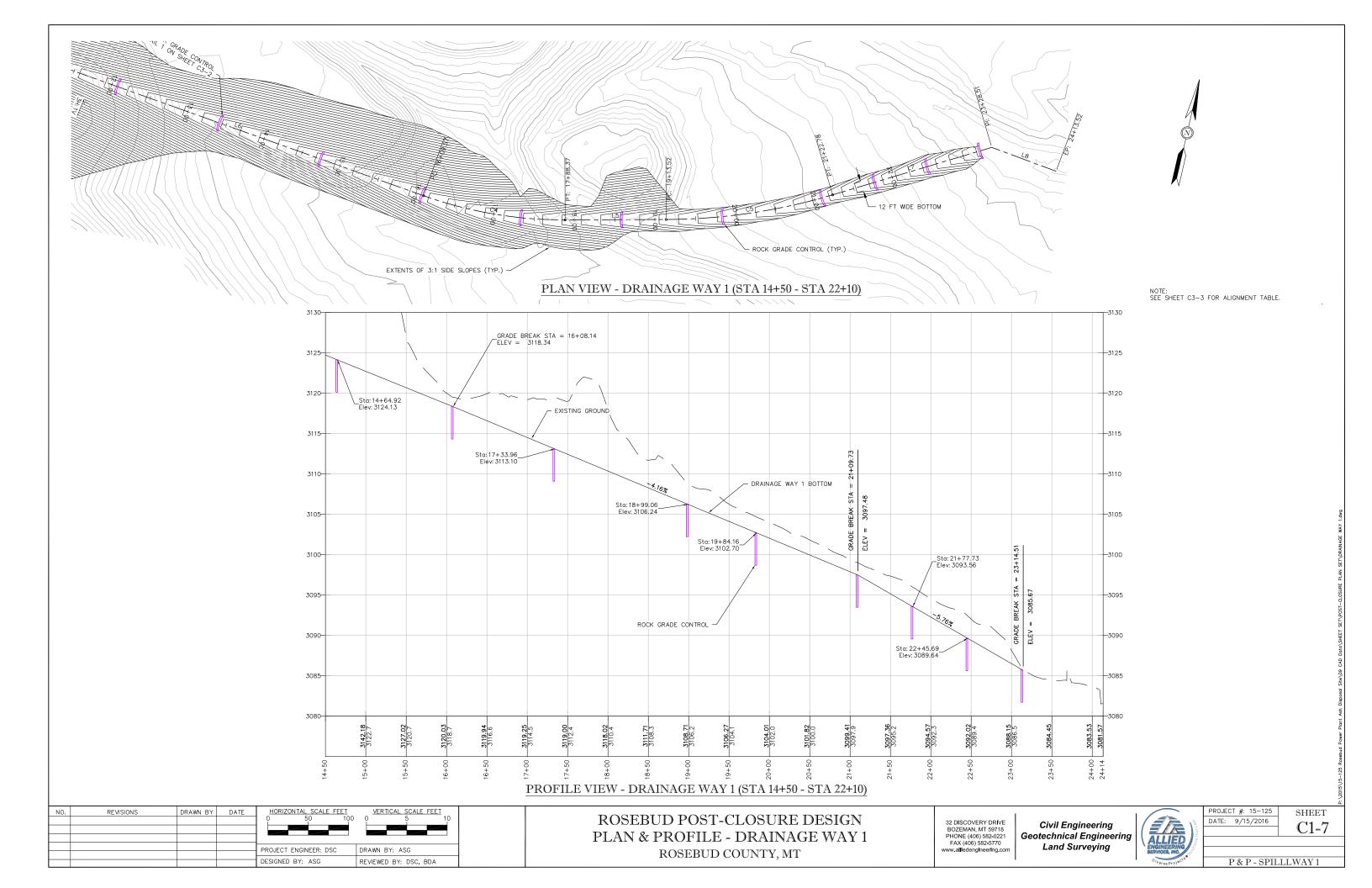
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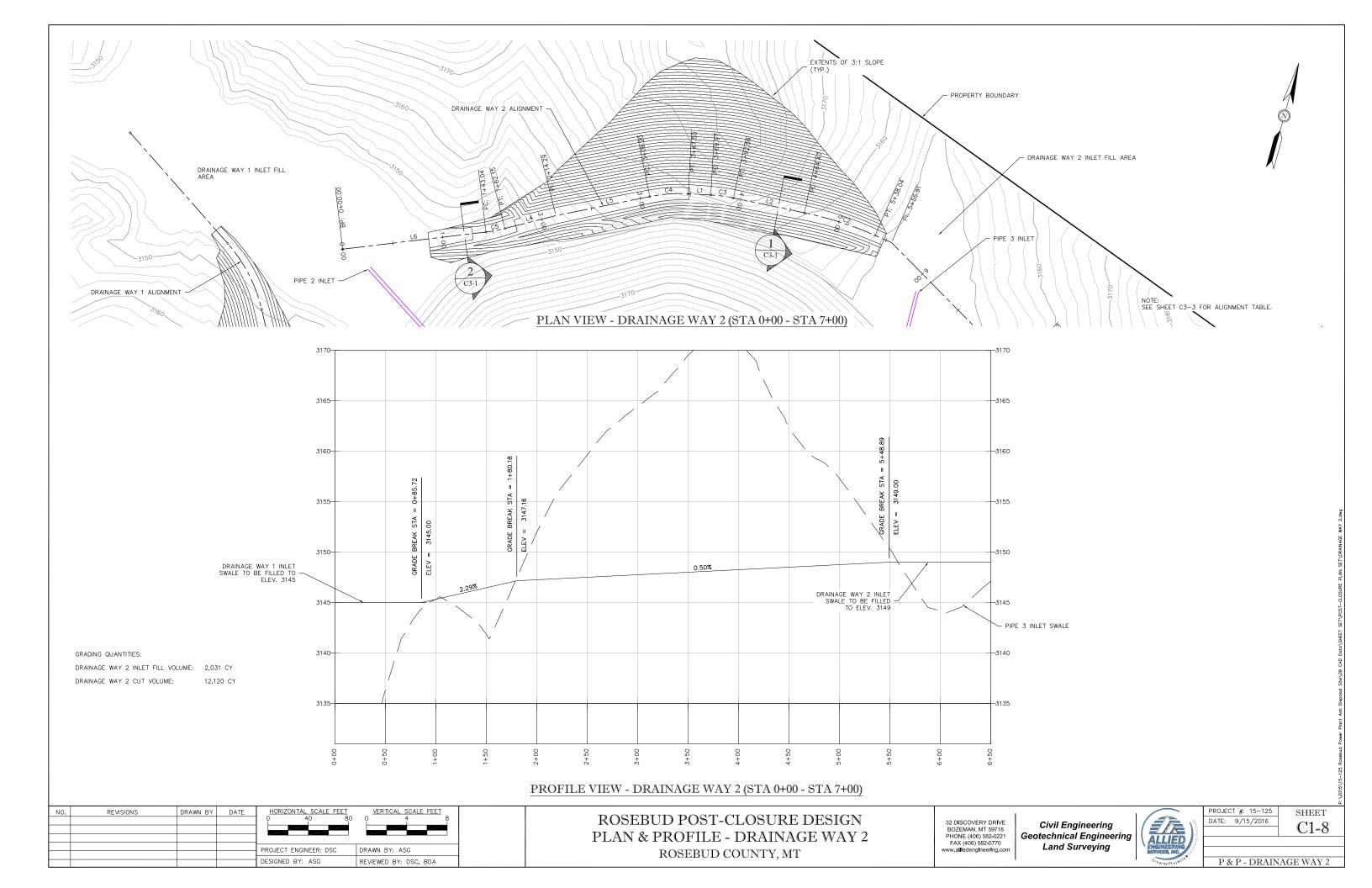


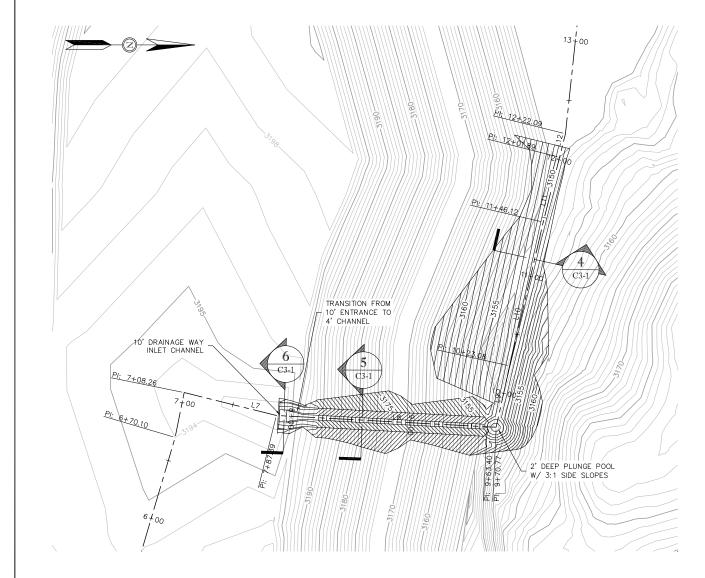
PROJECT #: 15-125 DATE: 9/15/2016

C1-5





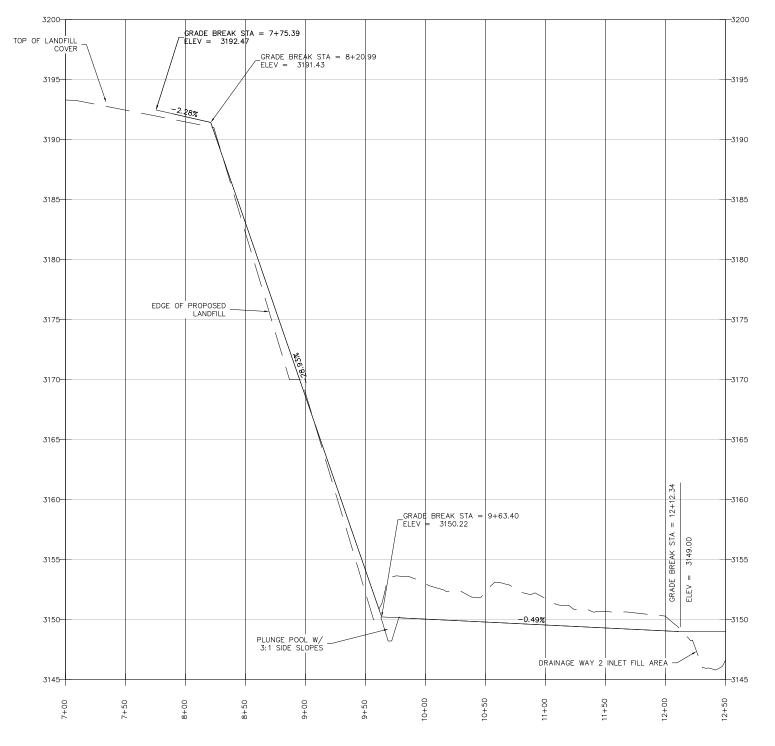




PLAN VIEW - DRAINAGE WAY 3 (STA 7+00 - STA 10+00)

CONSTRUCTION NOTES: ALIGNMENT TABLE: SEE SHEET C3-3

EROSION CONTROL: SEE SHEET C4-1 FOR CHANNEL TYPICAL CROSS-SECTIONS OF DRAINAGE WAY 3 ON SHEET C3-1.



PROFILE VIEW - DRAINAGE WAY 3 (STA 7+00 - STA 10+00)

0 40 80 0 4	NO.	REVISIONS DRAWN BY D	DATE	HORIZONTAL SCALE FEET VERTICAL SCALE FEET
				7 0 40 80 0 4 8
PROJECT ENGINEER: DSC   DRAWN BY: ASG				PROJECT ENGINEER: DSC   DRAWN BY: ASG
TROCEST ENGINEERS 550 BRAIN ST. ASO				TROSECT ENGINEERS BSC BROWN BT. 730
DESIGNED BY: ASG REVIEWED BY: DSC, BDA				DESIGNED BY: ASG REVIEWED BY: DSC, BDA

ROSEBUD POST-CLOSURE DESIGN PLAN & PROFILE - DRAINAGE WAY 3 ROSEBUD COUNTY, MT

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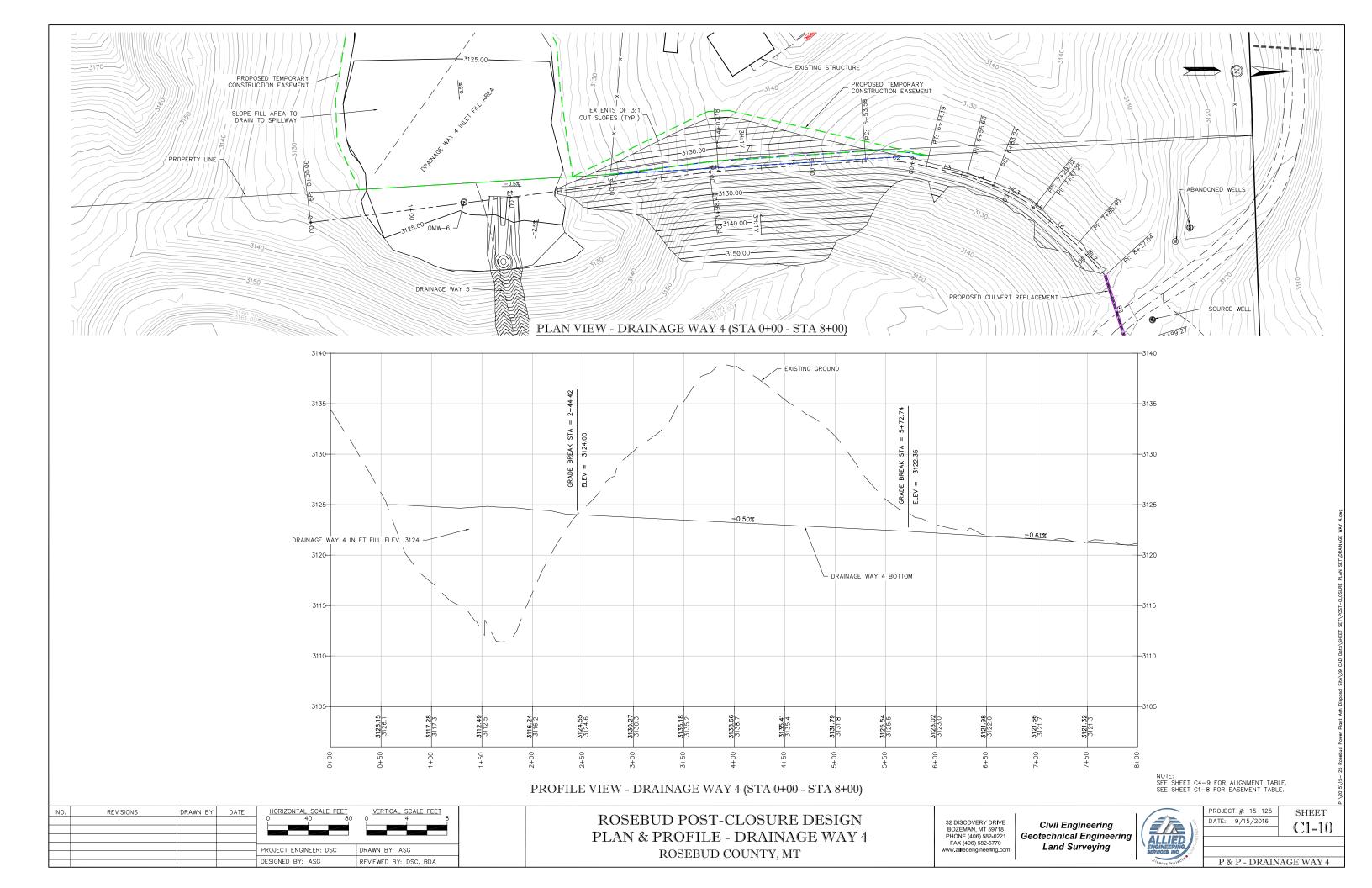
PROJECT	#:	15-125
DATE:	9/1	5/2016

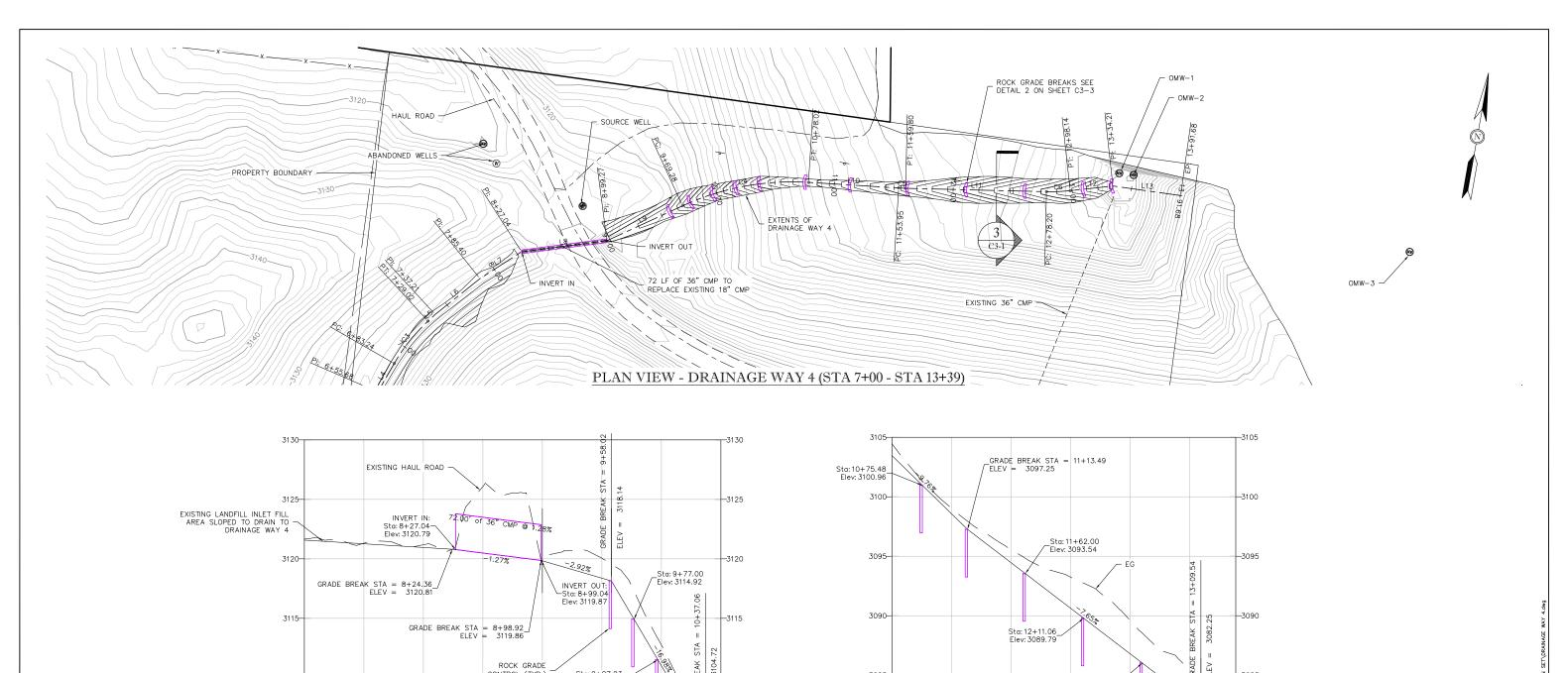
VACE WAY 2

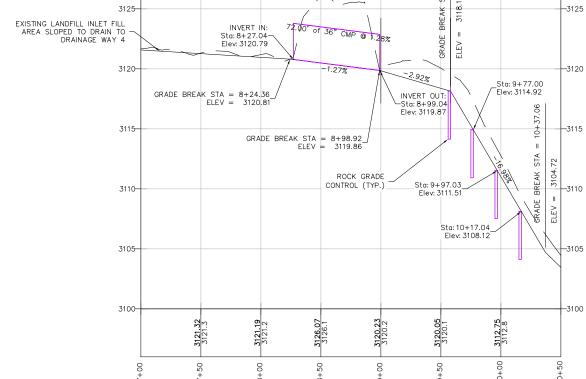
SHEET

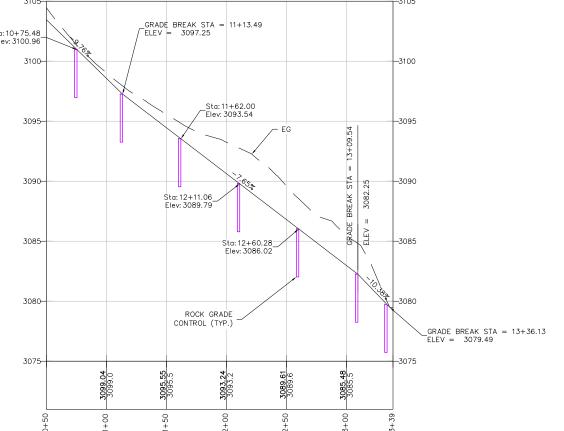
C1-9

P & P - DRAINAGE WAY 3









## PROFILE VIEW - DRAINAGE WAY 4 (STA 7+00 - STA 13+39)

NO.	REVISIONS	DRAWN BY	DATE	HORIZONTAL SCALE FEET	VERTICAL SCALE FEET
				0 40 80	0 4 8
				PROJECT ENGINEER: DSC	DRAWN BY: ASG
l					
				DESIGNED BY: ASG	REVIEWED BY: DSC, BDA

ROSEBUD POST-CLOSURE DESIGN PLAN & PROFILE - DRAINAGE WAY 4 ROSEBUD COUNTY, MT

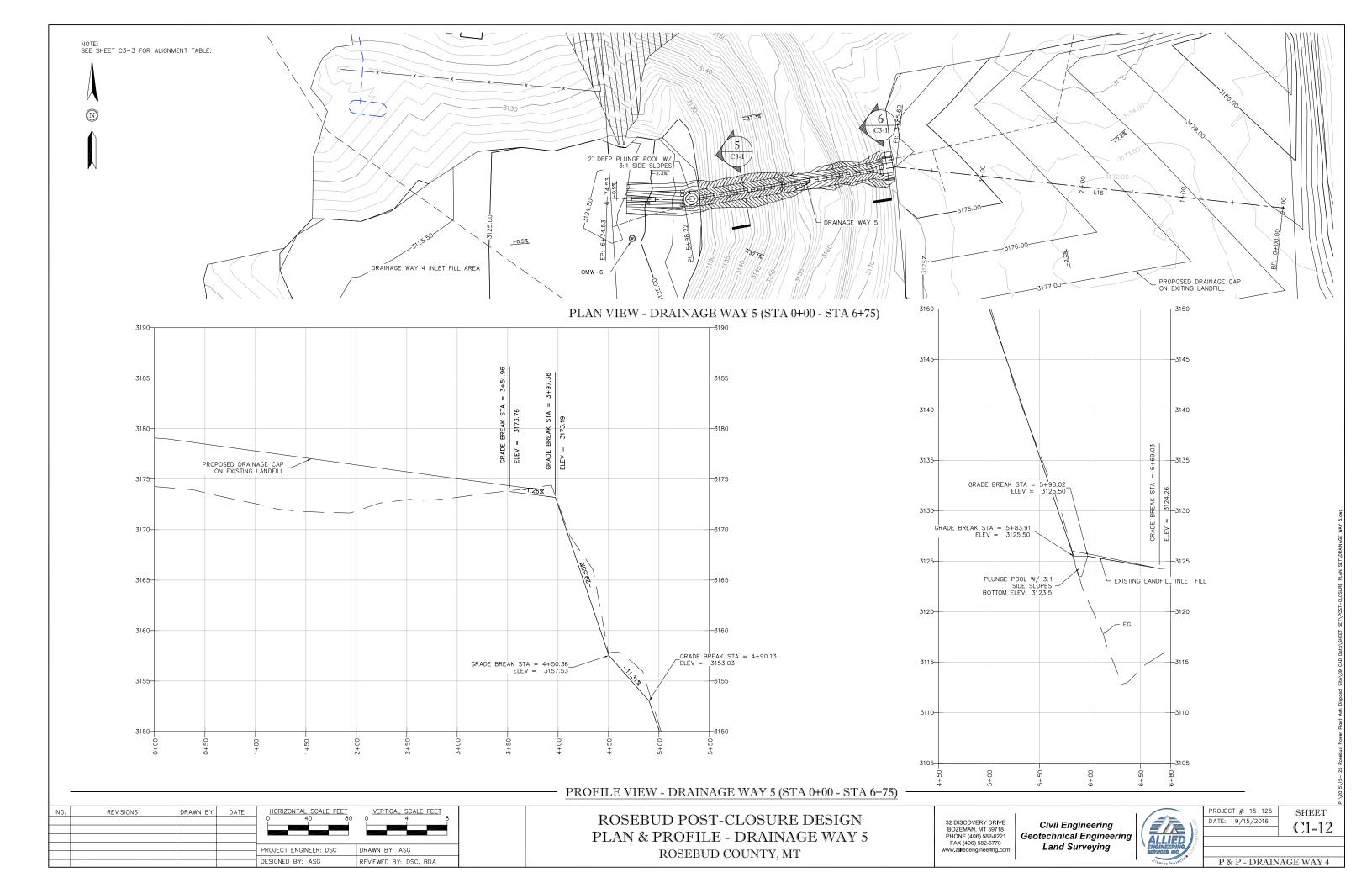
32 DISCOVERY DRIVE BOZEMAN, MT 59718 PHONE (406) 582-0221 FAX (406) 582-5770 www.allledengineering.com

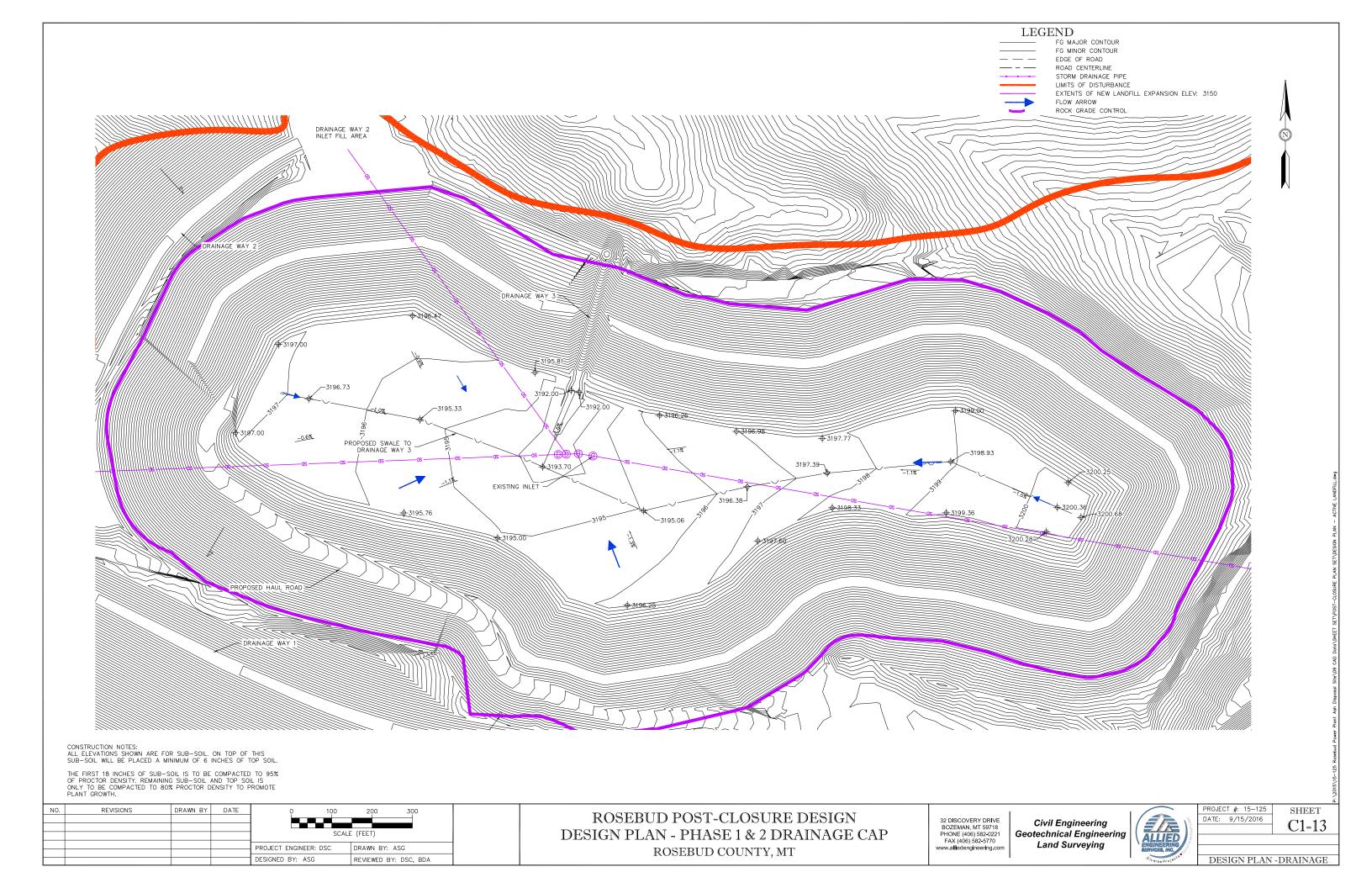
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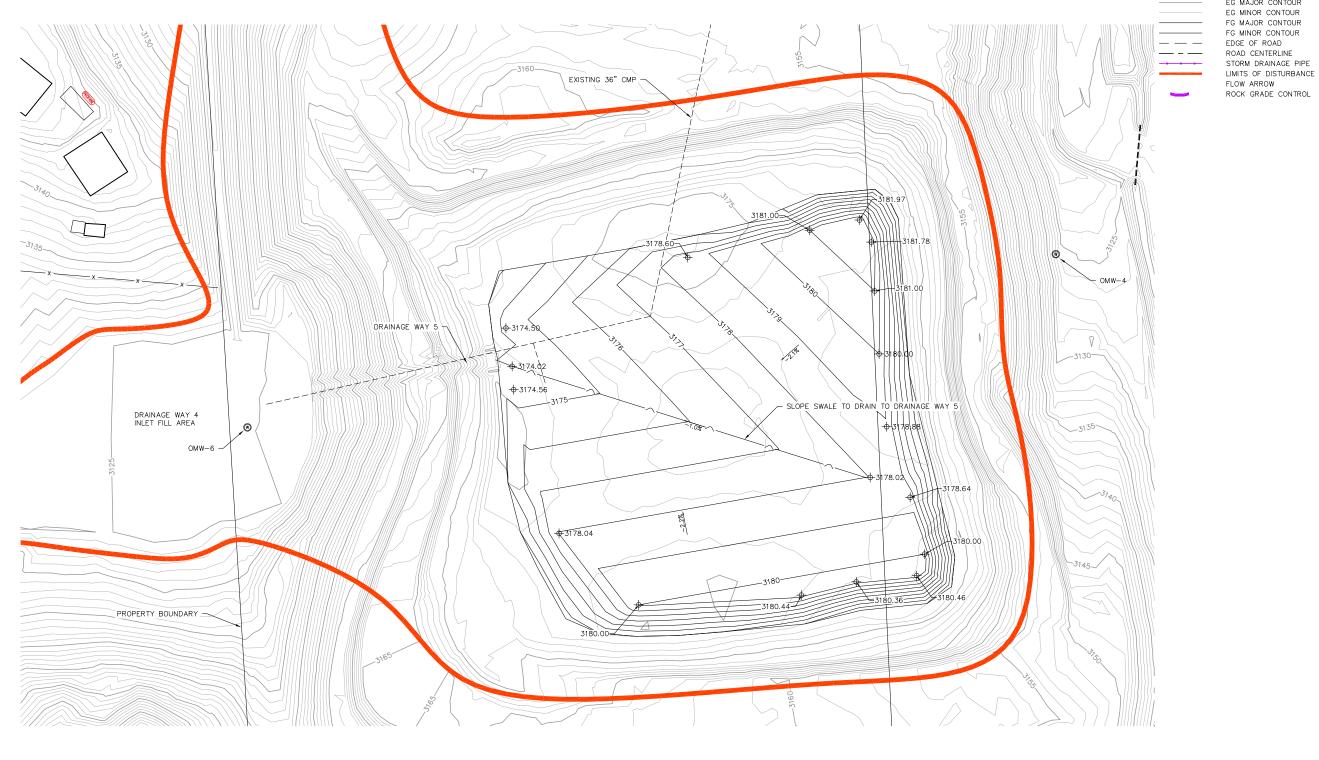


PROJECT #: 15-125	SHEET
DATE: 9/15/2016	Ø1 11
	C1-11

P & P - DRAINAGE WAY 4







CONSTRUCTION NOTES: ALL AREAS TO BE FILLED ARE TO BE STRIPPED OF ALL TOP SOIL.

ALL ELEVATIONS SHOWN ARE FOR SUB-SOIL. ON TOP OF THIS SUB-SOIL WILL BE PLACED A MINIMUM OF 6 INCHES OF TOP SOIL.

THE FIRST 18 INCHES OF SUB-SOIL IS TO BE COMPACTED TO 95% OF PROCTOR DENSITY. REMAINING SUB-SOIL AND TOP SOIL IS ONLY TO BE COMPACTED TO 80% PROCTOR DENSITY TO PROMOTE PLANT GROWTH.

NO.	REVISIONS	DRAWN BY	DATE	Q 1Q0	200 300
				LAO2	E (FEET)
				SCAL	E (FEET)
				PROJECT ENGINEER: DSC	DRAWN BY: ASG
				DESIGNED BY: ASG	REVIEWED BY: DSC, BDA
				DESIGNED D1. A30	REVIEWED BT. DSC, BDA

ROSEBUD POST-CLOSURE DESIGN DESIGN PLAN - EXISTING LANDFILL DRAINAGE CAP ROSEBUD COUNTY, MT

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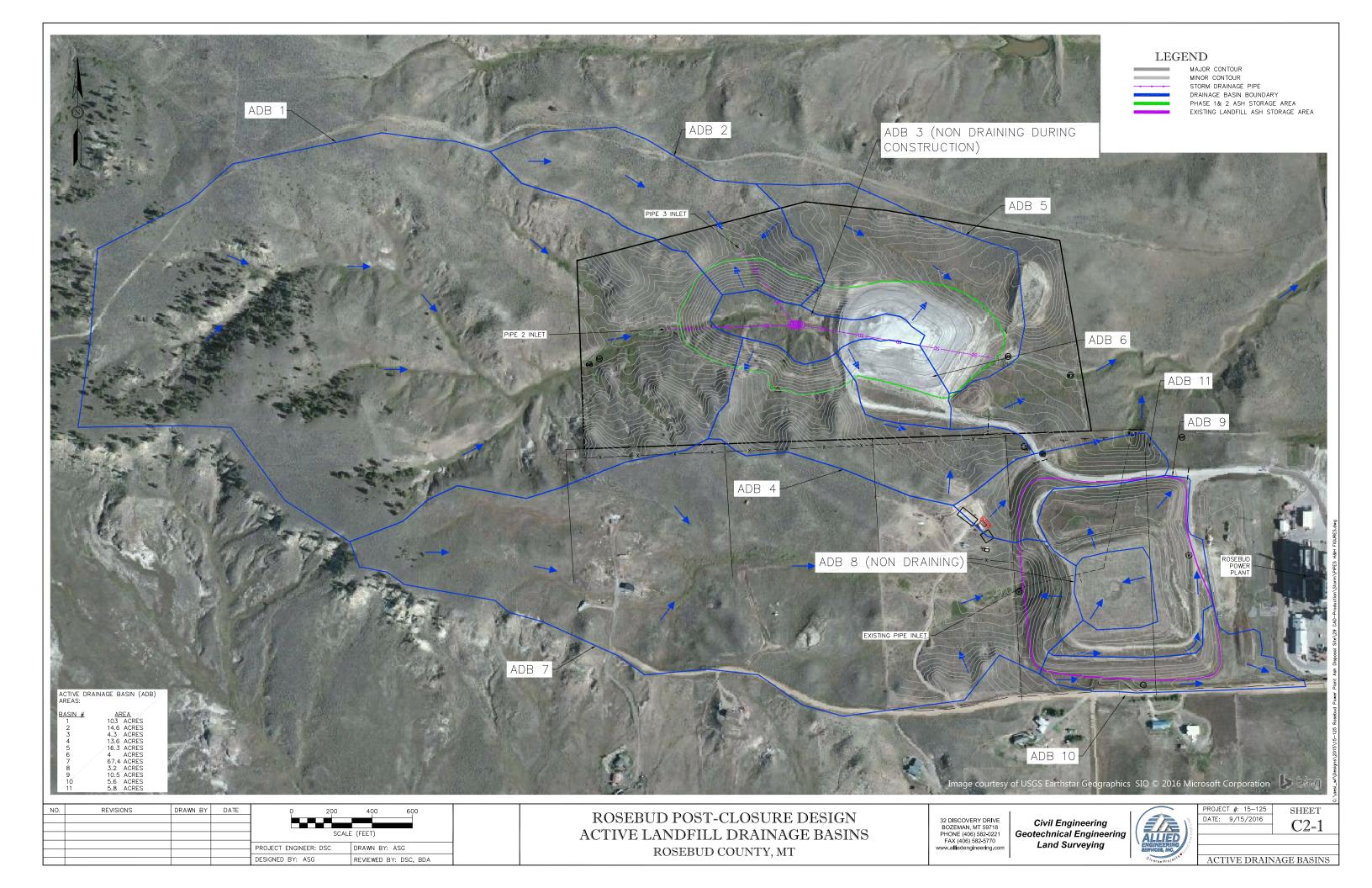
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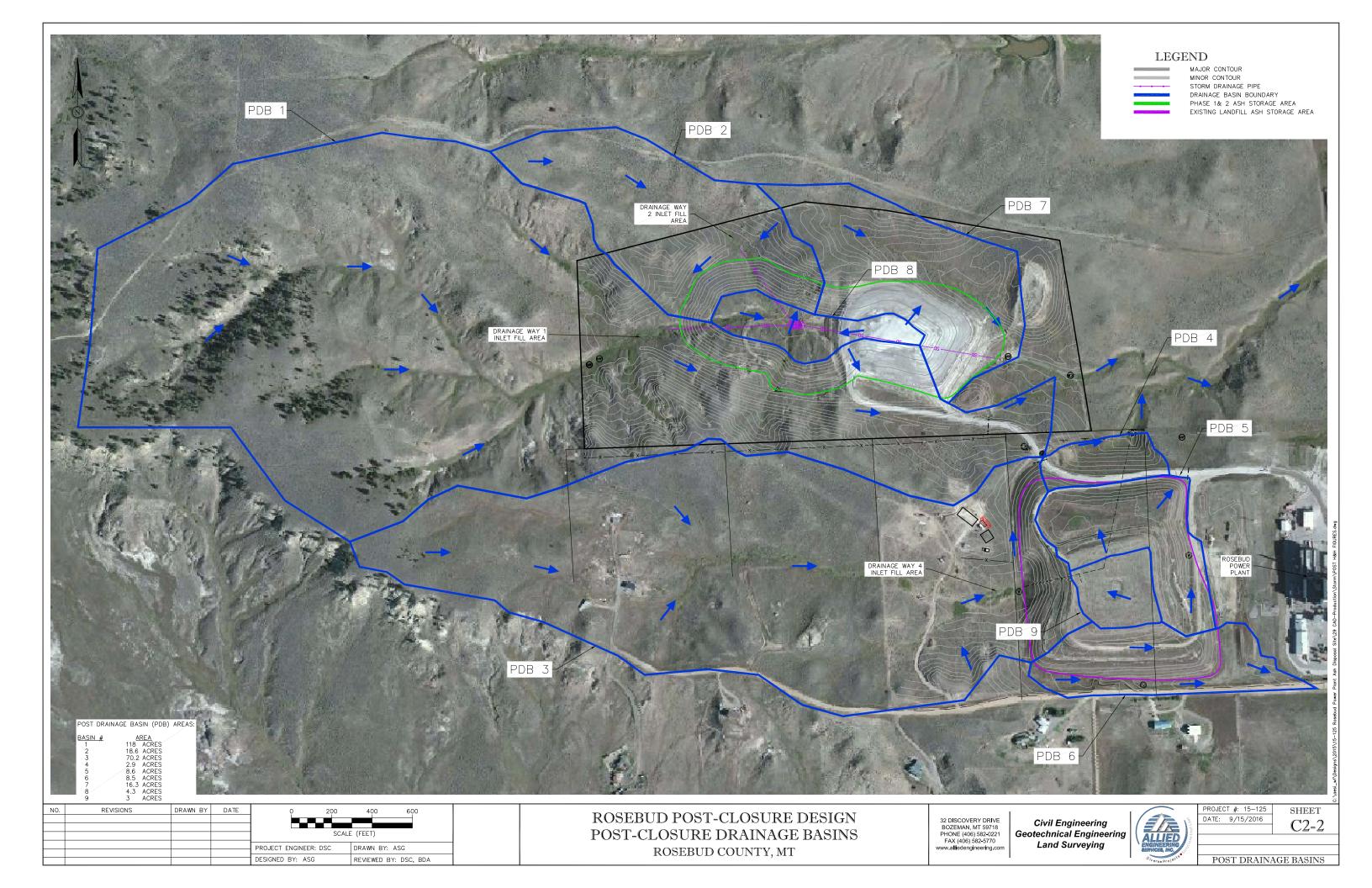


LEGEND

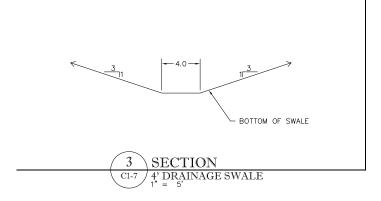
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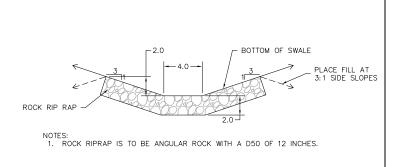
SHEET C1-14



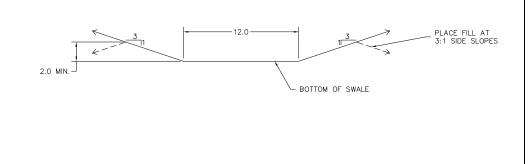




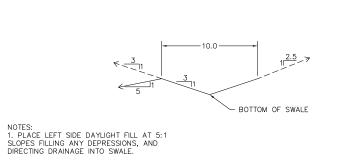




5 SECTION C1-6 4' DRAINAGE SWALE 1" = 5'

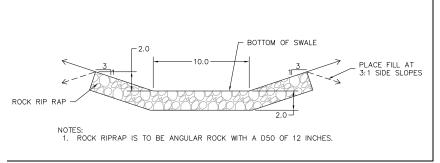


2 SECTION 12' DRAINAGE SWALE W/ RIGHT BERM 1" = 5'



2. CUT RIGHT SIDE DAYLIGHT TO A 2.5:1 OR GREATER DEPENDING ON SOIL CONDITIONS ENCOUNTERED.

SECTION
C1-9 SPILLWAY 4



6 SECTION
10° DRAINAGE SWALE

NO.	REVISIONS	DRAWN BY	DATE			
				PROJECT ENGINEER: DSC	DRAWN BY: ASG	1
						4
				DESIGNED BY: ASG	REVIEWED BY: DSC, BDA	

ROSEBUD POST-CLOSURE DESIGN DETAILS - SWALE SECTIONS ROSEBUD COUNTY, MT

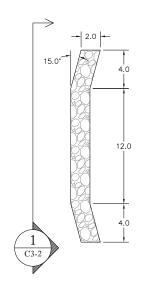
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PROJECT #: 15-125	SHEET
DATE: 9/15/2016	(12.1
	C3-1

DETAILS - SWALE SECTIONS



1 DETAIL

C2-2 SPILLWAY 1 GRADE CONTROL - PLAN VIEW

ROCK RIP RAP

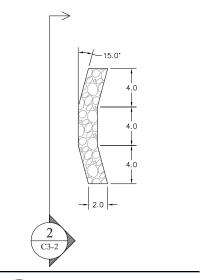
BOTTOM OF SWALE

NOTES:

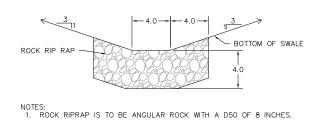
1. ROCK RIPRAP IS TO BE ANGULAR ROCK WITH A D50 OF 8 INCHES.

1 SECTION

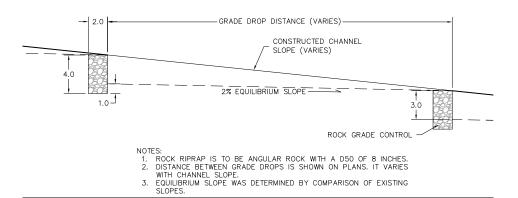
C3-2 SPILLWAY I GRADE CONTROL



2 DETAIL
SPILLWAY 3 GRADE CONTROL - PLAN VIEW



2 SECTION SPILLWAY 3 GRADE CONTROL



3 DETAIL
TYPICAL GRADE CONTROL PROFILE

NO. REVISIONS DRAWN BY DATE

PROJECT ENGINEER: DSC DRAWN BY: ASG
DESIGNED BY: ASG REVIEWED BY: DSC, BDA

ROSEBUD POST-CLOSURE DESIGN DETAILS - ROCK GRADE CONTROLS ROSEBUD COUNTY, MT

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PROJECT #: 15-125	SHEET
DATE: 9/15/2016	(12.2
	U3-2

DETAILS - ROCK CONTROL

18715-195 Brookind Dower Dlank Ash Disnasal CHA/ND PAD DARA/SHEET SETYDOST-M OSIDE DIAN S

DRAINAGE WAY 1 ALIGNMENT						
Number	Radius	Length	Line/Chord Direction	Start Station	End Station	Start Northing, Easting
L3		146.31	N88* 36' 59.04"E	0+00.00	1+46.31	643344.5741, 2687756.5228
C6	150.00	73.86	S77* 16' 41.83"E	1+46.31	2+20.16	643348.1068, 2687902.7880
L4		271.68	S63° 10' 22.69"E	2+20.16	4+91.85	643332.0065, 2687974.1047
C1	312.15	17.89	S64° 48′ 54.31″E	4+91.85	5+09.74	643209.3966, 2688216.5469
L1		77.78	S66* 27' 25.94"E	5+09.74	5+87.52	643201.7835, 2688232.7365
C2	1084.22	246.98	S72° 58' 58.71"E	5+87.52	8+34.50	643170.7161, 2688304.0411
L2		166.70	S79* 30' 31.48"E	8+34.50	10+01.19	643098.5926, 2688539.6957
С3	1614.37	117.37	S81° 35′ 29.84″E	10+01.19	11+18.57	643068.2396, 2688703.6054
L6		491.00	S83° 40' 28.20"E	11+18.57	16+09.57	643051.0800, 2688819.6928
C4	516.43	178.80	N86* 24' 25.40"E	16+09.57	17+88.37	642996.9829, 2689307.7071
L5		125.15	N76° 29' 19.00"E	17+88.37	19+13.52	643008.1319, 2689485.2646
C5	732.50	209.26	N68* 18' 16.74"E	19+13.52	21+22.78	643037.3726, 2689606.9542
L7		205.73	N60* 07' 14.48"E	21+22.78	23+28.51	643114.4664, 2689800.7281
L8		85.01	S82* 55' 28.98"E	23+28.51	24+13.52	643216.9581, 2689979.1158

DRAINAGE WAY 2 ALIGNMENT						
Number	Radius	Length	Line/Chord Direction	Start Station	End Station	Start Northing, Easting
L6		143.04	N33° 10' 00.74"E	0+00.00	1+43.04	643431.7828, 2687980.2610
C5	150.00	19.11	N29° 31′ 01.66″E	1+43.04	1+62.15	643551.5167, 2688058.5138
L4		52.14	N25° 52' 02.59"E	1+62.15	2+14.29	643568.1351, 2688067.9226
L5		94.91	N28° 30′ 48.36″E	2+14.29	3+09.20	643615.0533, 2688090.6719
C4	150.00	38.30	N35* 49' 38.90"E	3+09.20	3+47.50	643698.4554, 2688135.9809
L1		22.47	N43° 08' 29.44"E	3+47.50	3+69.97	643729.4211, 2688158.3366
C3	150.00	22.62	N47° 27′ 42.66″E	3+69.97	3+92.59	643745.8146, 2688173.6997
L2		71.88	N51° 46' 55.89"E	3+92.59	4+64.47	643761.0939, 2688190.3518
C2	355.54	73.57	N57° 42′ 36.31″E	4+64.47	5+38.04	643805.5653, 2688246.8288

	DRAINAGE WAY 4 ALIGNMENT					
Number	Radius	Length	Line/Chord Direction	Start Station	End Station	Start Northing, Easting
L1		398.47	N7* 12' 41.64"W	0+00.00	3+98.47	641989.0819, 2689783.7761
C1	150.00	8.71	N5° 32' 52.52"W	3+98.47	4+07.18	642384.3984, 2689733.7549
L2		146.40	N3* 53' 03.40"W	4+07.18	5+53.58	642393.0672, 2689732.9129
C2	200.00	60.61	N4* 47' 51.97"E	5+53.58	6+14.19	642539.1338, 2689722.9953
L3		41.48	N13* 28' 47.34"E	6+14.19	6+55.68	642599.3026, 2689728.0455
L4		27.57	N19* 55' 02.83"E	6+55.68	6+83.24	642639.6409, 2689737.7148
С3	150.00	45.78	N28* 39' 40.33"E	6+83.24	7+29.02	642665.5578, 2689747.1055
L5		8.19	N37° 24' 17.83"E	7+29.02	7+37.21	642705.5746, 2689768.9789
L6		48.18	N41° 16' 43.16"E	7+37.21	7+85.40	642712.0804, 2689773.9539
L7		41.65	N47° 12' 05.16"E	7+85.40	8+27.04	642748.2914, 2689805.7420
L8		72.23	N72* 35' 03.58"E	8+27.04	8+99.27	642776.5860, 2689836.2990
L9		70.01	N55* 15' 38.42"E	8+99.27	9+69.28	642798.2050, 2689905.2192
C4	219.87	108.74	N69° 25' 41.66"E	9+69.28	10+78.02	642838.0991, 2689962.7492
L10		75.94	N83* 35' 44.90"E	10+78.02	11+53.95	642875.9183, 2690063.5164
C5	150.00	5.84	N82* 28' 49.16"E	11+53.95	11+59.80	642884.3884, 2690138.9792
L11		118.41	N81° 21' 53.41"E	11+59.80	12+78.20	642885.1527, 2690144.7693
C6	150.00	19.94	N77* 33' 23.89"E	12+78.20	12+98.14	642902.9304, 2690261.8327
L12		36.07	N73° 44' 54.38"E	12+98.14	13+34.21	642907.2237, 2690281.2896
L13		57.47	N88° 02' 50.21"E	13+34.21	13+91.68	642917.3186, 2690315.9202

DRAINAGE WA				WAY 5 ALI	GNMENT	
Number	Radius	Length	Line/Chord Direction	Start Station	End Station	Start Northing, Easting
L14		76.31	N88* 27' 10.46"W	5+98.22	6+74.53	642178.8475, 2689815.0061
L15		212.62	S81° 05' 30.77"W	3+85.60	5+98.22	642211.7723, 2690025.0646
L16		385.60	N83° 58' 06.39"W	0+00.00	3+85.60	642171.2554, 2690408.5251

DRAINAGE WAY 3 ALIGNMENT						
Number	Radius	Length	Line/Chord Direction	Start Station	End Station	Start Northing, Easting
L7		79.14	N23* 58' 15.77"E	7+08.26	7+87.39	643460.8902, 2688626.0039
L8		176.01	N13* 05' 01.79"E	7+87.39	9+63.40	643533.2022, 2688658.1555
L9		52.31	N67* 32' 36.83"W	9+70.77	10+23.08	643711.8326, 2688699.6038
L10		123.04	N66° 51′ 54.52″W	10+23.08	11+46.12	643731.8139, 2688651.2609
L11		55.76	N65° 51' 12.83"W	11+46.12	12+01.89	643780.1573, 2688538.1121
L12		20.20	N66* 02' 56.78"W	12+01.89	12+22.09	643802.9681, 2688487.2288

REVISIONS DRAWN BY DATE PROJECT ENGINEER: DSC DRAWN BY: ASG DESIGNED BY: ASG REVIEWED BY: DSC, BDA

ROSEBUD POST-CLOSURE DESIGN DETAILS - ALIGNMENT TABLES ROSEBUD COUNTY, MT

32 DISCOVERY DRIVE BOZEMAN, MT 59718 PHONE (406) 582-0221 FAX (406) 582-5770 www.alliedengineering.com

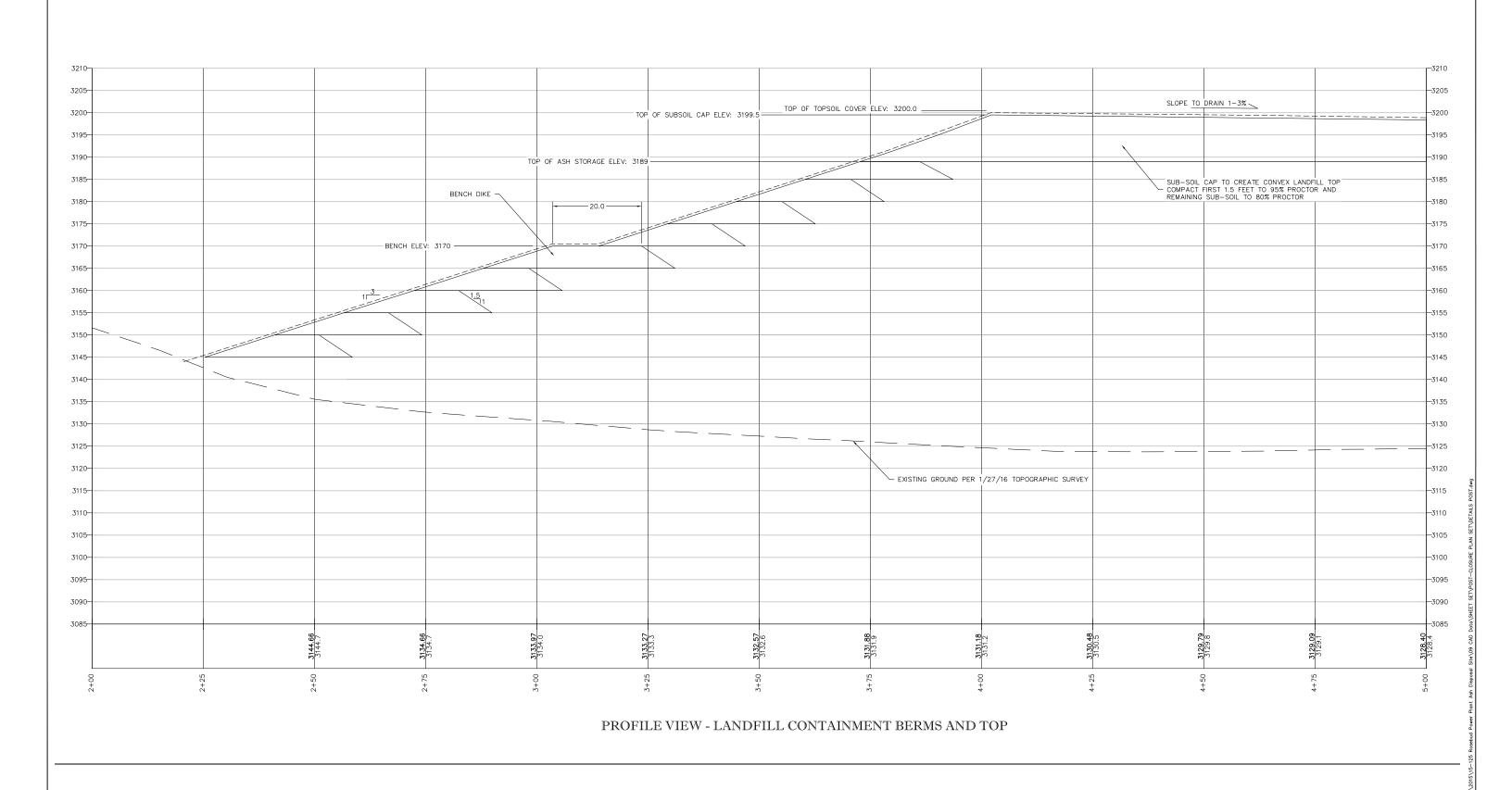
Civil Engineering
Geotechnical Engineering
Land Surveying Land Surveying



PROJECT #: 15-125
DATE: 9/15/2016

SHEET C3-3

DETAILS - TABLES



ROSEBUD POST-CLOSURE DESIGN

DETAILS - LANDFILL TOP

ROSEBUD COUNTY, MT

PROJECT #: 15-125

DETAILS - LANDFILL TOP

DATE: 9/15/2016

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32 DISCOVERY DRIVE BOZEMAN, MT 59718 PHONE (406) 582-0221 FAX (406) 582-5770 www.alliedengineering.com SHEET

VERTICAL SCALE FEET

DRAWN BY: ASG

REVIEWED BY: DSC, BDA

HORIZONTAL SCALE FEET

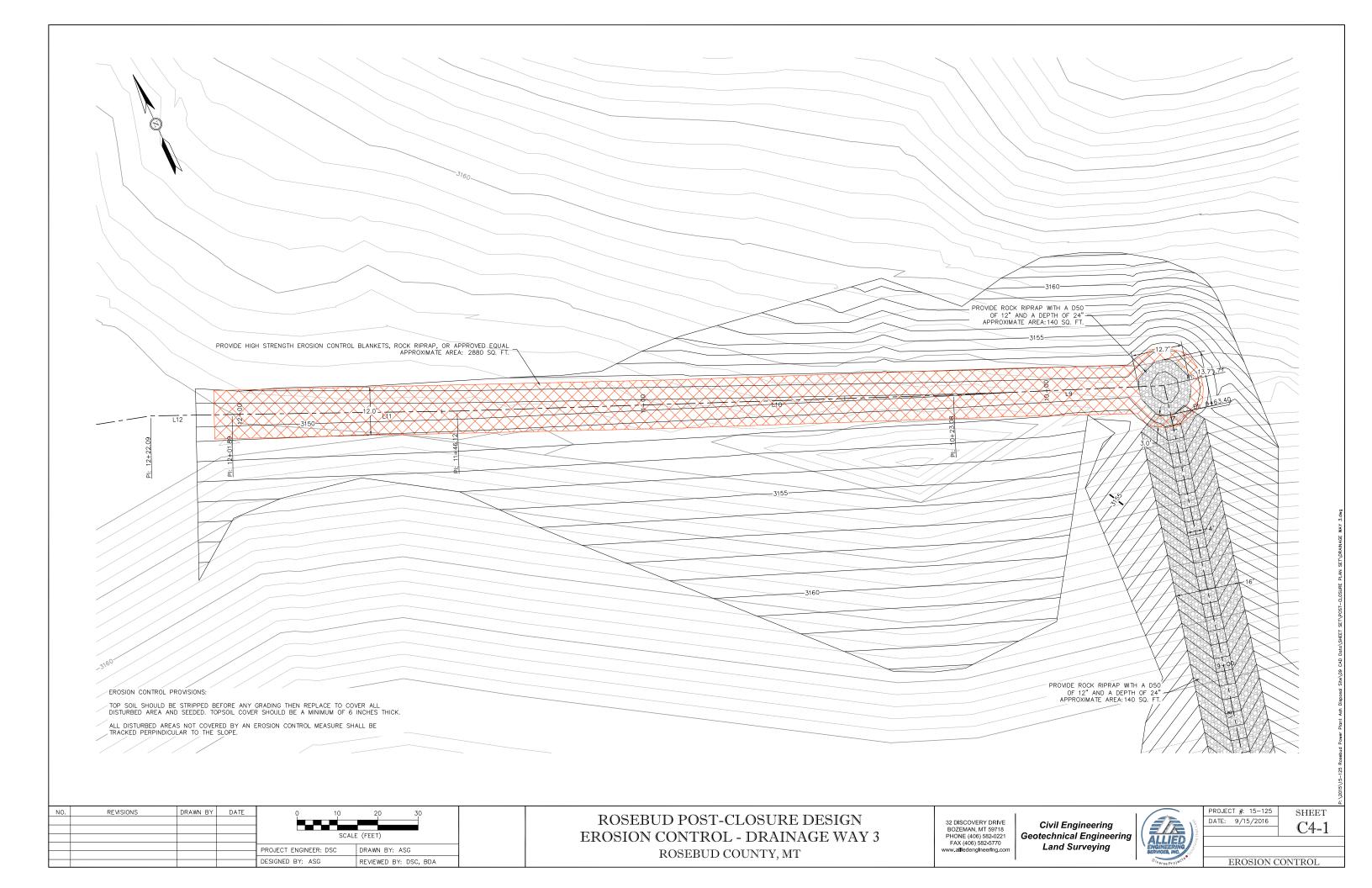
PROJECT ENGINEER: DSC

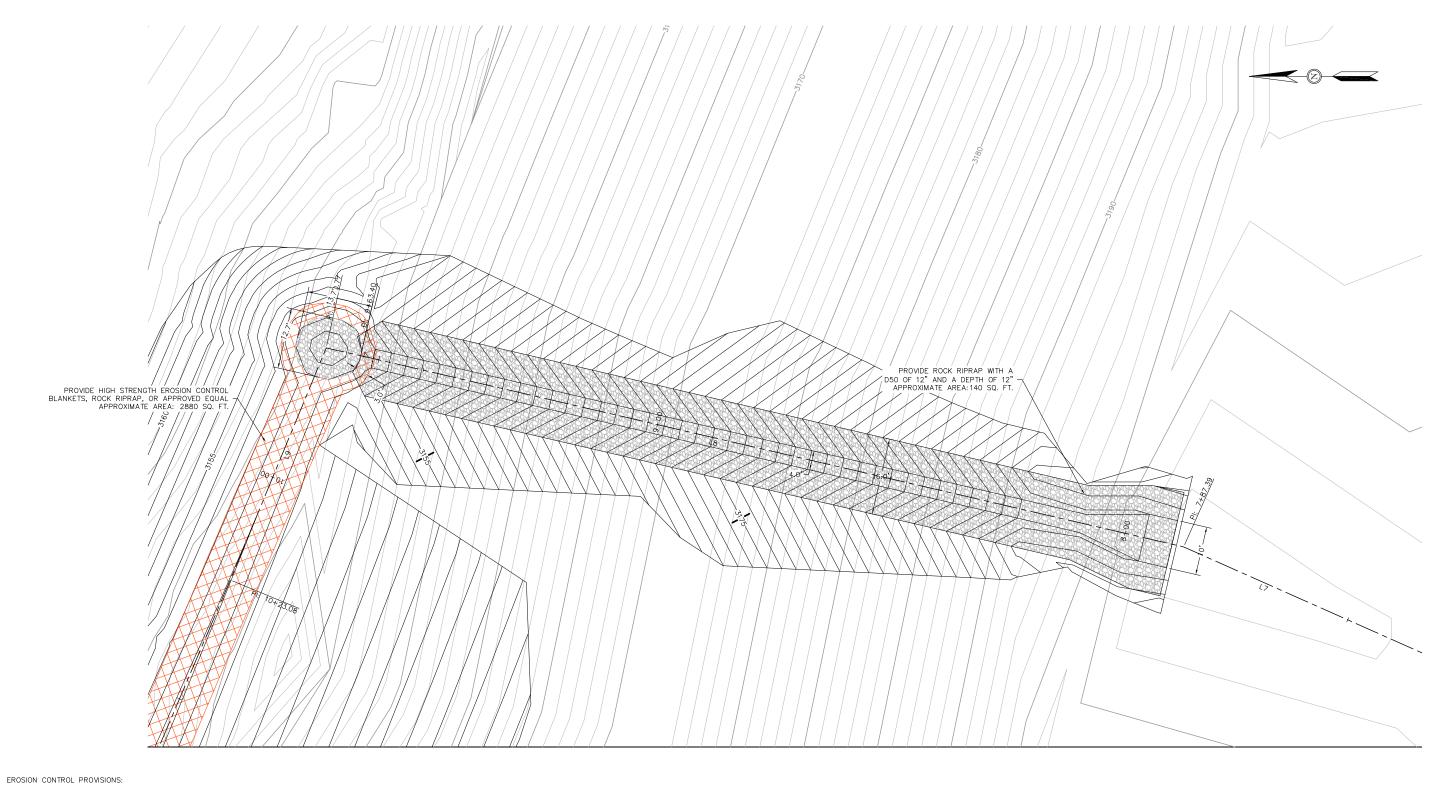
DESIGNED BY: ASG

REVISIONS

DRAWN BY

DATE





TOP SOIL SHOULD BE STRIPPED BEFORE ANY GRADING THEN REPLACE TO COVER ALL DISTURBED AREA AND SEEDED. TOPSOIL COVER SHOULD BE A MINIMUM OF 6 INCHES THICK.

ALL DISTURBED AREAS NOT COVERED BY AN EROSION CONTROL MEASURE SHALL BE TRACKED PERPENDICULAR TO THE SLOPE.

ALL DISTURBED AREAS ARE TO BE SEEDED.

NO.	REVISIONS	DRAWN BY	DATE	0 10	20 30
				SCAL	E (FEET)
				PROJECT ENGINEER: DSC	DRAWN BY: ASG
-				DESIGNED BY: ASG	REVIEWED BY: DSC, BDA
				BEGIGINES BIT 7,00	TRETIED BT. 000, BBA

ROSEBUD POST-CLOSURE DESIGN **EROSION CONTROL - DRAINAGE WAY 3** ROSEBUD COUNTY, MT

32 DISCOVERY DRIVE BOZEMAN, MT 59718 PHONE (406) 582-0221 FAX (406) 582-5770 www.allledengineering.com

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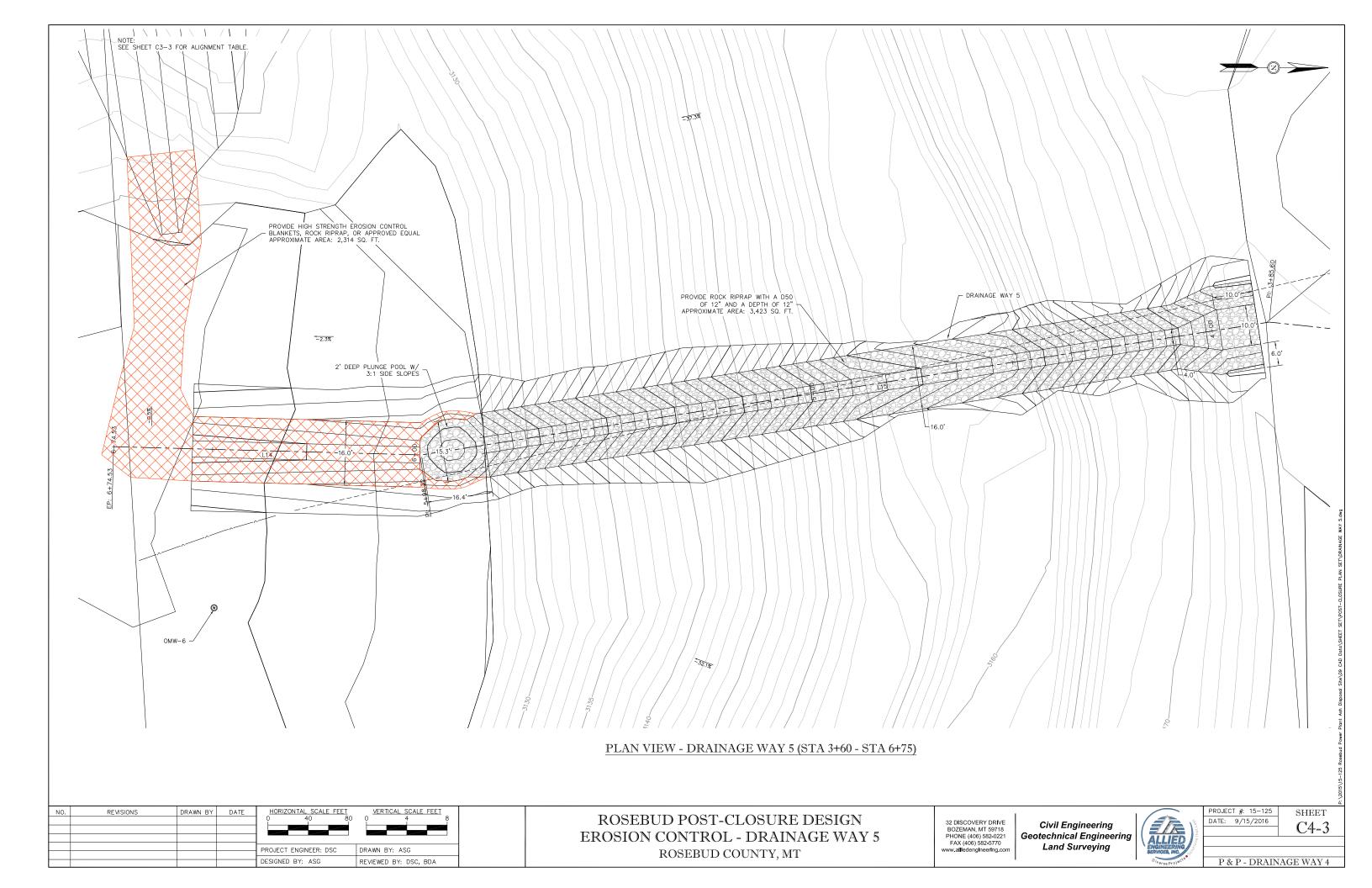
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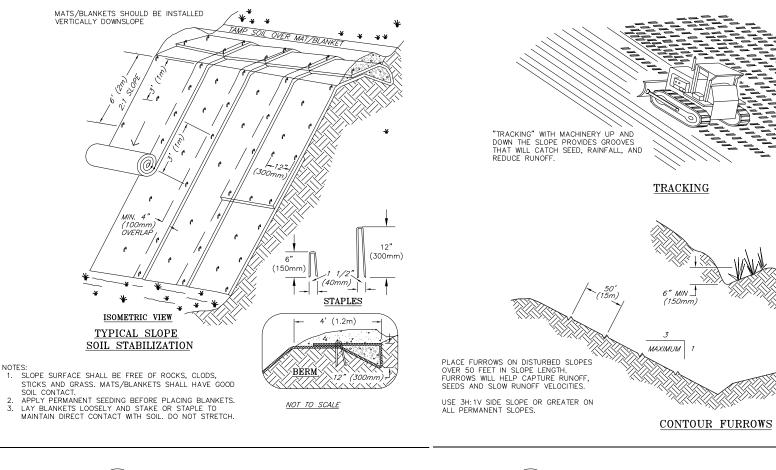
OJECT #: 15-125 ATE: 9/15/2016

EROSION CONTROL

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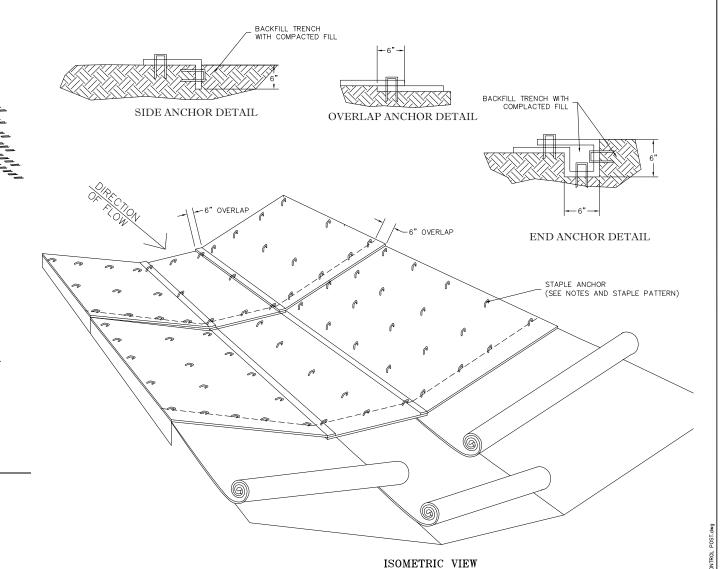
C4-2











DETAIL

### CONSTRUCTION NOTES:

EROSION BLANKETS IN A CHANNEL

- PREPARE SOIL SO THAT AREA IS SMOOTH, THEN ADD SEED. AND FERTILIZER AS NEEDED.
   START BY STAPLING THE BLANKET AT THE TOP OF THE CHANNEL IN A 6" DEEP X 6" WIDE TRENCH. BACKFILL AND COMPACT TRENCH SO THAT THE WATER WILL FLOW EVENLY ONTO THE BLANKET.
   ROLL CENTER BLANKET IN THE BOTTOM OF THE CHANNEL AND PLACE 4 STAPLES EVENLY SPACED PER SQUARE YARD.
   PLACE ADJOINING ENDS (SHINGLE STYLE) OVERLAPPING 6" SECURING THE OVERLAP WITH A DOUBLE ROW OF STAPLES STAGGERED 4" APART.

- PLACE ADJOINING ENDS (SHINGLE STYLE) OVERLAPPING 6" SECURING THE OVERLAP WITH A DOUBLE ROW OF STAPLES STAGGERED 4" APART. OVERLAP EDGES OF BLANKET A MINIMUM OF 6" WITH PARALLEL BLANKETS.

  THE FULL LENGTH OF THE BLANKET AT THE TOP OF THE CHANNEL MUST BE ANCHORED IN A 6"X6" TRENCH THEN BACKFILLED AND COMPACTED AFTER PLACING STAPLES IN THE TRENCH 3 FEET APART. INSURE COMPACTION SO THAT WATER CAN FLOW EVENLY ONTO THE BLANKETS FROM THE SIDES OF THE CHANNEL.

  PLACE A DOUBLE ROW OF STAGGERED STAPLES 4" APART EVERY 33 FEET.

  INSURE BLANKET IS PLACED ON SIDE BANKS OF CHANNEL 1 FOOT ABOVE FLOW LINE.

  AT THE TERMINAL END OF THE CHANNEL, THE BLANKET MUST BE ANCHORED SUCH THAT THE WATER WILL FLOW TO THE DESIRED AREA. IF THE END OF THE CHANNEL IS A CULVERT, THE BLANKET BUST BE PLACED UNDER THE CULVERT AND SECURED WITH STAPLES 4" APART IN A STACKEDED BATTER IS THE EMBIL OF THE THE BLANKET BUST BE PLACED. UNDER THE CULVERT AND SECURED WITH STAPLES 4" APART IN A STACKEDED BATTER IS THE BLANKET BUST AP ENGLED THE STAGGERED PATTER, IF THE TERMINAL END IS A ROCK OUTFALL, THE BLANKET BUST BE PLACED IN A 6" WIDE X6" DEEP TRENCH STAPLED THE BACKFILLED, COMPACTED THE ROCKS PLACED ON THE TRENCH TO CREATE A SMOOTH TRANSITION.

NO.	REVISIONS	DRAWN BY	DATE		
				PROJECT ENGINEER: DSC	DRAWN BY: ASG
				DESIGNED BY: ASG	REVIEWED BY: DSC, BDA

ROSEBUD POST-CLOSURE DESIGN EROSION CONTROL DETAILS ROSEBUD COUNTY, MT

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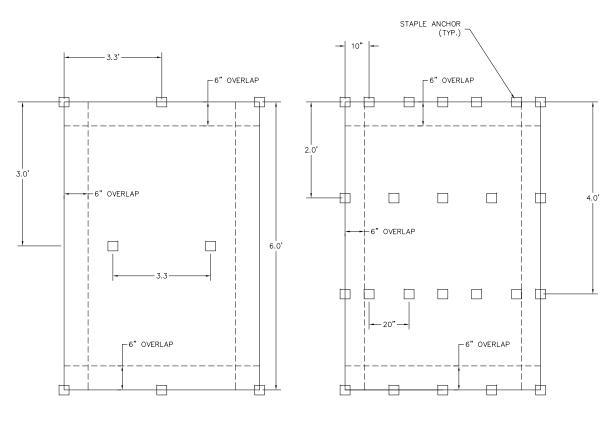
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PROJECT #: 15-125	SHEET
DATE: 9/15/2016	014 4
	C4-4

EROSION CONTROL

#### EROSION BLANKET ANCHORING PATTERNS



3:1 SIDE SLOPES

CHANNEL BOTTOM/HIGH FLOW AREAS

#### ANCHORING NOTES:

CHOICE OF STAPLES WILL DEPEND ON SOIL TYPE AND COMPACTION. STAPLES PLACED IN SOIL SHOULD NOT COME OUT EASILY BY HAND. STANDARD 6" STAPLES WILL BE USED IN MOST CONDITIONS. LONGER STAPLES 8"-12" MAY BE NEEDED IN SANDY SOILS. FOR VERY LOOSE SOILS A LONG PIN WITH WASHER MAY BE USED TO ANCHOR BLANKET.

BLANKET SHALL BE OVERLAPPED A MINIMUM OF 6" WITH THE UPSTREAM BLANKET COMING OVER THE DOWNSTREAM BLANKET (SHINGLE STYLE).



NO.	REVISIONS	DRAWN BY	DATE			
				PROJECT ENGINEER: DSC	DRAWN BY: ASG	
				DESIGNED BY: ASG	REVIEWED BY: DSC, BDA	Ì

ROSEBUD POST-CLOSURE DESIGN EROSION CONTROL DETAILS ROSEBUD COUNTY, MT

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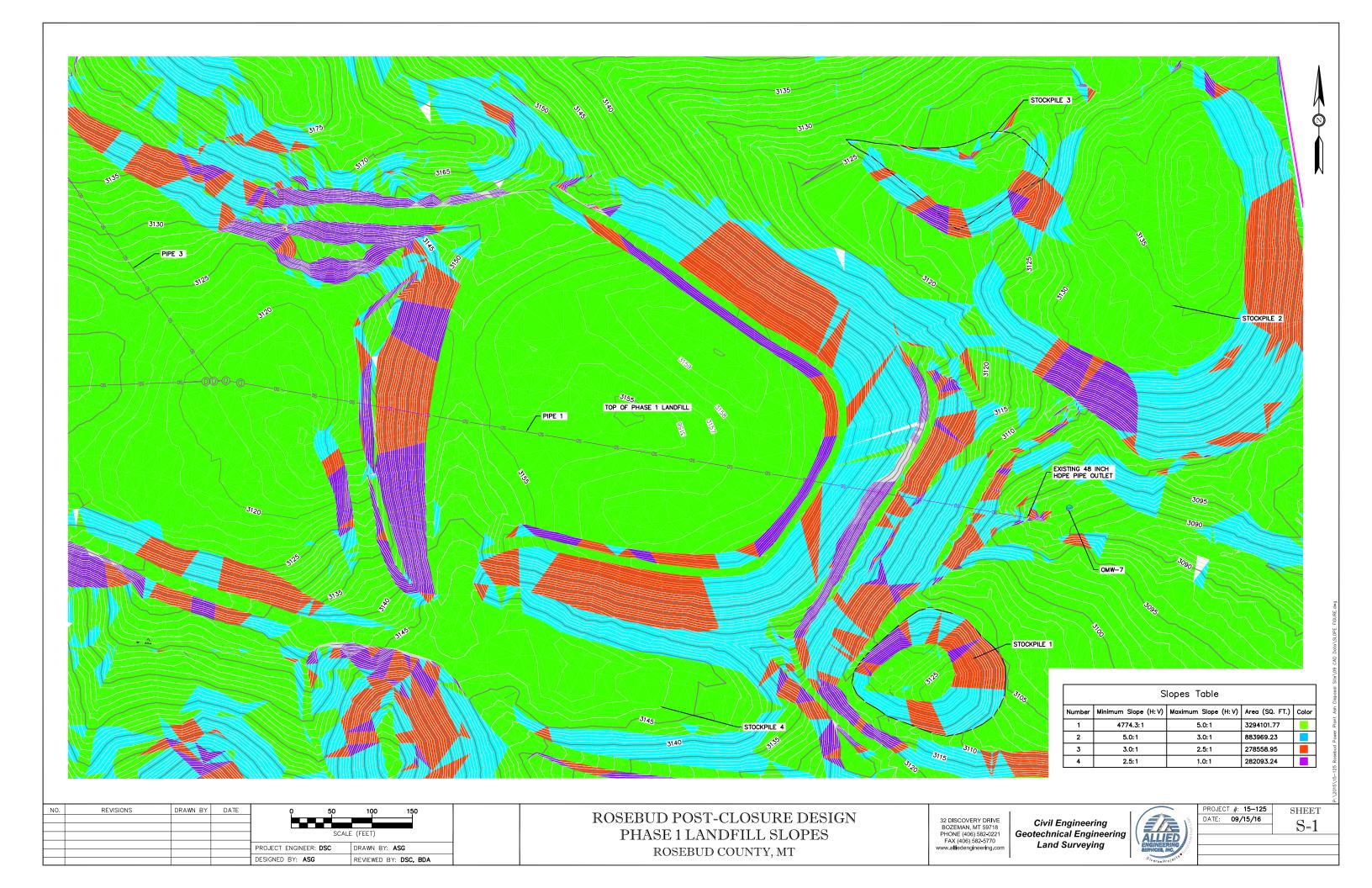
Civil Engineering Geotechnical Engineering Land Surveying

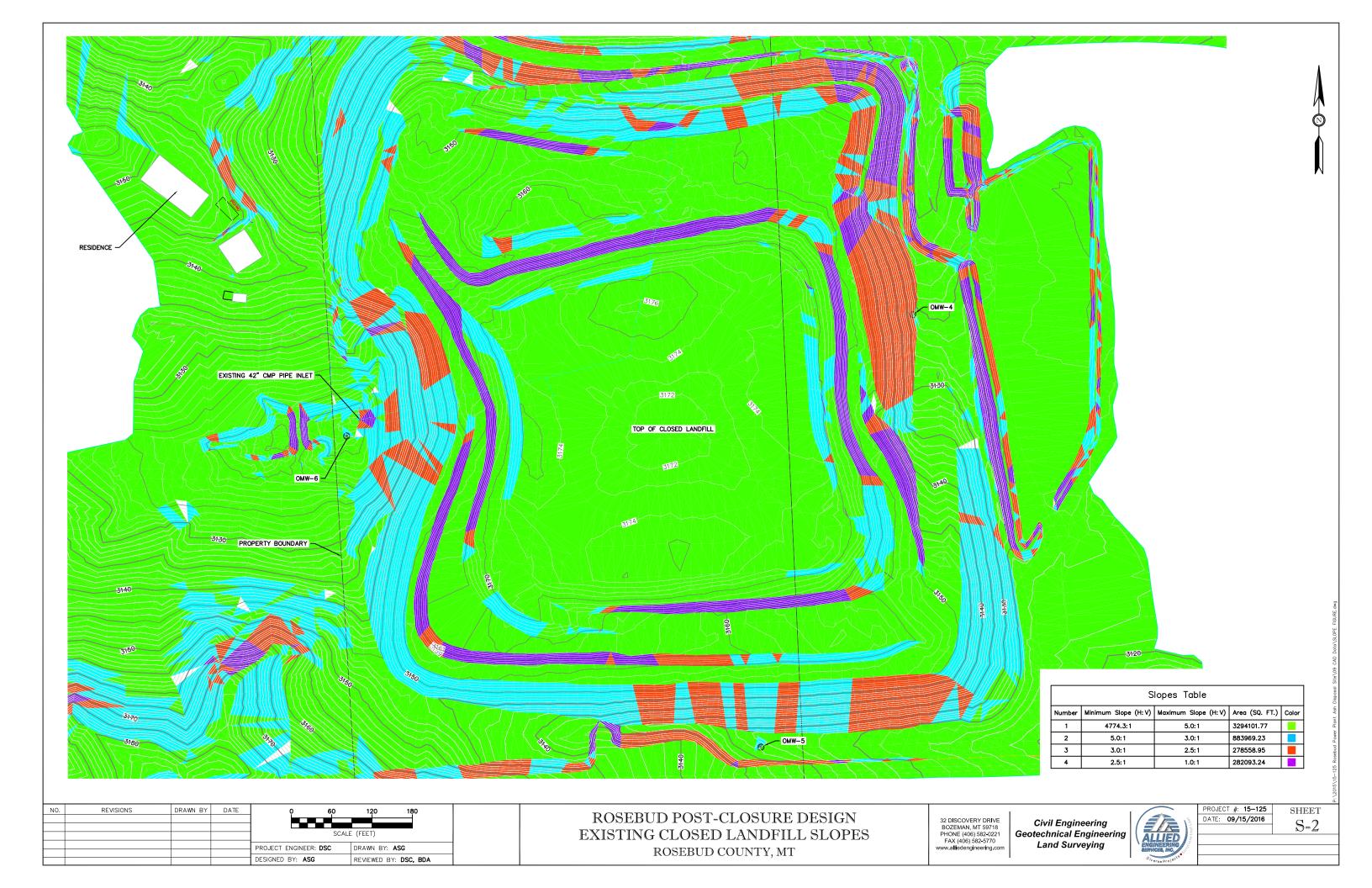
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EROSION CONTROL





## **APPENDIX B**

SSA 25, 50, and 100Year Storm Event Output Active Landfill Drainage Basins Post-Closure Drainage Basins Rainfall Hyetograph and Hydrograph

#### **Active Landfill**

Autodesk Storm and Sanitary Analysis - 25 Year Event Output

					Pipes							
Element	Pipe	Length	Inlet	Outlet	Total	Average	Pipe	Manning's	Peak	Max	Design	М
ID	Material		Invert	Invert	Drop	Slope	Diameter	Roughness	Flow	Flow	Flow	Flo
			Elevation	Elevation			or Height			Velocity	Capacity	De
		(ft)	(ft)	(ft)	(ft)	(%)	(inches)		(cfs)	(ft/sec)	(cfs)	(1
42" Fittings	Duromaxx	35	3112.90	3112.23	0.67	1.91	42	0.012	46.76	9.6	150.8	1
42" to 36" Section	Duromaxx	10	3113.09	3112.90	0.19	1.90	42	0.012	40.61	5.7	150.2	2
Pipe 1	HDPE	990	3111.78	3093.13	18.65	1.88	48	0.013	46.78	14.0	197.2	1
Pipe 2	Duromaxx	628	3129.52	3113.59	15.93	2.54	36	0.012	40.57	10.4	115.1	1
Pipe 3	Duromaxx	465	3136.12	3113.90	22.22	4.78	30	0.012	6.66	9.8	97.1	0
Pipe 4	CMP	1055	3110.13	3078.58	31.55	2.99	42	0.015	22.22	11.0	150.8	0
					Chanı	nels						
Element	Length	Inlet	Outlet	Total	Average	Channel	Channel	Channel	Channel	Peak	Max	De
ID		Invert	Invert	Drop	Slope	Type	Height	Width	Manning's	Flow	Flow	FI
		Elevation	Elevation						Roughness		Velocity	Сар
	(ft)	(ft)	(ft)	(ft)	(%)		(ft)	(ft)	_	(cfs)	(ft/sec)	(c
Outlet Swale from Pipe 1	440.00	3090.50	3082.00	8.50	1.93	Trapezoidal	3	26	0.05	46.7	4.0	36
				Reservoirs						]		
Element	Invert	Max	Max	Peak	Peak	Maximum	Maximum	Average	Average	I		
ID	Elevation	(Rim)	(Rim)	Inflow	Outflow	HGL	HGL	HGL	HGL			
	Licvation	Elevation	Offset	iiiiow	Cutilow	Elevation	Depth	Elevation	Depth			
	(ft)	(ft)	(ft)	(cfs)	(cfs)	(ft)	(ft)	(ft)	(ft)			
Pipe Dam 2	3129.50	3135.00	5.50	40.6	40.6	3130.75	1.25	3129.64	0.14			
Pipe Dam 3	3136.00	3141.00	5.00	6.70	6.70	3136.56	0.56	3136.14	0.14			
Flowers	Dete	Deinfall		nformation	Country	Datum	Dainfall	Dainfall	]			
Element ID	Data	Rainfall	Rain Units	State	County	Return	Rainfall	Rainfall				
טו	Source	Type	Units			Period	Depth	Distribution				
	ID					(years)	(inches)					
Rain Gage-01	25 Year	Cumulative	inches	Montana	Rosebud	25	2.9	SCS Type II 24-hr				
						_		7,	1			
Active Drainage Basin	Area	Drainage	Orainage Bas Weighted	in Information Rain Gage	Total	Total	Peak	Time	]			
ID	700	Node ID	Curve	ID	Precipitation	Runoff	Runoff	of				
			Number					Concentration				
	(acres)		· · · · · · · · · · · · · · · · · · ·		(inches)	(inches)	(cfs)	(min)				
1	103.0	PipeDam2	72	Rain Gage-01	2.90	0.75	40.9	52				
2	14.6	PipeDam3	72	Rain Gage-01	2.90	0.75	6.7	42				
3	4.3	Out-04	72	Rain Gage-01	2.90	0.75	2.6	27				
4	13.6	Out-04 Out-02	72	Rain Gage-01	2.90	0.75	3.9	80				
5	16.3	Out-02 Out-05	72 72	Rain Gage-01	2.90	0.75	6.1	55				
6	4.0	Out-03	72 72	Rain Gage-01	2.90	0.75	3.7	12				
7	4.0 67.4	Jun-07	72 72	Rain Gage-01	2.90	0.75	22.4	66				
8	3.2	Jun-07 Out-07	72 72	_	2.90	0.75		38				
8 9	3.2 10.5	Out-07	72 72	Rain Gage-01	2.90	0.75	1.6 5.4	36				
9 10			72 72	Rain Gage-01	2.90			36 25				
	5.6	Out-06		Rain Gage-01		0.75	3.7					
11	5.8	Out-01	72	Rain Gage-01	2.90	0.75	4.7	16				

Max Flow Depth (ft) 1.05

#### **Active Landfill**

Autodesk Storm and Sanitary Analysis - 100 Year Event Output

					Pipes							
Element	Pipe	Length	Inlet	Outlet	Total	Average	Pipe	Manning's	Peak	Max	Design	М
ID	Material		Invert	Invert	Drop	Slope	Diameter	Roughness	Flow	Flow	Flow	Fl
			Elevation	Elevation			or Height			Velocity	Capacity	De
		(ft)	(ft)	(ft)	(ft)	(%)	(inches)		(cfs)	(ft/sec)	(cfs)	(1
42" Fittings	Duromaxx	35	3112.90	3112.23	0.67	1.91	42	0.012	91.5	11.3	150.8	2
42" to 36" Section	Duromaxx	10	3113.09	3112.90	0.19	1.90	42	0.012	79.1	8.2	150.2	3
Pipe 1	HDPE	990	3111.78	3093.13	18.65	1.88	48	0.013	91.5	16.4	197.2	1
Pipe 2	Duromaxx	628	3129.52	3113.59	15.93	2.54	36	0.012	79.1	12.7	115.1	2
Pipe 3	Duromaxx	465	3136.12	3113.90	22.22	4.78	30	0.012	13.0	9.8	97.1	1
Pipe 4	CMP	1055	3110.13	3078.58	31.55	2.99	42	0.015	43.4	13.2	150.8	1
					Chann	iels						
Element	Length	Inlet	Outlet	Total	Average	Channel	Channel	Channel	Channel	Peak	Max	De
ID	Ū	Invert	Invert	Drop	Slope	Type	Height	Width	Manning's	Flow	Flow	FI
		Elevation	Elevation	•	•	•	Ü		Roughness		Velocity	Сар
	(ft)	(ft)	(ft)	(ft)	(%)		(ft)	(ft)		(cfs)	(ft/sec)	(0
Outlet Swale from Pipe 1	440.00	3090.50	3082.00	8.5	1.93	Trapezoidal	3	26	0.05	91.00	4.90	36
				Reservoirs								
Element	Invert	Max	Max	Peak	Peak	Maximum	Maximum	Average	Average			
ID	Elevation	(Rim)	(Rim)	Inflow	Outflow	HGL	HGL	HGL	HGL			
טו	Elevation	Elevation	Offset	illiow	Outilow	Elevation		Elevation				
	(f+\			(ofo)	(ofo)		Depth (ft)		Depth			
Dina Dam 3	(ft)	(ft)	(ft)	(cfs)	(cfs)	(ft)	(ft)	(ft)	(ft)			
Pipe Dam 2	3129.50	3135.00	5.50	79.2	79.1	3131.47	1.97	3129.71	0.21			
Pipe Dam 3	3136.00	3141.00	5.00	13.0	13.0	3136.74	0.74	3136.16	0.16			
				nformation					]			
Element	Data	Rainfall	Rain	State	County	Return	Rainfall	Rainfall				
ID	Source	Type	Units			Period	Depth	Distribution				
	ID											
						(years)	(inches)					
Rain Gage-01	100 Year	Cumulative	inches	Montana	Rosebud	100	3.82	SCS Type II 24-hr				
				in Information					]			
Active Drainage Basin	Area	Drainage	Weighted	Rain Gage	Total	Total	Peak	Time				
ID		Node ID	Curve	ID	Precipitation	Runoff	Runoff	of				
			Number					Concentration				
	(acres)				(inches)	(inches)	(cfs)	(min)				
1	103.0	PipeDam2	72	Rain Gage-01	3.82	1.34	79.4	52				
2	14.6	PipeDam3	72	Rain Gage-01	3.82	1.34	13.0	42				
3	4.3	Out-04	72	Rain Gage-01	3.82	1.34	5.1	27				
4	13.6	Out-02	72	Rain Gage-01	3.82	1.34	7.5	80				
4	16.3	Out-05	72	Rain Gage-01	3.82	1.34	11.9	55				
5		Out-09	72	Rain Gage-01	3.82	1.34	7.0	12				
	4.0	Out-09	, _									
5	4.0 67.4	Jun-07	72	Rain Gage-01	3.82	1.34	43.5	66				
5 6 7	67.4	Jun-07	72	Rain Gage-01								
5 6 7 8	67.4 3.2	Jun-07 Out-07	72 72	Rain Gage-01 Rain Gage-01	3.82	1.34	3.0	38				
5 6 7	67.4	Jun-07	72	Rain Gage-01								

Max Flow Depth (ft)

1.50

#### **Active Landfill**

Autodesk Storm and Sanitary Analysis - 500 Year Event Output

					Pipes								ı
Element ID	Pipe Material	Length	Inlet Invert Elevation	Outlet Invert Elevation	Total Drop	Average Slope	Pipe Diameter or Height	Manning's Roughness	Peak Flow	Max Flow Velocity	Design Flow Capacity	Max Flow Depth	
		(ft)	(ft)	(ft)	(ft)	(%)	(inches)		(cfs)	(ft/sec)	(cfs)	(ft)	
42" Fittings	Duromaxx	35	3112.90	3112.23	0.67	1.91	42	0.0120	118.4	13.81	150.80	2.92	
42" to 36" Section	Duromaxx	10	3113.09	3112.90	0.19	1.90	42	0.0120	100.7	10.47	150.24	3.50	
Pipe 1	HDPE	990	3111.78	3093.13	18.65	1.88	48	0.0130	118.4	17.35	197.20	2.14	
Pipe 2	Duromaxx	628	3129.52	3113.59	15.93	2.54	36	0.0120	100.7	14.24	115.08	3.00	
Pipe 3	Duromaxx	465	3136.12	3113.90	22.22	4.78	30	0.0120	19.4	9.59	97.13	1.63	
Pipe 4	CMP	1055	3110.13	3078.58	31.55	2.99	42	0.0150	65.1	14.61	150.79	1.65	
					Chan	nels							
Element	Length	Inlet	Outlet	Total	Average	Channel	Channel	Channel	Channel	Peak	Max	Design	
ID		Invert Elevation	Invert Elevation	Drop	Slope	Туре	Height	Width	Manning's Roughness	Flow	Flow Velocity	Flow Capacity	
	(ft)	(ft)	(ft)	(ft)	(%)		(ft)	(ft)		(cfs)	(ft/sec)	(cfs)	
Outlet Swale from Pipe 1	440	3090.50	3082.00	8.50	1.93	Trapezoidal	3	26	0.05	118.30	5.25	368.60	
				Reservoirs									
Element	Invert	Max	Max	Peak	Peak	Maximum	Maximum	Average	Average				
ID	Elevation	(Rim)	(Rim)	Inflow	Outflow	HGL	HGL	HGL	HGL				
		Elevation	Offset			Elevation	Depth	Elevation	Depth				
	(ft)	(ft)	(ft)	(cfs)	(cfs)	(ft)	(ft)	(ft)	(ft)				
Pipe Dam 2	3129.50	3135.00	5.50	119.1	100.5	3135.00	5.50	3129.85	0.35				
Pipe Dam 3	3136.00	3141.00	5.00	19.5	19.5	3136.88	0.88	3136.18	0.18				
				nformation									
Element	Data	Rainfall	Rain	State	County	Return	Rainfall	Rainfall					
ID	Source ID	Туре	Units			Period	Depth	Distribution					
						(years)	(inches)						
Rain Gage-01	Extrapolated	Cumulative	inches	Montana	Rosebud	500	4.66	SCS Type II 24-hr					
				sin Information									
Active Drainage Basin	Area	Drainage	Weighted	Rain Gage	Total	Total	Peak	Time					
ID		Node ID	Curve Number	ID	Precipitation	Runoff	Runoff	of Concentration					
	(acres)		Number		(inches)	(inches)	(cfs)	(min)					
1	103.0	PipeDam2	72	Rain Gage-01	4.66	1.94	119.1	52					
2	14.6	PipeDam3	72 72	Rain Gage-01	4.66	1.94	19.5	42					
3	4.3	Out-04	72 72	Rain Gage-01	4.66	1.94	7.6	27					
3 4	4.5 13.6	Out-04 Out-02	72 72	Rain Gage-01	4.66	1.94	11.3	80					
5	16.3	Out-02	72 72	Rain Gage-01	4.66	1.94	17.9	55					
6	4.0	Out-03	72 72	Rain Gage-01	4.66	1.94	10.3	12					
U	67.4	Jun-07	72 72	Rain Gage-01	4.66	1.94	65.1	66					
7	07.4	Juil-U/	12	Main Gage-UI	4.00	1.54	03.1						
7 8	ວ າ	Ou+ 07	72	Rain Gago 01	166	1 04	16	30					
8	3.2 10.5	Out-07	72 72	Rain Gage-01	4.66 4.66	1.94	4.6 15.5	38 36					
	3.2 10.5 5.6	Out-07 Out-08 Out-06	72 72 72	Rain Gage-01 Rain Gage-01 Rain Gage-01	4.66 4.66 4.66	1.94 1.94 1.94	4.6 15.5 10.4	38 36 25					

9

3.0

Jun-21 72.00

#### **Post-Closure**

Autodesk Storm and Sanitary Analysis - 25 Year Event Output

				Pipes								7
Pipe Material	Length	Inlet Invert Elevation	Outlet Invert Elevation	Total Drop	Average Slope	Pipe Diameter or Height	Manning's Roughness	Peak Flow	Max Flow Velocity	Design Flow Capacity	Max Flow Depth	4
Duromaxx	(ft) 72	<b>(ft)</b> 3120.97	(ft) 3119.72	(ft) 1.25	<b>(%)</b> 1.74	(inches) 36	0.019	(cfs) 29.3	(ft/sec) 8.0	(cfs) 60.1	(ft) 1.6	
				Chai	nnels							
Length	Inlet Invert Elevation	Outlet Invert Elevation	Total Drop	Average Slope	Channel Type	Channel Height	Channel Width	Channel Manning's Roughness	Peak Flow	Max Flow Velocity	Design Flow Capacity	Flo De
(ft)	(ft)	(ft)	(ft)	(%)		(ft)	(ft)		(cfs)	(ft/sec)	(cfs)	(1
875	3145.00	3140.62	4.38	0.50	Trapezoidal	2	24	0.032	41.90	3.20	152.26	0.
1295	3140.62	3088.97	51.65	3.99	Trapezoidal	2	21	0.032	41.53	5.65	252.22	0.
459	3149.00	3145.00	4.00	0.87	Trapezoidal	2	24	0.032	8.84	0.83	200.89	0.
143	3191.40	3150.22	41.18	28.80	Trapezoidal	2	16	0.032	2.12	1.32	563.21	0.
250	3150.22	3149.00	1.22	0.49	Triangular	2	6	0.032	2.89	3.67	17.22	0.
581	3124.00	3120.97	3.03	0.52	Trapezoidal	3	22	0.032	30.30	1.95	186.12	1.
438	3119.72	3079.44	40.28	9.20	Trapezoidal	2	16	0.032	29.97	8.29	318.27	0.
186	3173.20	3124.00	49.20	26.45	Trapezoidal	2	16	0.032	1.68	0.55	539.78	0.
216	3090.00	3088.00	2.00	0.93	Trapezoidal	2	22	0.035	8.22	2.07	164.61	0.
710	3085.00	3082.00	3.00	0.42	Trapezoidal	2	32	0.032	44.72	3.03	302.64	0.
			Reservoi	rs								
Invert	Max	Max	Peak	Peak	Maximum	Maximum	Average	Average				
Elevation	(Rim)	(Rim)	Inflow	Outflow	HGL	HGL	HGL	HGL				
	Elevation	Offset			Elevation	Depth	Elevation	Depth				
(ft)	(ft)	(ft)	(cfs)	(cfs)	(ft)	(ft)	(ft)	(ft)				
3145.00	3150.00	5	45.0	38.4	3146.20	1.2	3145.18	0.18				
3149.00	3152.00	3	8.3	8.3	3149.33	0.3	3149.04	0.04				
			all Information					]				
Data Source ID	Rainfall Type	Rain Units	State	County	Return Period	Rainfall Depth	Rainfall Distribution					
25 Year	Cumulative	inches	Montana	Rosebud	<b>(years)</b> 25	(inches) 2.9	SCS Type II 24-hr					
		Drainage	Rasin Informat	tion				1				
Δrea	Drainage				Total	Peak	Time					
Aica	Node ID	Curve	ID	Precipitation	Runoff	Runoff	of					
(acros)		. varibei		(inches)	(inches)	(cfe)						
	PineDam?	72 00	Rain Gage_01									
			-									
			-									
			-									
			-									
			_									
			_									
16 2	lun-10	72 00	Rain Gago_01	2 00	0.75	Q 1	30					
16.3 4.3	Jun-19 DW-3	72.00 72.00	Rain Gage-01 Rain Gage-01	2.90 2.90	0.75 0.75	8.1 2.1	38 38					
	Material  Duromaxx  Length  (ft) 875 1295 459 143 250 581 438 186 216 710  Invert Elevation (ft) 3145.00 3149.00  Data Source ID	Pipe   Material   (ft)   (ft	Pipe Material         Length (ft) (nyert Elevation (ft) (ft) (ft)           Duromaxx         72         3120.97           Length (ft) (ft) (ft) (ft) (ft) (ft) (ft) (ft)	Pipe Material         Length (ft) (ft) (ft) (ft) (ft) (ft)         Outlet Invert Elevation (ft) (ft) (ft)           Duromaxx         72         3120.97         3119.72           Length Inlet Invert Elevation (ft) (ft) (ft) (ft) (ft) (ft) (ft) (ft)	Pipe Material         Length Material         Inlet Invert	Pipe Material         Length Material         Inlet Invert Invert Invert Invert Invert Invert Proposed Slope         Coulet Proposed Slope           Buromaxx         72         3120.97         3119.72         1.25         1.74           Length Inlet Invert Elevation (ft) (ft) (ft) (ft) (ft) (ft) (ft) (ft)	Pipe Material         Length Material of the	Pipe   Material	Pipe	Pipe   Nation   Pipe   Pipe	Pipe   Maning's   Peak   Max   Max   Peak   Max   Max   Max   Peak   Max   Max   Max   Peak   Max   Max	Pipe

2.90

Rain Gage-01 Rain Gage-01

0.75

1.7

31

8

9

4.3

3.0

DW-3

Jun-21

72

72

Rain Gage-01

Rain Gage-01

3.82

3.82

1.34

1.34

4.2

3.3

38

31

#### Post-Closure

Autodesk Storm and Sanitary Analysis - 100 Year Event Output

		_		-	Pipes								
Element	Pipe	Length	Inlet	Outlet	Total	Average	Pipe	Manning's	Peak	Max	Design	Max	•
ID	Material		Invert	Invert	Drop	Slope	Diameter	Roughness	Flow	Flow	Flow	Flow	
			Elevation	Elevation			or Height			Velocity	Capacity	Depth	
		(ft)	(ft)	(ft)	(ft)	(%)	(inches)		(cfs)	(ft/sec)	(cfs)	(ft)	
Culvert Under Haul Road	Duromaxx	72	3120.97	3119.72	1.25	1.74	36	0.019	50.9	10.7	60.1	1.9	
					Chan								
Element	Length	Inlet	Outlet	Total	Average	Channel	Channel	Channel	Channel	Peak	Max	Design	M
ID		Invert	Invert	Drop	Slope	Type	Height	Width	Manning's	Flow	Flow	Flow	Flo
		Elevation	Elevation						Roughness		Velocity	Capacity	De
	(ft)	(ft)	(ft)	(ft)	(%)		(ft)	(ft)		(cfs)	(ft/sec)	(cfs)	(f
Drainage Way 1 Upper	875	3145	3140.62	4.38	0.5	Trapezoidal	2	24	0.032	86.26	4.20	152.26	1.
Drainage Way 1 Lower	1295	3140.62	3088.97	51.65	3.99	Trapezoidal	1.5	21	0.032	85.68	7.21	252.22	0.
Drainage Way 2	459	3149	3145	4	0.87	Trapezoidal	2	24	0.032	18.07	1.21	200.89	1.
Drainage Way 3 Upper	143	3191.4	3150.22	41.18	28.8	Trapezoidal	2	16	0.032	4.10	1.87	563.21	0.
Drainage Way 3 Lower	250	3150.22	3149	1.22	0.49	Triangular	2	6	0.032	4.13	3.94	17.22	0.
Drainage Way 4 Upper	581	3124	3120.97	3.03	0.52	Trapezoidal	3	22	0.032	57.77	2.18	186.12	2.
Drainage Way 4 Lower	438	3119.72	3079.44	40.28	9.2	Trapezoidal	2	16	0.032	52.04	9.70	318.27	0.
Drainage Way 5	186	3173.2	3124	49.2	26.45	Trapezoidal	2	16	0.032	3.22	0.64	539.78	1.
Existing Outlet Swale	216	3090	3088	2	0.93	Trapezoidal	2	22	0.035	15.91	2.47	164.61	0.
Existing Outlet Swale	710	3085	3082	3	0.42	Trapezoidal	2	32	0.032	92.38	3.90	302.64	1.
				Reservoir	S					-			
Element	Invert	Max	Max	Peak	Peak	Maximum	Maximum	Average	Average	•'			
ID	Elevation	(Rim)	(Rim)	Inflow	Outflow	HGL	HGL	HGL	HGL				
		Elevation	Offset			Elevation	Depth	Elevation	Depth				
	(ft)	(ft)	(ft)	(cfs)	(cfs)	(ft)	(ft)	(ft)	(ft)				
Inlet Fill Area 1	3145.00	3150.00	5.0	105.3	86.26	3146.77	1.77	3145.25	0.25				
Inlet Fill Area 2	3149.00	3152.00	3.0	20.2	18.07	3149.52	0.52	3149.06	0.06				
			Rainfa	III Information									
Element	Data	Rainfall	Rain	State	County	Return	Rainfall	Rainfall					
ID	Source ID	Туре	Units			Period	Depth	Distribution					
						(years)	(inches)						
Rain Gage-01	100 Year	Cumulative	inches	Montana	Rosebud	100	3.82	SCS Type II 24-hr					
			Drainage	Basin Informat	ion				]				
Drainage Basin	Area	Drainage	Weighted	Rain Gage	Total	Total	Peak	Time					
ID		Node ID	Curve	ID	Precipitation	Runoff	Runoff	of					
			Number					Concentration					
	(acres)				(inches)	(inches)	(cfs)	(min)					
1	118.0	PipeDam2	72	Rain Gage-01	3.82	1.34	87.6	55					
2	18.6	PipeDam3	72	Rain Gage-01	3.82	1.34	16.2	44					
3	70.2	ExtInletFill	72	Rain Gage-01	3.82	1.34	57.0	48					
4	2.9	Jun-16	72	Rain Gage-01	3.82	1.34	3.6	25					
5	8.6	Out-04	72	Rain Gage-01	3.82	1.34	10.0	29					
6	8.5	Out-03	72	Rain Gage-01	3.82	1.34	8.0	39					
7	16.3	Jun-19	72	Rain Gage-01	3.82	1.34	15.8	38					
			_					- <del>-</del>					

#### Post-Closure

Autodesk Storm and Sanitary Analysis - 500 Year Event Output

					Pipes								
Element ID	Pipe Material	Length	Inlet Invert Elevation	Outlet Invert Elevation	Total Drop	Average Slope	Pipe Diameter or Height	Manning's Roughness	Peak Flow	Max Flow Velocity	Design Flow Capacity	Max Flow Depth	
		(ft)	(ft)	(ft)	(ft)	(%)	(inches)		(cfs)	(ft/sec)	(cfs)	(ft)	
Culvert Under Haul Road	Duromaxx	72	3120.97	3119.72	1.25	1.74	36	0.019	58.2	11.52	60.13	2.05	
					Channels	i							
Element	Length	Inlet	Outlet	Total	Average	Channel	Channel	Channel	Channel	Peak	Max	Design	Ma
ID		Invert Elevation	Invert Elevation	Drop	Slope	Туре	Height	Width	Manning's Roughness	Flow	Flow Velocity	Flow Capacity	Flo Dep
	(ft)	(ft)	(ft)	(ft)	(%)		(ft)	(ft)		(cfs)	(ft/sec)	(cfs)	(f
Drainage Way 1 Upper	875	3145.00	3140.62	4.38	0.50	Trapezoidal	2	24	0.032	119.7	4.85	152.26	1.
Drainage Way 1 Lower	1295	3140.62	3088.97	51.65	3.99	Trapezoidal	2	21	0.032	119.6	8.04	252.22	0.9
Drainage Way 2	459	3149.00	3145.00	4.00	0.87	Trapezoidal	2	24	0.032	28.1	1.42	200.89	1.3
Drainage Way 3 Upper	143	3191.40	3150.22	41.18	28.80	Trapezoidal	2	16	0.032	6.2	1.22	563.21	0.8
Drainage Way 3 Lower	250	3150.22	3149.00	1.22	0.49	Triangular	2	6	0.032	5.6	4.02	17.22	1.0
Drainage Way 4 Upper	581	3124.00	3120.97	3.03	0.52	Trapezoidal	3	22	0.032	86.8	2.44	186.12	3.0
Drainage Way 4 Lower	438	3119.72	3079.44	40.28	9.20	Trapezoidal	2	16	0.032	88.4	11.20	318.27	1.0
Drainage Way 5	186	3173.20	3124.00	49.20	26.45	Trapezoidal	2	16	0.032	4.8	0.71	539.78	1.0
Existing Outlet Swale	216	3090.00	3088.00	2.00	0.93	Trapezoidal	2	22	0.035	23.4	2.71	164.61	0.9
Existing Outlet Swale	710	3085.00	3082.00	3.00	0.42	Trapezoidal	2	32	0.032	129.7	4.37	302.64	1.2
				Reservoirs									
Element	Invert	Max	Max	Peak	Peak	Maximum	Maximum	Average	Average				
ID	Elevation	(Rim)	(Rim)	Inflow	Outflow	HGL	HGL	HGL	HGL				
		Elevation	Offset			Elevation	Depth	Elevation	Depth				
	(ft)	(ft)	(ft)	(cfs)	(cfs)	(ft)	(ft)	(ft)	(ft)				
Inlet Fill Area 1	3145.00	3150.00	5.0	158.7	119.71	3147.33	2.33	3145.33	0.33				
Inlet Fill Area 2	3149.00	3152.00	3.0	29.8	28.11	3149.67	0.67	3149.07	0.07				
			Rainfall II	nformation					Ī				
Element	Data	Rainfall	Rain	State	County	Return	Rainfall	Rainfall					
ID	Source ID	Туре	Units		·	Period	Depth	Distribution					
	ıb					(years)	(inches)						
Rain Gage-01	Extrapolated	Cumulative	inches	Montana	Rosebud	500	4.66	SCS Type II 24-hr					
				in Information					I				
Drainage Basin	Area	Drainage	Weighted	Rain Gage	Total	Total	Peak	Time					
		Node ID	Curve	ID	Precipitation	Runoff	Runoff	of					
ID			Number		(:l)	(:h)	(-4-)	Concentration					
U	(acres)				(inches)	(inches)	(cfs)	(min)					
	(acres)	Dino Dam?	72	Dain Cago 01		1.04	121 F						
1	118.0	PipeDam2	72 72	Rain Gage-01	4.66	1.94	131.5	55					
1 2	118.0 18.6	PipeDam3	72	Rain Gage-01	4.66 4.66	1.94	24.3	44					
1 2 3	118.0 18.6 70.2	PipeDam3 ExtInletFill	72 72	Rain Gage-01 Rain Gage-01	4.66 4.66 4.66	1.94 1.94	24.3 85.6	44 48					
1 2 3 4	118.0 18.6 70.2 2.9	PipeDam3 ExtInletFill Jun-16	72 72 72	Rain Gage-01 Rain Gage-01 Rain Gage-01	4.66 4.66 4.66 4.66	1.94 1.94 1.94	24.3 85.6 5.4	44 48 25					
1 2 3 4 5	118.0 18.6 70.2 2.9 8.6	PipeDam3 ExtInletFill Jun-16 Out-04	72 72 72 72	Rain Gage-01 Rain Gage-01 Rain Gage-01 Rain Gage-01	4.66 4.66 4.66 4.66 4.66	1.94 1.94 1.94 1.94	24.3 85.6 5.4 14.9	44 48 25 29					
1 2 3 4 5	118.0 18.6 70.2 2.9 8.6 8.5	PipeDam3 ExtInletFill Jun-16 Out-04 Out-03	72 72 72 72 72	Rain Gage-01 Rain Gage-01 Rain Gage-01 Rain Gage-01 Rain Gage-01	4.66 4.66 4.66 4.66 4.66 4.66	1.94 1.94 1.94 1.94 1.94	24.3 85.6 5.4 14.9 12.0	44 48 25 29 39					
1 2 3 4 5	118.0 18.6 70.2 2.9 8.6	PipeDam3 ExtInletFill Jun-16 Out-04	72 72 72 72	Rain Gage-01 Rain Gage-01 Rain Gage-01 Rain Gage-01	4.66 4.66 4.66 4.66 4.66	1.94 1.94 1.94 1.94	24.3 85.6 5.4 14.9	44 48 25 29					

# Rosebud Power Plant Rainfall Hyetograph and Hydrograph Post-Closure Drainage Basins

