



BHB STRUCTURAL

Structural Calculations

BHB Project # 201247

Salt Lake Community College Remodel

4600 South Redwood Road
Taylorsville, UT 84123

Prepared For:

JRCA Architects, Inc.
577 South 200 East
Salt Lake City, Utah 84111

Prepared By:

AP

Rev 0
12/4/2020



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	Width	Depth	in2	ft2	Weight	
Slab	60	5	300	2.083333	313	lbs
Beam	7	20	210	1.458333	219	lbs
					531	lbs
				/60	106	psf
Gravel	50	psf				
Misc	15	psf				
D	171	psf				
L	100	psf				
Wall D	112.5	psf				
lt	11	ft				
Wall D	50	psf				
lt	11.5	ft				
	1813	plf				



Project:

Sheet: **2**

Job#:

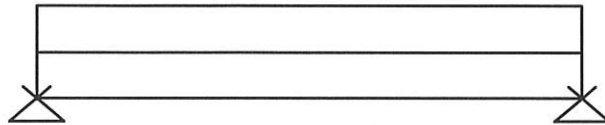
Date: 12/4/20

2766 South Main Street • Salt Lake City • Utah 84115
Phone: 801.355.5656 • Fax: 801.355.5950

By: AP

Steel Beam Design per AISC 360

File Name



Section Input			
Fy	50	ksi	<input checked="" type="radio"/> W Section
E	29000	ksi	<input type="radio"/> HSS Rectangle
Beam	W16X26		<input type="radio"/> HSS Square
Enter Beam Size			

Loads Input		
Trib	15	ft
DL	171	psf
LL	100	psf
Lr	0	psf

ASD Load Combinations

1. D
2. D+L
3. D+(Lr or S)
4. D+0.75L+0.75(Lr or S)

LRFD Load Combinations

1. 1.4D
2. 1.2D+1.6L+0.5(Lr or S)
3. 1.2D+1.6(Lr or S)+f₁L

f₁ = 1 for floors in places of public assemble for live loads in excess of 100 psf and for parking gargages

Design Aid

Distribute Loads

Clear Loads

Controlling Load Combination = 2

Beam Criteria								
Span - L	Lb	SR max	LL Defl.	TL Defl.	Axis of Bending	Design Method	Ω	f ₁
10.00 ft	1.00 ft	0.90	360	600	Strong Axis	ASD	1.67	0.5

Uniform and Trapezoidal Loads											
	Location		Dead Loads			Live Loads			Roof Live Loads		
	X Start	X End		Start	End		Start	End		Start	End
w1	0.00	10.00	ft	2.565	2.565	klf	1.500	1.500	klf	0.000	0.000
w2	0.00	10.00	ft	2.000	2.000	klf	0.000	0.000	klf	0.000	0.000
w3	0.00	0.00	ft	0.000	0.000	klf	0.000	0.000	klf	0.000	0.000
w4	0.00	0.00	ft	0.000	0.000	klf	0.000	0.000	klf	0.000	0.000

Concentrated Loads						
	Location		DL		LL	Lr
P1	0.00	ft	0.00	k	0.00	0.00
P2	0.00	ft	0.00	k	0.00	0.00
P3	0.00	ft	0.00	k	0.00	0.00
P4	0.00	ft	0.00	k	0.00	0.00

Fixed End Moments			
	Left	Right	
DL	0.000	0.000	k-ft
LL	0.000	0.000	k-ft
Lr	0.000	0.000	k-ft

NOTE: Positive = CCW

Output					
SHAPE	NAME	Lp (ft)	Lr (ft)	Z provided (in3)	I provided (in4)
W	W16X26	3.96	11.21	44.20	301.00

Allowable Live Load Deflection	0.3333333	in	Actual Live Load Deflection	0.04	in	Pass
Allowable Total Load Deflection	0.20	in	Actual Total Load Deflection	0.16	in	Pass
Mn/Ω	110.3	k-ft	Ma	75.8	k-ft	Pass

Ma	75.8	k-ft
Va	30.33	k

Unfactored Reactions			
	Left	Right	
Dead Loads	22.825	22.825	k
Live/Snow Loads	7.5	7.5	k
Total Loads	30.325	30.325	k

Loads are acceptable
Live load deflections are acceptable
Total load deflections are acceptable



Load Combination		Max Stress Ratios		Summary of Moment Values							Summary of Shear Values		
Segment Length	Span #	M	V	Mmax +	Mmax -	Ma Max	Mnx	Mnx/Omega	Cb	Rm	Va Max	Vnx	Vnx/Omega
+D+H													
Dsgn. L = 12.00 ft	1	0.561	0.313	2.00	-75.53	75.53	225.00	134.73	2.70	1.00	27.35	131.18	87.45
Dsgn. L = 3.00 ft	2	0.561	0.313		-75.53	75.53	225.00	134.73	1.00	1.00	27.35	131.18	87.45
+D+L+H, LL Comb Run (*L)													
Dsgn. L = 12.00 ft	1	0.759	0.425	0.01	-102.23	102.23	225.00	134.73	2.34	1.00	37.15	131.18	87.45
Dsgn. L = 3.00 ft	2	0.759	0.425		-102.23	102.23	225.00	134.73	1.00	1.00	37.15	131.18	87.45
+D+L+H, LL Comb Run (L*)													
Dsgn. L = 12.00 ft	1	0.561	0.313	8.80	-75.53	75.53	225.00	134.73	3.00	1.00	27.35	131.18	87.45
Dsgn. L = 3.00 ft	2	0.561	0.313		-75.53	75.53	225.00	134.73	1.00	1.00	27.35	131.18	87.45
+D+L+H, LL Comb Run (LL)													

Title Block Line 1
You can change this area
using the "Settings" menu item
and then using the "Printing &
Title Block" selection.
Title Block Line 6

Project Title:
Engineer:
Project ID:
Project Descr:

4

Printed: 2 DEC 2020, 8:31AM

Steel Beam

File = C:\Users\Alexp\Desktop\JRCAL\SLCC\CALCUL-1\SLCC.ec6
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Lic. #: KW-06005009

BHB CONSULTING ENGINEERS

DESCRIPTION: Cantilevered steel beam

Load Combination		Max Stress Ratios		Summary of Moment Values							Summary of Shear Values		
Segment Length	Span #	M	V	Mmax +	Mmax -	Ma Max	Mnx	Mnx/Omega	Cb	Rm	Va Max	Vnx	Vnx/Omega
Dsgn. L = 12.00 ft	1	0.759	0.425	3.49	-102.23	102.23	225.00	134.73	2.74	1.00	37.15	131.18	87.45
Dsgn. L = 3.00 ft	2	0.759	0.425		-102.23	102.23	225.00	134.73	1.00	1.00	37.15	131.18	87.45
+D+Lr+H, LL Comb Run (*L)													
Dsgn. L = 12.00 ft	1	0.561	0.313	2.00	-75.53	75.53	225.00	134.73	2.70	1.00	27.35	131.18	87.45
Dsgn. L = 3.00 ft	2	0.561	0.313		-75.53	75.53	225.00	134.73	1.00	1.00	27.35	131.18	87.45
+D+Lr+H, LL Comb Run (L*)													
Dsgn. L = 12.00 ft	1	0.561	0.313	2.00	-75.53	75.53	225.00	134.73	2.70	1.00	27.35	131.18	87.45
Dsgn. L = 3.00 ft	2	0.561	0.313		-75.53	75.53	225.00	134.73	1.00	1.00	27.35	131.18	87.45
+D+Lr+H, LL Comb Run (LL)													
Dsgn. L = 12.00 ft	1	0.561	0.313	2.00	-75.53	75.53	225.00	134.73	2.70	1.00	27.35	131.18	87.45
Dsgn. L = 3.00 ft	2	0.561	0.313		-75.53	75.53	225.00	134.73	1.00	1.00	27.35	131.18	87.45
+D+S+H													
Dsgn. L = 12.00 ft	1	0.561	0.313	2.00	-75.53	75.53	225.00	134.73	2.70	1.00	27.35	131.18	87.45
Dsgn. L = 3.00 ft	2	0.561	0.313		-75.53	75.53	225.00	134.73	1.00	1.00	27.35	131.18	87.45
+D+0.750Lr+0.750L+H, LL Comb Run (*)													
Dsgn. L = 12.00 ft	1	0.709	0.397	0.19	-95.55	95.55	225.00	134.73	2.41	1.00	34.70	131.18	87.45
Dsgn. L = 3.00 ft	2	0.709	0.397		-95.55	95.55	225.00	134.73	1.00	1.00	34.70	131.18	87.45
+D+0.750Lr+0.750L+H, LL Comb Run (L)													
Dsgn. L = 12.00 ft	1	0.561	0.313	6.86	-75.53	75.53	225.00	134.73	2.98	1.00	27.35	131.18	87.45
Dsgn. L = 3.00 ft	2	0.561	0.313		-75.53	75.53	225.00	134.73	1.00	1.00	27.35	131.18	87.45
+D+0.750Lr+0.750L+H, LL Comb Run (L)													
Dsgn. L = 12.00 ft	1	0.709	0.397	3.11	-95.55	95.55	225.00	134.73	2.73	1.00	34.70	131.18	87.45
Dsgn. L = 3.00 ft	2	0.709	0.397		-95.55	95.55	225.00	134.73	1.00	1.00	34.70	131.18	87.45
+D+0.750L+0.750S+H, LL Comb Run (*L)													
Dsgn. L = 12.00 ft	1	0.709	0.397	0.19	-95.55	95.55	225.00	134.73	2.41	1.00	34.70	131.18	87.45
Dsgn. L = 3.00 ft	2	0.709	0.397		-95.55	95.55	225.00	134.73	1.00	1.00	34.70	131.18	87.45
+D+0.750L+0.750S+H, LL Comb Run (L')													
Dsgn. L = 12.00 ft	1	0.561	0.313	6.86	-75.53	75.53	225.00	134.73	2.98	1.00	27.35	131.18	87.45
Dsgn. L = 3.00 ft	2	0.561	0.313		-75.53	75.53	225.00	134.73	1.00	1.00	27.35	131.18	87.45
+D+0.750L+0.750S+H, LL Comb Run (LI)													
Dsgn. L = 12.00 ft	1	0.709	0.397	3.11	-95.55	95.55	225.00	134.73	2.73	1.00	34.70	131.18	87.45
Dsgn. L = 3.00 ft	2	0.709	0.397		-95.55	95.55	225.00	134.73	1.00	1.00	34.70	131.18	87.45
+D+0.60W+H													
Dsgn. L = 12.00 ft	1	0.561	0.313	2.00	-75.53	75.53	225.00	134.73	2.70	1.00	27.35	131.18	87.45
Dsgn. L = 3.00 ft	2	0.561	0.313		-75.53	75.53	225.00	134.73	1.00	1.00	27.35	131.18	87.45
+D+0.750Lr+0.450W+H, LL Comb Run (*)													
Dsgn. L = 12.00 ft	1	0.561	0.313	2.00	-75.53	75.53	225.00	134.73	2.70	1.00	27.35	131.18	87.45
Dsgn. L = 3.00 ft	2	0.561	0.313		-75.53	75.53	225.00	134.73	1.00	1.00	27.35	131.18	87.45
+D+0.750Lr+0.450W+H, LL Comb Run (I)													
Dsgn. L = 12.00 ft	1	0.561	0.313	2.00	-75.53	75.53	225.00	134.73	2.70	1.00	27.35	131.18	87.45
Dsgn. L = 3.00 ft	2	0.561	0.313		-75.53	75.53	225.00	134.73	1.00	1.00	27.35	131.18	87.45
+D+0.750Lr+0.450W+H, LL Comb Run (I)													
Dsgn. L = 12.00 ft	1	0.561	0.313	2.00	-75.53	75.53	225.00	134.73	2.70	1.00	27.35	131.18	87.45
Dsgn. L = 3.00 ft	2	0.561	0.313		-75.53	75.53	225.00	134.73	1.00	1.00	27.35	131.18	87.45
+D+0.750S+0.450W+H													
Dsgn. L = 12.00 ft	1	0.561	0.313	2.00	-75.53	75.53	225.00	134.73	2.70	1.00	27.35	131.18	87.45
Dsgn. L = 3.00 ft	2	0.561	0.313		-75.53	75.53	225.00	134.73	1.00	1.00	27.35	131.18	87.45
+0.60D+0.60W+0.60H													
Dsgn. L = 12.00 ft	1	0.336	0.188	1.20	-45.32	45.32	225.00	134.73	2.70	1.00	16.41	131.18	87.45
Dsgn. L = 3.00 ft	2	0.336	0.188		-45.32	45.32	225.00	134.73	1.00	1.00	16.41	131.18	87.45
+D+0.70E+0.60H													
Dsgn. L = 12.00 ft	1	0.561	0.313	2.00	-75.53	75.53	225.00	134.73	2.70	1.00	27.35	131.18	87.45
Dsgn. L = 3.00 ft	2	0.561	0.313		-75.53	75.53	225.00	134.73	1.00	1.00	27.35	131.18	87.45
+D+0.750L+0.750S+0.5250E+H, LL Con													
Dsgn. L = 12.00 ft	1	0.709	0.397	0.19	-95.55	95.55	225.00	134.73	2.41	1.00	34.70	131.18	87.45
Dsgn. L = 3.00 ft	2	0.709	0.397		-95.55	95.55	225.00	134.73	1.00	1.00	34.70	131.18	87.45
+D+0.750L+0.750S+0.5250E+H, LL Con													
Dsgn. L = 12.00 ft	1	0.561	0.313	6.86	-75.53	75.53	225.00	134.73	2.98	1.00	27.35	131.18	87.45
Dsgn. L = 3.00 ft	2	0.561	0.313		-75.53	75.53	225.00	134.73	1.00	1.00	27.35	131.18	87.45
+D+0.750L+0.750S+0.5250E+H, LL Con													
Dsgn. L = 12.00 ft	1	0.709	0.397	3.11	-95.55	95.55	225.00	134.73	2.73	1.00	34.70	131.18	87.45
Dsgn. L = 3.00 ft	2	0.709	0.397		-95.55	95.55	225.00	134.73	1.00	1.00	34.70	131.18	87.45
+0.60D+0.70E+H													
Dsgn. L = 12.00 ft	1	0.336	0.188	1.20	-45.32	45.32	225.00	134.73	2.70	1.00	16.41	131.18	87.45
Dsgn. L = 3.00 ft	2	0.336	0.188		-45.32	45.32	225.00	134.73	1.00	1.00	16.41	131.18	87.45

Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
	1	0.0000	0.000	+D+L+H	-0.0913	7.584

Title Block Line 1
 You can change this area
 using the "Settings" menu item
 and then using the "Printing &
 Title Block" selection.
 Title Block Line 6

Project Title:
 Engineer:
 Project ID:
 Project Descr:



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Steel Beam

File = C:\Users\Alexp\Desktop\JRCA\SLCC\CALCUL~1\SLCC.ec6
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BHB CONSULTING ENGINEERS

DESCRIPTION: Cantilevered steel beam

Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
+D+L+H	2	0.1926	3.000		0.0000	7.584

Vertical Reactions

Support notation : Far left is #1

Values in KIPS

Load Combination	Support 1	Support 2	Support 3
Overall MAXimum	6.006	57.969	
Overall MINimum	0.181	3.600	
+D+H	2.406	42.344	
+D+L+H, LL Comb Run (*L)	0.181	54.369	
+D+L+H, LL Comb Run (L*)	6.006	45.944	
+D+L+H, LL Comb Run (LL)	3.781	57.969	
+D+Lr+H, LL Comb Run (*L)	2.406	42.344	
+D+Lr+H, LL Comb Run (L*)	2.406	42.344	
+D+Lr+H, LL Comb Run (LL)	2.406	42.344	
+D+S+H	2.406	42.344	
+D+0.750Lr+0.750L+H, LL Comb Run (*)	0.737	51.363	
+D+0.750Lr+0.750L+H, LL Comb Run (L)	5.106	45.044	
+D+0.750Lr+0.750L+H, LL Comb Run (L)	3.437	54.063	
+D+0.750L+0.750S+H, LL Comb Run (*L)	0.737	51.363	
+D+0.750L+0.750S+H, LL Comb Run (L)	5.106	45.044	
+D+0.750L+0.750S+H, LL Comb Run (L)	3.437	54.063	
+D+0.60W+H	2.406	42.344	
+D+0.750Lr+0.450W+H, LL Comb Run (*)	2.406	42.344	
+D+0.750Lr+0.450W+H, LL Comb Run (L)	2.406	42.344	
+D+0.750Lr+0.450W+H, LL Comb Run (L)	2.406	42.344	
+D+0.750S+0.450W+H	2.406	42.344	
+0.60D+0.60W+0.60H	1.444	25.406	
+D+0.70E+0.60H	2.406	42.344	
+D+0.750L+0.750S+0.5250E+H, LL Con	0.737	51.363	
+D+0.750L+0.750S+0.5250E+H, LL Con	5.106	45.044	
+D+0.750L+0.750S+0.5250E+H, LL Con	3.437	54.063	
+0.60D+0.70E+H	1.444	25.406	
D Only	2.406	42.344	
Lr Only, LL Comb Run (*L)			
Lr Only, LL Comb Run (L*)			
Lr Only, LL Comb Run (LL)			
L Only, LL Comb Run (*L)	-2.225	12.025	
L Only, LL Comb Run (L*)	3.600	3.600	
L Only, LL Comb Run (LL)	1.375	15.625	
S Only			
W Only			
E Only			
H Only			



BHB STRUCTURAL

Project:

Sheet:

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Job#:

Date:

12/4/20

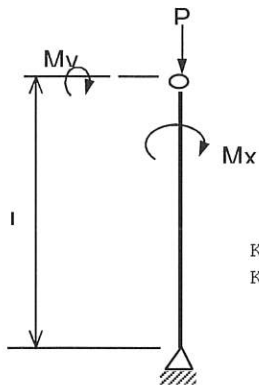
By:

AP

2766 South Main Street - SLC, Utah 84115
Phone: 801.355.5656 - Fax: 801.355.5950

Steel Column

File Name



Kx

1.0

Ky

1.0

Column Loads

P_{DL}	0.00	k
P_{LL}	58.00	k
$P_{S/LF}$	0.00	k
P_W	0.00	k
P_E	0.00	k
M_{DL-X}	0.00	k-ft
M_{DL-Y}	0.00	k-ft
M_{LL-X}	0.00	k-ft
M_{LL-Y}	0.00	k-ft
$M_{S/LF-X}$	0.00	k-ft
$M_{S/LF-Y}$	0.00	k-ft
M_{WIND-X}	0.00	k-ft
M_{WIND-Y}	0.00	k-ft
M_{SEIS-X}	0.00	k-ft
M_{SEIS-Y}	0.00	k-ft
f_1	1	
f_2	0.5	

Beam Geometry

Col. unbraced L_x =	12.0	ft
Col. unbraced L_y =	12.0	ft
Beam unbraced L_x =	12.0	ft
Beam unbraced L_y =	12.0	ft

Load Combinations per IBC 2018

1. D
2. D+L
3. D+(Lr or S)
4. D+0.75L+0.75(Lr or S)
5. D+(0.6W or 0.7E)
6. D+0.75(0.6W or 0.7E)+0.75L+0.75(Lr or S)
7. 0.6D+0.6W
8. 0.6D+0.7E

Controlling Load Combination

2

Member Properties

Section	HSS4x4x3/8	
A_g	4.78	in ²
S_x	5.13	in ³
S_y	5.13	in ³
r_x	1.47	in
r_y	1.47	in
W_t	17.20	lbs/ft
I_x	10.3	in ⁴
I_y	0	in ⁴

Material Properties

Steel Type	A500 gr. C	
F_y	50	ksi
E	29000	ksi
S_{DS}	0.21	
Ω	2.5	

Design Controls

Code Year	2018
Design Criteria	ASD
<input checked="" type="checkbox"/> Pin Connection at Base Plate	

Cross Section

 $\Omega_c/b = 1.67$ 

Analysis

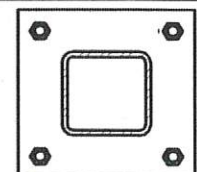
Nominal Compressive Strength ($P_n = F_c A_g$)	118	k
Allowable Axial Compressive Strength ($P_c = P_n / \Omega_c$)	71	k
Nominal Flexural Strength ($M_{nx} = F_y Z_x$)	27	k-ft
Nominal Flexural Strength ($M_{ny} = F_y Z_y$)	27	k-ft
Allowable Flexural Strength ($M_{cx} = M_{nx} / \Omega_b$)	16	k-ft
Allowable Flexural Strength ($M_{cy} = M_{ny} / \Omega_b$)	16	k-ft

Unity Check

Required Axial Compressive Strength (P_r)	58.0	k
Required Flexural Strength (M_{cx})	0.0	k-ft
Required Flexural Strength (M_{cy})	0.0	k-ft
Eq H1-1a: $P_r / P_c \geq 0.2$ $P_r / P_c + 8/9 (M_{rx} / M_{cx} + M_{ry} / M_{cy})$	0.817	Pass
Eq H1-1b: $P_r / P_c < 0.2$ $P_r / (2P_c) + (M_{rx} / M_{cx} + M_{ry} / M_{cy})$	NA	

Base Plate

- ☒ Type 1
☐ Type 2



Use 7/8 Base Plate Type 1 Minimum

Company:		Date:	12/2/2020
Engineer:		Page:	1/5
Project:			
Address:			
Phone:			
E-mail:			

1. Project information

Customer company:
 Customer contact name:
 Customer e-mail:
 Comment:

Project description:
 Location:
 Fastening description:

2. Input Data & Anchor Parameters

General

Design method: ACI 318-14
 Units: Imperial units

Anchor Information:

Anchor type: Concrete screw
 Material: Carbon Steel
 Diameter (inch): 0.750
 Nominal Embedment depth (inch): 6.000
 Effective Embedment depth, h_{ef} (inch): 4.640
 Code report: ICC-ES ESR-2713
 Anchor category: 1
 Anchor ductility: No
 h_{min} (inch): 9.58
 c_{ac} (inch): 7.00
 c_{min} (inch): 1.75
 s_{min} (inch): 3.00

Base Material

Concrete: Normal-weight
 Concrete thickness, h (inch): 12.00
 State: Cracked
 Compressive strength, f'_c (psi): 4000
 $\Psi_{c,v}$: 1.0
 Reinforcement condition: B tension, B shear
 Supplemental reinforcement: Not applicable
 Reinforcement provided at corners: No
 Ignore concrete breakout in tension: No
 Ignore concrete breakout in shear: No
 Ignore 6do requirement: Not applicable
 Build-up grout pad: No

Base Plate

Length x Width x Thickness (inch): 12.00 x 19.00 x 0.50
 Yield stress: 24000 psi

Profile type/size: W16X31

Recommended Anchor

Anchor Name: Titen HD® - 3/4"Ø Titen HD, h_{nom} : 6" (152mm)
 Code Report: ICC-ES ESR-2713



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Load and Geometry

Load factor source: ACI 318 Section 5.3

Load combination: not set

Seismic design: No

Anchors subjected to sustained tension: Not applicable

Apply entire shear load at front row: No

Anchors only resisting wind and/or seismic loads: No

Strength level loads:

N_{ua} [lb]: 0

V_{uax} [lb]: 0

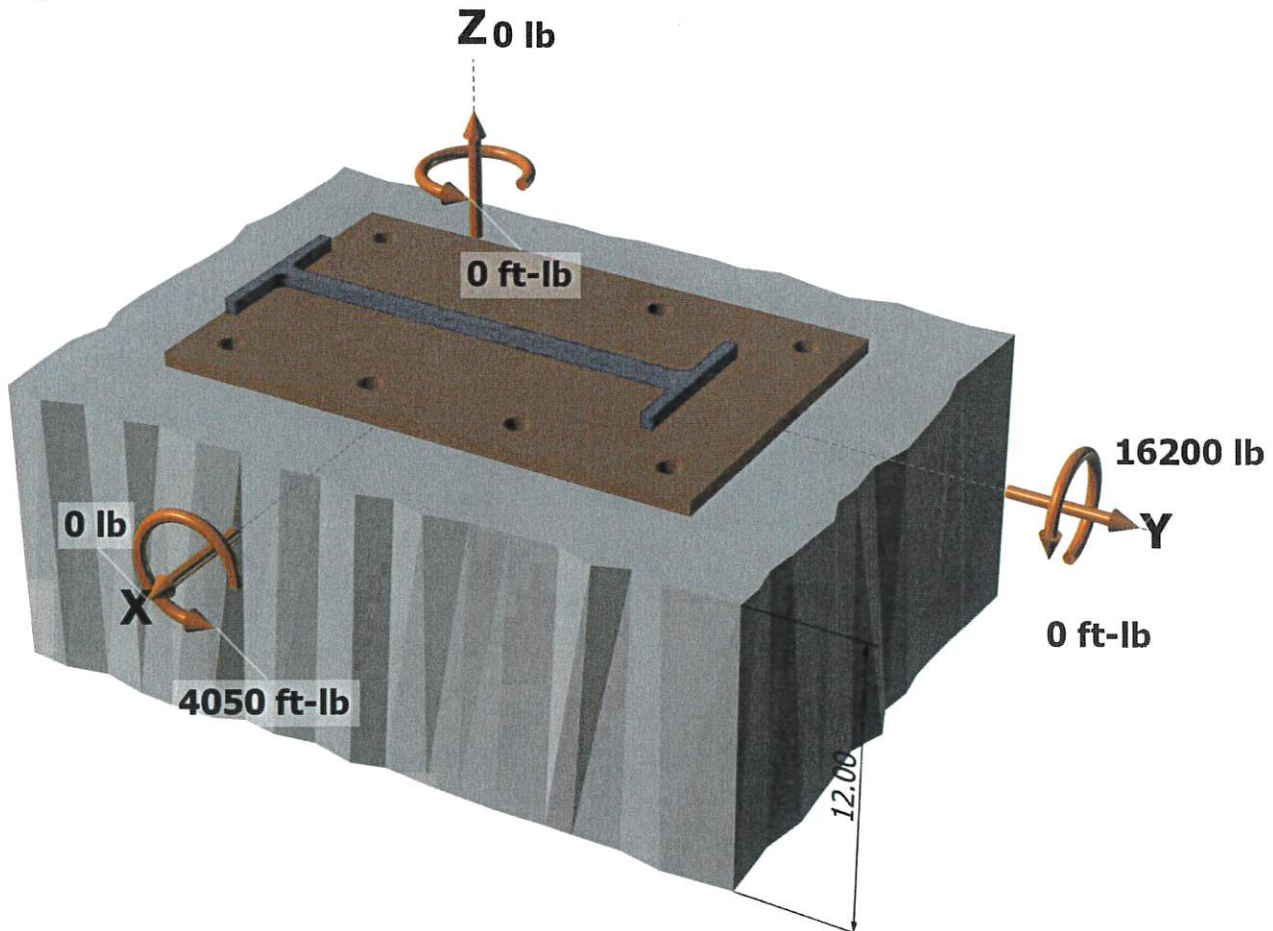
V_{uay} [lb]: 16200

M_{ux} [ft-lb]: 4050

M_{uy} [ft-lb]: 0

M_{uz} [ft-lb]: 0

<Figure 1>

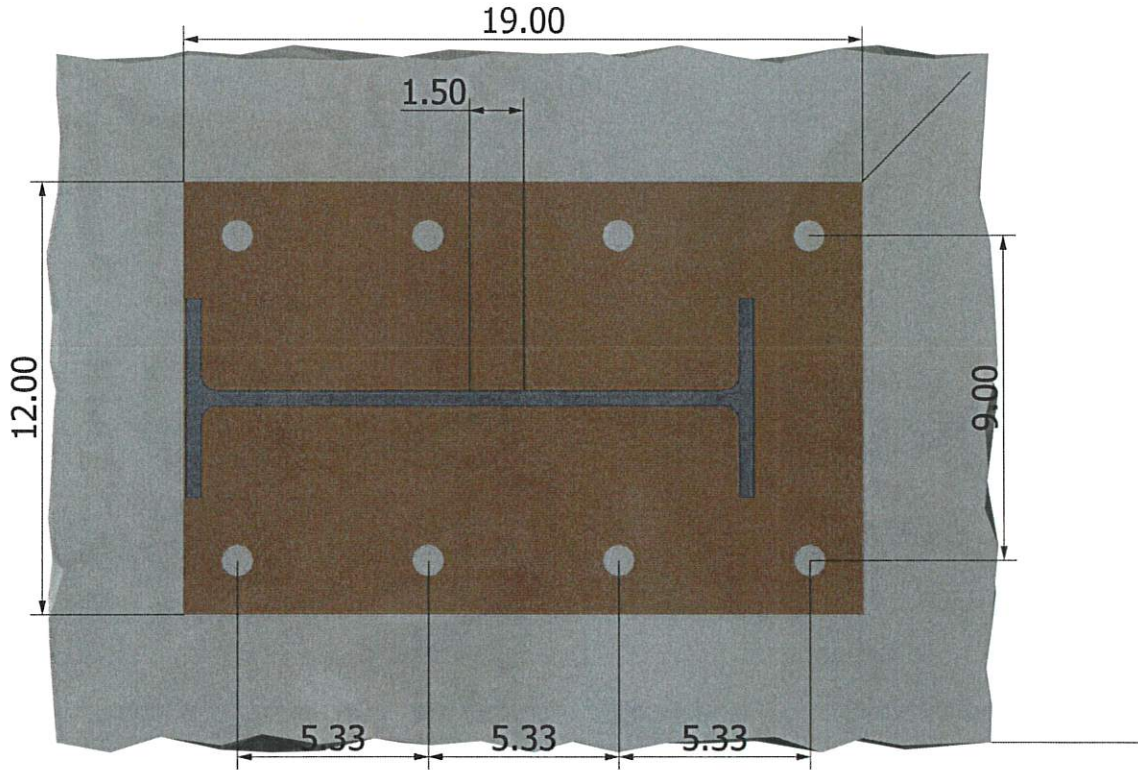


Input data and results must be checked for agreement with the existing circumstances, the standards and guidelines must be checked for plausibility.

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<Figure 2>



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3. Resulting Anchor Forces

Anchor	Tension load, N_{ua} (lb)	Shear load x, V_{uax} (lb)	Shear load y, V_{uay} (lb)	Shear load combined, $\sqrt{(V_{uax})^2 + (V_{uay})^2}$ (lb)
1	0.0	0.0	2025.0	2025.0
2	163.3	0.0	2025.0	2025.0
3	616.5	0.0	2025.0	2025.0
4	1069.7	0.0	2025.0	2025.0
5	1069.7	0.0	2025.0	2025.0
6	616.5	0.0	2025.0	2025.0
7	163.3	0.0	2025.0	2025.0
8	0.0	0.0	2025.0	2025.0
Sum	3698.9	0.0	16200.0	16200.0

Maximum concrete compression strain (%): 0.03

Maximum concrete compression stress (psi): 125

Resultant tension force (lb): 3699

Resultant compression force (lb): 3699

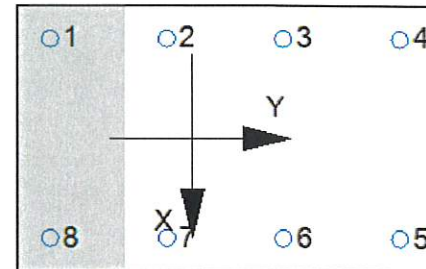
Eccentricity of resultant tension forces in x-axis, e'_{nx} (inch): 0.00

Eccentricity of resultant tension forces in y-axis, e'_{ny} (inch): 2.61

Eccentricity of resultant shear forces in x-axis, e'_{vx} (inch): 0.00

Eccentricity of resultant shear forces in y-axis, e'_{vy} (inch): 0.00

<Figure 3>



4. Steel Strength of Anchor in Tension (Sec. 17.4.1)

N_{sa} (lb)	ϕ	ϕN_{sa} (lb)
45540	0.65	29601

5. Concrete Breakout Strength of Anchor in Tension (Sec. 17.4.2)

$N_b = k_c \lambda_a \sqrt{f'_c} h_{ef}^{1.5}$ (Eq. 17.4.2.2a)

k_c	λ_a	f'_c (psi)	h_{ef} (in)	N_b (lb)
17.0	1.00	4000	4.640	10746

$\phi N_{cbg} = \phi (A_{Nc} / A_{Nco}) \Psi_{ec,N} \Psi_{ed,N} \Psi_{c,N} \Psi_{cp,N} N_b$ (Sec. 17.3.1 & Eq. 17.4.2.1b)

A_{Nc} (in ²)	A_{Nco} (in ²)	$c_{a,min}$ (in)	$\Psi_{ec,N}$	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	ϕ	ϕN_{cbg} (lb)
563.37	193.77	-	0.727	1.000	1.00	1.000	10746	0.65	14767

6. Pullout Strength of Anchor in Tension (Sec. 17.4.3)

$\phi N_{pn} = \phi \Psi_{c,P} \lambda_a N_p (f'_c / 2,500)^n$ (Sec. 17.3.1, Eq. 17.4.3.1 & Code Report)

$\Psi_{c,P}$	λ_a	N_p (lb)	f'_c (psi)	n	ϕ	ϕN_{pn} (lb)
1.0	1.00	6820	4000	0.50	0.65	5607

Input data and results must be checked for agreement with the existing circumstances, the standards and guidelines must be checked for plausibility.

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Software
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8. Steel Strength of Anchor in Shear (Sec. 17.5.1)

V_{sa} (lb)	ϕ_{grout}	ϕ	$\phi_{grout}\phi V_{sa}$ (lb)
16840	1.0	0.60	10104

10. Concrete Pryout Strength of Anchor in Shear (Sec. 17.5.3)

$\phi V_{cp} = \phi k_{cp} N_{cbg} = \phi k_{cp} (A_{Nc} / A_{Nco}) \Psi_{ec,N} \Psi_{ed,N} \Psi_{c,N} \Psi_{cp,N} N_b$ (Sec. 17.3.1 & Eq. 17.5.3.1b)

k_{cp}	A_{Nc} (in ²)	A_{Nco} (in ²)	$\Psi_{ec,N}$	$\Psi_{ed,N}$	$\Psi_{c,N}$	$\Psi_{cp,N}$	N_b (lb)	ϕ	ϕV_{cp} (lb)
2.0	685.54	193.77	1.000	1.000	1.000	1.000	10746	0.70	53228

11. Results

Interaction of Tensile and Shear Forces (Sec. 17.6.)

Tension	Factored Load, N_{ua} (lb)	Design Strength, ϕN_n (lb)	Ratio	Status
Steel	1070	29601	0.04	Pass
Concrete breakout	3699	14767	0.25	Pass (Governs)
Pullout	1070	5607	0.19	Pass

Shear	Factored Load, V_{ua} (lb)	Design Strength, ϕV_n (lb)	Ratio	Status
Steel	2025	10104	0.20	Pass
Pryout	16200	53228	0.30	Pass (Governs)

Interaction check	$N_{ua}/\phi N_n$	$V_{ua}/\phi V_n$	Combined Ratio	Permissible	Status
Sec. 17.6..2	0.00	0.30	30.4%	1.0	Pass

3/4"Ø Titen HD, hnom:6" (152mm) meets the selected design criteria.

Base Plate Thickness

Required base plate thickness: 0.350 inch

12. Warnings

- Minimum spacing and edge distance requirement of 6da per ACI 318 Sections 17.7.1 and 17.7.2 for torqued cast-in-place anchor is waived per designer option.
- Designer must exercise own judgement to determine if this design is suitable.
- Refer to manufacturer's product literature for hole cleaning and installation instructions.

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BHB CONSULTING ENGINEERS

DESCRIPTION: Spot footing

Code References

Calculations per ACI 318-11, IBC 2012, CBC 2013, ASCE 7-10

Load Combinations Used : ASCE 7-16

General Information

Material Properties

f'_c : Concrete 28 day strength	=	2.50 ksi
f_y : Rebar Yield	=	60.0 ksi
E_c : Concrete Elastic Modulus	=	3,122.0 ksi
Concrete Density	=	145.0 pcf
ϕ Values Flexure	=	0.90
Shear	=	0.750

Analysis Settings

Min Steel % Bending Reinf.	=	
Min Allow % Temp Reinf.	=	0.00180
Min. Overturning Safety Factor	=	1.0 : 1
Min. Sliding Safety Factor	=	1.0 : 1
Add Ftg Wt for Soil Pressure	:	Yes
Use ftg wt for stability, moments & shears	:	Yes
Add Pedestal Wt for Soil Pressure	:	No
Use Pedestal wt for stability, mom & shear	:	No

Soil Design Values

Allowable Soil Bearing	=	1.50 ksf
Increase Bearing By Footing Weight	=	No
Soil Passive Resistance (for Sliding)	=	250.0 pcf
Soil/Concrete Friction Coeff.	=	0.30

Increases based on footing Depth

Footing base depth below soil surface	=	0.0 ft
Allow press. increase per foot of depth when footing base is below	=	0.0 ksf
	=	0.0 ft

Increases based on footing plan dimension

Allowable pressure increase per foot of depth when max. length or width is greater than	=	0.0 ksf
	=	0.0 ft

Dimensions

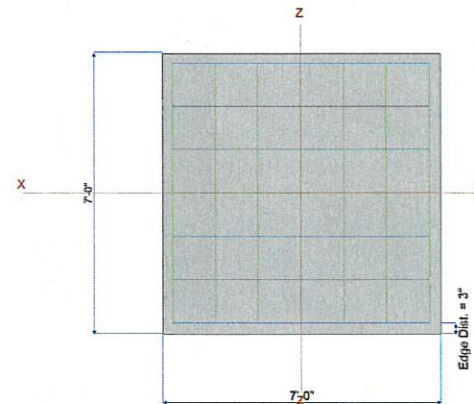
Width parallel to X-X Axis	=	7.0 ft
Length parallel to Z-Z Axis	=	7.0 ft
Footing Thickness	=	13.0 in

Pedestal dimensions...

p_x : parallel to X-X Axis	=	10.0 in
p_z : parallel to Z-Z Axis	=	10.0 in
Height	=	0.0 in

Rebar Centerline to Edge of Concrete...
at Bottom of footing

3.0 in



Reinforcing

Bars parallel to X-X Axis

Number of Bars	=	7.0
Reinforcing Bar Size	=	# 5

Bars parallel to Z-Z Axis

Number of Bars	=	7.0
Reinforcing Bar Size	=	# 5

Bandwidth Distribution Check (ACI 15.4.4.2)

Direction Requiring Closer Separation

n/a

Bars required within zone

n/a

Bars required on each side of zone

n/a

Applied Loads

		D	Lr	L	S	W	E	H
P : Column Load	=	60.0	0.0	0.0	0.0	0.0	0.0	0.0 k
OB : Overburden	=	0.0	0.0	0.0	0.0	0.0	0.0	0.0 ksf
M-xx	=	0.0	0.0	0.0	0.0	0.0	0.0	0.0 k-ft
M-zz	=	0.0	0.0	0.0	0.0	0.0	0.0	0.0 k-ft
V-x	=	0.0	0.0	0.0	0.0	0.0	0.0	0.0 k
V-z	=	0.0	0.0	0.0	0.0	0.0	0.0	0.0 k

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BHB CONSULTING ENGINEERS

DESCRIPTION: Spot footing

DESIGN SUMMARY

Design OK

	Min. Ratio	Item	Applied	Capacity	Governing Load Combination
PASS	0.9213	Soil Bearing	1.382 ksf	1.50 ksf	D Only about Z-Z axis
PASS	n/a	Overturning - X-X	0.0 k-ft	0.0 k-ft	No Overturning
PASS	n/a	Overturning - Z-Z	0.0 k-ft	0.0 k-ft	No Overturning
PASS	n/a	Sliding - X-X	0.0 k	0.0 k	No Sliding
PASS	n/a	Sliding - Z-Z	0.0 k	0.0 k	No Sliding
PASS	n/a	Uplift	0.0 k	0.0 k	No Uplift
PASS	0.6063	Z Flexure (+X)	8.149 k-ft/ft	13.441 k-ft/ft	+1.40D
PASS	0.6063	Z Flexure (-X)	8.149 k-ft/ft	13.441 k-ft/ft	+1.40D
PASS	0.6063	X Flexure (+Z)	8.149 k-ft/ft	13.441 k-ft/ft	+1.40D
PASS	0.6063	X Flexure (-Z)	8.149 k-ft/ft	13.441 k-ft/ft	+1.40D
PASS	0.4267	1-way Shear (+X)	32.0 psi	75.0 psi	+1.40D
PASS	0.4267	1-way Shear (-X)	32.0 psi	75.0 psi	+1.40D
PASS	0.4267	1-way Shear (+Z)	32.0 psi	75.0 psi	+1.40D
PASS	0.4267	1-way Shear (-Z)	32.0 psi	75.0 psi	+1.40D
PASS	0.6597	2-way Punching	98.952 psi	150.0 psi	+1.40D

Detailed Results

Soil Bearing

Rotation Axis & Load Combination...	Gross Allowable	Xeccc	Zeccc (in)	Actual Soil Bearing Stress @ Location				Actual / Allow Ratio
				Bottom, -Z	Top, +Z	Left, -X	Right, +X	
X-X, D Only	1.50	n/a	0.0	1.382	1.382	n/a	n/a	0.921
X-X, +0.60D	1.50	n/a	0.0	0.8289	0.8289	n/a	n/a	0.553
Z-Z, D Only	1.50	0.0	n/a	n/a	n/a	1.382	1.382	0.921
Z-Z, +0.60D	1.50	0.0	n/a	n/a	n/a	0.8289	0.8289	0.553

Overturning Stability

Rotation Axis & Load Combination...	Overturning Moment	Resisting Moment	Stability Ratio	Status
Footing Has NO Overturning				
				All units k

Sliding Stability

Force Application Axis Load Combination...	Sliding Force	Resisting Force	Stability Ratio	Status
Footing Has NO Sliding				

Footing Flexure

Flexure Axis & Load Combination	Mu k-ft	Side	Tension Surface	As Req'd in^2	Gvrn. As in^2	Actual As in^2	Phi*Mn k-ft	Status
X-X, +1.40D	8.149	+Z	Bottom	0.2808	Min Temp %	0.310	13.441	OK
X-X, +1.40D	8.149	-Z	Bottom	0.2808	Min Temp %	0.310	13.441	OK
X-X, +1.20D	6.985	+Z	Bottom	0.2808	Min Temp %	0.310	13.441	OK
X-X, +1.20D	6.985	-Z	Bottom	0.2808	Min Temp %	0.310	13.441	OK
X-X, +0.90D	5.239	+Z	Bottom	0.2808	Min Temp %	0.310	13.441	OK
X-X, +0.90D	5.239	-Z	Bottom	0.2808	Min Temp %	0.310	13.441	OK
Z-Z, +1.40D	8.149	-X	Bottom	0.2808	Min Temp %	0.310	13.441	OK
Z-Z, +1.40D	8.149	+X	Bottom	0.2808	Min Temp %	0.310	13.441	OK
Z-Z, +1.20D	6.985	-X	Bottom	0.2808	Min Temp %	0.310	13.441	OK
Z-Z, +1.20D	6.985	+X	Bottom	0.2808	Min Temp %	0.310	13.441	OK
Z-Z, +0.90D	5.239	-X	Bottom	0.2808	Min Temp %	0.310	13.441	OK
Z-Z, +0.90D	5.239	+X	Bottom	0.2808	Min Temp %	0.310	13.441	OK

One Way Shear

Load Combination...	Vu @ -X	Vu @ +X	Vu @ -Z	Vu @ +Z	Vu:Max	Phi Vn	Vu / Phi*Vn	Status
+1.40D	32.00 psi	32.00 psi	32.00 psi	32.00 psi	32.00 psi	75.00 psi	0.43	OK
+1.20D	27.43 psi	27.43 psi	27.43 psi	27.43 psi	27.43 psi	75.00 psi	0.37	OK
+0.90D	20.57 psi	20.57 psi	20.57 psi	20.57 psi	20.57 psi	75.00 psi	0.27	OK

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BHB CONSULTING ENGINEERS

DESCRIPTION: Spot footing

Two-Way "Punching" Shear

All units k

Load Combination...	Vu	Phi*Vn	Vu / Phi*Vn	Status
+1.40D	98.95 psi	150.00 psi	0.6597	OK
+1.20D	84.82 psi	150.00 psi	0.5654	OK
+0.90D	63.61 psi	150.00 psi	0.4241	OK