

Displacive versus diffusional transformations the determining factors

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1. Background – some remarks

There is no "versus"!

It is generally accepted that a transformation may be both displacive and diffusion controlled!

But: Many authors mean diffusionless when they say displacive.







Two "versus":

- Reconstructive/displacive
 - refers to the details of the crystallographic changes at the phase interface.
- Diffusional/diffusionless
 - Refers to if there is a change in composition at the phase interface







Displacive transformations:

- Interface migration by coordinated motion of atoms (transformation dislocations)
- Coherent or semi-coherent interfaces
- Crystallographic orientation relationships
- Shape changes

Reconstructive

- Incoherent interfaces
- Interface migration by random jumps of atoms
- No crystallographic orientation relationships







Examples of reactions involving FCC \rightarrow BCC in steels

Reaction	Displacive	Reconstructive	Diffusional	Diffusionless
Allotriomorphic		Х	Х	
Widmanstätten	Х		Х	
Martensitic	Х			Х
Massive		Х		Х
Bainitic	Х		Х	
Pearlite		X	X	







Content

- 1. Background some remarks
- 2. Thermodynamic limits
- 3. Kinetic limits
- 4. Modelling of local state at a sharp phase interface
- 5. Transition diffusional/diffusionless growth
- 6. Application to bainite in steel







What determines if a transformation is diffusional or diffusionless?

Thermodynamic limits Kinetic limits







2.Thermodynamic limits

The T_0 line: Thermodynamic limit for diffusionless transformation $\beta \rightarrow \alpha$.

















Deviation from local equilibrium during $\gamma \rightarrow \alpha$ in Fe-C when some extra driving force (undercooling) needed.

- Temperature for start of reaction.
- a) Diffusion control
- b) Diffusionless







3. Kinetic limits

Even if a transformation is thermodynamically possible the kinetics may be such that it cannot occur.

Depends on the balance between the different processes e.g. long-range diffusion and interfacial reactions.

The local state of the migrating phase interface must be understood.





The local state at phase interface

Conventional view:

-atoms jump individually from the parent phase across the phase interface and attach to the growing phase.

Problem: All atoms must have a lower chemical potential in the growing phase. This is not the case during a diffusionless transformation.









4. Modelling of local state at a sharp phase interface

Hillert 1960 (FCC \rightarrow BCC in Fe-C) Aziz 1982 (for solidification) Ågren 1989 (FCC \rightarrow BCC in Fe-C) Olson et al. 1989 (FCC \rightarrow BCC in Fe-C)

Two processes coupled in series at the interface

- change in composition (trans interface diffusion)
- change of crystalline structure (intrinsic interface mobility)





These models all predict:

Diffusion controlled growth at high temperatures (low driving forces) – the growing phase has a different composition.

Transition to diffusionless growth at low temperatures (high driving forces) – the growing phase has the same composition as the parent phase.







Modeling the local state of the moving phase interface

Response functions (Baker and Cahn 1971) For example in a binary system $\gamma \rightarrow \alpha$:

 $f_1(x_{B,}^{\gamma} x_{B,}^{\alpha} v, T) = 0$ $f_2(x_{B,}^{\gamma} x_{B,}^{\alpha} v, T) = 0$

Simplest case: Local equilibrium.

- The interfacial properties do not enter into the problem except for the effect of interfacial energy of a curved interface (Gibbs-Thomson) and the interface velocity does not enter.

$$\Delta \mu_A^{\gamma/\alpha} = \mu_A^{\gamma}(x_B^{\gamma}, T) - \mu_A^{\alpha}(x_B^{\alpha}, T) = 0$$

$$\Delta \mu_B^{\gamma/\alpha} = \mu_B^{\gamma}(x_B^{\gamma}, T) - \mu_B^{\alpha}(x_B^{\alpha}, T) = 0$$



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Deviation from local equilibrium during $\gamma \rightarrow \alpha$ in Fe-C.

Carbon diffuses across interface from α to γ . Driving force for trans-interface diffusion: Driving force for change of crystalline lattice:

All quantities expressed per mole of Fe atoms.

 $z_{C} = N_{C} / N_{Fe} = x_{C} / x_{Fe}$





Trans-interface diffusion



$$J_{C}^{t} = -L_{CC} \left(\mu_{C}^{\gamma/\alpha} - \mu_{C}^{\alpha} \right) = -L_{CC} \Delta \mu_{C}^{\gamma/\alpha}$$

The Gibbs energy dissipation from this process

$$-\dot{G} = -J_C^t \Delta \mu_C^{\gamma/\alpha} = \frac{v}{V_s} \Delta G_{Fe}^t$$

 ΔG_{Fe}^{t} is the driving force for trans-interface diffusion per mole of Fe. Understeadystate at the phase interface: $\Delta G_{Fe}^{t} = -(z_{C}^{\gamma/\alpha} - z_{C}^{\alpha})\Delta \mu_{C}^{\gamma/\alpha}$





Finite interface mobility

The totalavailable chemical driving force is (per mole Fe): $\Delta G_{Fe}^{chem} = \left(\mu_{Fe}^{\gamma/\alpha} - \mu_{Fe}^{\alpha}\right) + z_{C}^{\alpha}\left(\mu_{C}^{\gamma/\alpha} - \mu_{C}^{\alpha}\right) = \Delta \mu_{Fe}^{\gamma/\alpha} + z_{C}^{\alpha}\Delta \mu_{C}^{\gamma/\alpha}$ and the driving force to overcome the finite interface mobility is obtained from: $\Delta G_{Fe}^{chem} = \Delta G_{Fe}^{m} + \Delta G_{Fe}^{t} \quad \text{i.e.} \quad \Delta G_{Fe}^{m} = \Delta G_{Fe}^{chem} - \Delta G_{Fe}^{t} :$ $\Delta G_{Fe}^{m} = \Delta \mu_{Fe} + z_{C}^{\gamma/\alpha}\Delta \mu_{C} = \frac{v}{M}V_{s}$







The response functions become: $f_1(z_C^{\gamma/\alpha}, z_C^{\alpha}, v) = \Delta \mu_C^{\gamma/\alpha}(z_C^{\gamma/\alpha}, z_C^{\alpha}) + \frac{v}{V_s L_{cc}} \left(z_C^{\gamma/\alpha} - z_C^{\alpha} \right) = 0$ $f_2(z_C^{\gamma/\alpha}, z_C^{\alpha}, v) = \Delta \mu_{Fe}^{\gamma/\alpha}(z_C^{\gamma/\alpha}, z_C^{\alpha}) - \frac{v}{V_s} \left(\frac{V_s^2}{M} + \frac{z_C^{\gamma/\alpha}}{L_{cc}} \left(z_C^{\gamma/\alpha} - z_C^{\alpha} \right) \right) = 0$

 $\Delta \mu_{C}^{\gamma/\alpha}(z_{C}^{\gamma/\alpha}, z_{C}^{\alpha})$ and $\Delta \mu_{Fe}^{\gamma/\alpha}(z_{C}^{\gamma/\alpha}, z_{C}^{\alpha})$ may be described by suitable thermodynamic models of the γ and α phase, respectively.

The composition on each side of interface may be calculated for a given interface velocity.

In the limit of very low velocity we recover local equilibrium.







5. Transition diffusional/diffusionless growth



The compositions on each side of the phase interface depend on interface velocity and they approach each other.

$$u_B^{\alpha} = f(T, v) \rightarrow u_B^{\alpha eq} \text{ as } v \rightarrow 0$$
$$u_B^{\gamma} = g(T, v) \rightarrow u_B^{\gamma eq} \text{ as } v \rightarrow 0$$

Above a critical velocity transformation turns partitionless.







Maximum possible growth rate for alloy 1













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Aziz model for transinterface diffusion(1982)

Similar as the previous sharp interface model but:

$$\frac{x_B^{\alpha}}{x_B^{\gamma}} = k_B^{\alpha/\gamma} = \frac{\beta + {}^{eq} k_B^{\alpha/\gamma}}{\beta + 1} \quad \beta = \frac{\nu}{D^i / \lambda}$$

 D^i : diffusivity in interface λ : Thickness of interface



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Calculated limit of the massive transformation in Fe-Ni alloys (dashed lines) calculated for two different assumptions on properties of interface.

(Odqvist et al. 2002)

Exp: Borgenstam and Hillert 2000













Kinetic limit for partitionless transformation





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One conclusion:

It is not possible to have a slow (compared to rate of diffusion) diffusionless reaction, i.e. a diffusionless reaction has to be very fast compared to the rate of diffusion.





6. Application to bainite in steel

- the crystallographic aspects are those of a displacive transformation.
- the microstructure formed at low temperatures looks similar to martensite
 But ...
- The kinetics is much slower and similar to what is expected for C-diffusion control.







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Thermodynamic limit for bainite

1960 – Hillert analyzed experimental growth rates of Widmanstätten ferrite and upper bainite in high-purity Fe-C. He evaluated the temperature where acicular ferrite could start growing.





5



Assume C partitioning:









For alloys assume the same barrier and para equilibrium



Exp. data from Sugimoto et al (2000)

Exp. data from Sugimoto et al (2002)







Conclusions

A reaction that is slow enough to allow diffusion can never be diffusionless.

A displacive reaction can be diffusional or diffusionless.

The bainitic reaction is an example of displacive reaction that is controlled by the rate of carbon diffusion.



