





#### Interphase Precipitation Model

S. Clark, V. Janik, Y. Lan, and S. Sridhar: *ISIJ Int.*, **57**, (2017), 524–532.



#### Modelling of Interphase Precipitation – Experimental Facts

Interphase precipitation refines with reducing interphase velocity. (T. Murakami, H. Hatano, G. Miyamoto, and T. Furuhara: ISIJ Int., 52, (2012), 616–25.)





#### **Prediction of Inter-Sheet Spacing**



H. K. D. H. Bhadeshia: Phys. Status Solidi a-Applied Res., 69, (1982), 745–50.



## **Gibbs Energy Balance Model**



Chemical  
Driving Force  
$$\downarrow \\ \Delta G_m^{\gamma \to \alpha} = \Delta G_m^{diff} + \Delta G_m^{frict}$$

Dissipation Inside the Interphase

H. Chen and S. van der Zwaag: Acta Mater., 72, (2014), 1–12.





G. R. Purdy and Y. J M Bréchet: Acta Metall. Mater., 43, (1995), 3763–74.

## **Gibbs Energy Balance Model**







## **Modelled Inter-sheet Spacing**







#### Prediction of Transformation Kinetics









#### Interphase Precipitation Model

New improvements

Summary

#### Improved GEB Model





Prior  $\gamma\gamma$  Grain Boundary

#### Improved GEB Model







## Intrinsic Mobility of Ledge Risers

$$M_m^{\gamma \alpha^*} = 0.058 exp\left(\frac{-140 \times 10^3}{RT}\right) \quad [mmol. J^{-1} \ s^{-1}]$$

G.P. Krielaart, J. Sietsma, and S. van der Zwaag: Mater. Sci. ..., (1997).



 $\Delta G_m^{frict} = \frac{v_L}{M_m^{\gamma \alpha R}} \approx \frac{v}{M_m^{\gamma \alpha^*}}$ 

Prior  $\gamma\gamma$  Grain Boundary







#### **Case Studies**

Element	Ref. HSLA[wt%]	V HSLA [wt%]
Mn	1.60	1.60
Si	0.20	0.18
v	~	0.20
С	0.038	0.047

Samples were isothermally transformed at 973 [K] for 300 [s]. The austenite grain size was estimated to be  $15.2 \pm 9.6 \ [\mu m]$  and  $12.4 \pm 6.5 \ [\mu m]$ , for the Ref-HSLA and V-HSLA respectively. **Measured using** *in-situ* EBSD.



#### Prior $\gamma\gamma$ Grain Boundary







#### **Adapted GEB Model - Kinetics**





#### Adapted GEB Model - Comparison





#### **Intrinsic Mobility**

$$\Delta G_m^{frict} = \frac{v_L}{M_m^{\gamma \alpha R}} \approx \frac{v}{M_m^{\gamma \alpha^*}}$$

$$M_m^{\gamma \alpha R} = \mathbf{0.58} exp\left(\frac{-140 \times 10^3}{RT}\right) \quad [mmol. J^{-1} s^{-1}]$$





## Improved Model - Possibilities



Combine many 'unit models' to account for factors such as heterogeneous austenite grain size.

# Summary

- 1. A model is presented using the solute drag model of Purdy and Bréchet, the GEB concept, and the theory of the diffusional formation of super-ledges by Bhadeshia.
- 2. Rather the inter-sheet spacing is controlled by a complex interplay between the factors of interfacial energy, interfacial segregation.
- 3. The intrinsic mobility of ledge risers us estimated to be 10 times greater than previously suggested relationships for planar disordered interphases.



