

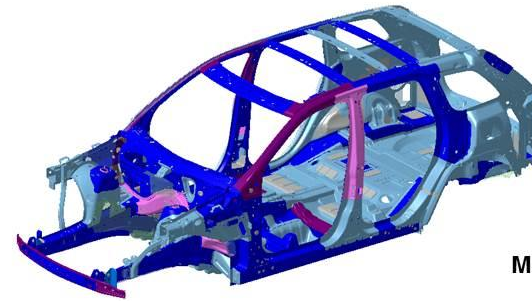
Kinetic of Martensite/austenite interface migration and carbon partitioning during the Q&P process

Zongbiao Dai, Ran Ding,
Zhigang Yang, Chi Zhang, Hao Chen

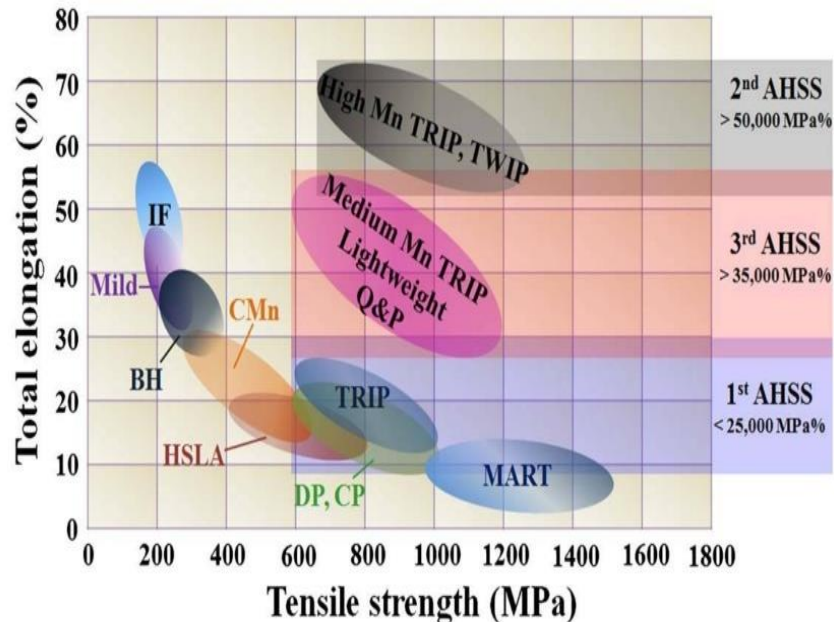
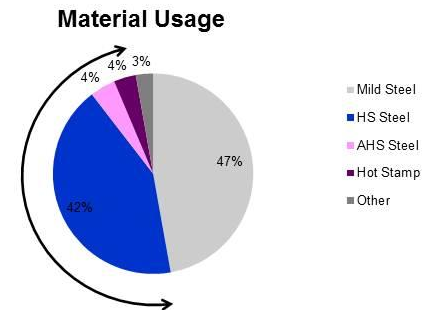
Key laboratory for Advanced Materials of Ministry of Education,
School of Materials Science and Engineering,
Tsinghua University, Beijing 100084, China

2017-06-27

- Vehicle emissions and exhaust
- Fuel consumption
- **Safety and Lightweight**



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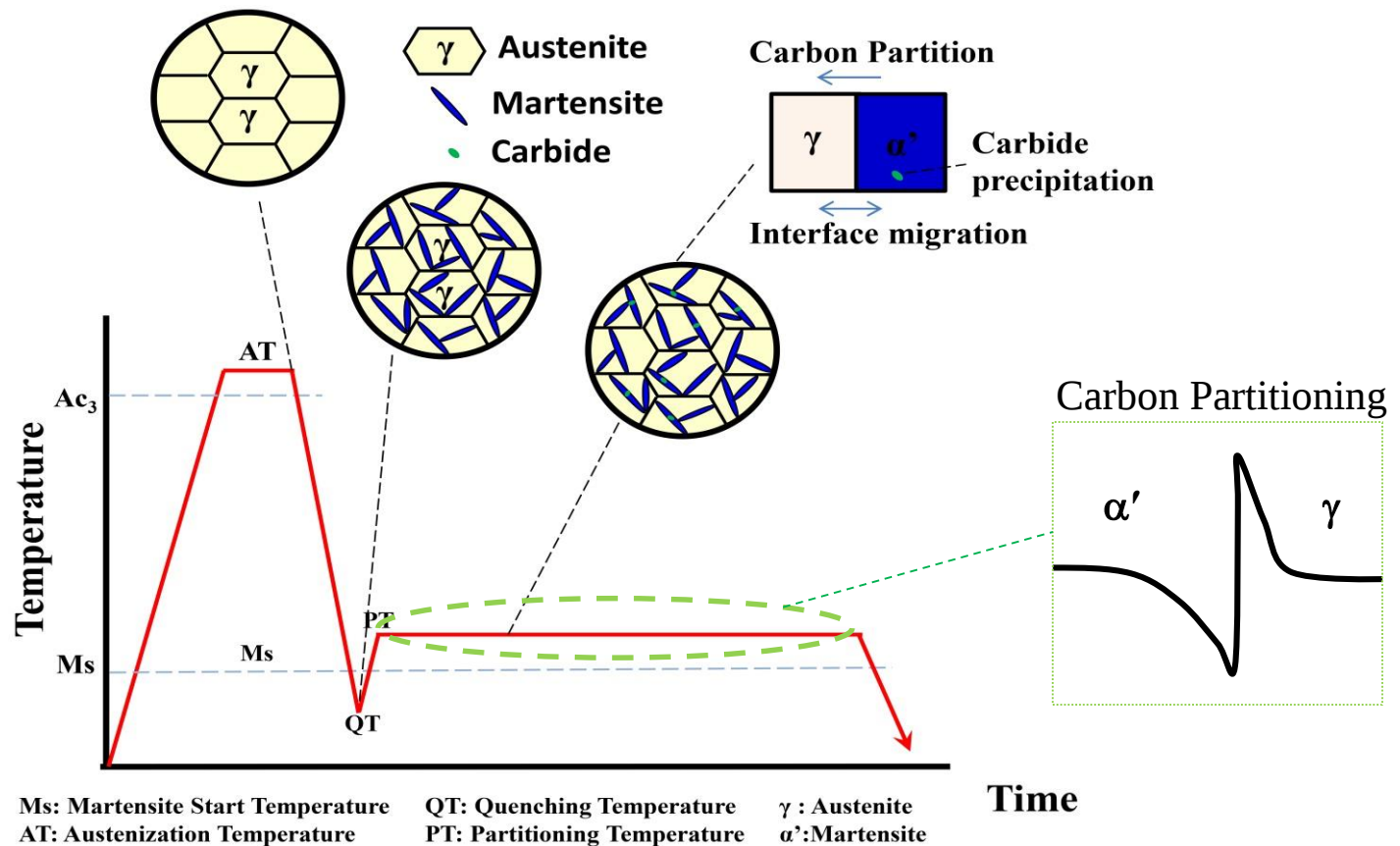
Y.-K. Lee et al. MST, 2015

Retained Austenite

Retained Austenite + Martensite (Q&P)

*Retained Austenite + Ferrite + Bainitic Ferrite
Ferrite + Martensite*

Quenching & Partitioning Process



Scientific questions:

1. Is the α'/γ interface mobile or not? How?
2. Is there partitioning of substitutional alloying elements during the Q&P process?
3. Will partitioning of substitutional alloying elements affect the interface migration and carbon partitioning?

□ Immobile Interface : (*CCE Theory*)

- Toji et al, Acta Mater., 65 (2014) 215
- Seo et al, Acta Mater., 107 (2016) 354
- Seo et al, Acta Mater., 113 (2016) 124
- Bigg et al, JAC, 577S (2013) 695
- Thomas et al, MST, 30 (2014) 998

• • •

□ Mobile Interface :

- Zhong et al, JMST, 22 (2006) 751.

□ Interface migrates from BCC to FCC:

- Santofimia et al, MSEA, 527 (2010)
- Santofimia et al, Acta Mater., 59 (2011)
- Allain et al, Scripta Mater., 131 (2017)

• • •

□ Interface migrates from FCC to BCC:

- De Knijf et al, Acta Mater., 90 (2015)
- Thomas et al, MST, 30 (2014) 998

Dilatometer

Dilatometer

Dilatometer

In-situ Neutron diffractometry

EBSD

Ex-situ TEM

Dilatometer

Dilatometer

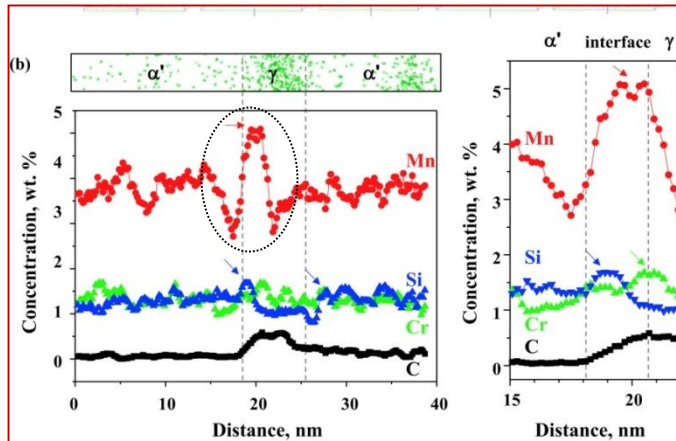
In-situ HE-XRD

In-situ HR-TEM

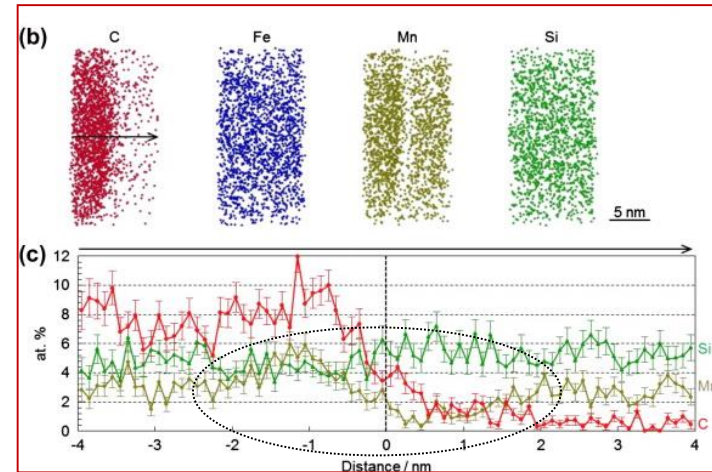
EBSD

Complex and Controversial !

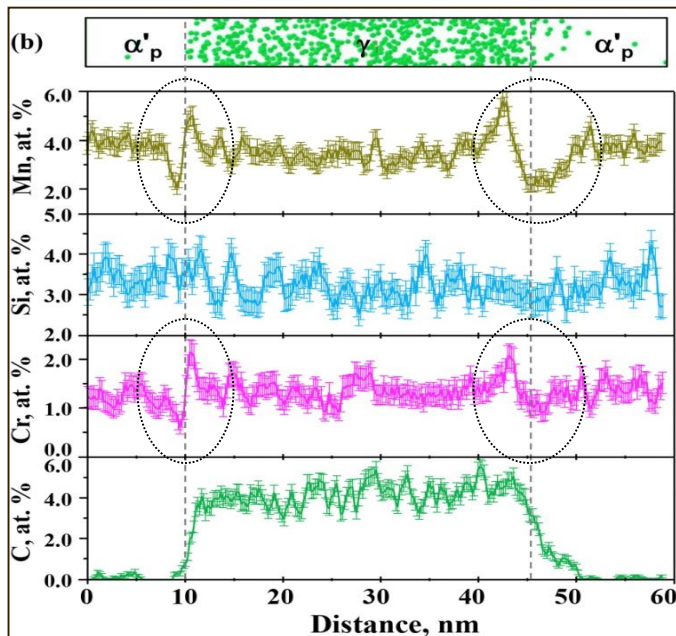
Mn and Cr Partition or not?!



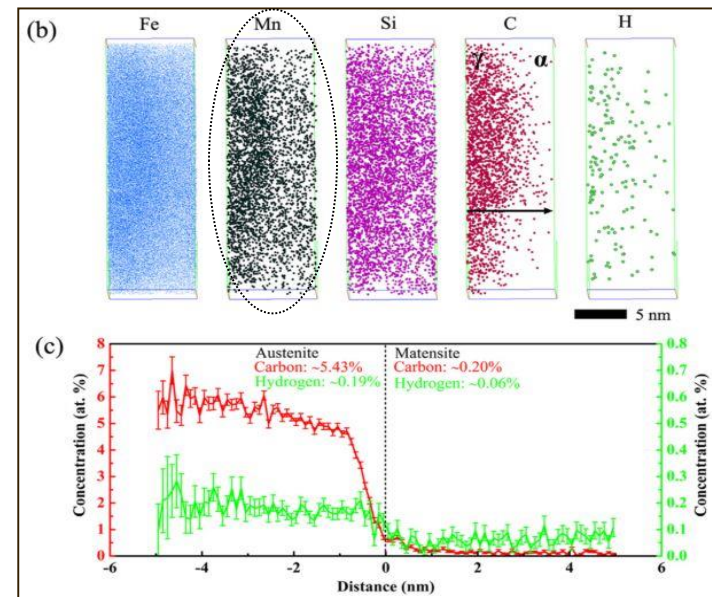
Seo et al. *Acta Mater.*, 2016



Toij et al. *Acta Mater.*, 2014



Seo et al. *Acta Mater.*, 2016



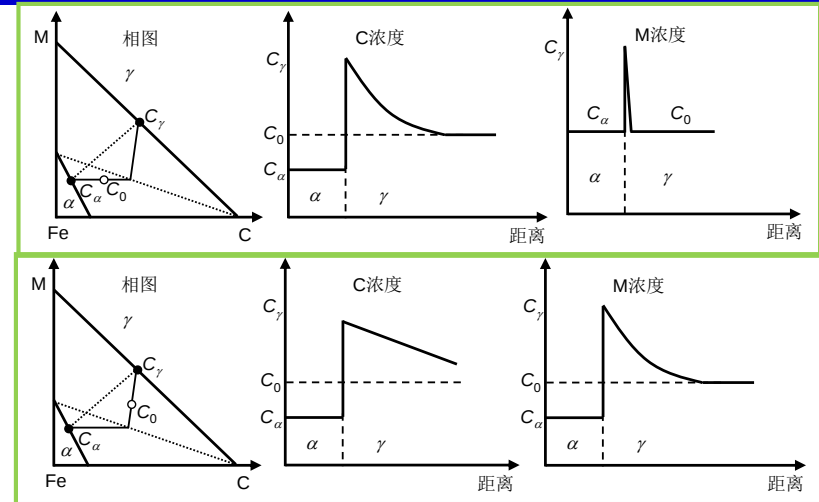
Zhu et al. *Int. J. Hydrogen Energy*, 2014

Models

LE--Local equilibrium:

$$\mu_i^\gamma = \mu_i^\alpha$$

NP-LE :
C diffusion controlled



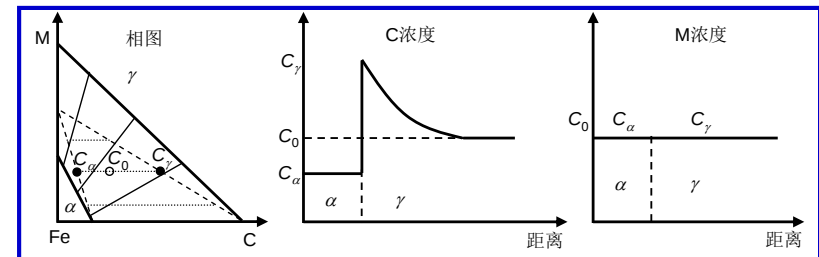
P-LE :
M diffusion controlled

PE--Paraequilibrium:

$$\mu_C^\gamma = \mu_C^\alpha$$

$$(\mu_M^\gamma - \mu_M^\alpha) = -\frac{X_{Fe}}{X_M} (\mu_{Fe}^\gamma - \mu_{Fe}^\alpha)$$

PE :
C diffusion
Mn indiffusible

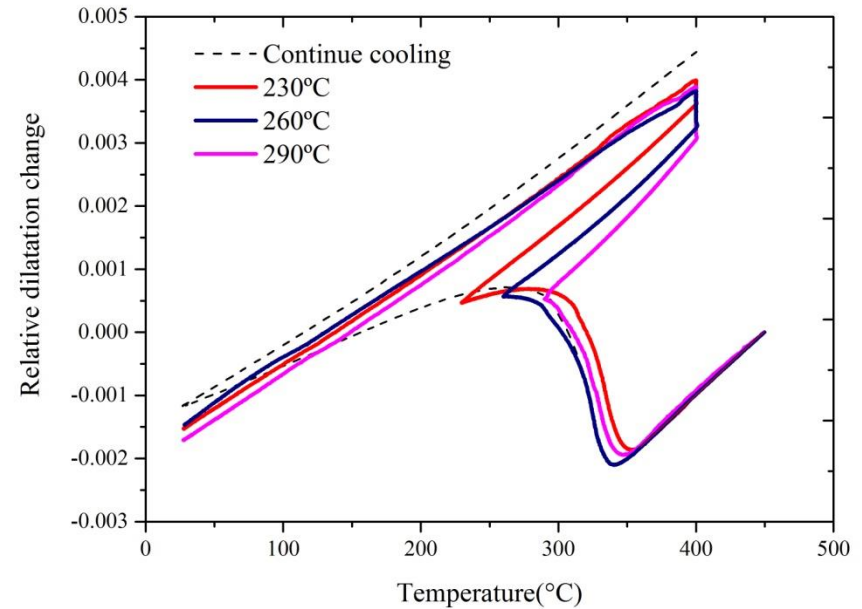
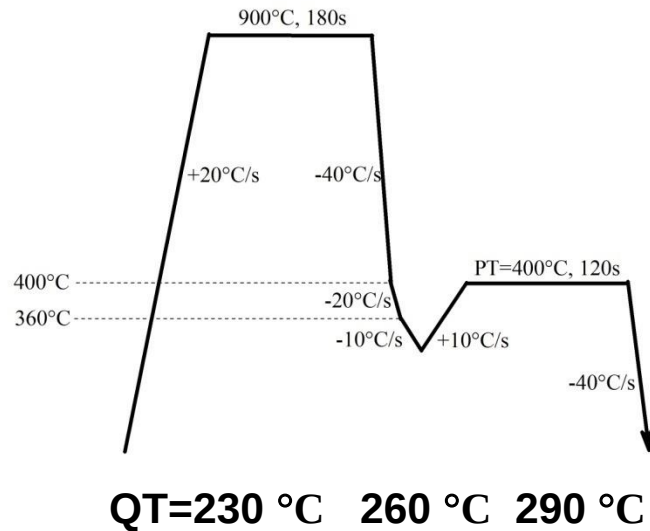


CCE—Constrain Carbon Equilibrium:

$$\mu_C^\gamma = \mu_C^\alpha$$

Martensite/austenite interface is immobile

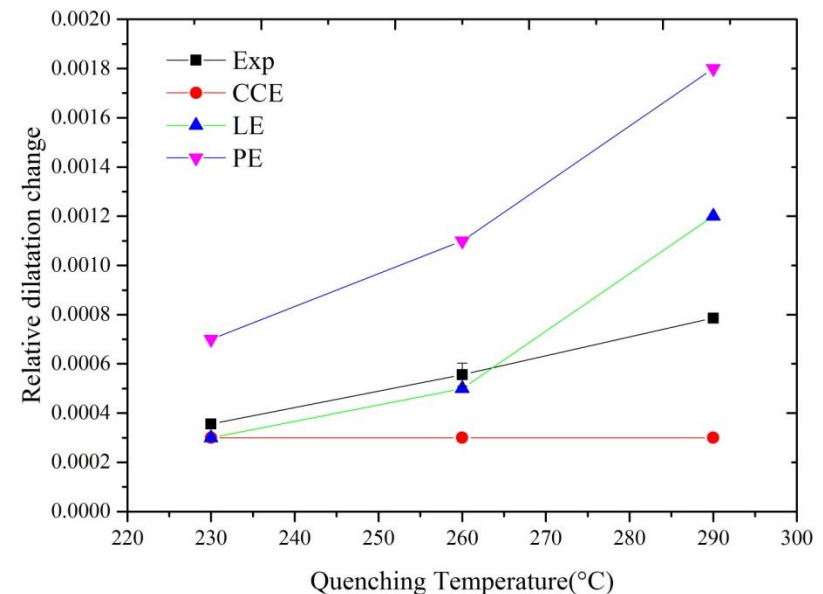
Fe-0.25C-2.1Mn-1.1Si (wt.%)



Calculation of relative dilatation strain:

$$\frac{\Delta L}{L_0} = \frac{L - L_0}{L_0} \approx \frac{1}{3} \frac{V - V_0}{V_0}$$

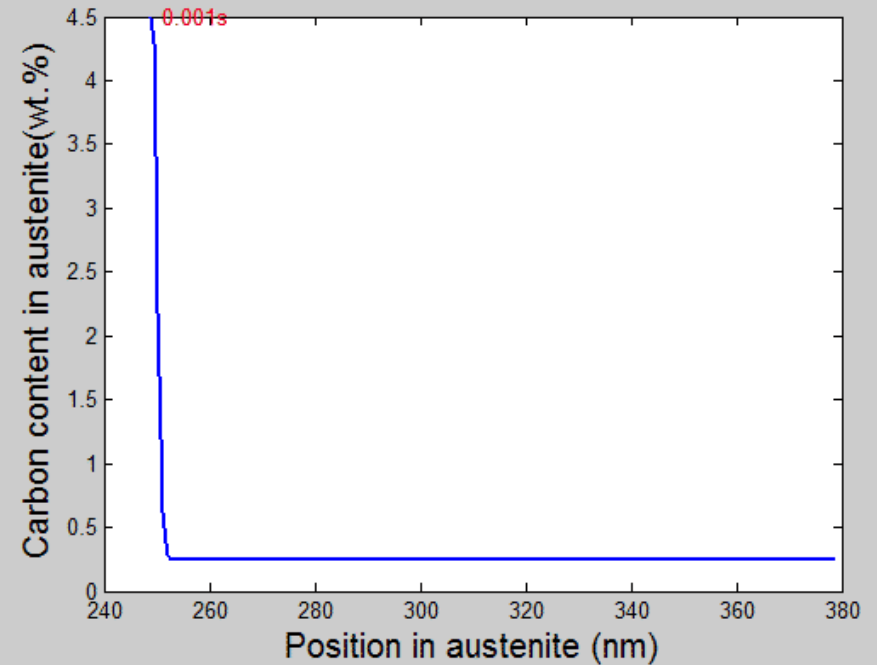
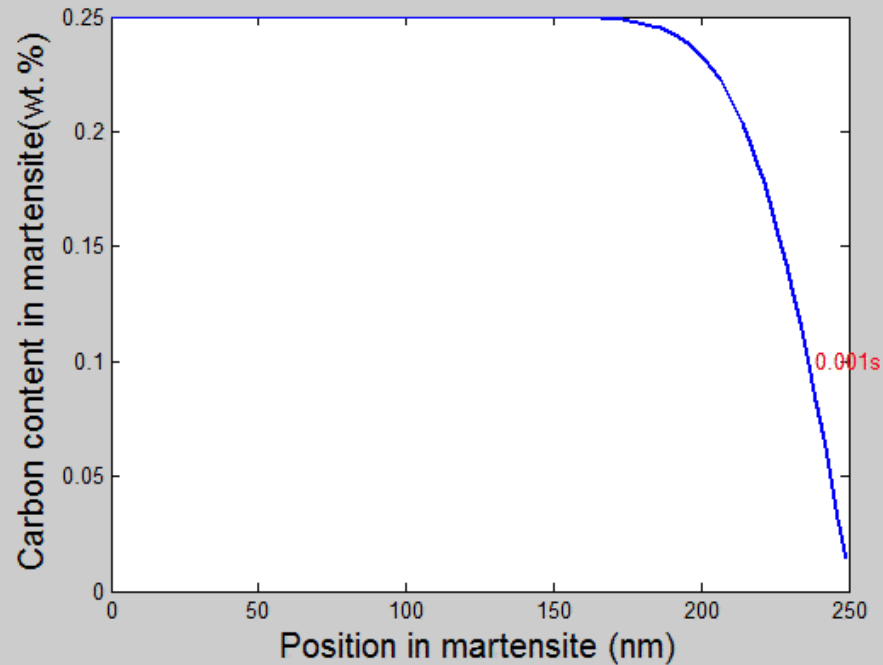
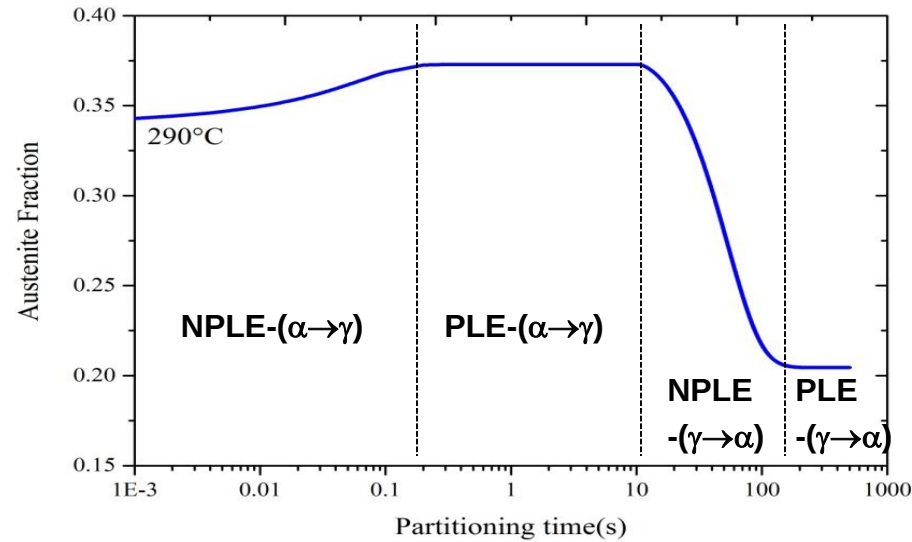
$$\frac{\Delta L}{L_0} = \frac{2V_{\alpha'}(1-x_C^{\alpha'})a_{\alpha'}^2c_{\alpha'} + [1-V_{\alpha'} - (x_{C0}^{\gamma} - V_{\alpha'}x_C^{\alpha'})]a_{\gamma}^3 - (1-x_{C0}^{\gamma})a_{\gamma 0}^3}{3(1-x_{C0}^{\gamma})a_{\gamma 0}^3}$$



Case for martensite growth

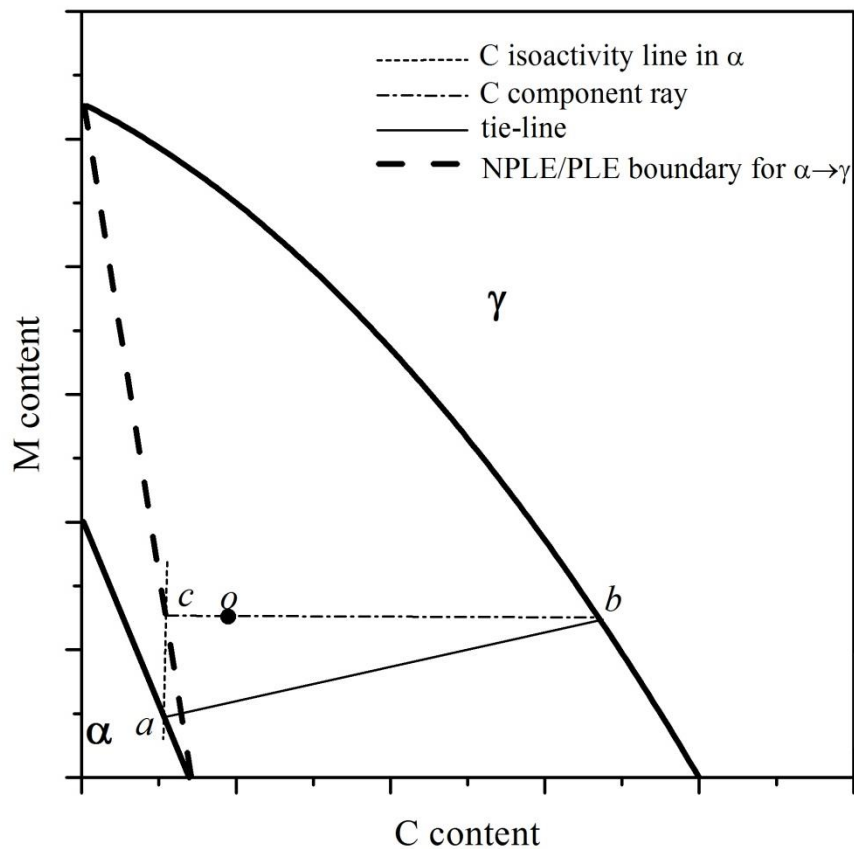
QT=290°C

PT=400°C



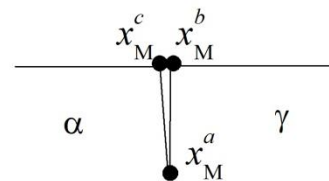
Case for martensite growth

Stage I: NPLE-($\alpha \rightarrow \gamma$)

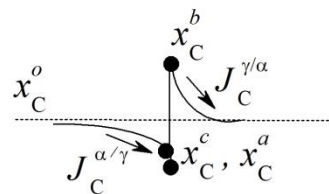


a)

NPLE Mode:



M Profile



C Profile

$$v = \frac{J_C^{\gamma/\alpha} - J_C^{\alpha/\gamma}}{x_C^{\gamma/\alpha} - x_C^{\alpha/\gamma}}$$

$$J_i^\phi = - \frac{D_i^\phi x_i^\phi}{RT} \nabla \mu_i^\phi$$

$$x_C^{\alpha'} = x_C^\gamma = x_{C0}$$

$$\nabla \mu_C^\alpha > \nabla \mu_C^\gamma$$

$$D_C^\alpha \square D_C^\gamma$$

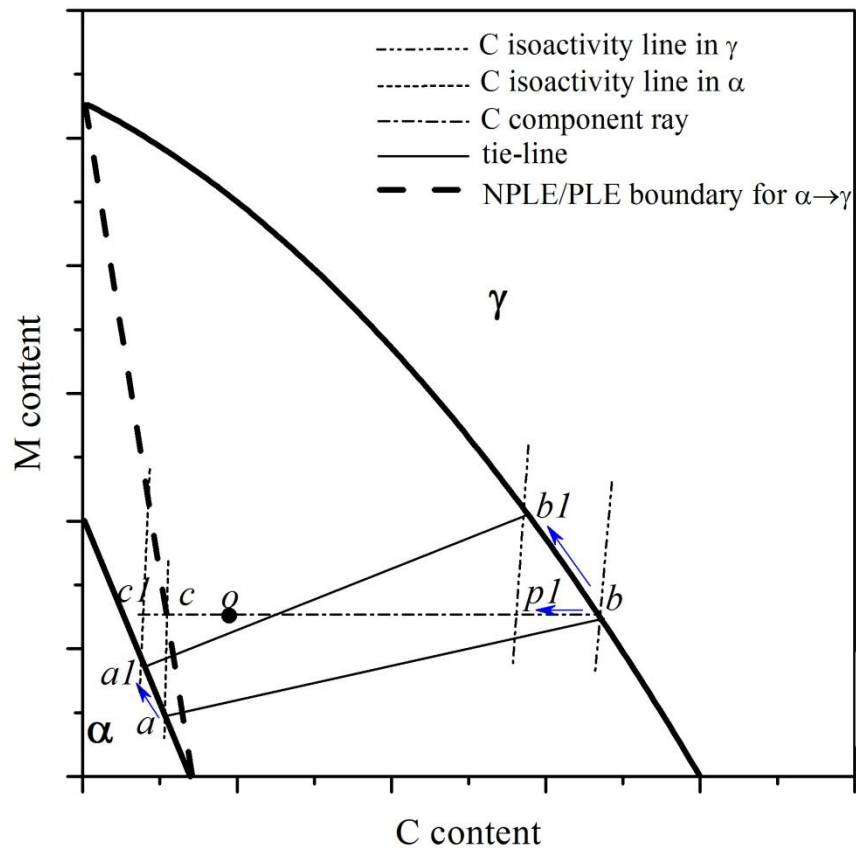
$$J_C^{\alpha/\gamma} \square J_C^{\gamma/\alpha}$$

$$v = \frac{J_C^{\gamma/\alpha} - J_C^{\alpha/\gamma}}{x_C^{\gamma/\alpha} - x_C^{\alpha/\gamma}} \approx - \frac{J_C^{\alpha/\gamma}}{x_C^{\gamma/\alpha}}$$

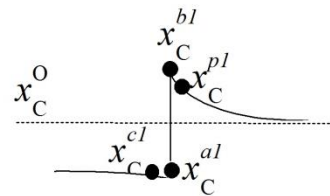
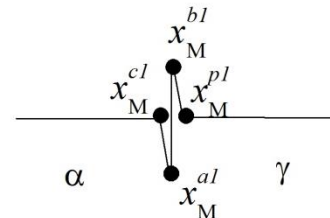
Controlled by Carbon diffusion in martensite

Case for martensite growth

Stage II: PLE-($\alpha \rightarrow \gamma$)



PLE Mode:



$$J_C^{\alpha/\gamma} \downarrow$$

$$J_C^{\gamma/\alpha} - J_C^{\alpha/\gamma} \approx 0$$

$$v = \frac{J_C^{\gamma/\alpha} - J_C^{\alpha/\gamma}}{x_C^{\gamma/\alpha} - x_C^{\alpha/\gamma}} \approx 0$$

$$v \approx 0$$

$$D_{Mn}^{\alpha} \square D_{Mn}^{\gamma}$$

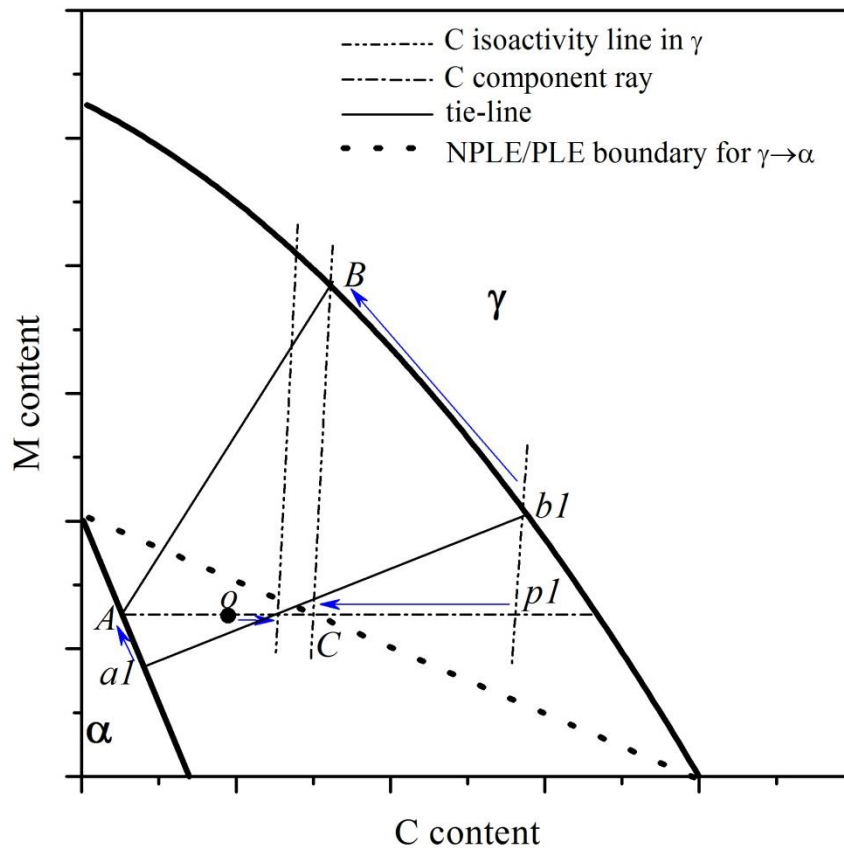


Mn spike in martensite decrease : $aa1$ line

Mn spike in austenite is built up : $bb1$ line

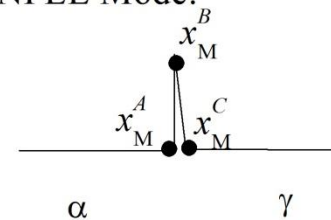
Case for martensite growth

Stage III: NPLE-($\gamma \rightarrow \alpha$)



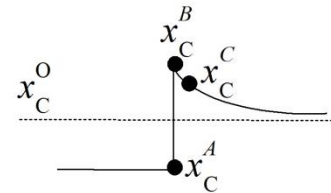
c)

NPLE Mode:



M Profile

$$v = \frac{J_C^{\gamma/\alpha} - J_C^{\alpha/\gamma}}{x_C^{\gamma/\alpha} - x_C^{\alpha/\gamma}} \approx \frac{J_C^{\gamma/\alpha}}{x_C^{\gamma/\alpha}}$$

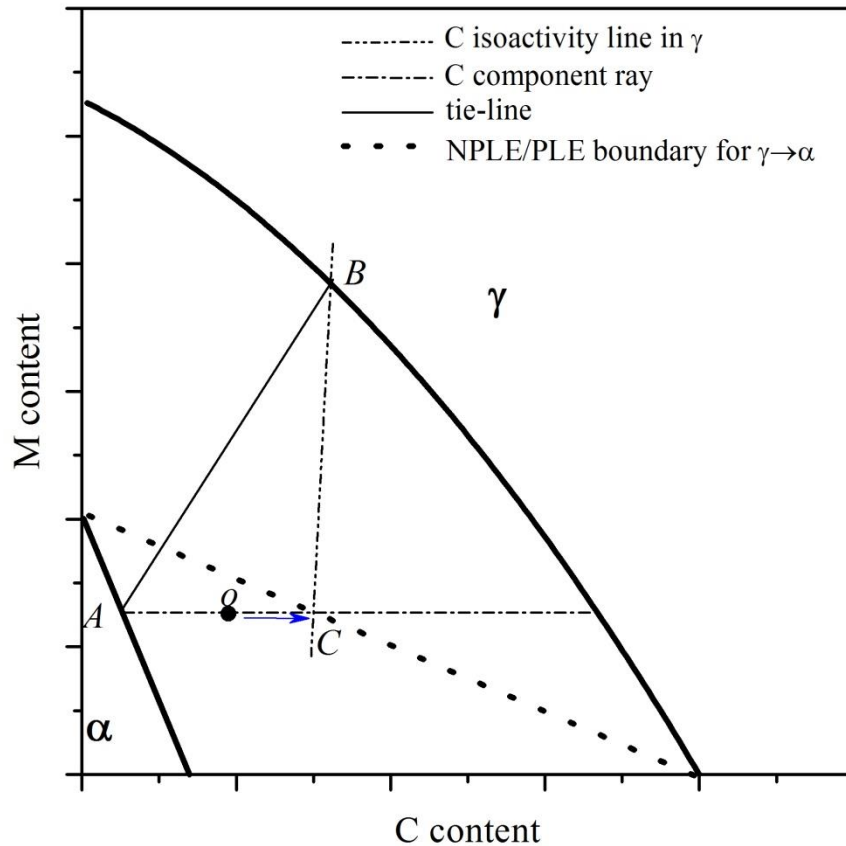


C Profile

Controlled by Carbon diffusion in austenite

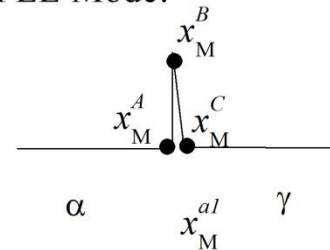
Case for martensite growth

Stage IV: PLE-($\gamma \rightarrow \alpha$)

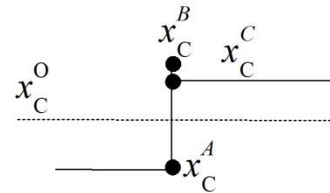


d)

PLE Mode:



M Profile



C Profile

$$J_C^{\gamma/\alpha} \downarrow$$

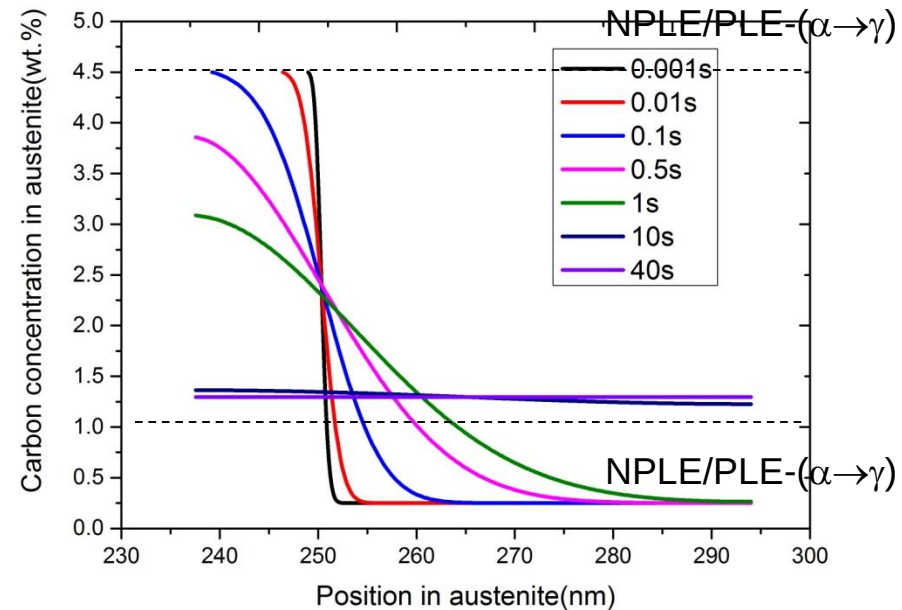
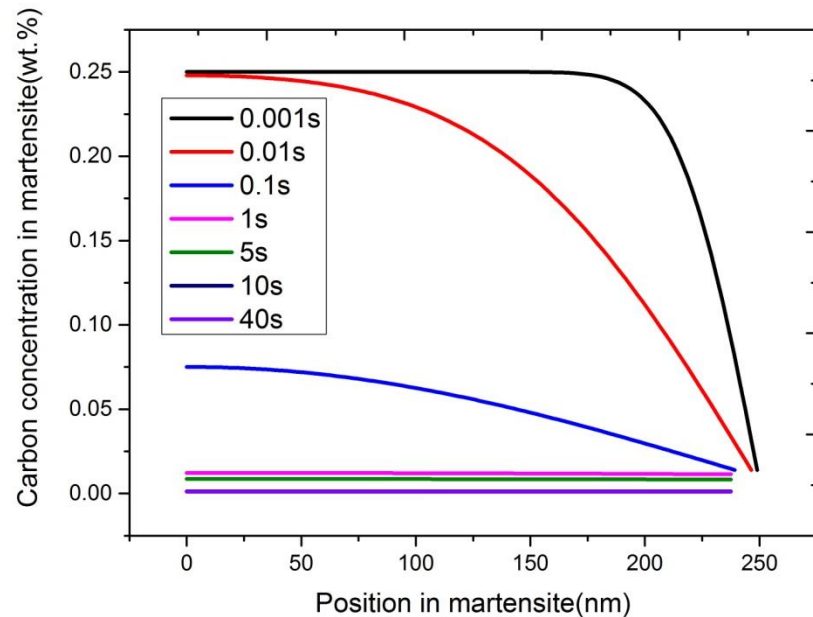
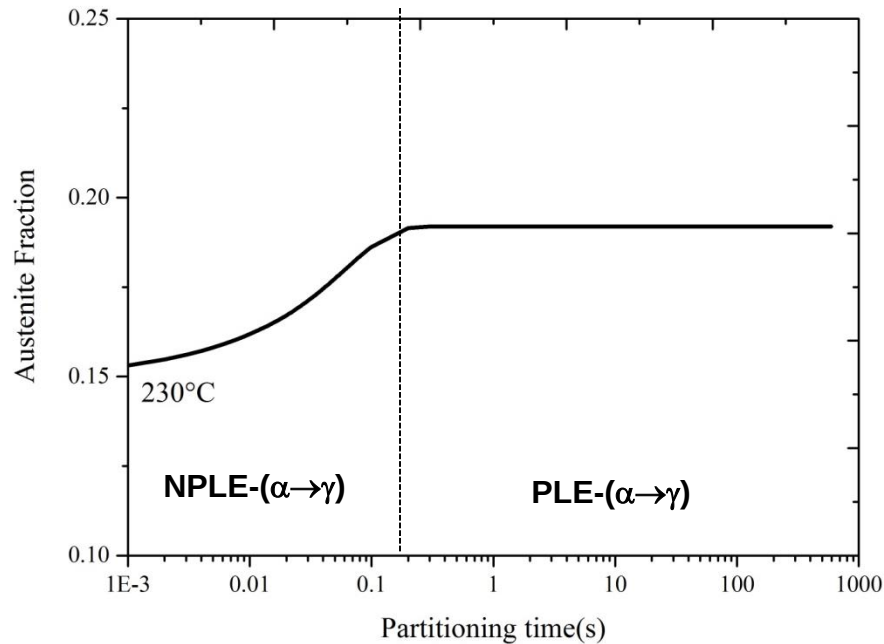
$$J_C^{\gamma/\alpha} \approx 0$$

$$v = \frac{J_C^{\gamma/\alpha} - J_C^{\alpha/\gamma}}{x_C^{\gamma/\alpha} - x_C^{\alpha/\gamma}} \approx 0$$

Carbon concentration in austenite will be determined by NPLE/PLE-($\gamma \rightarrow \alpha$) (i.e. Point C)

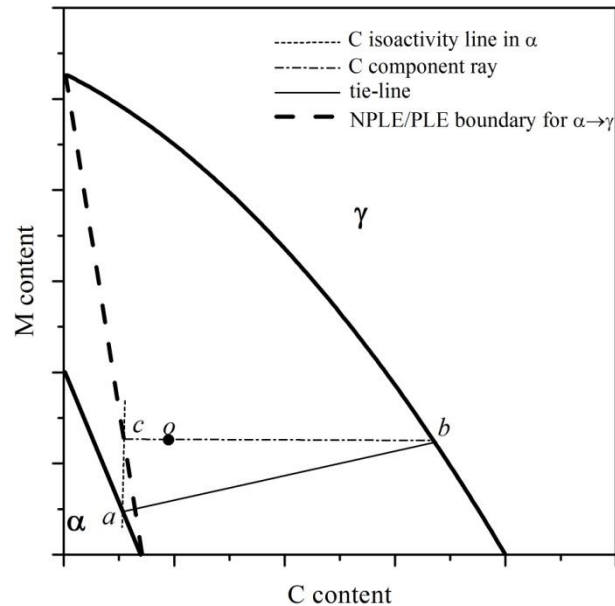
Case for Immobile interface

QT=230°C



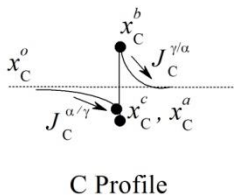
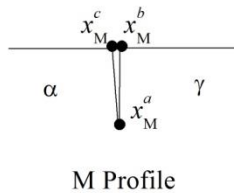
Case for Immobile interface

Stage I: NPLE-($\alpha \rightarrow \gamma$)

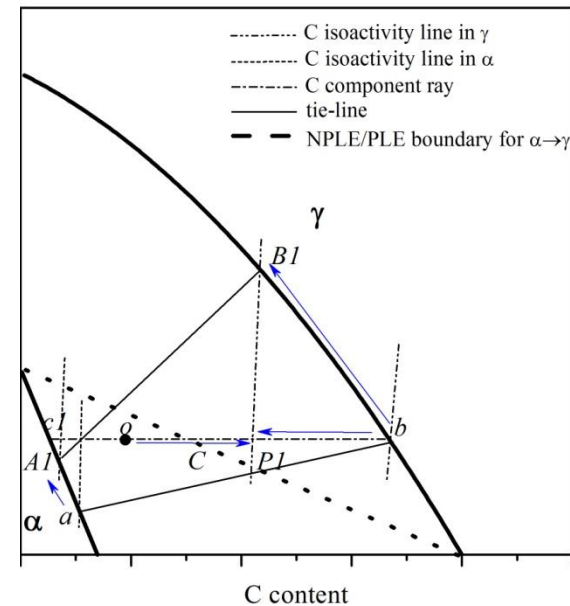


a)

NPLE Mode:

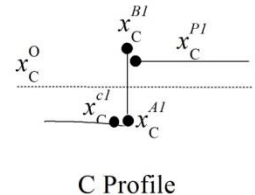
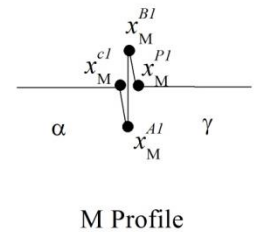


Stage II: PLE-($\alpha \rightarrow \gamma$)

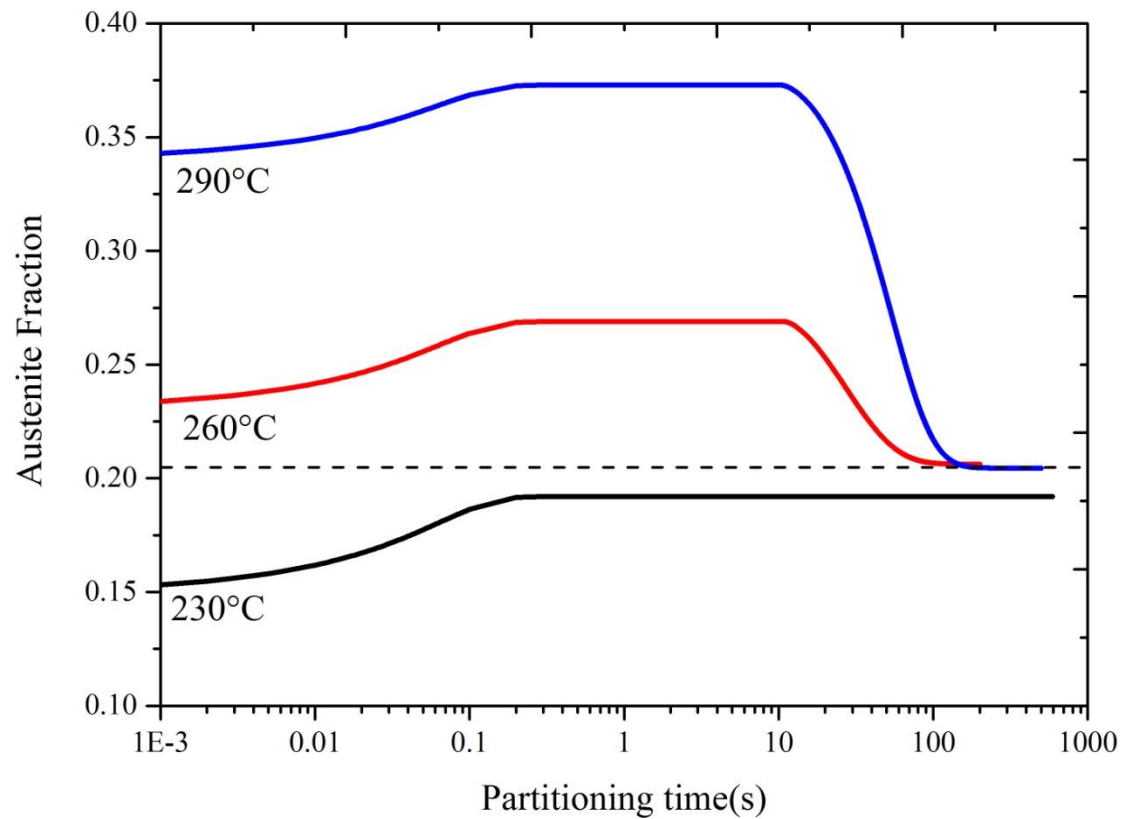


b)

PLE Mode:



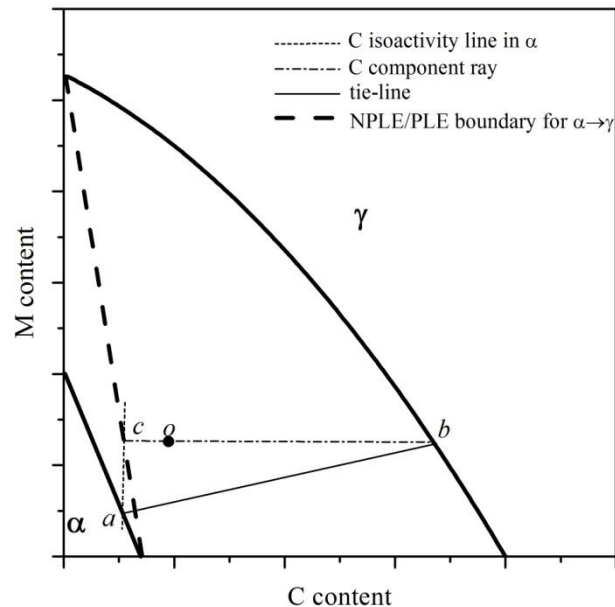
Carbon concentration in austenite (Point P1) will be located between NPLE/PLE-($\alpha \rightarrow \gamma$) (i.e. Point b) and NPLE/PLE-($\gamma \rightarrow \alpha$) (i.e. Point C)





Extreme cases for austenite growth

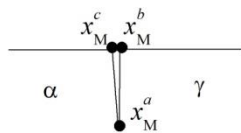
Stage I: NPLE-($\alpha \rightarrow \gamma$)



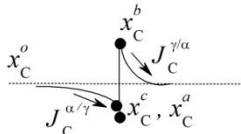
a)

$$v = \frac{J_C^{\gamma/\alpha} - J_C^{\alpha/\gamma}}{x_C^{\gamma/\alpha} - x_C^{\alpha/\gamma}} \approx - \frac{J_C^{\alpha/\gamma}}{x_C^{\gamma/\alpha}}$$

NPLE Mode:

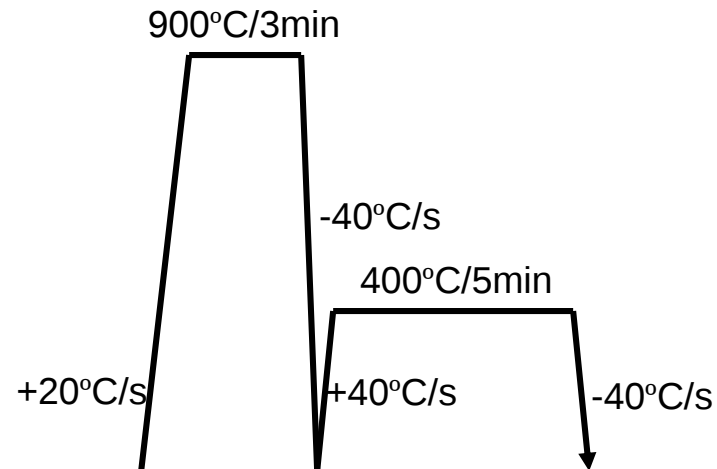


M Profile



C Profile

Fe-**0.59C**-2.9Mn-2.0Si (wt.%)



QT=Room temperature

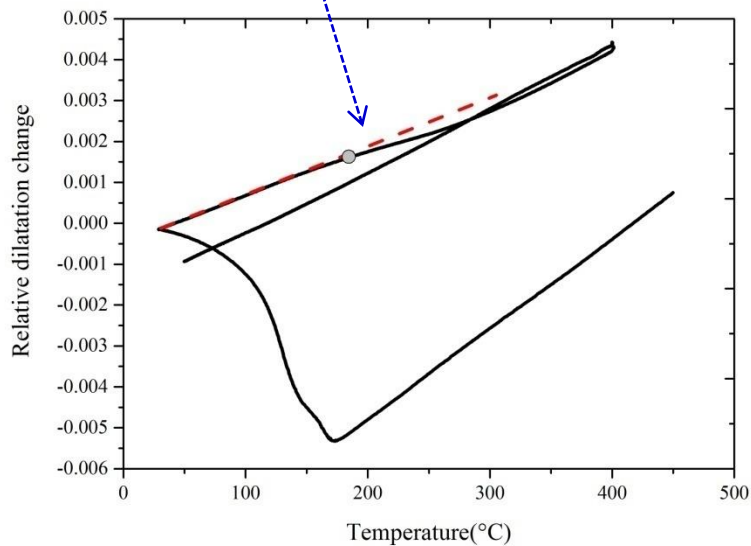
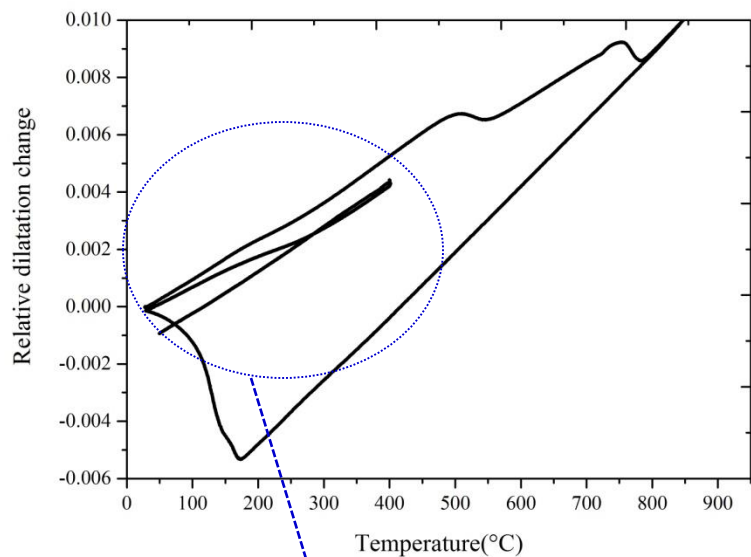
$V_\gamma \approx 8\%$ at QT

Controlled by Carbon diffusion in martensite

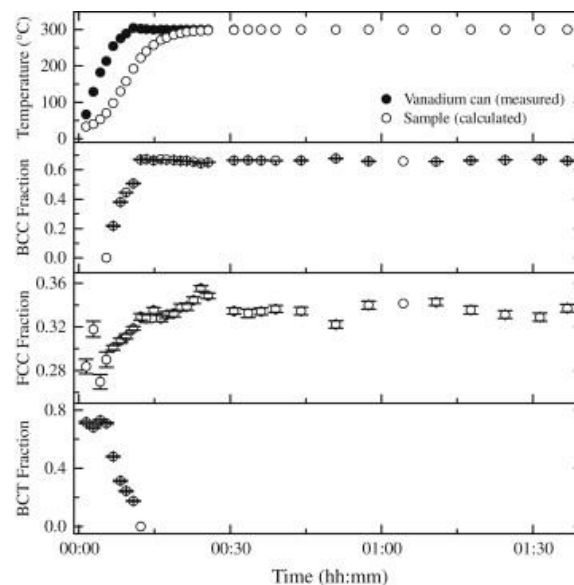


Extreme cases for austenite growth

Fe-0.59C-2.9Mn-2.0Si (wt.%)

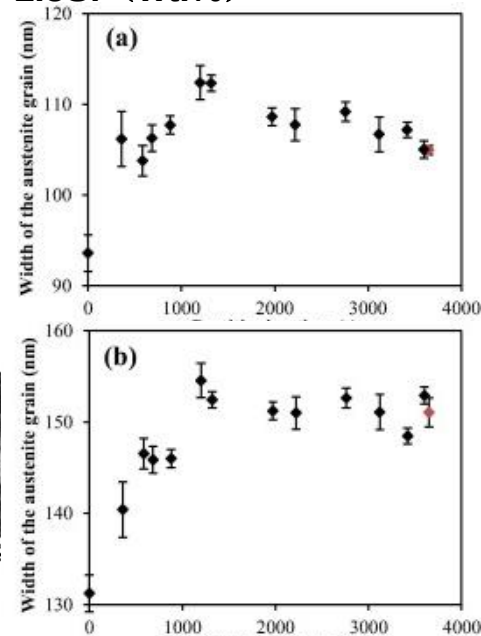
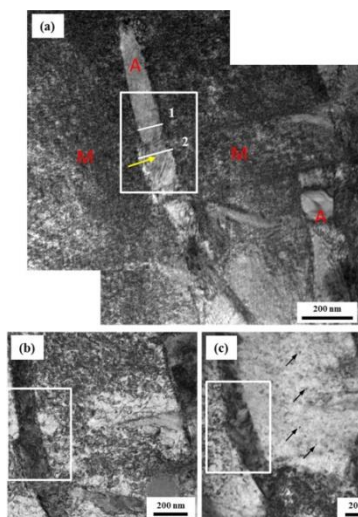


Fe-0.64C-4.57Mn-1.3Si (wt.%)



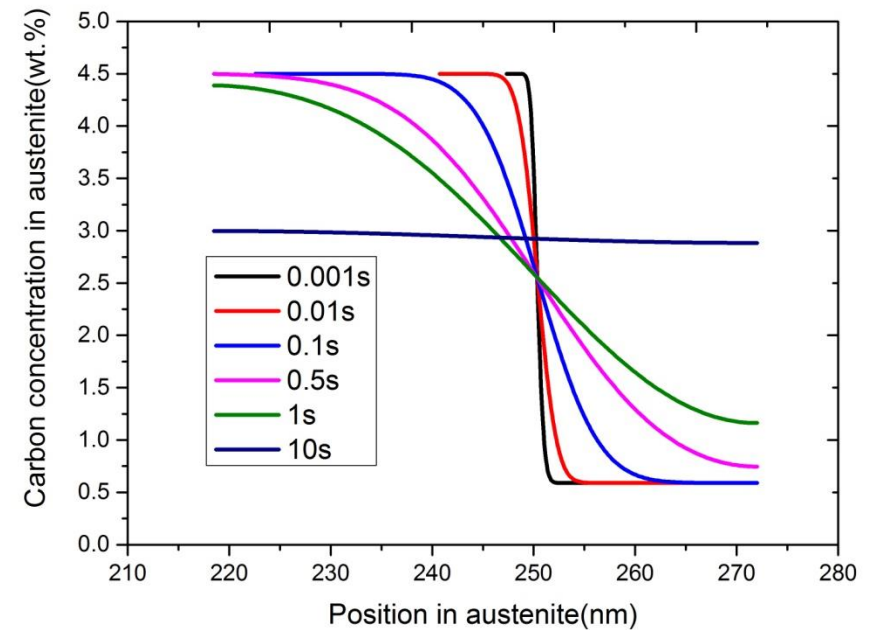
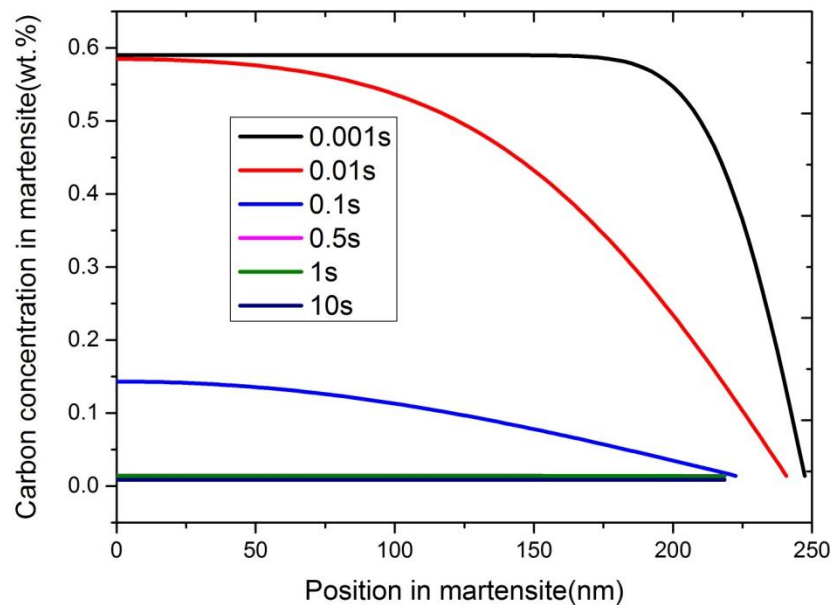
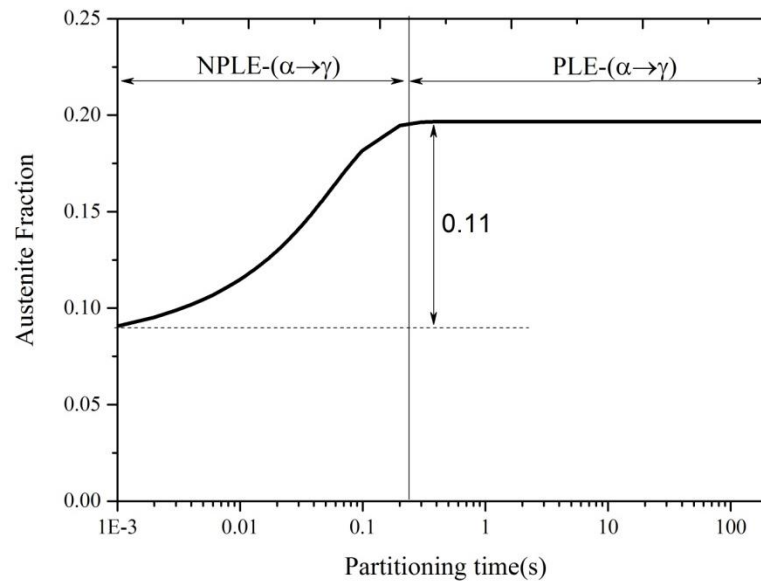
Bigg et al.
JAC
2013

Fe-1.0C-3.0Mn-1.5Si (wt.%)



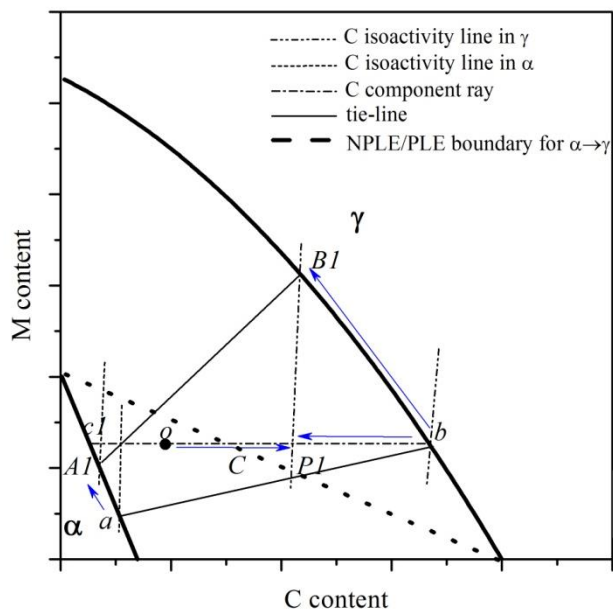
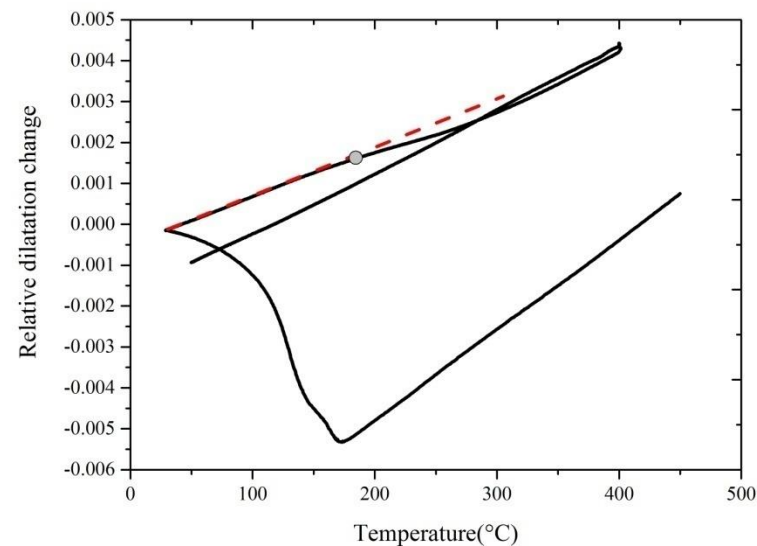
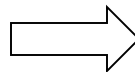
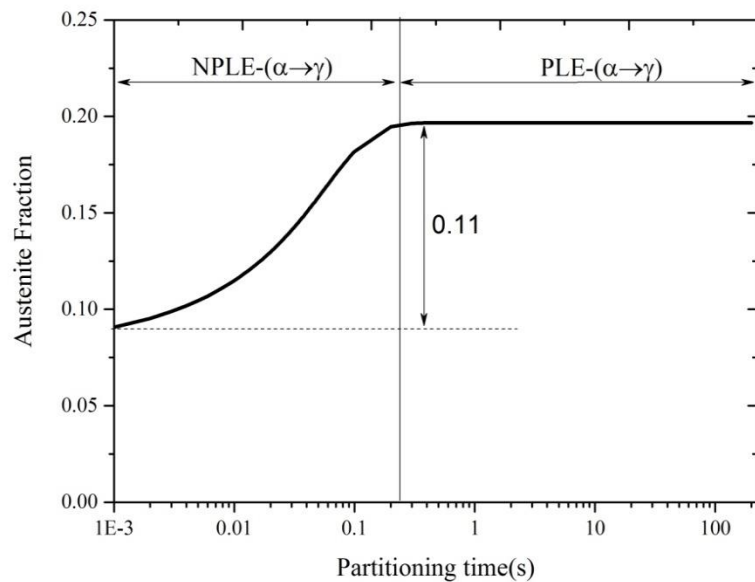
De Knijf et al.
Acta Mater.
2015

Extreme cases for austenite growth

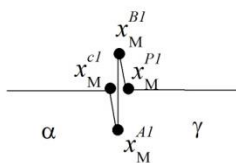




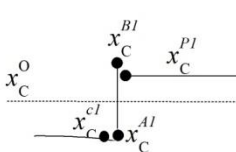
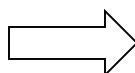
Extreme cases for austenite growth



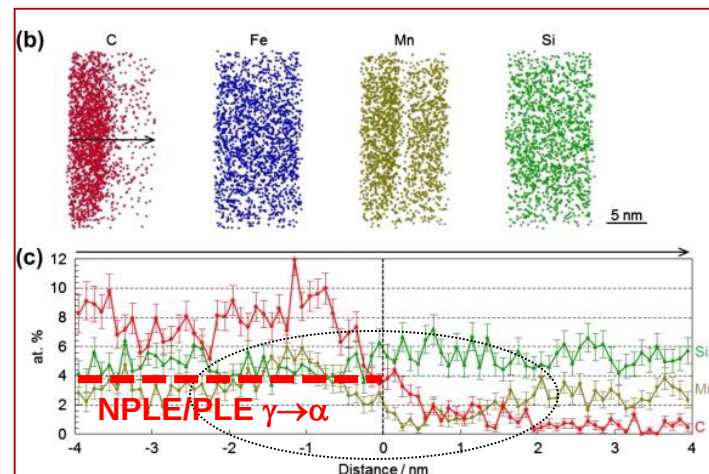
PLE Mode:



M Profile



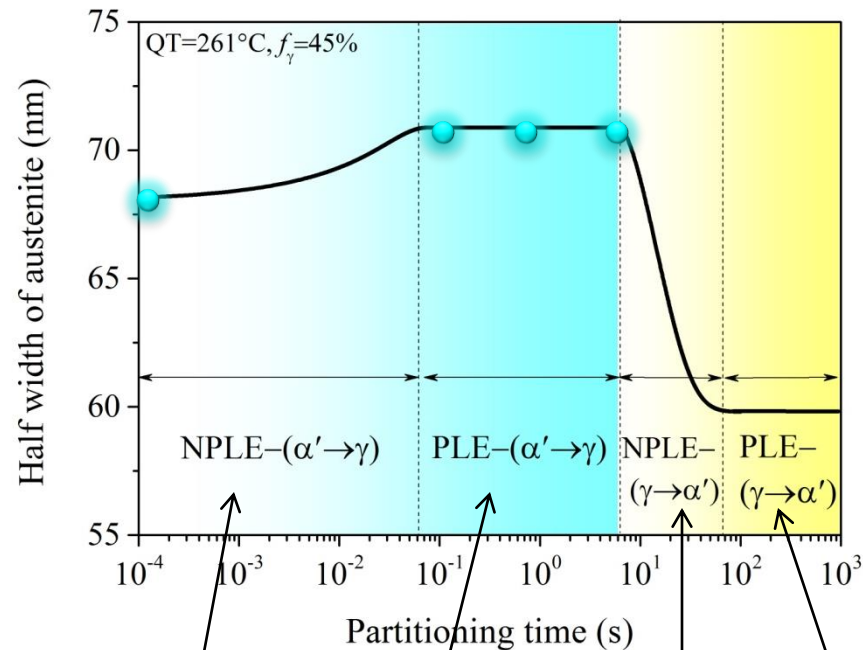
C Profile



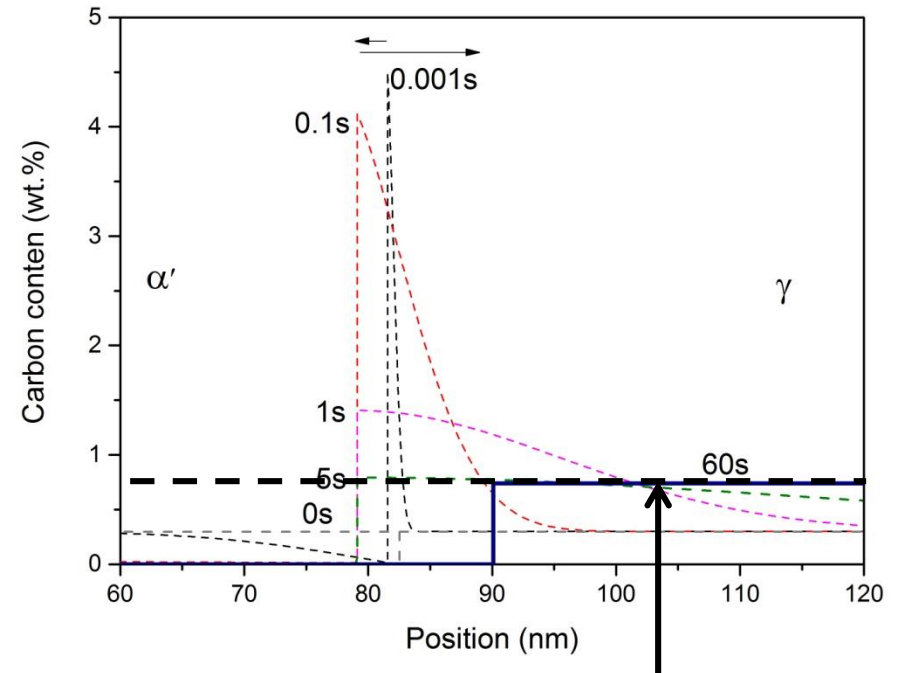
- ❑ Interfacial partitioning of substitutional alloying elements plays a significant role in interface migration behavior and C content in austenite.
- ❑ Kinetics of interface migration. Based on the LE model, the kinetics of interface migration can be generally divided into four stages: $\text{NPLe}-(\alpha' \rightarrow \gamma) \rightarrow \text{PLE}-(\alpha' \rightarrow \gamma) \rightarrow \text{NPLe}-(\gamma \rightarrow \alpha') \rightarrow \text{PLE}-(\gamma \rightarrow \alpha')$. Presence of the $\gamma \rightarrow \alpha'$ stages or not depends on QT.
- ❑ Alloying elements partitioning. After the partitioning process, C content in austenite could be located between the NPLe/PLE boundaries for the $\gamma \rightarrow \alpha'$ and $\alpha' \rightarrow \gamma$ transformation. Substitutional alloying elements partitioning across the interface is predicted to occur.

Thank You !

QT=261°C ($f_\gamma=45\%$), PT=400 °C

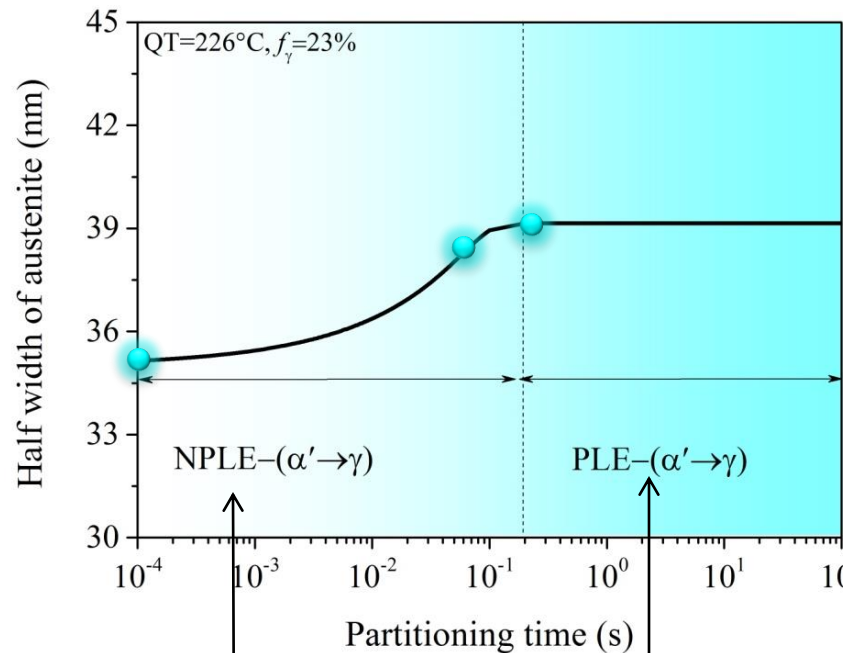


C diffusion in α' controlled Mn/Si diffusion in α' controlled C diffusion in γ controlled Mn/Si diffusion in γ controlled



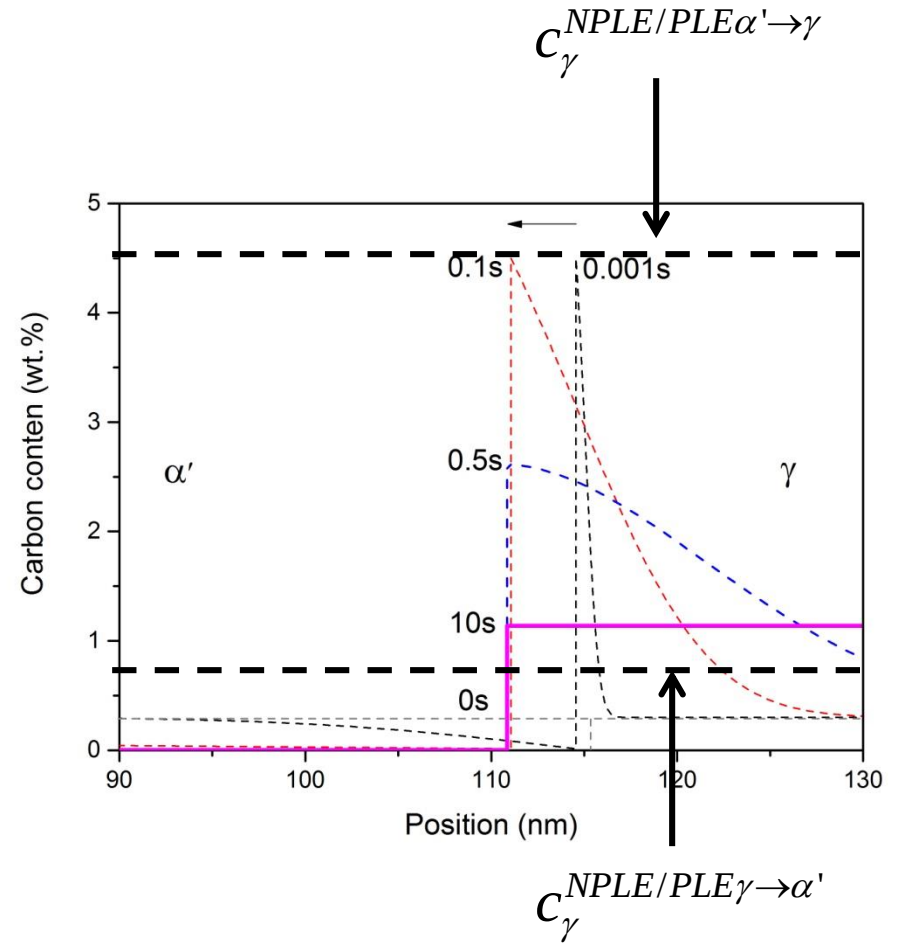
$C_\gamma^{NPLe/PLE \gamma \rightarrow \alpha'}$

QT=226°C ($f_\gamma=23\%$), PT=400 °C

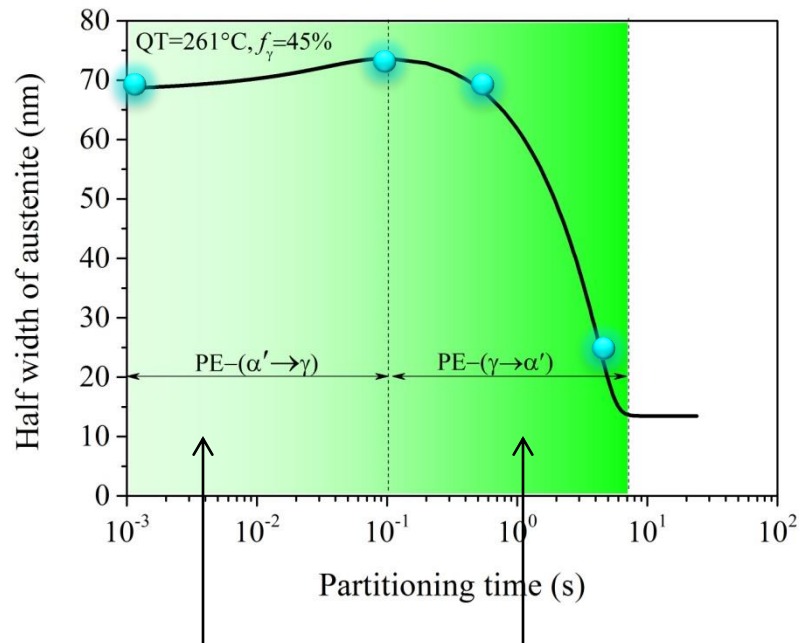


C diffusion
in α' controlled

Mn/Si diffusion
in α' controlled

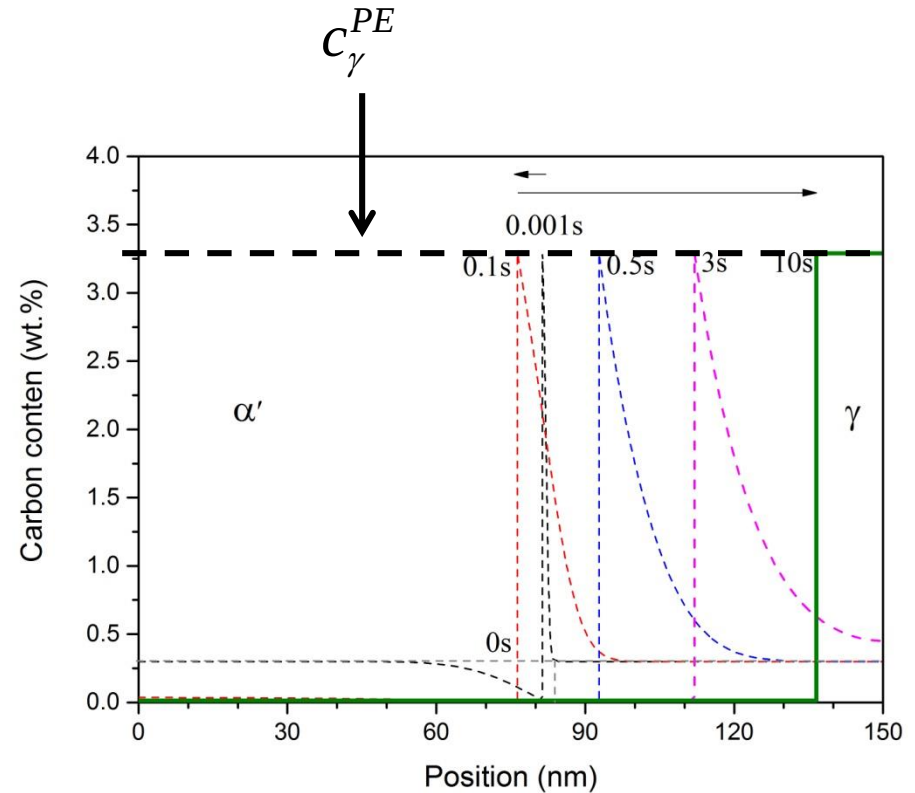


QT=261 °C, PT=400 °C

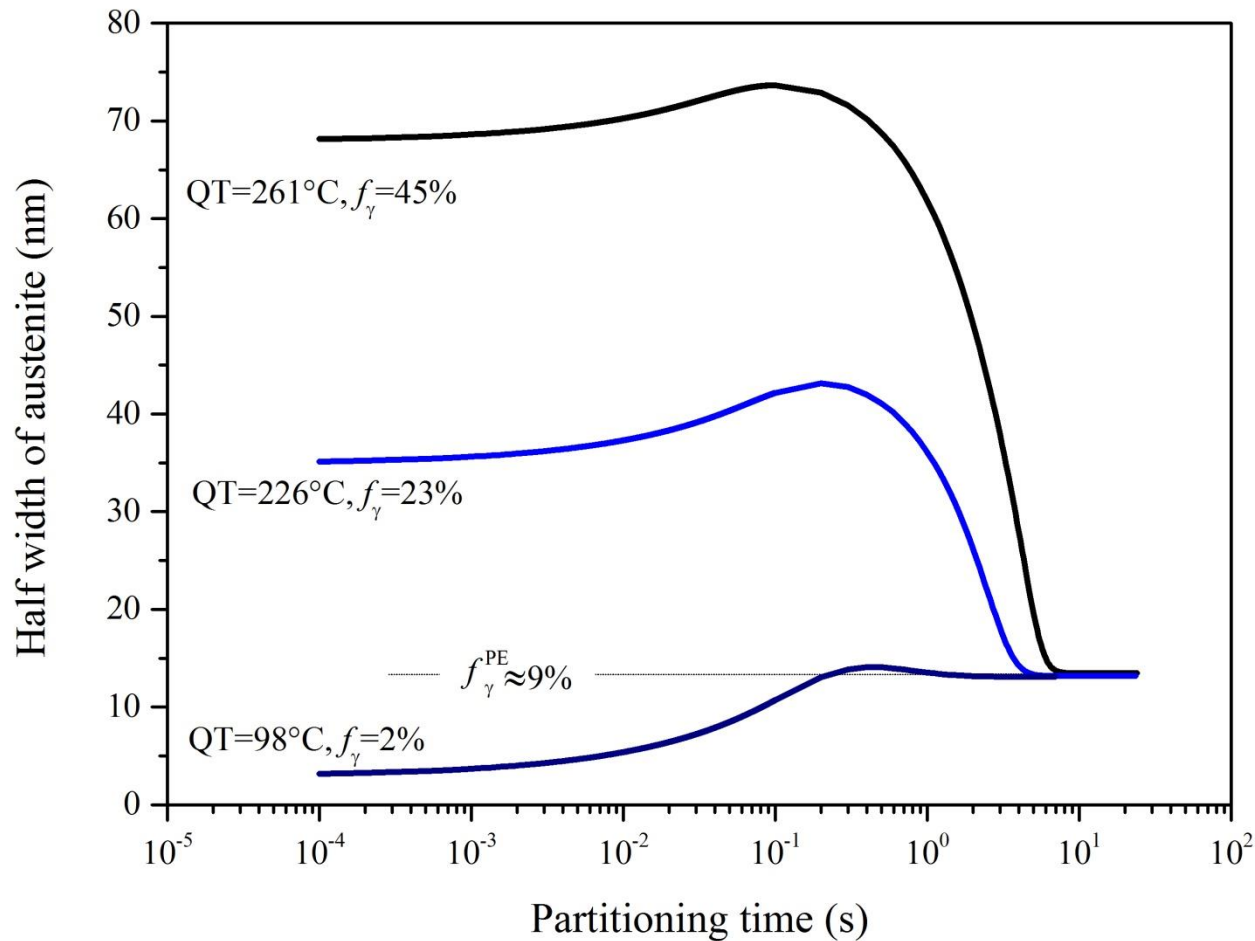


C diffusion
in α' controlled

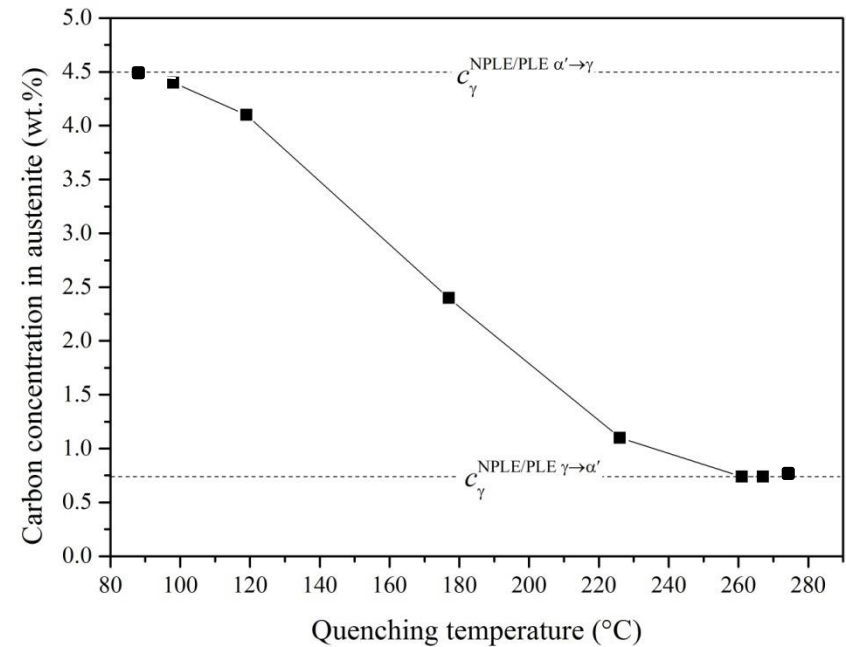
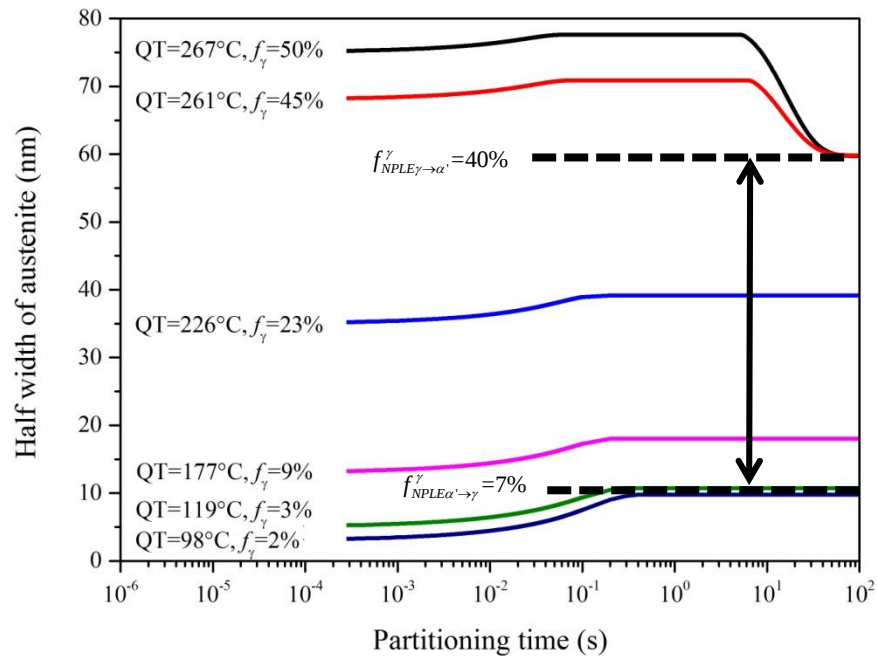
C diffusion
in γ controlled



QT=261 / 226 / 98 °C, PT=400 °C



QT=267 ~ 98 °C, PT=400 °C

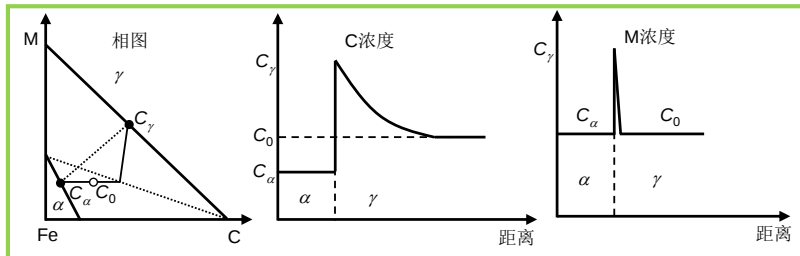


C content in austenite is between $C_\gamma^{NPLE/PLE\gamma\rightarrow\alpha'}$ and $C_\gamma^{NPLE/PLE\alpha'\rightarrow\gamma}$!

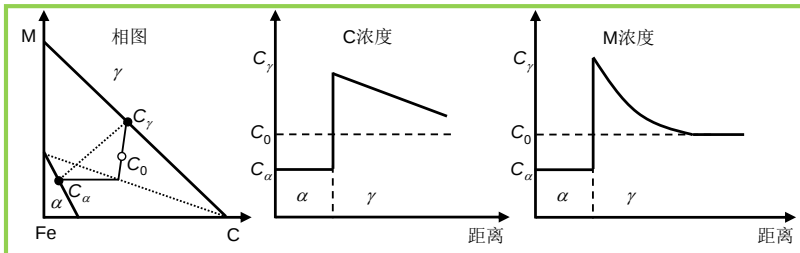
QP-LE--Local equilibrium:

$$\mu_i^\gamma = \mu_i^\alpha$$

Negligible Partitioning-Local Equilibrium (NP-LE) : C diffusion controlled



Partitioning-Local Equilibrium (P-LE) : M diffusion controlled



Diffusion Controlled Kinetic Process :

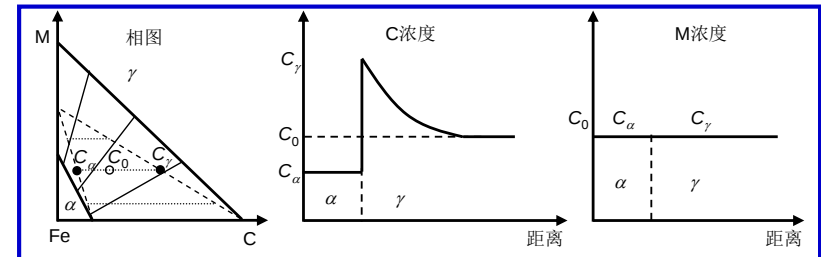
$$\frac{c_{i,j+1} - c_{i,j}}{\Delta t} = D \frac{c_{i-1,j} - 2c_{i,j} + c_{i+1,j}}{\Delta x^2} + v \frac{N-i}{N-1} \frac{c_{i+1,j} - c_{i-1,j}}{2\Delta x} \quad (2)$$

QP-PE--Paraequilibrium:

$$\mu_C^\gamma = \mu_C^\alpha$$

$$(\mu_M^\gamma - \mu_M^\alpha) = -\frac{X_{Fe}}{X_M} (\mu_{Fe}^\gamma - \mu_{Fe}^\alpha)$$

PE : C diffusion AND Mn indiffusible



$$\frac{\partial c}{\partial t} = \nabla \cdot (D \nabla c) \quad (1)$$

$$v = \left(D^{\alpha'} \frac{\partial c^{\alpha'}}{\partial x} - D^\gamma \frac{\partial c^\gamma}{\partial x} \right) / (c^{\gamma/\alpha'} - c^{\alpha'/\gamma}) \quad (3)$$