

The interaction between moving α/γ interface and interface precipitation carbides during the cyclic phase transformations in low alloy steels

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Introduction



Ricks R A, Howell P R. Metal Science, 1982

How to quantitatively determine the PF?



Experiment Design

Temperature NPLE/PLE $\alpha \rightarrow \gamma$ PLE NPLE/PLE $\gamma \rightarrow \alpha$ Carbon content in austenite





> Chemical composition:

Volume fraction of ferrite –

Alloy	Composition, mass%					
	С	Si	Mn	Nb	Fe	
0Nb	0.1	0.05	1.5	_	Bal.	
0.1Nb	0.08	0.05	1.5	0.1	Bal.	

Vickers Hardness: 0Nb: 118.1±2.2HV 0.1Nb: 136.8±9.1HV

> OM (Isothermal holding at 700° C):





0Nb: 72.05 \pm 2.37% \rightarrow Lever rule: 0.357 \pm 0.033%

0.1Nb: 76.85 \pm 1.77% \rightarrow Lever rule: 0.332 \pm 0.024%



Experiment Design



	Composition, mass%						
Alloy	С	Si	Mn	Nb	Fe		
0Nb	0.1	0.05	1.5		Bal.		
0.1Nb	0.08	0.05	1.5	0.1	Bal.		

> PLE/NPLE line:



> Heat Treatment:





Experimental Results: TEM Characterization

> Isothermally hold at 700 $^{\circ}$ C for 40min, 0.1Nb



Plane of interphase precipitation: $\sim(-110)$

Inter-sheet spacing: 18~22nm

Size of NbC carbides: 5-7nm





Experimental Results: Dilatometry





Experimental Results: Dilatometry





Experimental Results: Dilatometry



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Experimental Results: Kinetics of $\alpha \rightarrow \gamma$ **Transformation**

> Cyclic Transformation at 780 $^{\circ}$ C and 790 $^{\circ}$ C



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Discussion: Determination of Pinning Force

> The chemical driving force for $\alpha \rightarrow \gamma$ transformation: $\Delta G_{m}^{chem} = \sum_{i}^{n} x_{i}^{0} \left[\mu_{i}^{\alpha/\gamma} \left(x_{i}^{\alpha/\gamma} \right) - \mu_{i}^{\gamma/\alpha} \left(x_{i}^{\gamma/\alpha} \right) \right]$ a a a > The dissipation of Gibbs energy due to solute drag effect: 220 $\Delta G_m^{diff} = -\int_0^\infty (X - X_0) \left(\frac{dE}{dx}\right) dx$ Dissipation(Mn) 780°C, 0.1Nb 200 Dissipation(Nb) Dissipation(Si) 180 **Total Dissipation** Interface Interface Gibbs energy (J/mol) 160 140 120 a a 100 80 60 $\Delta E = \frac{\mu_{\gamma}^0 - \mu_{\alpha}^0}{2}$ μ_{α}^{0} μ^0_{α} 40 Nb Si $2|\Delta E|$ $2|\Delta E|$ Mn 20 a a V 0 1E-10 1E-9 1E-7 1E-6 1E-8 1E-5 1E-4 0.001 Interface velocity (m/s) $-\delta$ $+\delta$



Discussion: Determination of Pinning Force

> Analysis of PF for 780°C Cyclic Phase Transformation





Discussion: Determination of Pinning Force

> Analysis of PF for 790°C Cyclic Phase Transformation





ThermoCalc calculation for volume fraction of NbC vs Temperature



 $lg([Nb] \bullet [C])_{\alpha} = 5.43 - 10960/T^{[2]}$ $lg([Nb] \bullet [C])_{\gamma} = 2.206 - 6746/T$

[2] 雍岐龙. 钢铁材料中的第二相. 北京: 冶金工业出版社, 2006

• 700°C, The Solubility of NbC in Ferrite : $1.47 \times 10^{-6} \%^2$

PE: $w_c^{\alpha} = 1.32 \times 10^{-2}$ %, $w_{Nb}^{\alpha} = 1.11 \times 10^{-4}$ % $\ll 0.1$ %*Nb* (bulk)

• 790°C, The Solubility of NbC in Ferrite: $1.32 \times 10^{-5} \%^2$

PE: $w_c^{\alpha} = 4.46 \times 10^{-3}$ %, $w_{Nb}^{\alpha} = 2.96 \times 10^{-3}$ % $\ll 0.1$ %*Nb* (bulk)

• 790°C, The Solubility of NbC in Austenite: $7.26 \times 10^{-5} \%^2$ *PE*: $w_c^{\gamma} = 0.144\%$, $w_{Nb}^{\gamma} = 5.04 \times 10^{-4}\% \ll 0.1\%Nb$ (bulk)

Almost no carbide dissolved during cyclic phase transformation !



Conclusion

- ✓ The cyclic phase transformation experiments have been proposed to study the interaction between the moving α/γ interfaces and IP carbides.
- ✓ According to the dilatometric experiments, 780°C is defined as the critical unpinning temperature for Fe-0.1C-1.5Mn-0.1Nb steels.
- ✓ The value of pinning force quantitatively determined by the GEB model is approximately 20J/mol, which can generate significant effects on transformation kinetics when the driving force is relatively small. The GEB model including PF can well predict the kinetics of $\alpha \rightarrow \gamma$ phase transformation at higher temperature.
- ✓ It can be speculated that almost no carbide is dissolved during cyclic phase transformation based on the thermodynamic analysis.



Thank You