



***ALEMI***



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# Contact conditions at migrating interfaces

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**<sup>3</sup>Österreichische Akademie der Wissenschaften, ESI, Austria**



# Contents and Structure



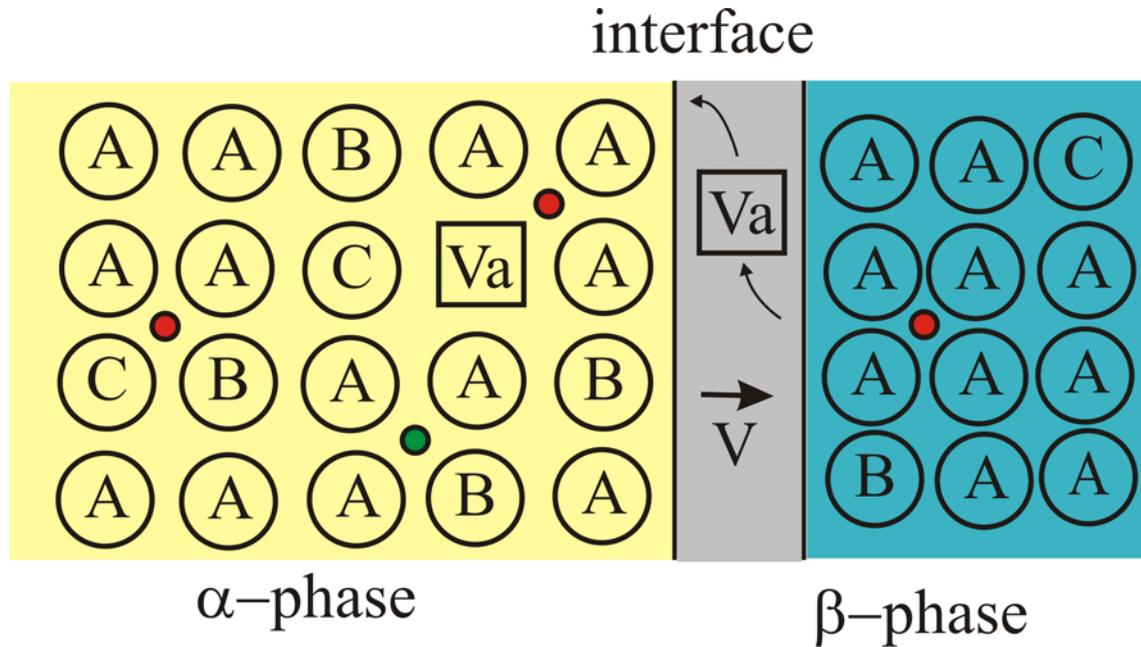
- **Kinetics of diffusional phase transformations (sharp interface)**
  - Total Gibbs energy in the system
  - Balance relations
  - Dissipation at the sharp interface
  - Contact conditions
  - “Equal jump” contact conditions
  
- **Limitations of the sharp interface approach**
  - Intrinsic and effective interface mobility
  - Comparison with experiments
  - “Quasi-thick” interface model
  - Results of the quasi-thick interface model
  - Solid-liquid phase transformation
  
- **Thick interface**
  - Diffusion processes inside the interface
  - Comparison to the sharp interface model
  
- **Conclusions and Outlook**



# Kinetics of diffusional phase transformations



One-dimensional system of unit cross-sectional area



$\textcircled{A}$   $\textcircled{B}$   $\textcircled{C}$  Components A, B, C

$\bullet$   $\bullet$  interstitial components



# Total Gibbs energy in the system



Chemical potential of component  $i$  in phase  $\varphi$ :

$$\mu_i^\varphi = \mu_i^\varphi(x_1, \dots, x_N, T)$$

Total chemical Gibbs energy in a system of  $\varphi = \alpha, \beta, \gamma, \dots$  phases, each consisting of  $i = 1, \dots, N$  components.

$$g_{\text{chem}}^\varphi = \frac{1}{V_m} \cdot \sum_{i=1}^N \int_{z_1}^{z_2} x_i^\varphi \mu_i^\varphi dz$$

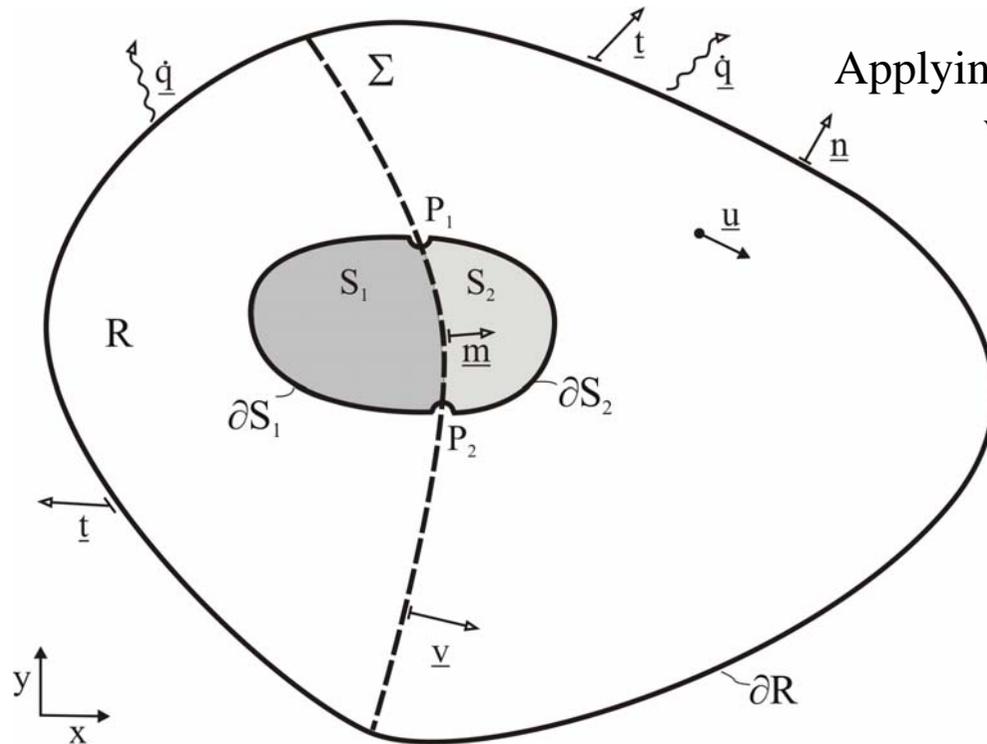
The total Gibbs energy of the system generally also consists of a mechanical part related to the elastic energies  $U'$ .

$$U' = \frac{1}{2} \underline{\underline{\sigma : \varepsilon}}$$

- **Incoherent** or partly coherent **interfaces**, no external stresses
- **Relaxation by a vacancy mechanism.**



# Balance relations



Applying divergence and transport theorem and volumes of  $S_1 \rightarrow 0$  and  $S_2 \rightarrow 0$ .

## Mass balances

Interface:

$$\llbracket x_i / V_m \rrbracket v = \llbracket j_i \rrbracket, i = 1, 2, \dots, N$$

$$\sum_{i=1}^s \llbracket x_i / V_m \rrbracket v = -\llbracket j_{va} \rrbracket$$

Bulk:

$$\frac{\partial (x_i / V_m)}{\partial t} = -\underline{\nabla} \cdot \underline{j}_i$$

F.D. Fischer, N.K. Simha: "Influence of material fluxes on the jump relations at a singular interface in a multicomponent solid" *Acta Mech.* **171** (2004) 213.



# Dissipation at the sharp interface



mass balance

$$Q_{\text{int}} = \sum_{i=1}^N \llbracket \mu_i \rrbracket \cdot \left\langle \frac{x_i}{V_m} \cdot \nu - j_i \right\rangle \geq 0$$

F.D. Fischer, N.K. Simha: "Influence of material fluxes on the jump relations at a singular interface in a multicomponent solid" *Acta Mech.* **171** (2004) 213.

$$Q_{\text{int}} = \sum_{i=1}^N \frac{x_i^{\text{tf}}}{V_m} \llbracket \mu_i \rrbracket \cdot \nu$$

$$x_i^{\text{tf}} = x_i^{\text{o}} - (V_m / \nu) \cdot j_i^{\text{o}} = x_i^{\text{n}} - (V_m / \nu) \cdot j_i^{\text{n}}$$

M. Hillert, M. Rettenmayr: "Deviation from local equilibrium at migrating phase interfaces" *Acta Mater.* **51** (2003) 2803.

$x_i^{\text{tf}}$  ... mathematical construct – mole fraction?

Is the concept of **trans**-interface diffusion in the framework of a sharp interface model required (allowed)?!

M. Hillert: "Overview No.135. Solute drag, solute trapping and diffusional dissipation of Gibbs energy" *Acta Mater.* **47** (1999) 4481.



# Contact conditions I



A diffusional phase transformation with  **$N$  components** is a problem that comprises  **$(2N-1)$  independent variables** at the interface.

- $N-1$  ... independent fluxes or mole fractions in the parent (old) phase
- $N-1$  ... independent fluxes or mole fractions in the new phase
- 1 ... interface velocity

## Equilibrium concepts

$$M \rightarrow \infty$$

$$\Delta f = \frac{v}{M} = 0$$

### • Local equilibrium contact conditions

$$N \text{ c.c. } \boxed{[[\mu_i]] = 0, i = 1, \dots, N} \quad (N-1) \text{ m.b. } \boxed{[[x_i/V_m]]v = [[j_i]], i = 1, 2, \dots, N}$$

### • Paraequilibrium contact conditions

$$(N-s-1) \text{ c.c. } \boxed{[[\mu_i]] = 0} \quad (N-s-1) \text{ m.b. } \boxed{[[x_i/V_m]]v = [[j_i]]} \quad i = s+1, \dots, N \text{ (Interstitials)}$$

$$2s \text{ c.c. } \boxed{K_i = y_i^o / \sum_{i=1}^s y_i^o = y_i^n / \sum_{i=1}^s y_i^n, i = 1, \dots, s \text{ (Substitutionals)}} \quad 1 \text{ pe. c. } \boxed{\Delta f = \sum_{i=1}^s x_i^n \cdot \frac{[[\mu_i]]}{V_m} = 0}$$



# Contact conditions II



## Non-equilibrium concepts

$M$  (finite, intrinsic interface mobility?!)

$$\Delta f = \frac{v}{M}$$

### • No substitutional diffusion

$(N-s-1)$  c.c.  $[[\mu_i]] = 0$   $(N-s-1)$  m.b.  $[[x_i/V_m]]v = [[j_i]]$   $i = s+1, \dots, N$  (Interstitials)

$2s$  c.c.  $K_i = y_i^o / \sum_{i=1}^s y_i^o = y_i^n / \sum_{i=1}^s y_i^n$ ,  $i = 1, \dots, s$  (Substitutionals)  $1$  kinetic c.  $\Delta f = \sum_{i=1}^s x_i^n \cdot \frac{[[\mu_i]]}{V_m}$

### • „Equal jump“ contact condition

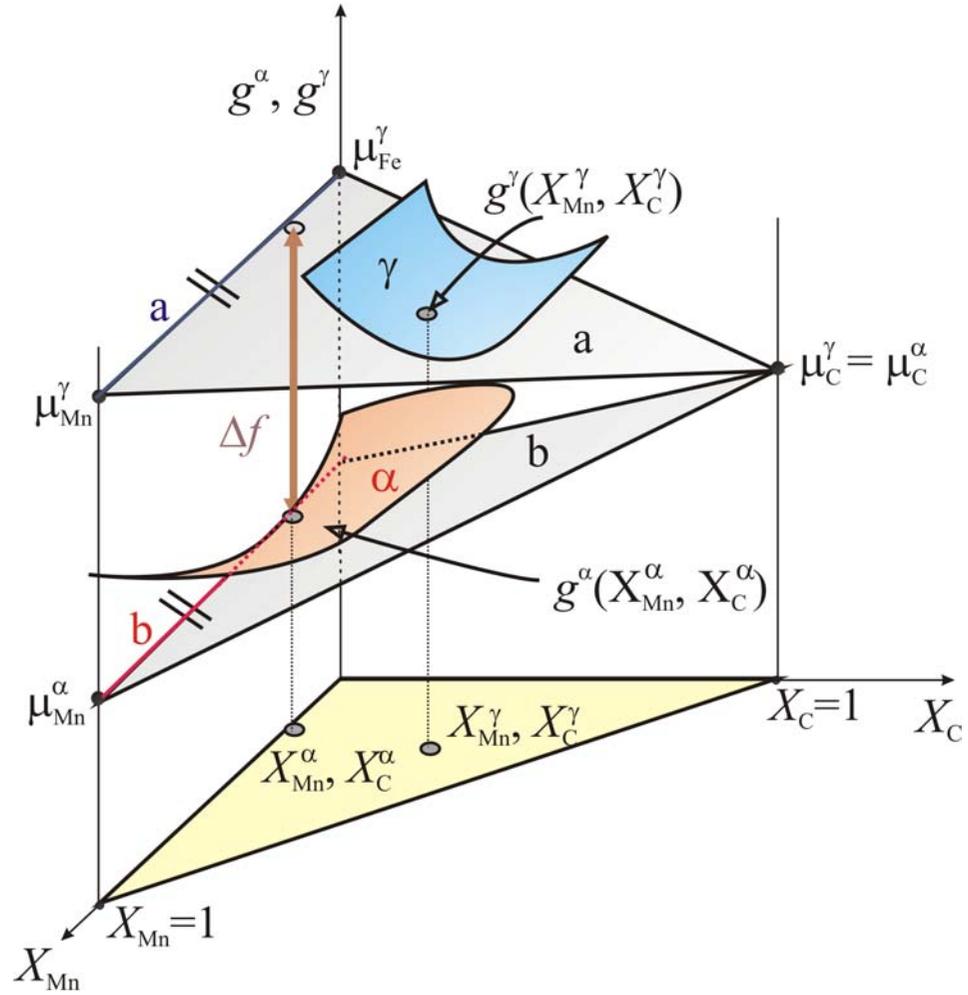
$(N-1)$  c.c.  $[[\mu_i]] = 0$ ,  $i = s+1, \dots, N$  (interstitials),  
 $[[\mu_i]] = [[\mu_N]]$ ,  $i = 1, \dots, s$  (substitutionals).

$1$  kinetic c.  $\Delta f = \sum_{i=1}^s x_i^n \cdot \frac{[[\mu_i]]}{V_m}$   $(N-1)$  m.b.  $[[x_i/V_m]]v = [[j_i]]$ ,  $i = 1, 2, \dots, N$



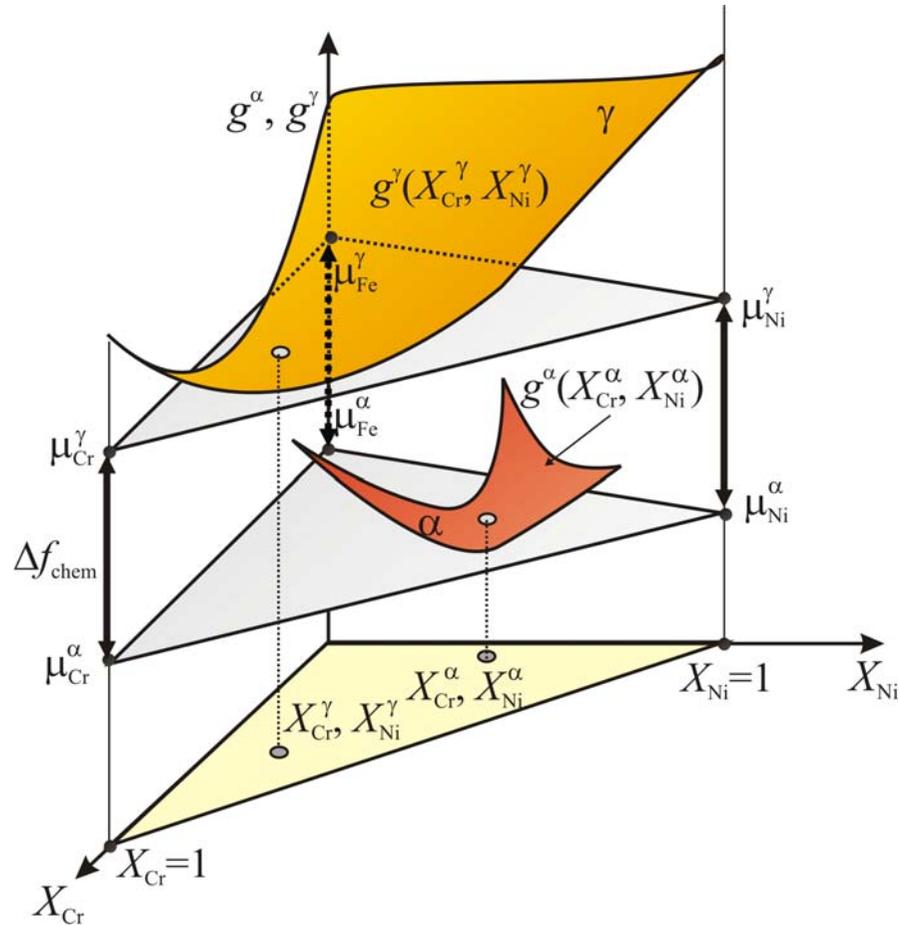


# „Equal jump“ contact conditions





# „Equal jump“ contact conditions





# Derivation of the „equal jump“ conditions by the thermodynamic extremal principle



## Energy balance

$$Q_{\text{int}} = Q = -\dot{G} \quad Q_{\text{int}} = v^2 / M \quad \text{Volumes of } S_1 \rightarrow 0 \text{ and } S_2 \rightarrow 0.$$

$$\dot{G} = \sum_{i=1}^N j_i^o \cdot [[\mu_i]] - \sum_{i=1}^N \frac{x_i^o}{V_m} v \cdot [[\mu_i]]$$

## Thermodynamic extremal principle

$$\frac{\partial}{\partial \dot{q}_i} [Q + \eta(\dot{G} + Q)] = 0 \rightarrow \eta = -2 \rightarrow \frac{\partial \dot{G}}{\partial \dot{q}_i} = -\frac{1}{2} \frac{\partial Q}{\partial \dot{q}_i}$$

## Contact conditions

$$v = \frac{M}{V_m} \cdot \sum_{i=1}^N x_i^o [[\mu_i]] = \frac{M}{V_m} \cdot \Delta f \quad \frac{\partial \dot{G}}{\partial j_i^o} = [[\mu_i]] - [[\mu_N]] = \frac{\partial Q}{\partial j_i^o} = 0$$



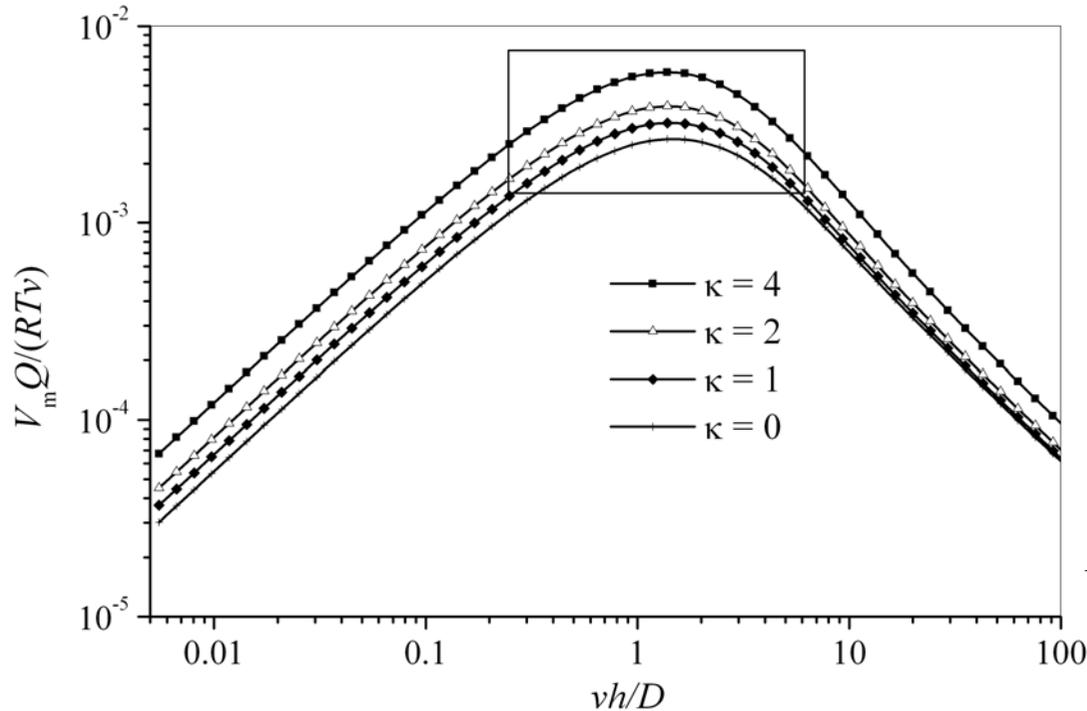
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# Intrinsic and effective interface mobility



J. Svoboda, F. D. Fischer, E. Gamsjäger: “Influence of solute segregation and drag on properties of migrating interfaces”, *Acta mater.*, **50**, 967-977, 2002.

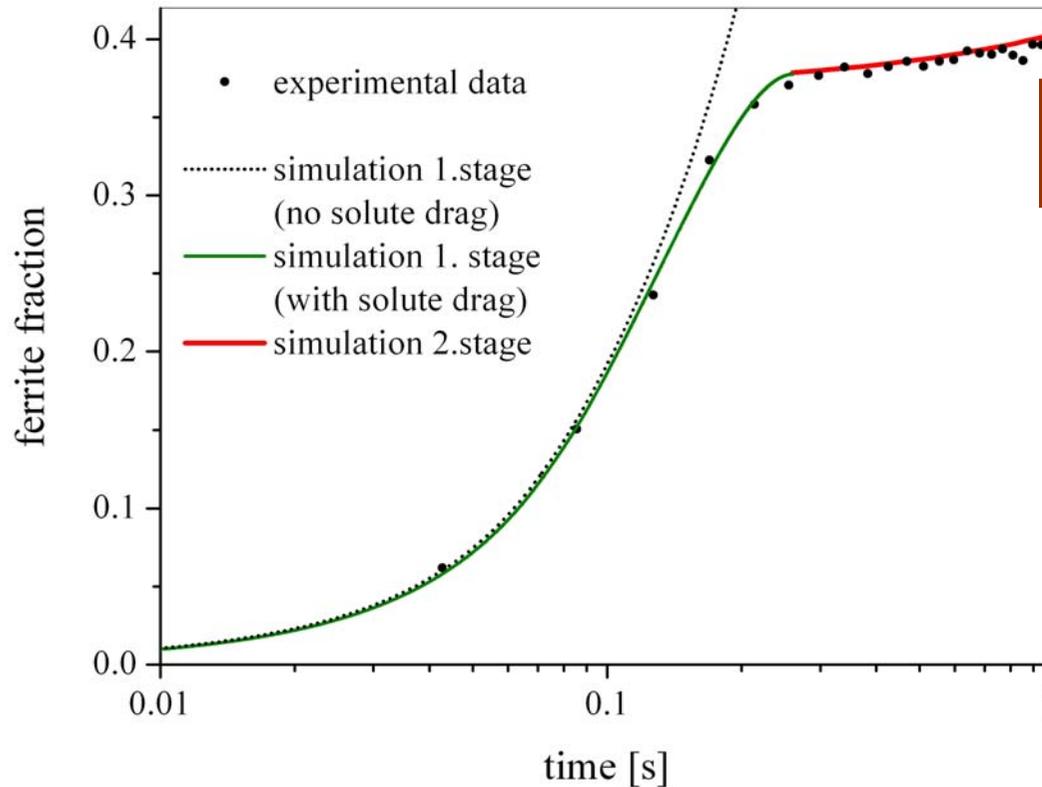
$$M_{\text{eff}} = \left( \frac{1}{M_{\text{intr}}} + \frac{Q_{\text{sd}}}{v^2} \right)^{-1}, \quad \frac{Q_{\text{sd}}}{v} = \text{const.} \Rightarrow$$

$$M_{\text{eff}} = \left( \frac{1}{M_{\text{intr}}} + \frac{C}{v} \right)^{-1}$$

$C$  depends linearly on time



# Comparison: Theory and experiment



**Non – equilibrium  
No substitutional diffusion**

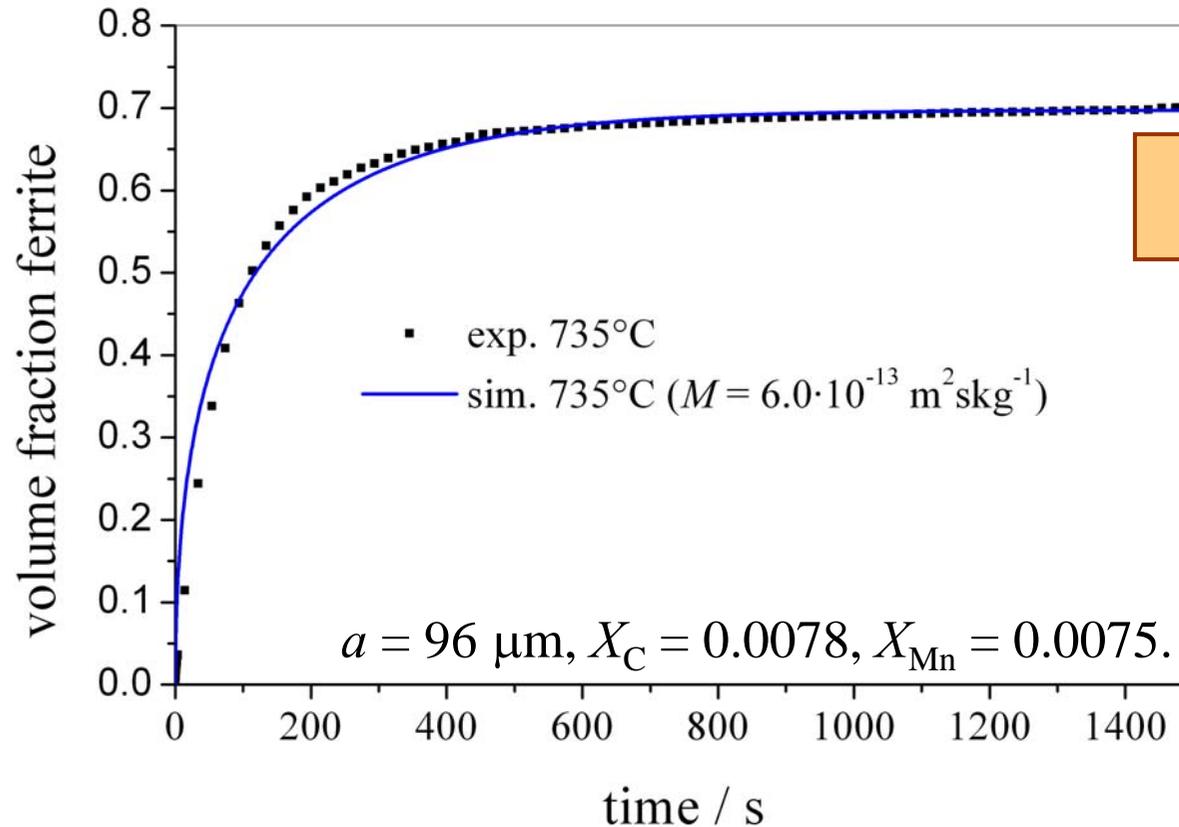
E. Kozeschnik, E. Gamsjäger, “High-Speed Quenching Dilatometer Investigation of the Austenite to Ferrite Transformation in low to ultra low carbon steel”, *Metall. Mater. Trans.* **37A** (2006) 1791-1797.

E. Gamsjäger: “Kinetics of the austenite-to-ferrite phase transformation – From the intrinsic to an effective mobility”, *Materials Science Forum* **539-543** (2007) 2570-2575.



# Comparison with experimental data\*

## Fe-C-Mn ( $\vartheta = 735^\circ\text{C}$ )



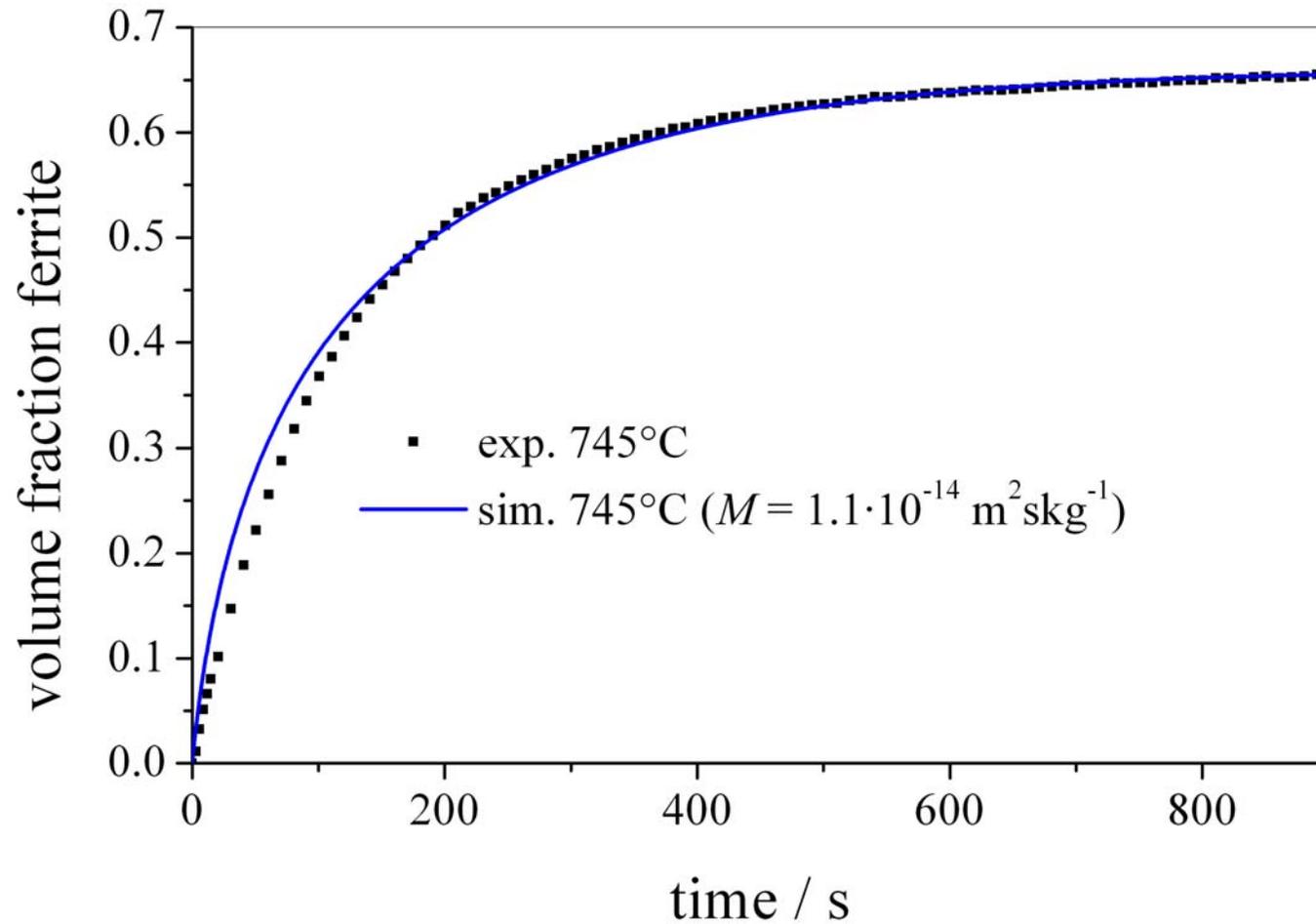
**Non – equilibrium  
No substitutional diffusion**

\*F. Fazeli, M. Militzer; Modelling the effects of alloying elements on the ferrite transformation kinetics, 44<sup>th</sup> Mechanical Working and Steel Processing Conf. Proc., 2002.

E. Gamsjäger, J. Svoboda, F.D. Fischer: “Austenite-to-ferrite phase in low-alloyed steels”, *Comp.Mat. Sci.* **32** (2005) 360-369.

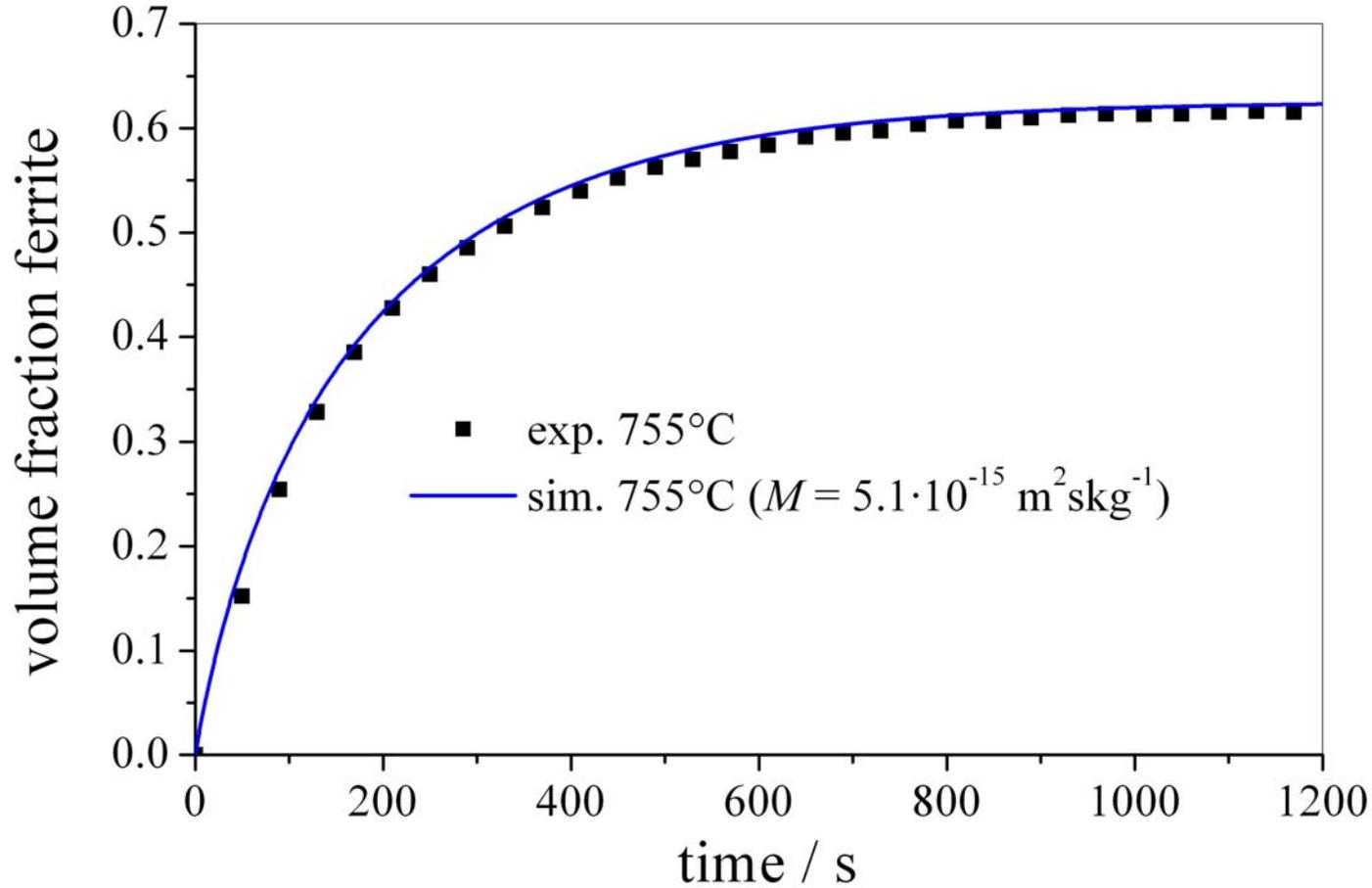


# Comparison with experimental data Fe-C-Mn ( $\vartheta = 745^{\circ}\text{C}$ )



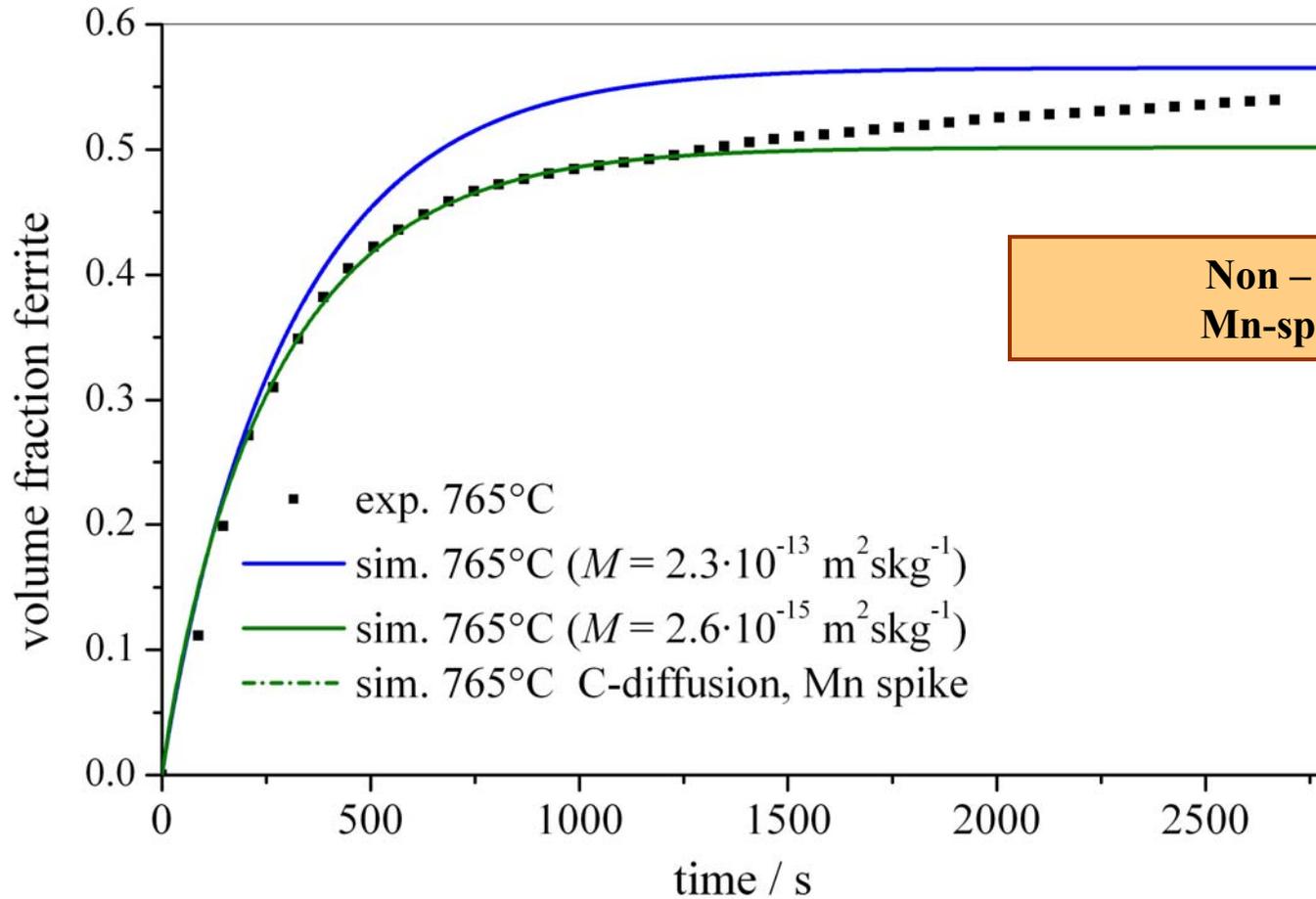


# Comparison with experimental data Fe-C-Mn ( $\vartheta = 755^\circ\text{C}$ )





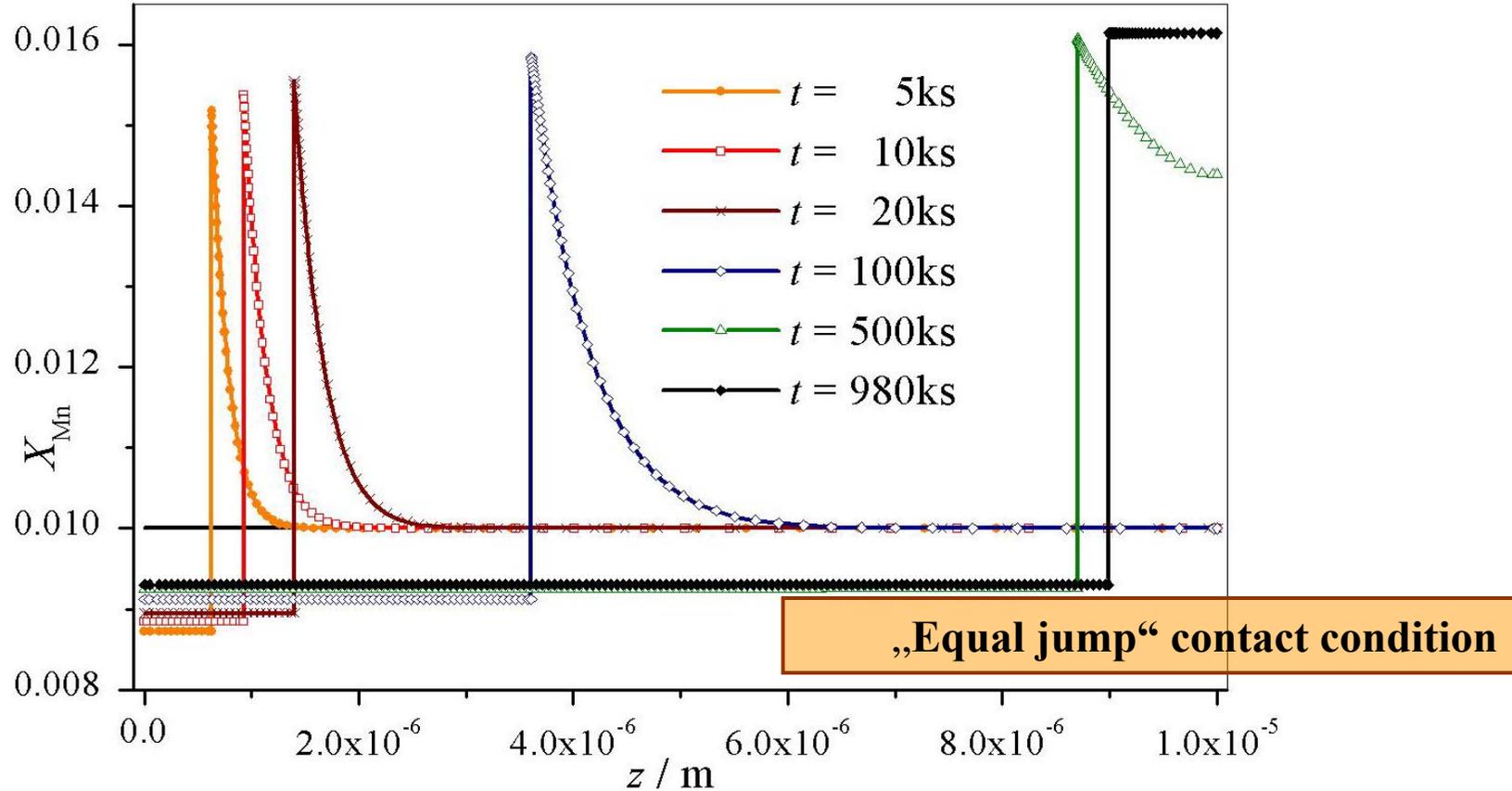
# Comparison with experimental data Fe-C-Mn ( $\vartheta = 765^\circ\text{C}$ )



Non – equilibrium  
Mn-spike diffusion

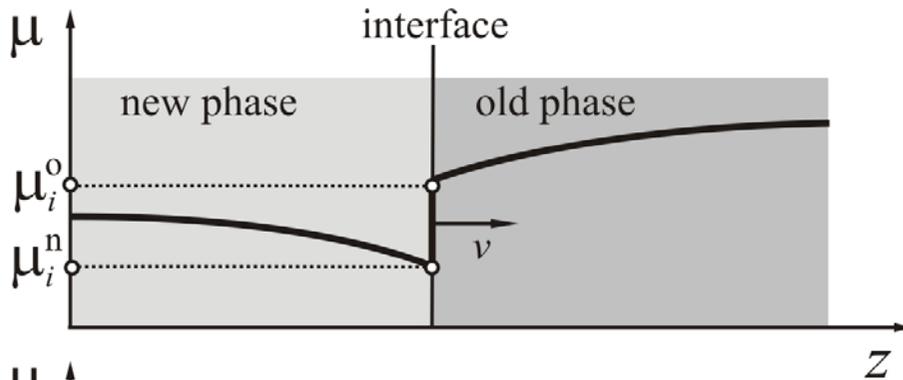


# Mobility and diffusion controlled growth: Fe-Mn-Profiles ( $T = 1123\text{K}$ )





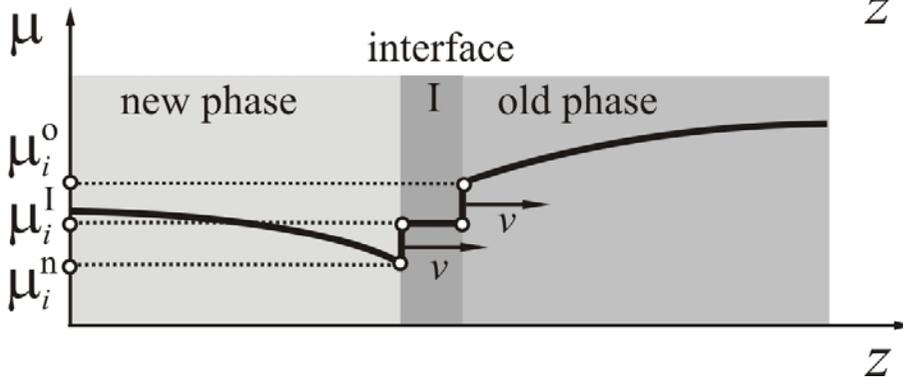
# „Quasi-thick“ interface



**Model**  $j_i^I = 0$

$$d_{\text{chem},n/I} = \sum_{i=1}^N [[\mu_i]]_{n/I} (x_i^I / V_m) v, \quad [[\mu_i]]_{n/I} = \mu_i^I - \mu_i^n$$

$$d_{\text{chem},I/o} = \sum_{i=1}^N [[\mu_i]]_{I/o} (x_i^I / V_m) v, \quad [[\mu_i]]_{I/o} = \mu_i^o - \mu_i^I$$



$$v = M_{n/I} \cdot \Delta f_{n/I} = M_{I/o} \cdot \Delta f_{I/o} \quad \frac{1}{M} = \frac{1}{M_{I/o}} + \frac{1}{M_{n/I}}$$

$$v = \frac{M_{I/o} \cdot M_{I/n}}{M_{I/o} + M_{I/n}} \cdot \sum_{i=1}^N [[\mu_i]]_{n/o} \cdot x_i^I = M \cdot \sum_{i=1}^N [[\mu_i]] \cdot x_i^I$$



# Results of the „quasi-thick“-interface approach



- “Quasi-thick“-interface – descriptive way to visualize the situation at a sharp interface.

$$x_i^{\text{tf}} = x_i^{\text{o}} - (V_m / v) \cdot j_i^{\text{o}} = x_i^{\text{n}} - (V_m / v) \cdot j_i^{\text{n}} = x_i^{\text{I}}$$

$x_i^{\text{tf}}$  ... mathematical construct

$x_i^{\text{I}}$  ... mole fraction inside the interface ( $0 \leq x_i^{\text{I}} \leq 1$ )

- “Quasi-thick“-interface – is consistent with the “equal jump“-condition.

## Limitations of the sharp interface approach

Only valid for ( $0 \leq x_i^{\text{tf}} \leq 1$ )

**Fluxes inside the interface cannot be considered.**

⇒

**Contact conditions at real interfaces  $\neq$   
Contact conditions at ideally sharp interfaces**



# Applicability of the sharp interface model

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Solid-liquid phase transformations – *yes*

Solid-solid transformation – *yes,*  
*if dissipation by diffusion processes in the interface is negligible.*

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# Solid-liquid phase transformation



## Experimental set-up

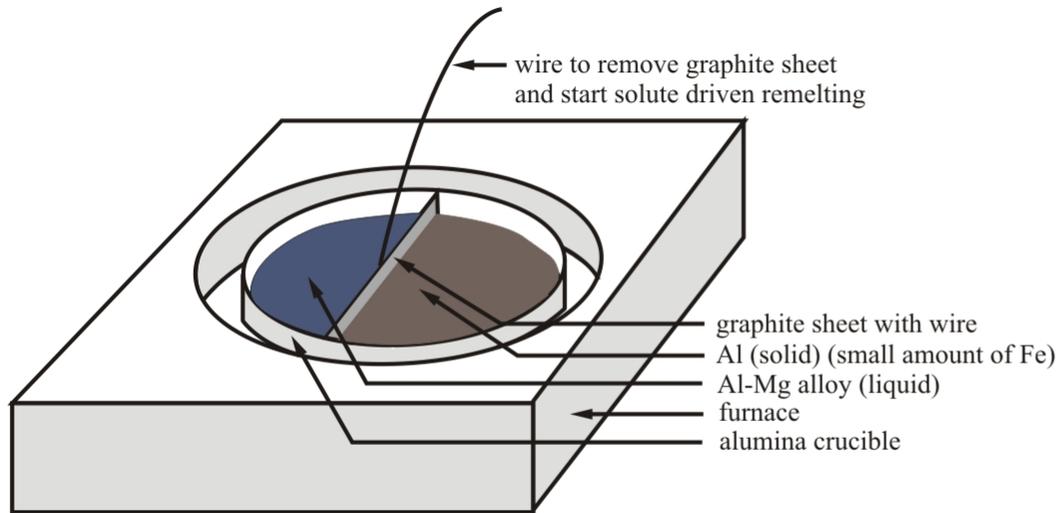


Fig 1: Liquid Al-Mg and solid Al half cylinder separated by a graphite sheet.

## Phase diagram

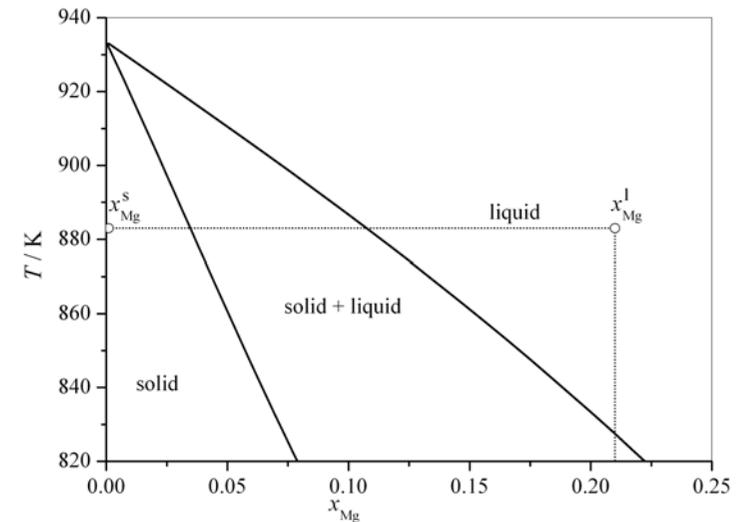


Fig 2: Al-rich side of the Al-Mg phase diagram. Initial mole fraction in the solid and liquid phase.

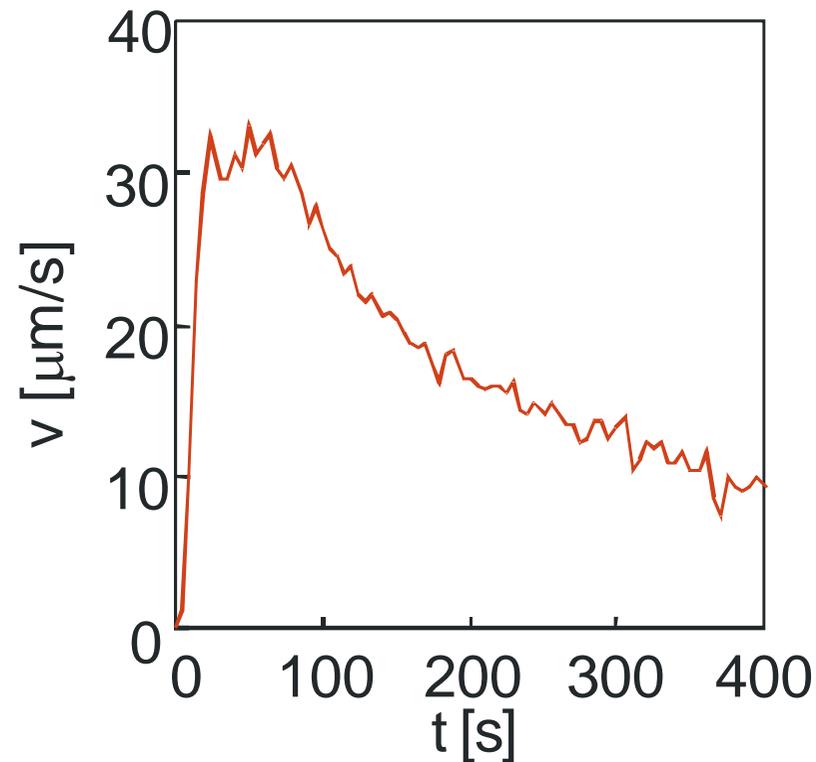
M. Rettenmayr, O. Warketin, M. Rappaz, H. E. Exner: "Simulation of solutal remelting", *Acta mater.* **49** (2001) 2499-2510.



# Experimental data



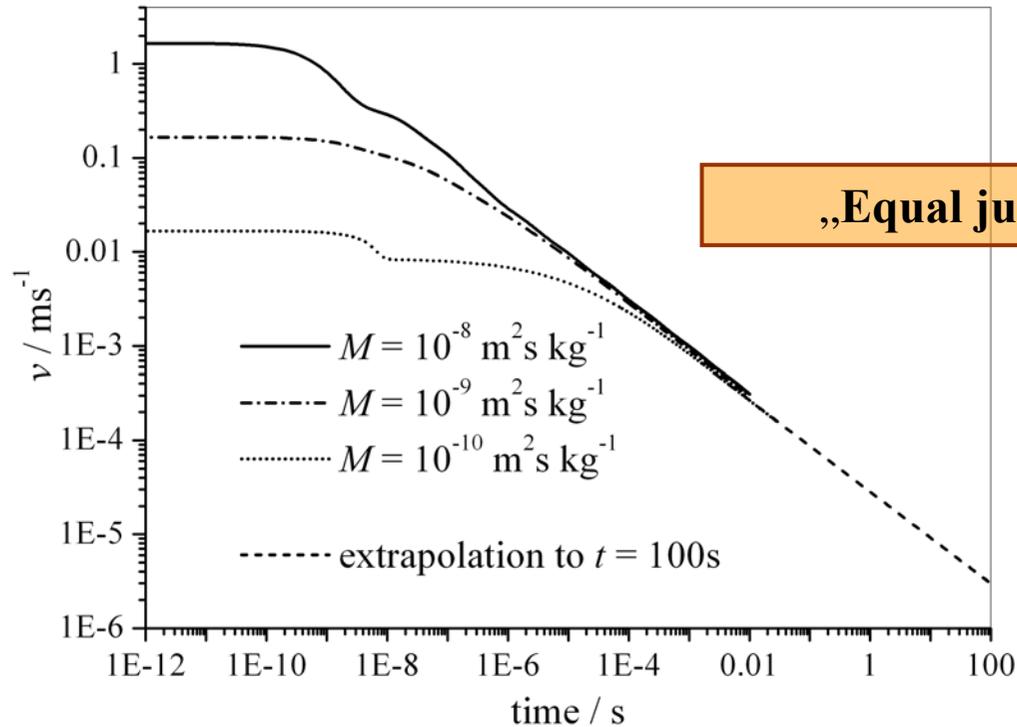
Time-temperature data  $\Rightarrow$  heat balance equation  $\Rightarrow$  time vs. velocity



Interface velocity:  $x_{\text{Mg}} = 0.204$ ,  $T = 883\text{K}$ .



# Calculations



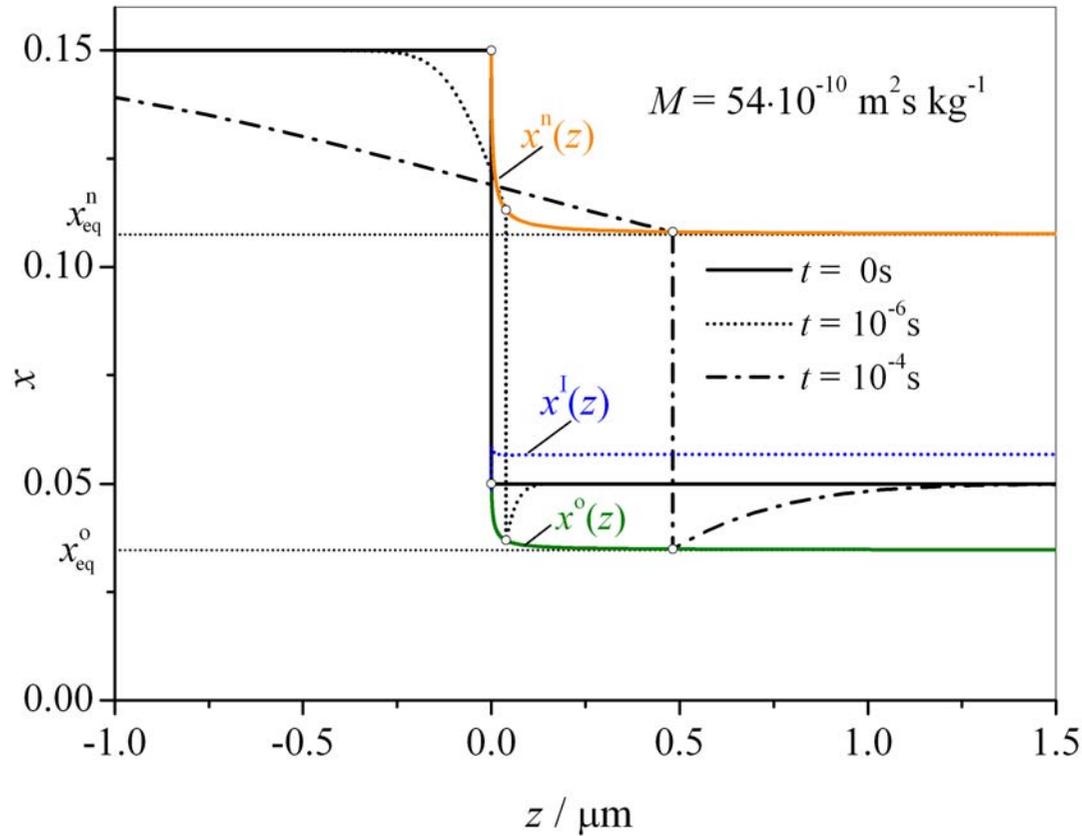
Interface velocity for three different interface mobilities.

Local equilibrium is reached at very small transformation times.



# Solid-liquid transformation in the Al-Mg system

$$x^n = 0.15, x^o = 0.05, T = 883\text{K}$$

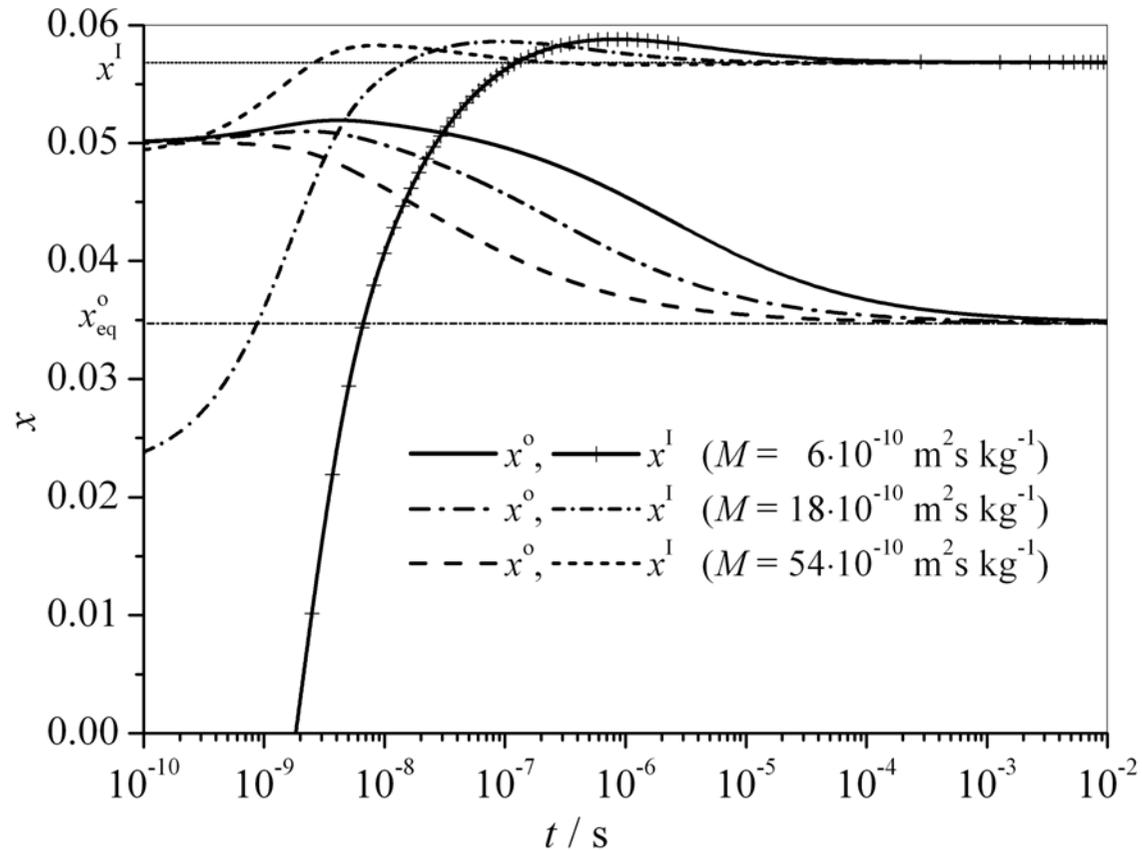


The mole fractions  $x^o$ ,  $x^n$  and  $x^l$  are depicted versus the spatial variable  $z$  (grey lines). The mole fraction profiles are plotted at different transformation times.



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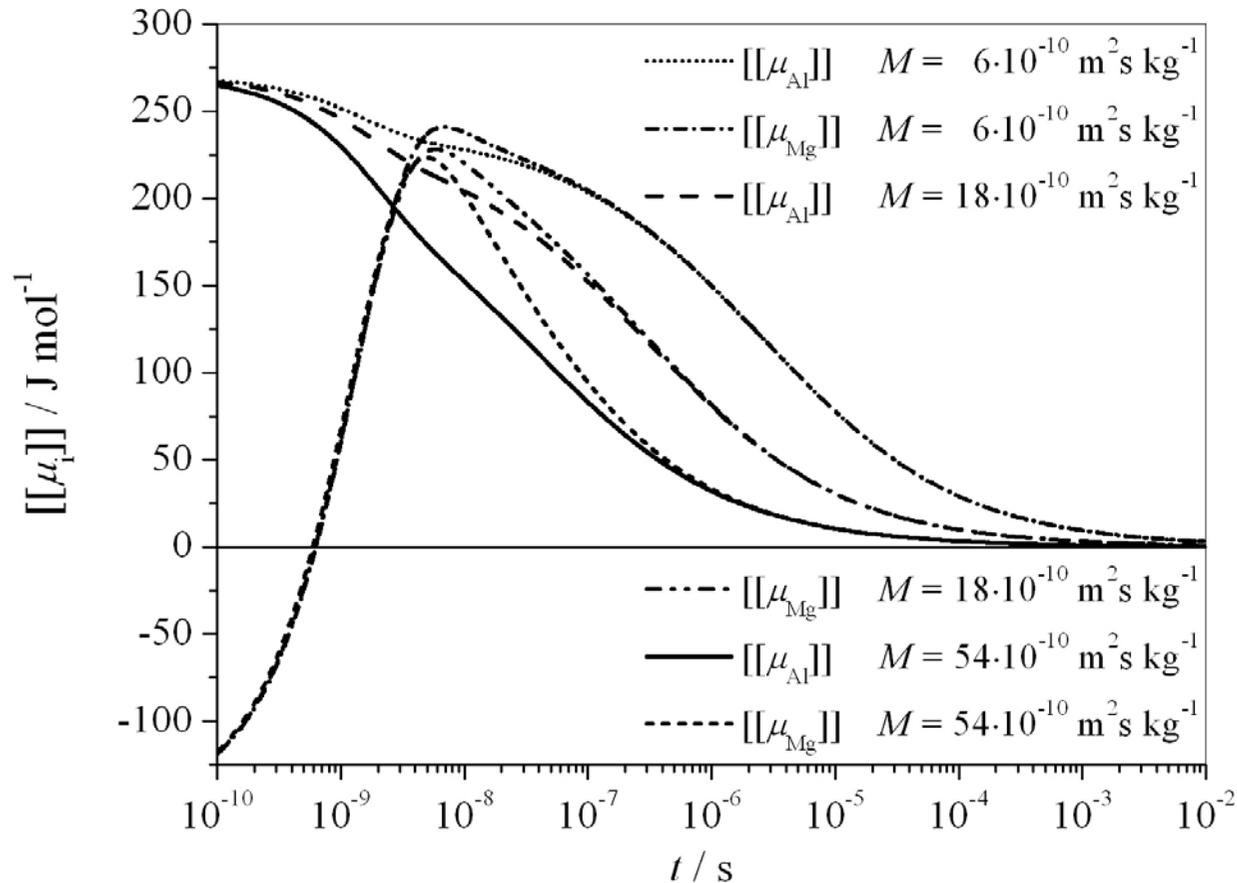


The time-dependent evolution of the mole fractions  $x^o$  and  $x^l$  at three interface different interface mobilities  $M$ .



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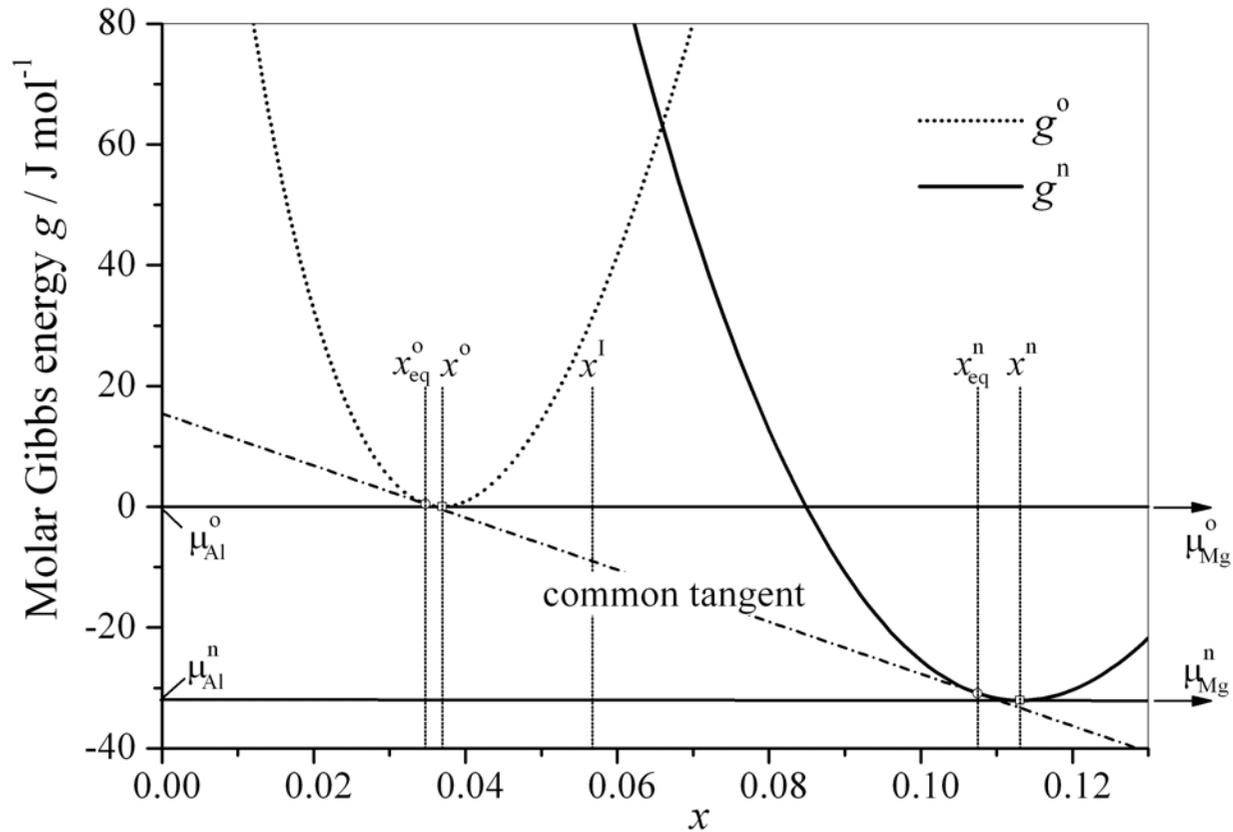


The jumps of the chemical potentials,  $[[\mu_{\text{Al}}]]$  and  $[[\mu_{\text{Mg}}]]$  vs. time.



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$$x^n = 0.15, x^o = 0.05, T = 883\text{K}$$



Calculated molar Gibbs energy diagram for a certain deviation from local equilibrium ( $t = 1\mu\text{s}$ ).



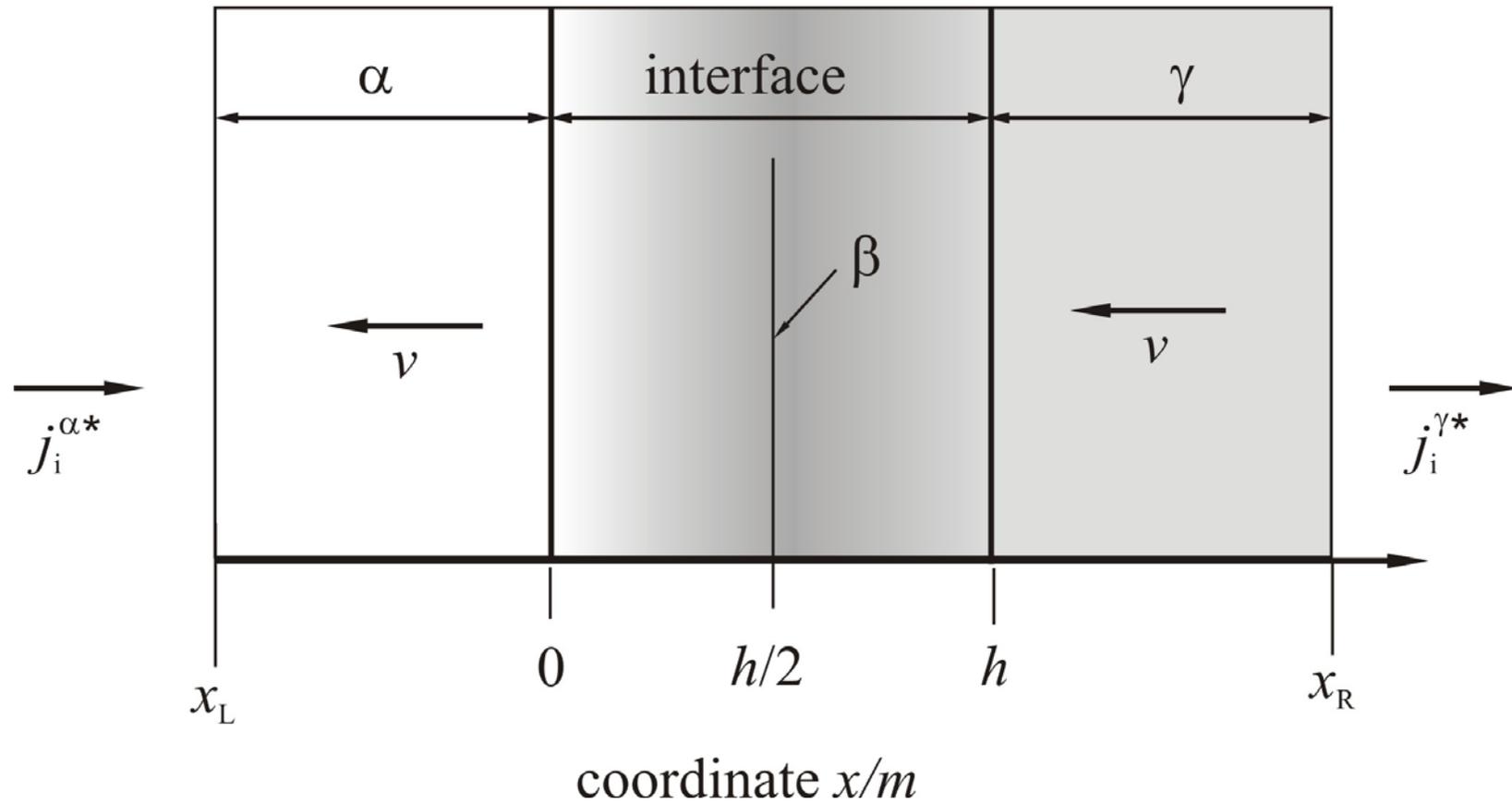
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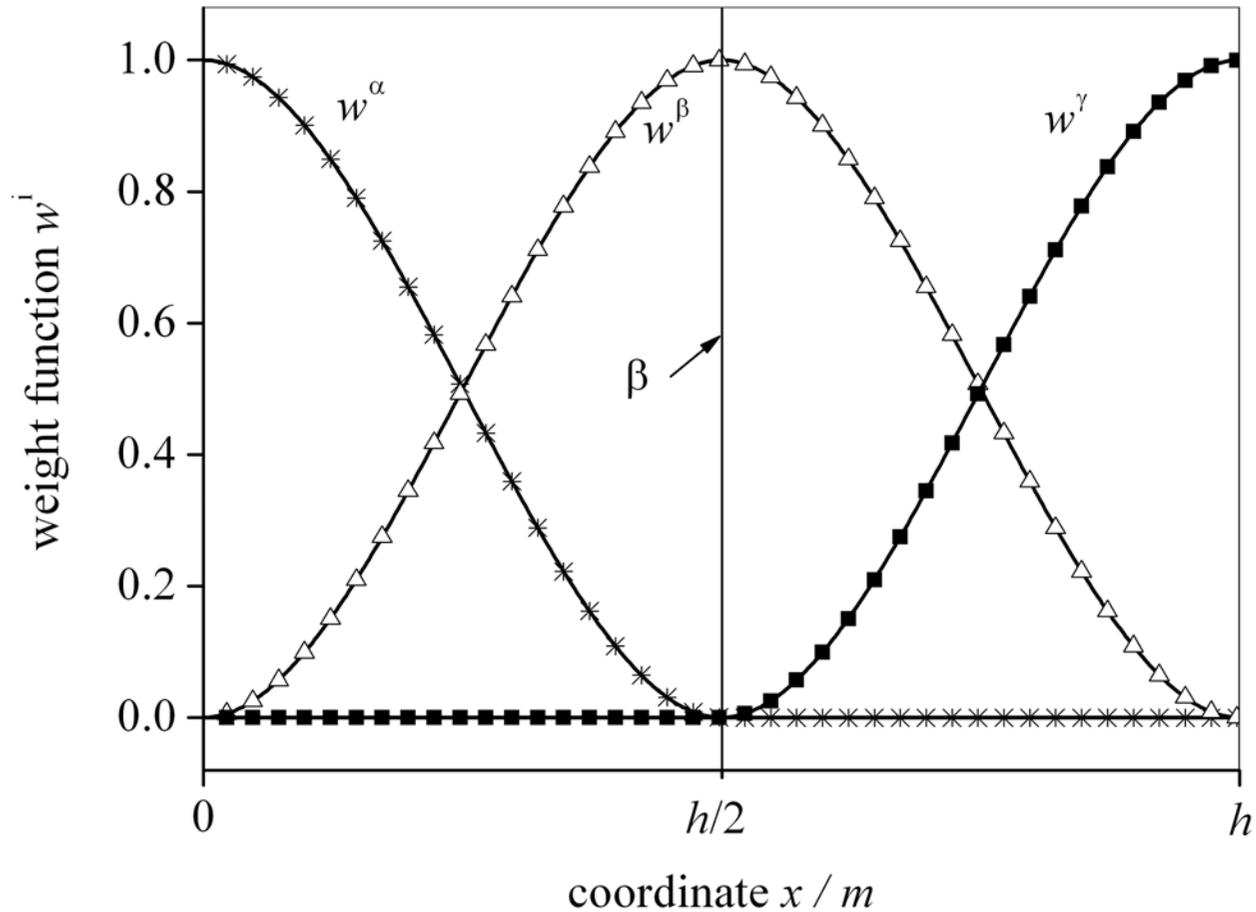


# Thick interface - steady state solutions



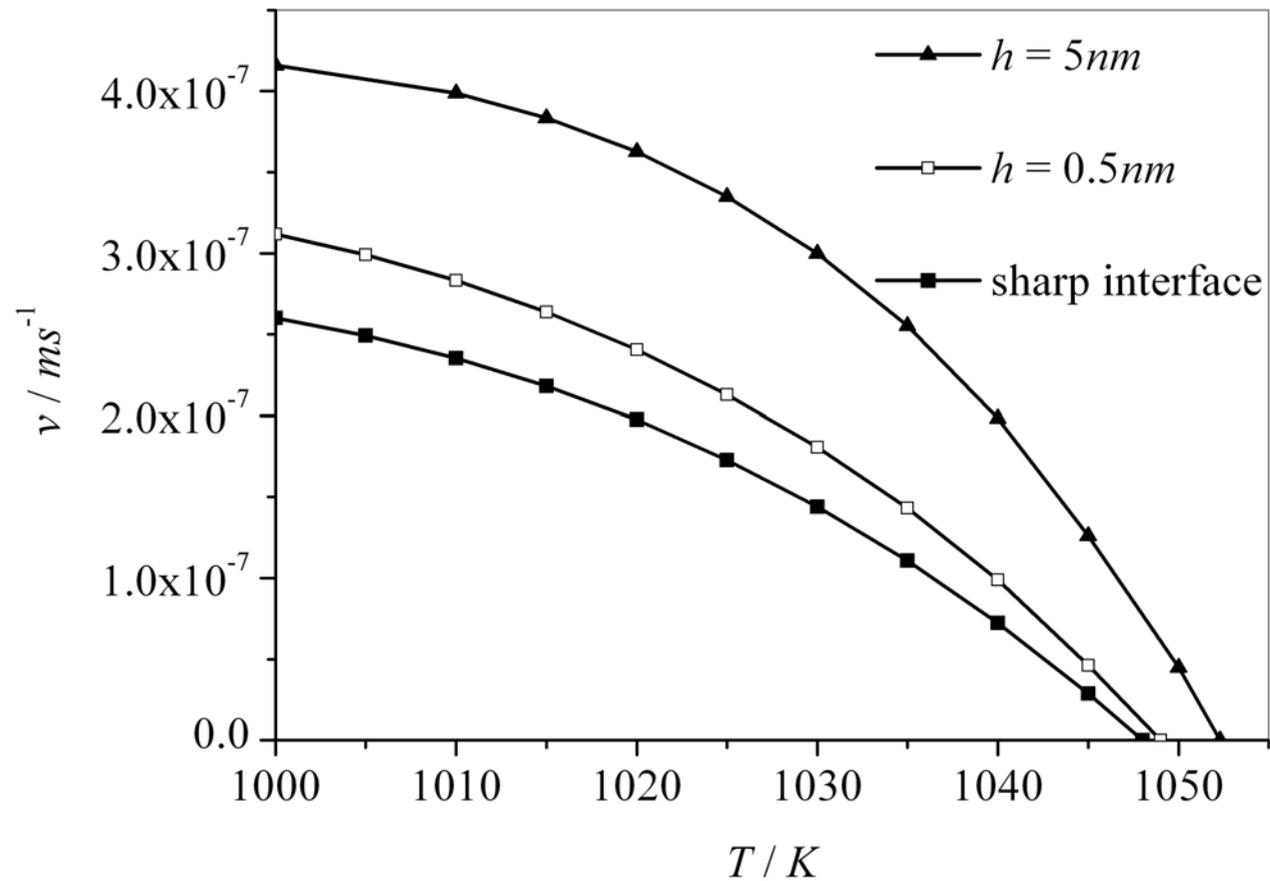


# Thick interface – weight functions



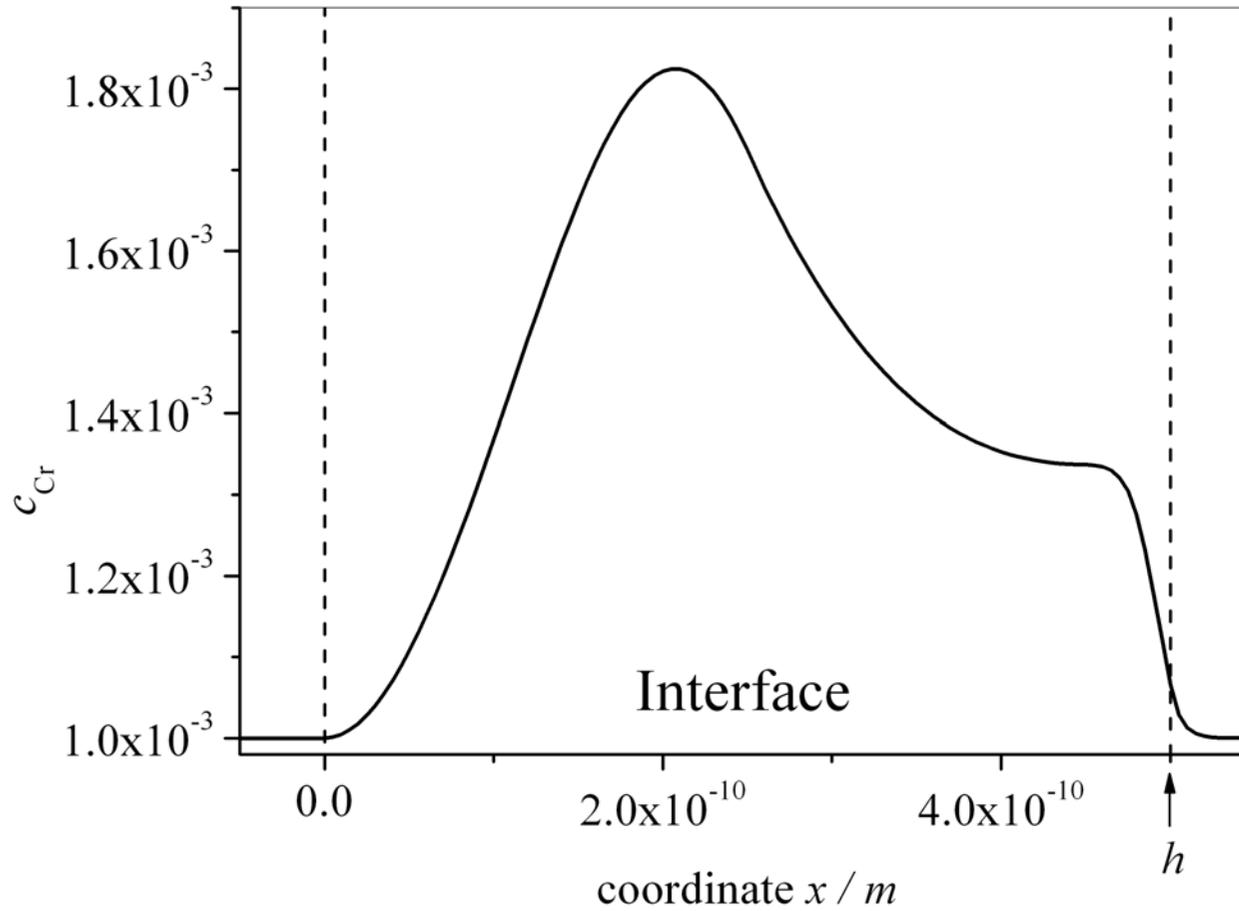


## Temperature dependence of the interface velocity $v$ for different values of the interface thickness $h$ .



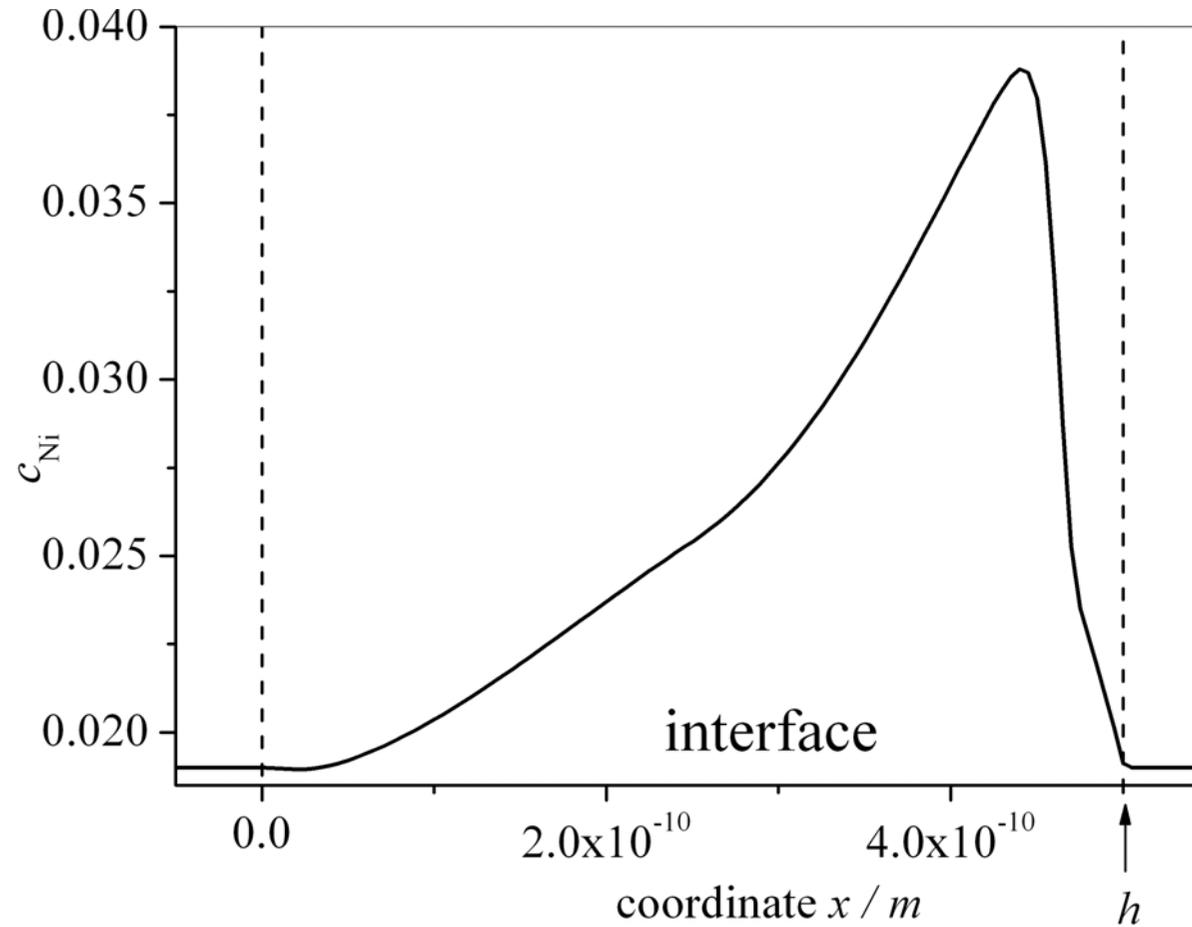


# Thick interface – Cr-Profile





## Thick interface – Ni-Profile





# Conclusions and Outlook

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- Sharp interface – equal jump contact conditions
  - Thick interface with zero fluxes can describe a sharp interface  $\Rightarrow$   
Trans-interface diffusion is not required for a sharp interface
  - Comparison of modelling results with experimental data
  - Thick interface – steady state solutions
- 

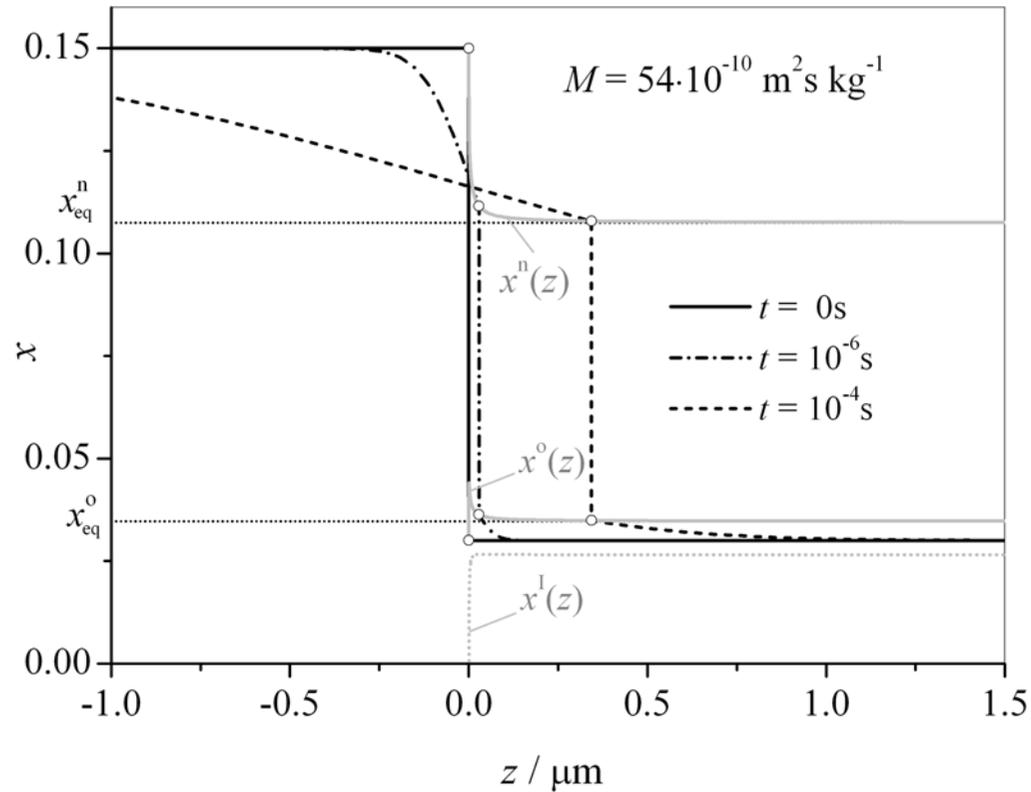
## Next goal:

- Thick interface model – general solution
-



# Solid-liquid transformation in the Al-Mg system

Case I:  $x^n = 0.15$ ,  $x^o = 0.03$ ,  $T = 883\text{K}$

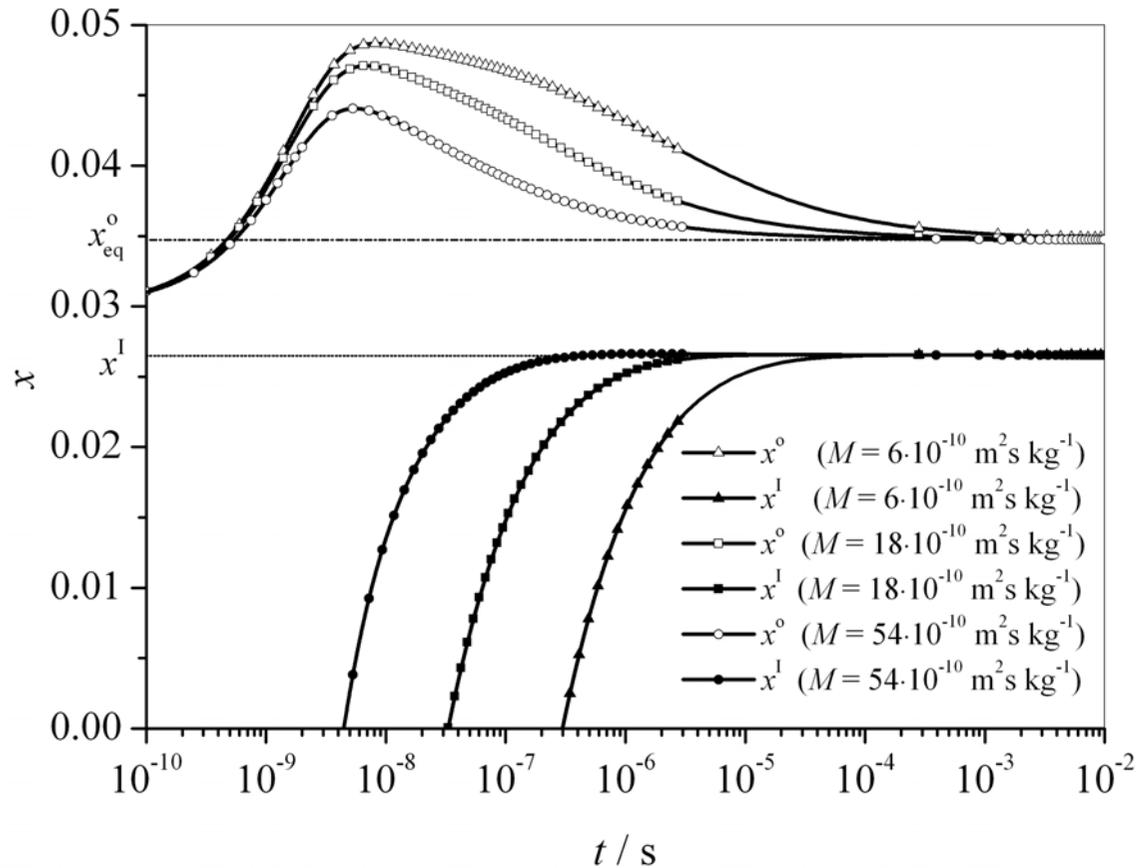


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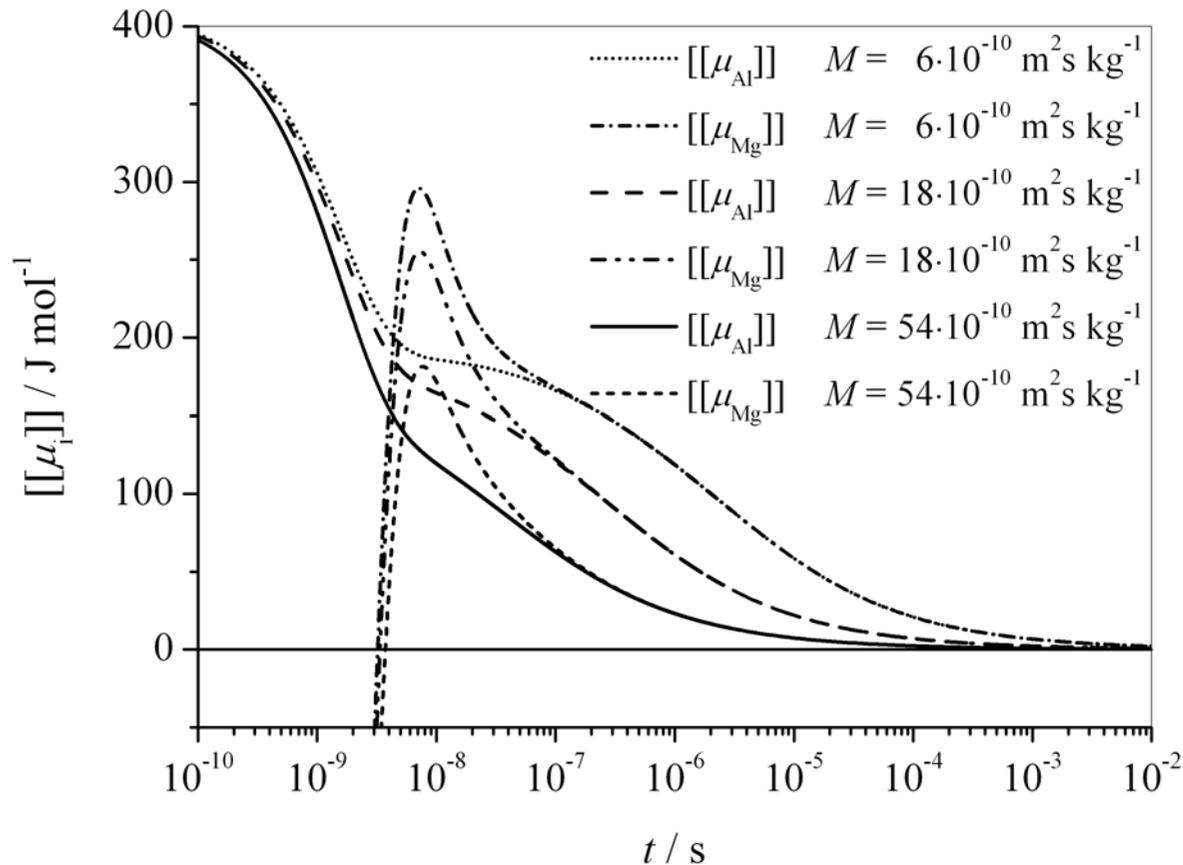


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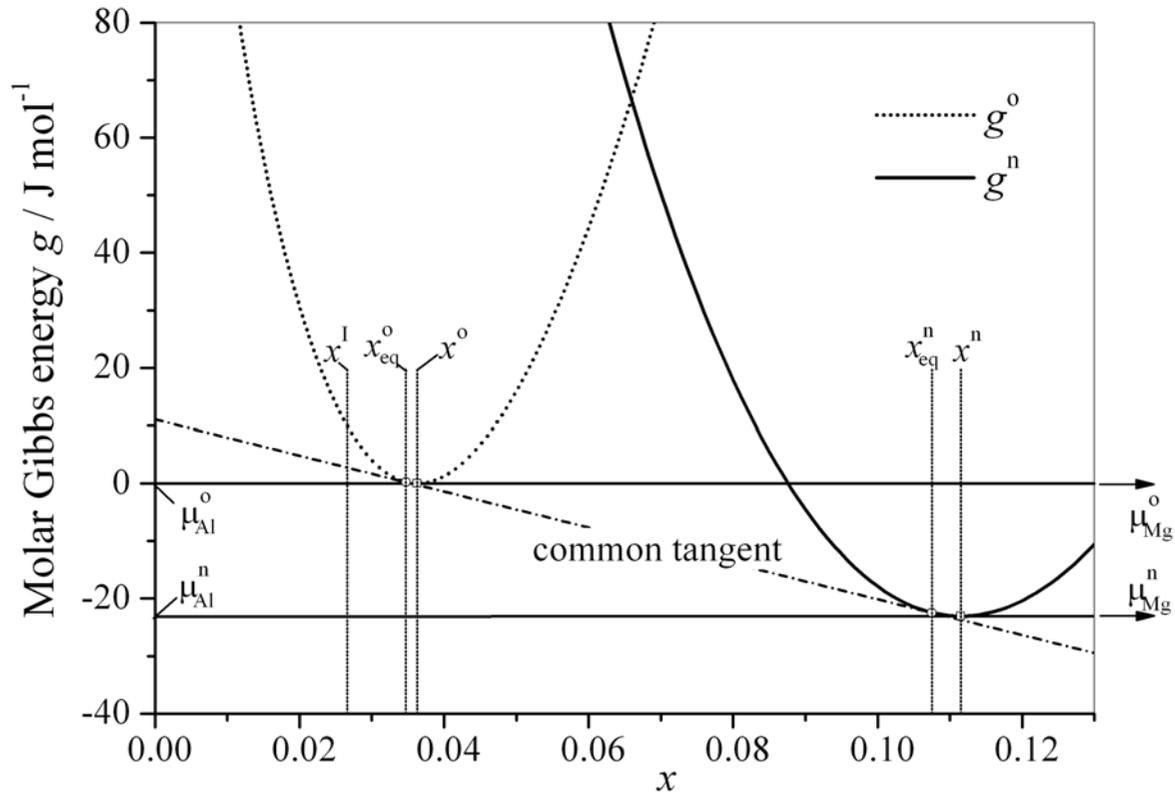


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