
Decarburization of 0.21C-1.3Mn-0.2Si steel at various heating temperatures

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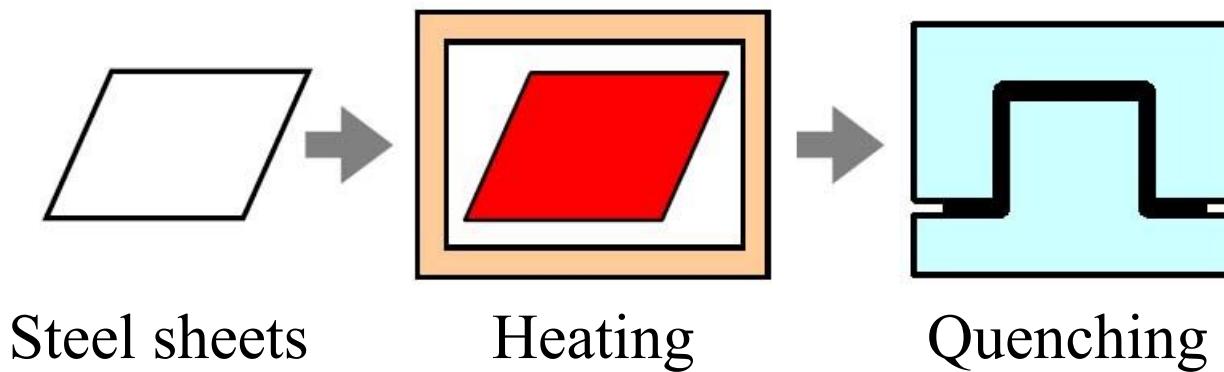
- Background & Purpose
Hot stamping, Decarburization
- Experimental Procedure
Chemical composition, Heat treatment
- Results & Discussion
Temperature dependence of microstructure
Growth behavior of decarburized ferrite
- Conclusions
Optimum heat treatment conditions
Rate-controlled process



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Background

- Hot stamping method
Automotive parts with fully martensite structure



- Heating conditions
 - Austenitic temperature ($\sim 1173\text{K}$) : High temperature
 - Ambient or gas atmosphere : Oxidation atmosphere
- ↓
- Decarburization conditions

Purpose

Microstructure of carbon steel due to decarburization

Ferrite



Pearlite

High temperature oxidation
of metals, Cambridge Univ.
Press, p152

Effects of decarburization on mechanical properties

Advantage	Bendability, Impact strength
Disadvantage	Tensile strength, Fatigue strength

Purpose : Examine the effect of **annealing temperatures**
on **decarburization** using a Fe-0.21C-1.3Mn-0.2Si steel



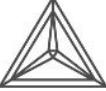
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Experimental Procedure

- Cold rolled sheet steel

Thickness: 2.4mm

Chemical composition and A_{e3} of steel in mass%:



	C	Si	Mn	P	S	A_{e3}
	0.21	0.2	1.3	0.01	0.003	1078K

- Heating conditions

Rapid heating

Water quenching

- Microstructure analysis

Laser scanning microscope (LSM)

Electron probe microanalysis (EPMA)



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Heating conditions

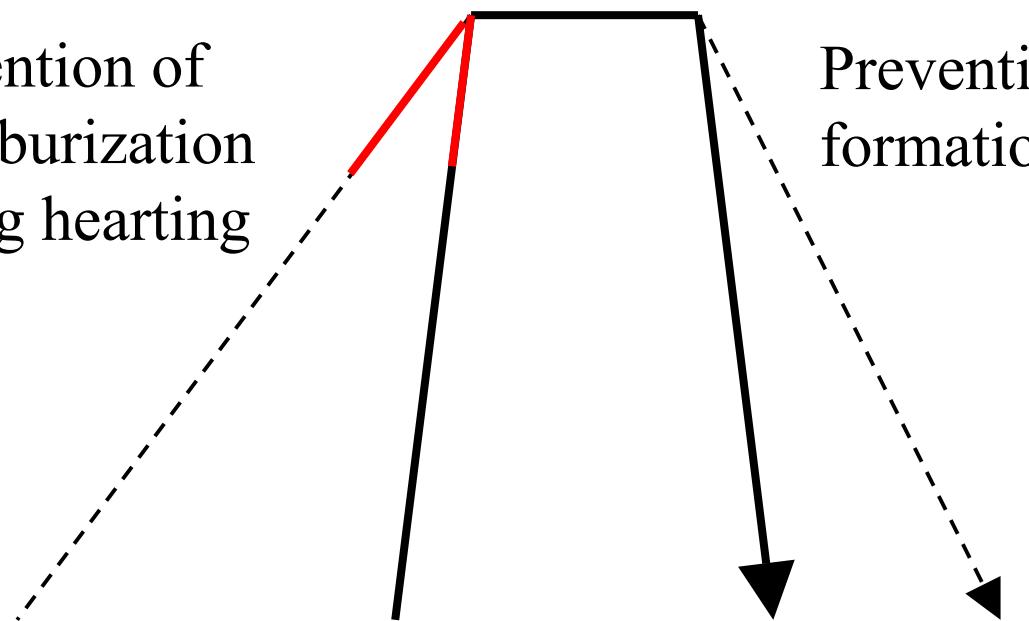
Rapid heating & Water quenching method

Ambient atmosphere

Prevention of decarburization during heating

Isothermal annealing

$T = 773-1173\text{K}$, $t = 100-12800\text{s}$



Direct Electric
Current Heating

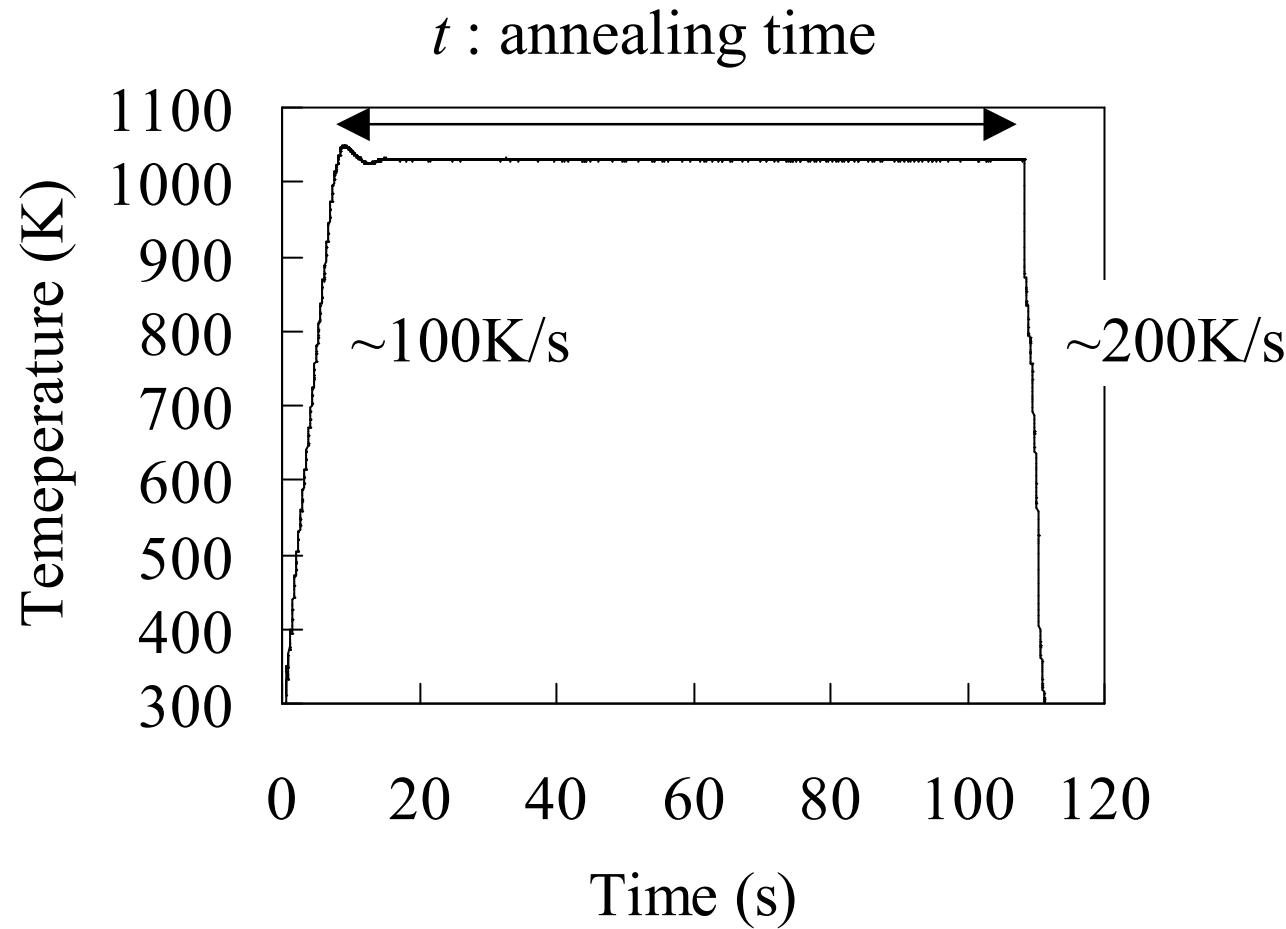
Water Quenching



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Temperature during Heat treatment

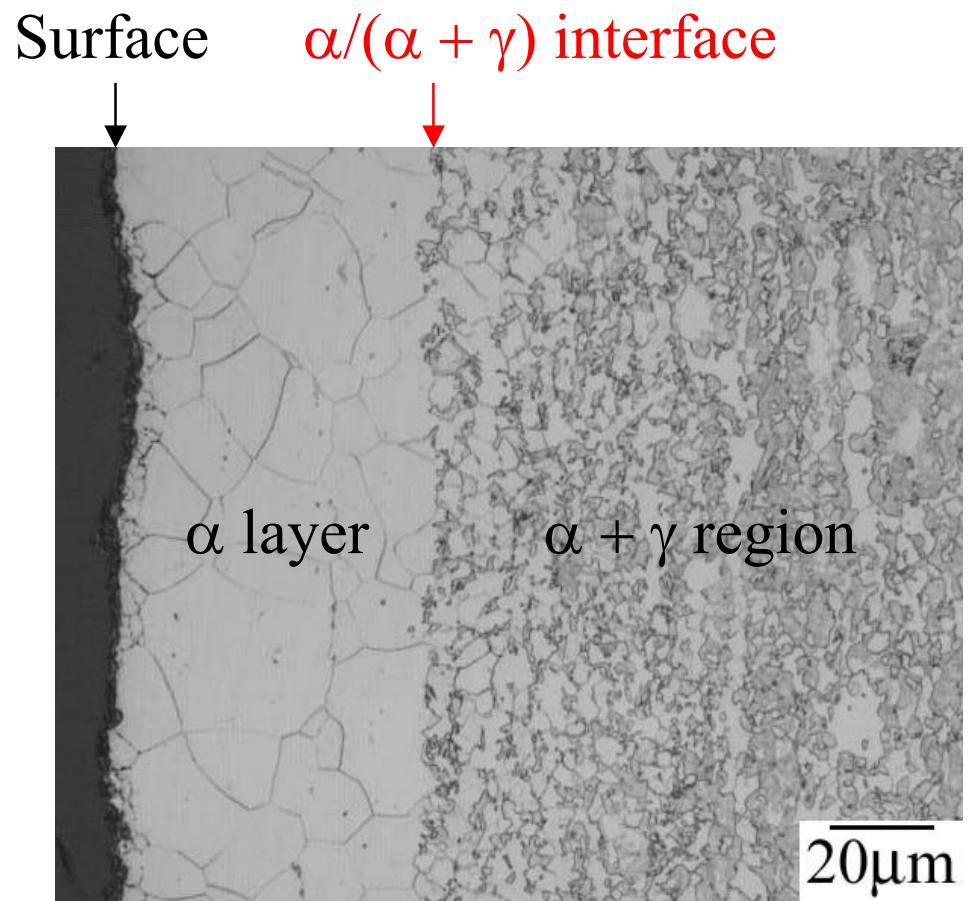
Annealed at 1033K for 100s



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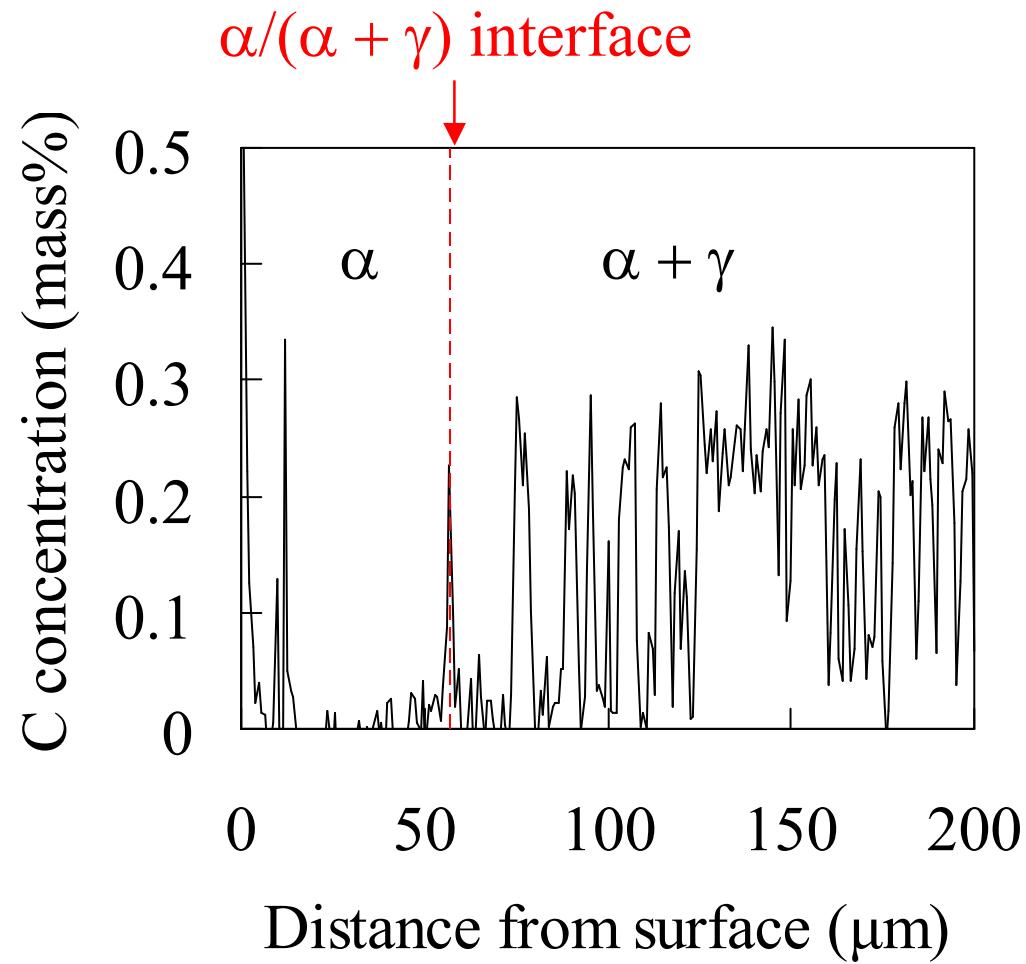
Microstructure

Annealed at 1033K for 1600s



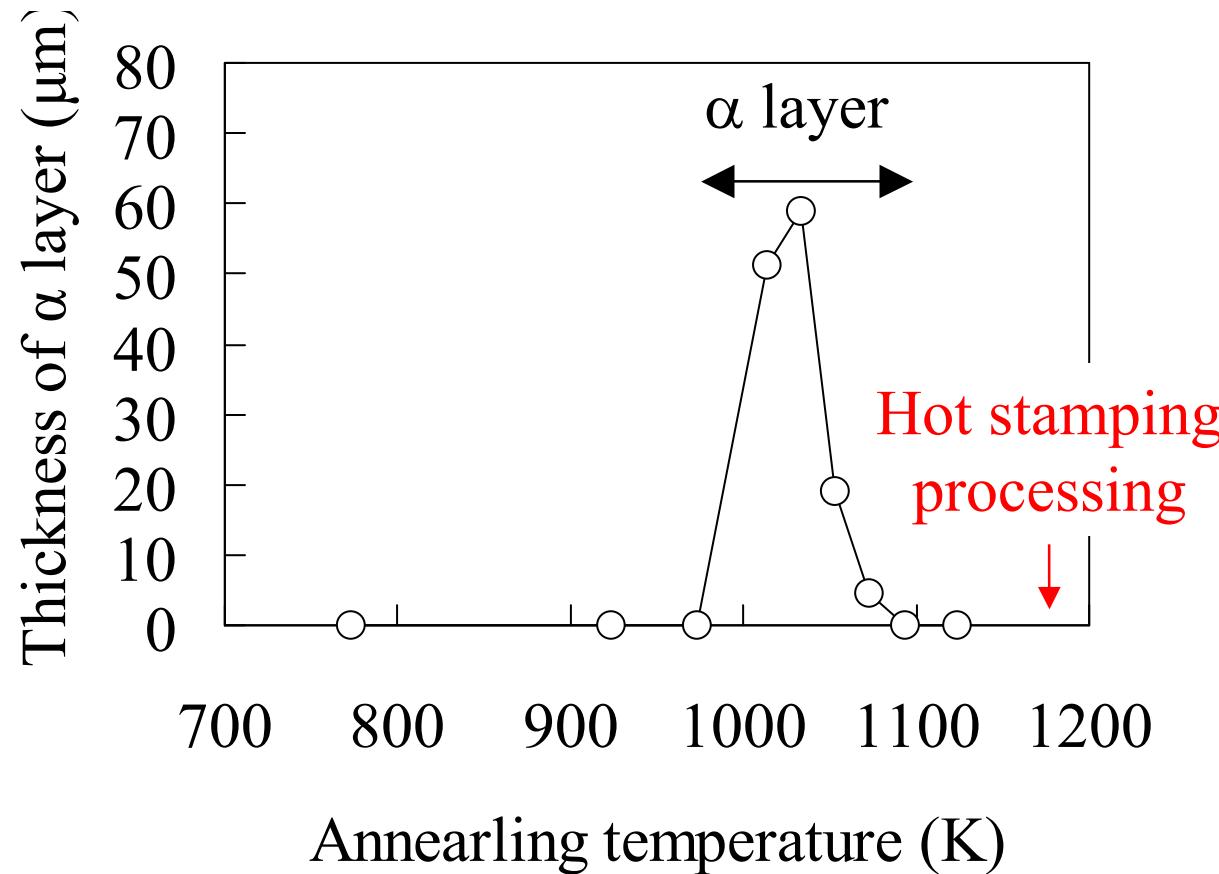
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C concentration profile



Thickness of α layer vs. temperature

Annealed for 1600s



Summary of microstructure observation

Fe–0.21C–1.3Mn–0.2Si, $T = 773\text{--}1173\text{K}$, $t = 1600\text{s}$

- Formation of the ferrite layer at the surface due to decarburization

$T = 1013\text{--}1073\text{K}$

- The peak temperature

$T_p = 1033\text{K}$.

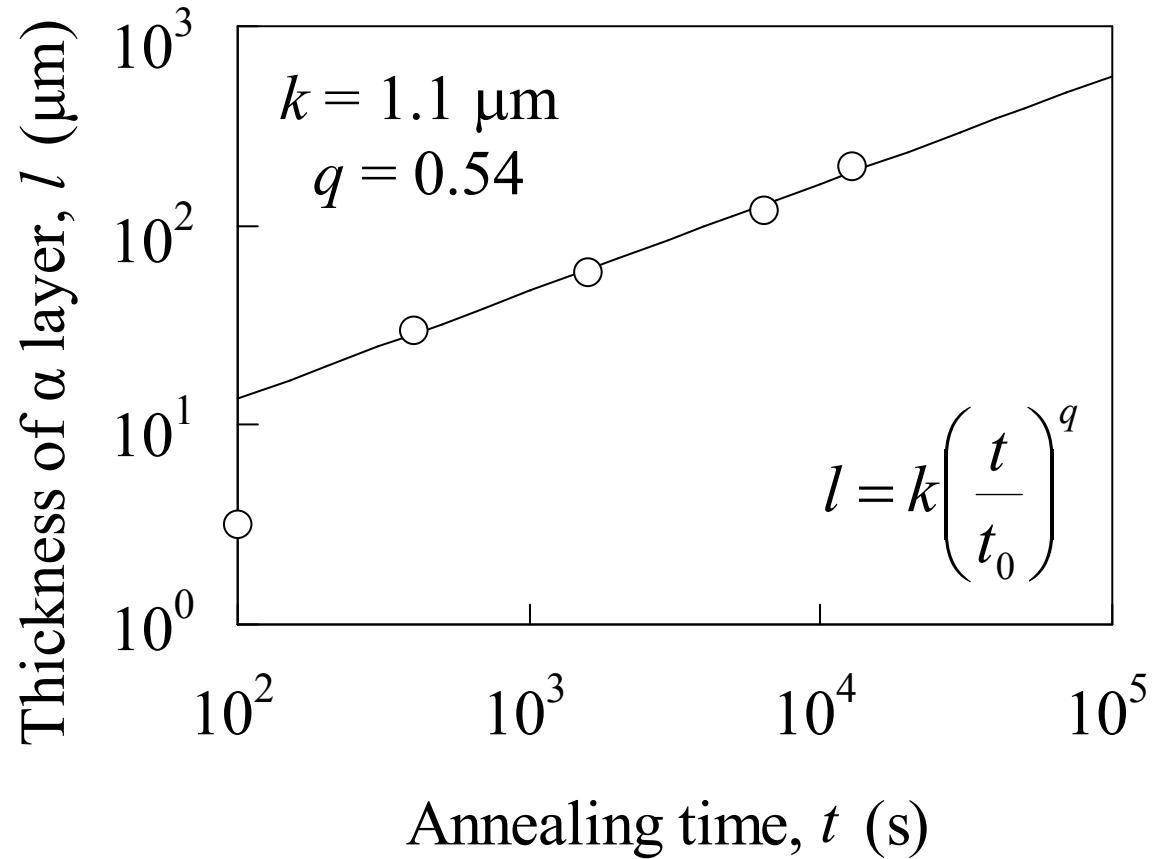
- Heating at $T > 1093\text{K}$

Prevention of the ferrite formation



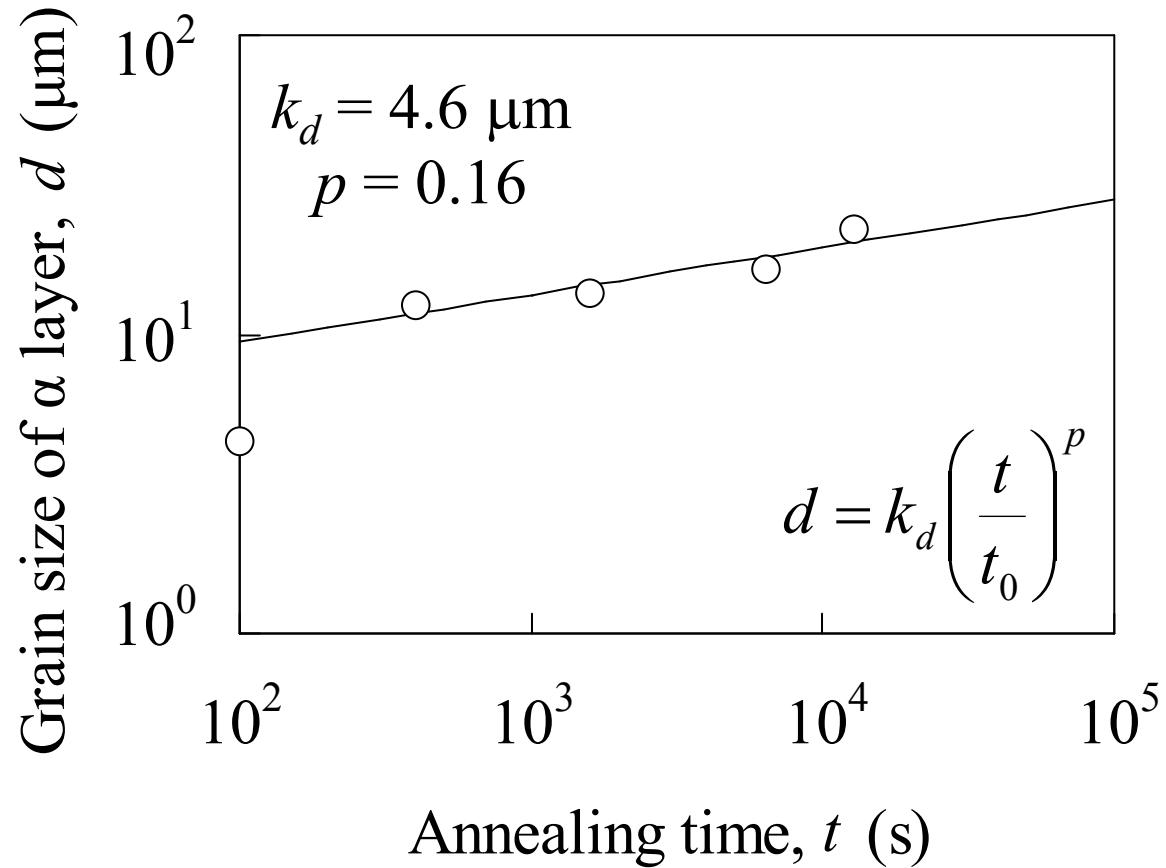
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Growth behavior of α layer



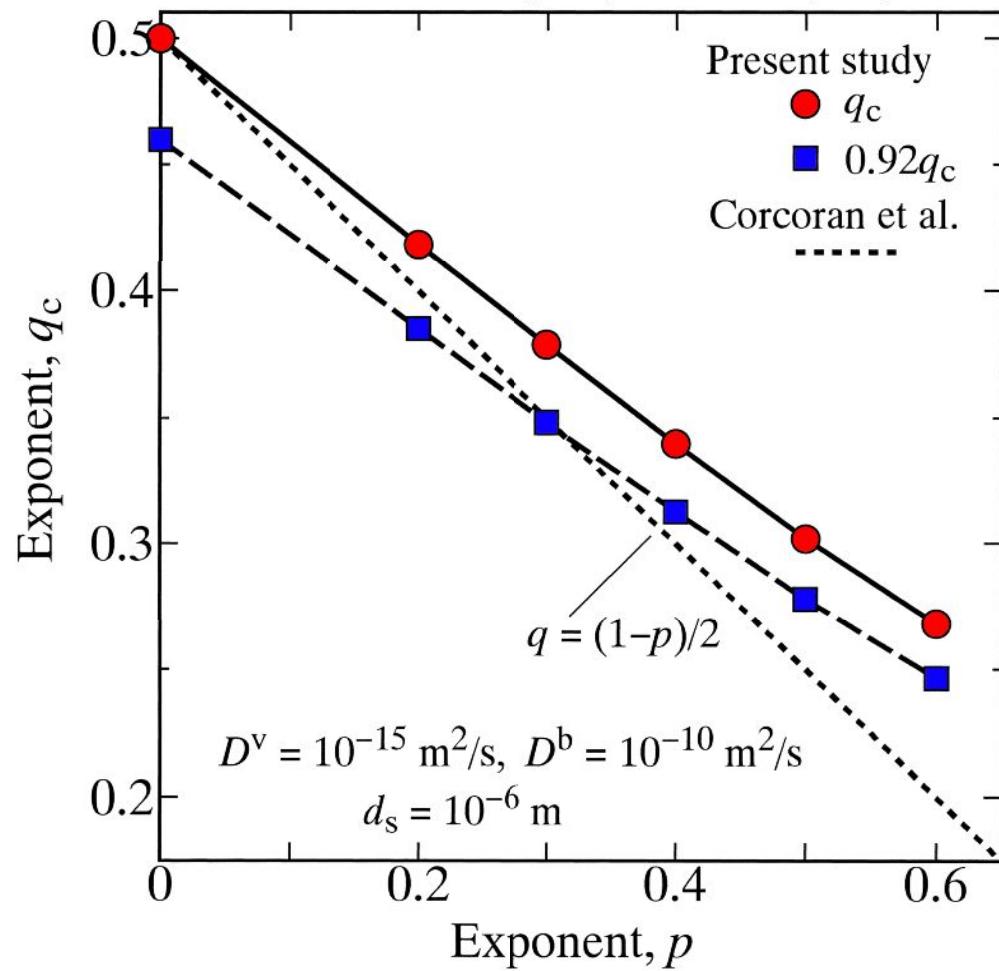
t_0 : unin time (1s), k : proportionality coefficient, q : exponent

Grain growth in α layer



t_0 : unin time (1s), k_d : proportionality coefficient, p : exponent

Relationship between q and p



A. Furuto & M. Kajihara,
Mater. Trans., (2008)

Boundary diffusion
with grain growth

$$q_{cal} = \frac{1 - p_{exp}}{2} = 0.42$$

Y. L. Corcoran et al.,
J. Electron. Mater., (1990)



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Conclusion

Fe-0.21C-1.3Mn-0.2Si, $T = 773\text{--}1173\text{K}$, $t = 100\text{--}12800\text{s}$

- Formation of the ferrite layer at the surface
 $T = 1013\text{--}1073\text{K}$, $T_P = 1033\text{K}$ for 1600s

- Heating at $T > 1093\text{K}$
Prevention of the ferrite formation
- Growth behavior of the ferrite layer
 l vs. t , Parabolic relation ($q \sim 0.5$)
- Rate-controlling process for the ferrite layer during annealing at 1033K

Volume diffusion



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