

Simplified Modelling of the PE / LENP transition

Grenoble, May 9 2006



Growth of ferrite

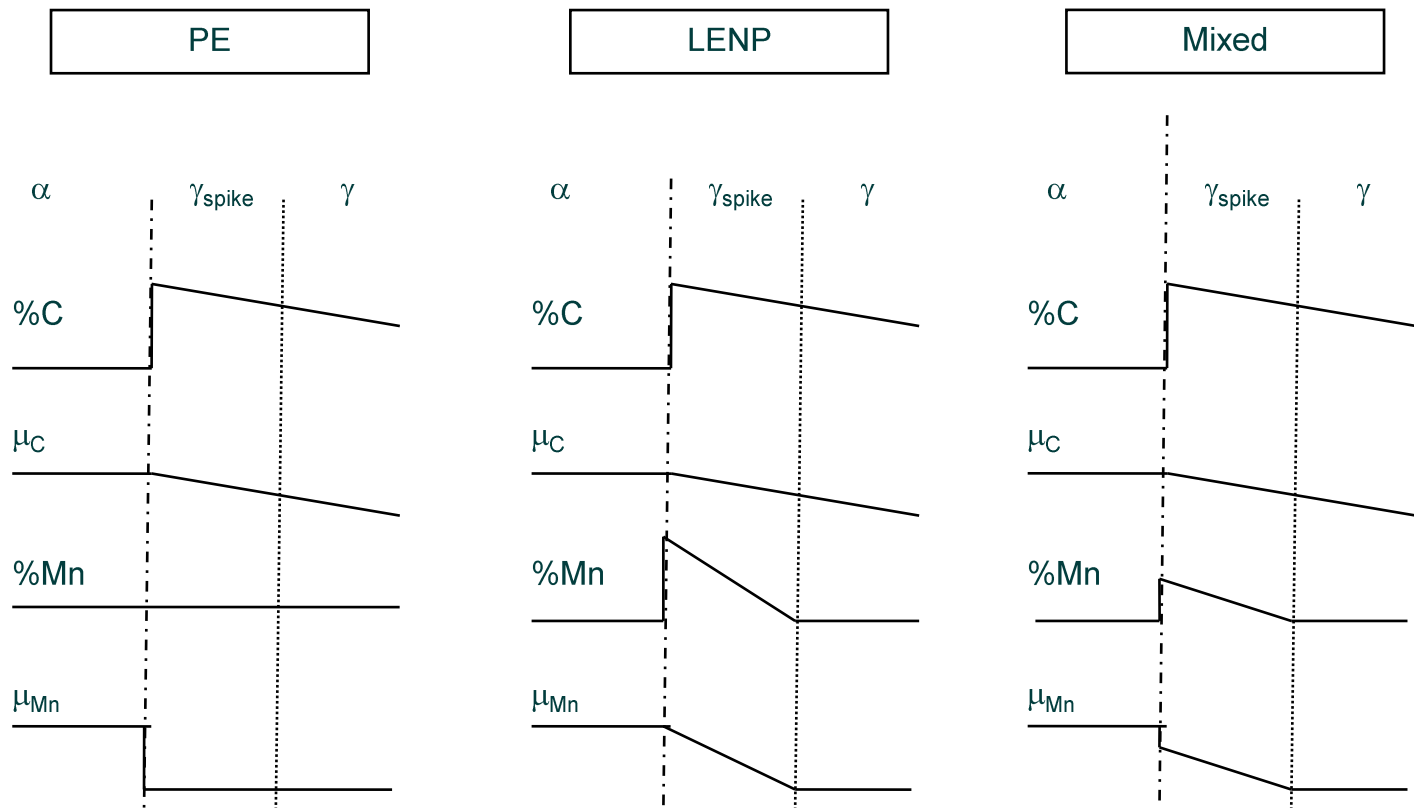
■ Models

- Based on carbon diffusion in austenite
 - Finite difference scheme
- 2 thermodynamic bounds possible
 - LENP
 - Para-equilibrium
 - Mixed mode + dissipation in interface
- Spherical geometry
- Initial system
 - Austenite homogeneous carbon rich
 - Radius determine by the size of the system and the fractions
 - Radius = $0.5 \times \text{distance between centers of 2 ferrite grains}$ ~4μm



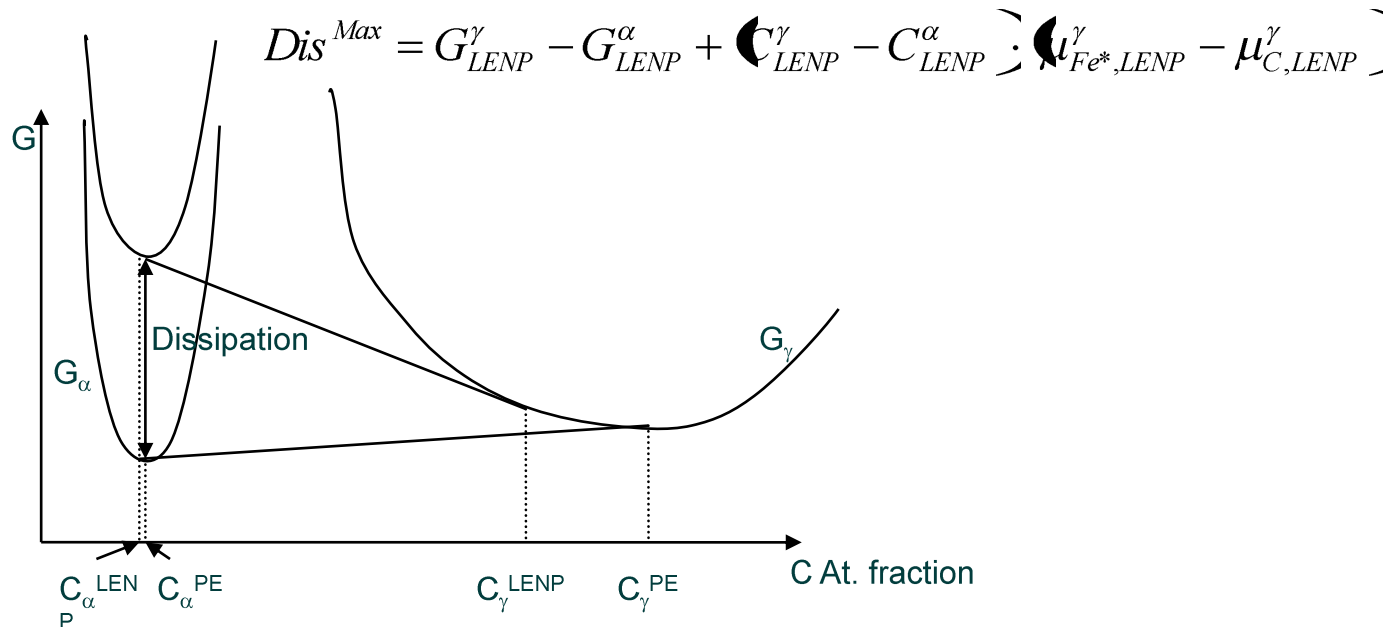
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- Development of a mixed mode model : comparison PE, LENP, mixed mode



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■ Condition at interface



- $LENP = PE + \text{dissipation of energy in the spike}$
- Idea: dissipation in the spike can vary between 0 and the LENP value



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- Flux through the interface

$$-L_{\text{int}} \cdot \frac{d\mu}{dt} = \frac{v}{V_m} \cdot (\mu_k - \mu_k^\alpha) = J_{\text{int}}$$

- Driving force for jump of 1 mole through the interface

$$\Delta\mu_{jn} = (\mu_j - \mu_n) - (\mu_j^\alpha - \mu_n^\alpha)$$

- Hypothesis:

- no accumulation in interface in function of time
- Dissipation = Dissipation spike + dissipation interface

$$J = J_{\text{int}} = J_{\text{spike}}$$

$$\Delta\mu = \Delta\mu_{\text{int}} + \Delta\mu_{\text{spike}}$$



$$J = -L \cdot \Delta\mu$$

$$\frac{1}{L} = \frac{1}{L_{\text{int}}} + \frac{1}{L_{\text{spike}}}$$

- Extreme cases

- PE: dissipation = 0 $\leftrightarrow L_{\text{int}} \sim \infty$
- LENP: dissipation = dissipation LENP



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▪ LENP case

- $\Delta \mu \sim 0$

$$Dissipation = -\frac{V_m}{v} \cdot \left(I_{spike} \cdot \Delta \mu^{spike} \right)$$

$$Dissipation = -\frac{V_m}{v} \cdot \left(L_{spike} \cdot \Delta \mu \right) \cdot \Delta \mu = \frac{V_m}{v} \cdot \frac{v}{V_m} \cdot \left(y_k - y_k^\alpha \right) \cdot \Delta \mu$$

$$L_{spike} = -\frac{v}{V_m} \cdot \frac{\left(y_k - y_k^\alpha \right)}{\Delta \mu^{spike}}$$

$$\frac{Dis^{LENP}}{\Delta \mu^2} = \frac{\left(y_k - y_k^\alpha \right)}{\Delta \mu}$$

Assumed to
be constant



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■ Mixed case

$$Dis = \frac{V_m}{v} \cdot \left(\frac{1}{L_{int}} + \frac{1}{\frac{v}{V_m} \cdot \left(\frac{Dis^{LENP}}{\Delta\mu} \right)} \right)^{-1} \cdot \Delta\mu$$

or

$$Dis = \frac{L_{int} \cdot Dis^{LENP}}{L_{int} + \frac{v}{V_m} \cdot \frac{Dis^{LENP}}{\Delta\mu}}$$



V >> -> PE
V << -> LENP

Transition from PE to LENP function of
L_{int} and v



Estimation for Lint

- Lint

- Assumption: related to grain boundary diffusion

$$J = -D \cdot \frac{\partial C}{\partial x}$$

or

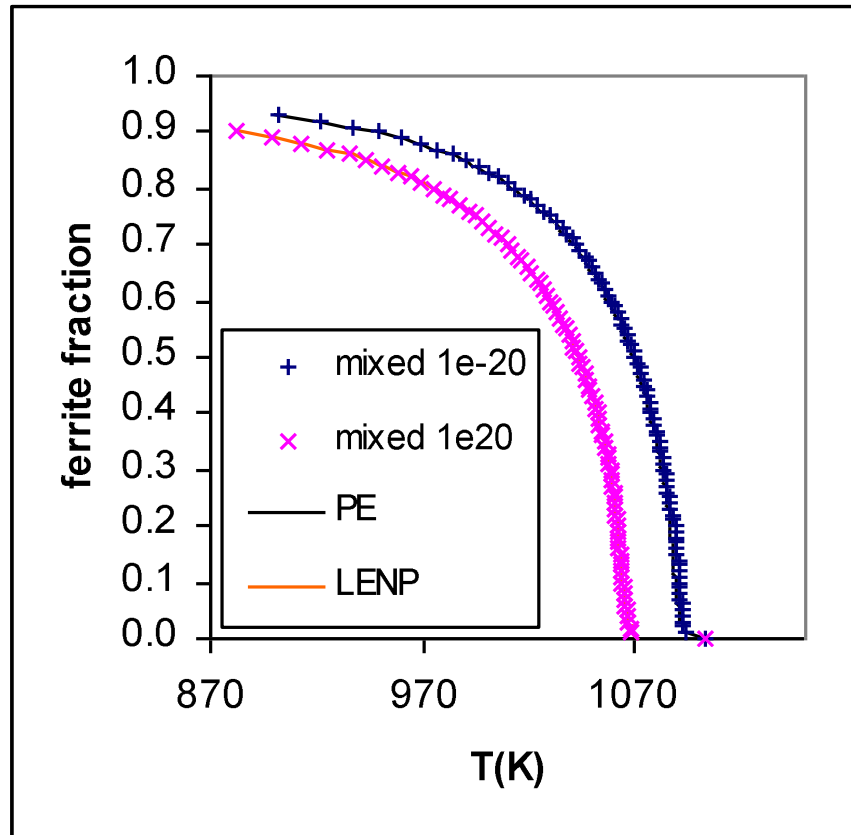
$$J = -D \cdot \frac{dC}{d\mu} \frac{\partial \mu}{\partial x}$$

$$L_{\text{int}} = \lambda \frac{D_{Ni}^{GBfcc}}{a} \cdot \frac{dC}{d\mu}$$



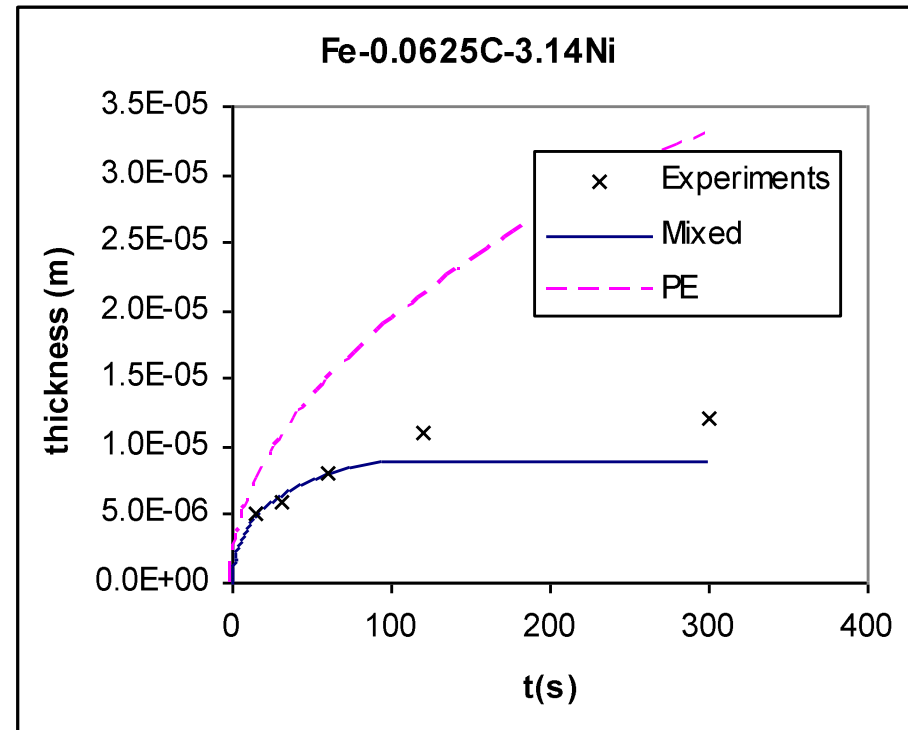
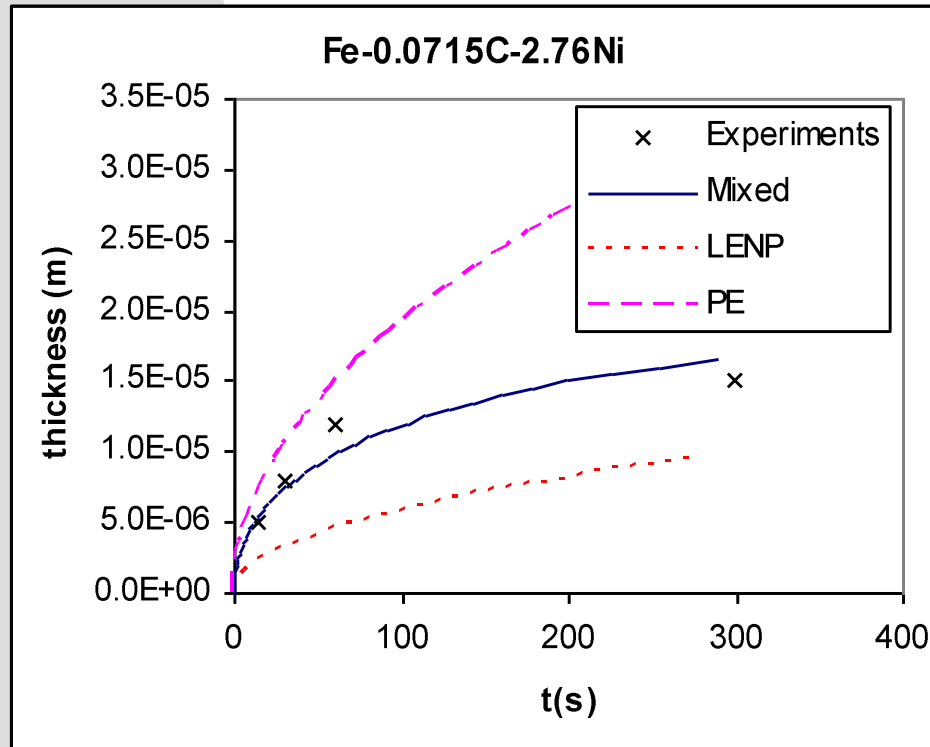
Examples

- 0.1%C, 1%Mn, $R=10\mu\text{m}$, 1°C/s , 3D



Comparison with work of C. Hutchinson (2003)

- $\Lambda \sim 100$



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- Estimation from intercritical annealing (RFCS project)

Steel	C	Mn	Si	Cr	Mo
1	0.09	1.4	0.15	0.75	/
2	0.14	1.46	0.45	0.2	0.07



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- Comparison with experimental results (martensite fraction)

Composition	Holding T (°C)	Quench Temperature (°C)	Cooling rate (°C/s)	Measured	LENP	PE a	Mixed mode
1	800	800	WQ	55	/	/	/
1	800	675	10	15	25	11	20
1	800	550	10	10	13	5	7
1	800	675	25	23	31	11	18
1	800	550	25	11	14	5	8
1	800	675	90	19	43	16	32
1	800	675	90	17	25	7	13
2	810	810	WQ	50	/	/	/
2	810	700	3	19	41	19	29
2	810	600	3	13	17	10	15
2	810	20	3	14 (*)	14	10	10
2	840	840	WQ	100	/	/	/
2	840	730	10	82	96	32	74
2	840	640	10	14	38	13	20
2	840	540	10	11	22	8	11



Better description with the mixed mode than with LENP or PE hypothesis



Conclusion

- Simplified mixed mode model has been developed, with only computation of carbon diffusion
- Fitting of the interface condition is based on grain boundary conditions
- Possibility to reproduce with a good agreement the experimental results of C.Hutchinson between LENP and PE.
- Perspective
 - Determination of the size of the cell remains the key parameter to master the phase transformation kinetics.

