85-1186-14792

Province of British Columbia

Ministry of Energy, Mines and Petroleum Resources

ASSESSMENT REPORT TITLE PAGE AND SUMMARY

TYPE OF REPORT/SURVEY(S) Geochemical; Geophysical

TOTAL COST $10,000.00

AUTHOR(S) A.M.S. Clark SIGNATURE(S) [signature]

DATE STATEMENT OF EXPLORATION AND DEVELOPMENT FILED Dec. 11, 1985 YEAR OF WORK 1985

PROPERTY NAME(S) Whymp

COMMODITIES PRESENT --

B.C. MINERAL INVENTORY NUMBER(S), IF KNOWN --

MINING DIVISION Victoria NTS 92C/16E

LATITUDE 49°56.5' LONGITUDE 124°11.5'

NAMES and NUMBERS of all mineral tenures in good standing (when work was done) that form the property [Examples: TAX 1-4, FIRE 2 (12 units); PHOENIX (Lot 1706); Mineral Lease M 123; Mining or Certified Mining Lease ML 12 (claims involved)]:

Whymp 1 (18 units)

Whump 2 (20 units)

OWNER(S)

(1) Imperial Metals Corporation

MAILING ADDRESS

#800-601 West Hastings St.
Vancouver, B.C. V6B 5A6

OPERATOR(S) (that is, Company paying for the work)

(1)

MAILING ADDRESS

#800 - 601 West Hastings St.
Vancouver, B.C. V6B 5A6

SUMMARY GEOLOGY (lithology, age, structure, alteration, mineralization, size, and attitude):

The property is underlain by Middle Pennsylvanian Sicker Group sediments, Upper Triassic Karmutsen basaltic volcanics and Jurassic Island Intrusions.

REFERENCES TO PREVIOUS WORK Muller, J.W. 1977. Geology of Vancouver Island Geol. Surv. Canada, Open File 463.
Clark, A.M.S., 1984. Assessment Report.

(over)

TYPE OF WORK IN THIS REPORT	EXTENT OF WORK (IN METRIC UNITS)	ON WHICH CLAIMS	COST APPORTIONED
GEOLOGICAL (scale, area)			
Ground			
Photo			
GEOPHYSICAL (line-kilometres)			
Ground			
Magnetic			
Electromagnetic	8.75 km	Whymp 1,2	400
Induced Polarization			
Radiometric			
Seismic			
Other			
Airborne			
GEOCHEMICAL (number of samples analysed for ....)			
Soil	208; multiplement., Au	Whump 1,2	8,400
Silt			
Rock			
Other			
DRILLING (total metres; number of holes, size)			
Core			
Non-core			
RELATED TECHNICAL			
Sampling/assaying			
Petrographic			
Mineralogic			
Metallurgic			
PROSPECTING (scale, area)			
PREPARATORY/PHYSICAL			
Legal surveys (scale, area)			
Topographic (scale, area)			
Photogrammetric (scale, area)			
Line/grid (kilometres)	8.75 km	Whymp 1,2	1,200
Road, local access (kilometres)			
Trench (metres)			
Underground (metres)			
		TOTAL COST	10,000

FOR MINISTRY USE ONLY	NAME OF PAC ACCOUNT	DEBIT	CREDIT	REMARKS:
Value work done (from report)				
Value of work approved				
Value claimed (from statement)				
Value credited to PAC account				
Value debited to PAC account				
Accepted .... Date	Rept. No.			Information Class

TABLE OF CONTENTS

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LIST OF ILLUSTRATIONS

SUMMARY

Soil samples were collected along contour lines on each side of the Central Chemainus Valley, as well as on a grid at the north end of the property. Results show generally weak base and precious metals anomalies showing no distinctive pattern of association. A VLF-EM survey was also undertaken with only weak pseudo-anomalies, apart from one strong (negative) dip angle anomaly which should be checked in the field.

INTRODUCTION

Objectives

A previous regional stream-silt sampling program had indicated silt samples with anomalous values of gold, copper, silver, arsenic and zinc from streams draining the area of the claims. In 1984, contour-based soil samples taken as follow-up of the stream samples indicated anomalous gold and copper values in the soils at the source of Chemainus River. The 1985 program consisted of soil sampling on a grid at this anomalous location and also contour soil sampling of hill-slopes not previously sampled.

Location

The Whymp #1 and #2 claims are situated approximately 30 kms southwest of Nanaimo at the headwaters of the Chemainus River on Mt. Whymper (Figures 1 and 2).

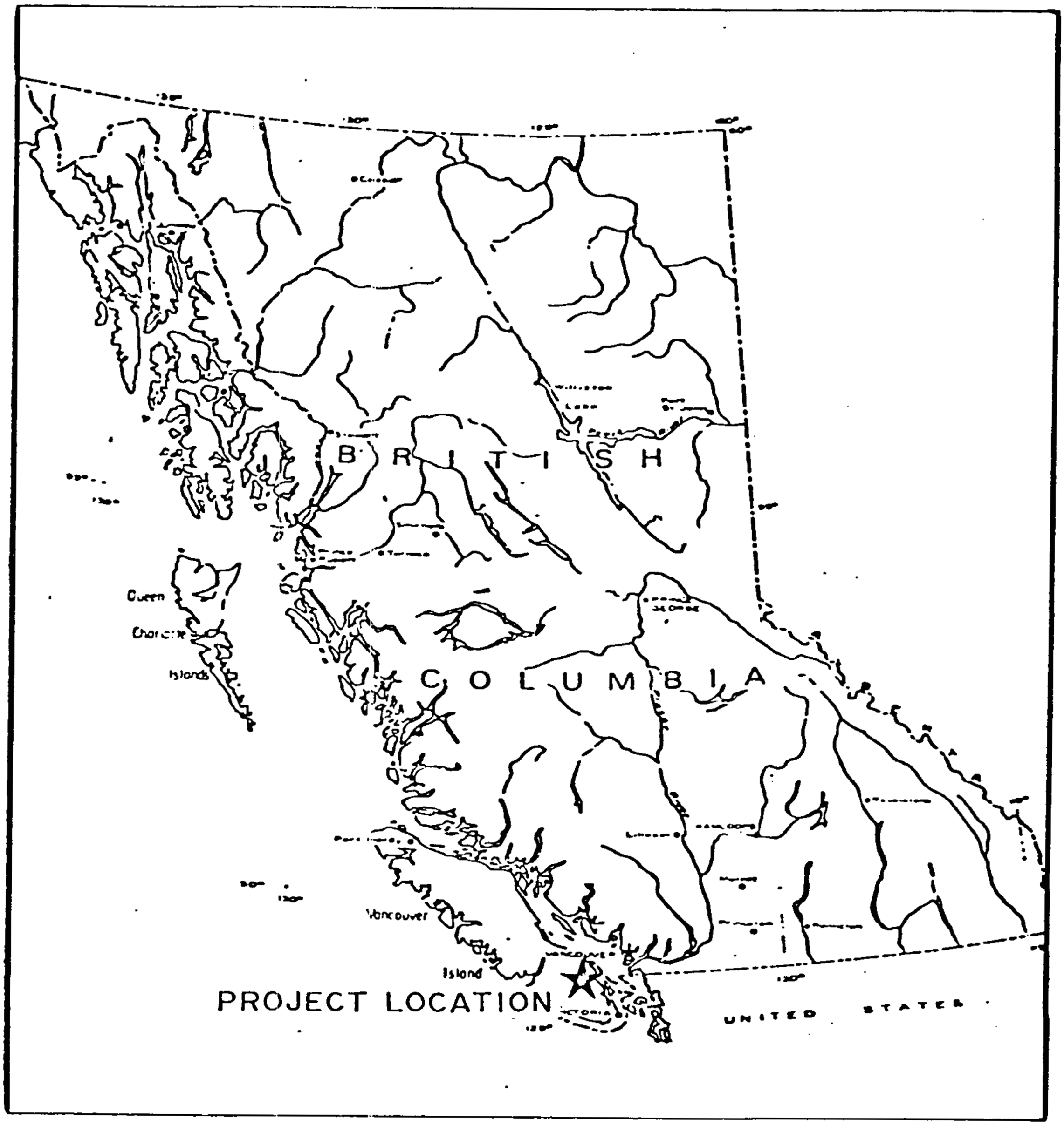
Property

The property consists of 2 adjoining claims (Figure 3).

Name	Units	Record No.
Whymp #1	18	1150
Whymp #2	20	1151

Access

Access is by logging road (MacMillan-Bloedel Ltd.) from South Wollaston, south of Nanaimo, along the Nitinat road then down the Nanaimo River turn-off to the south to Jump Lake, or from Duncan along the Copper Canyon road and up to the Chemainus headwaters.



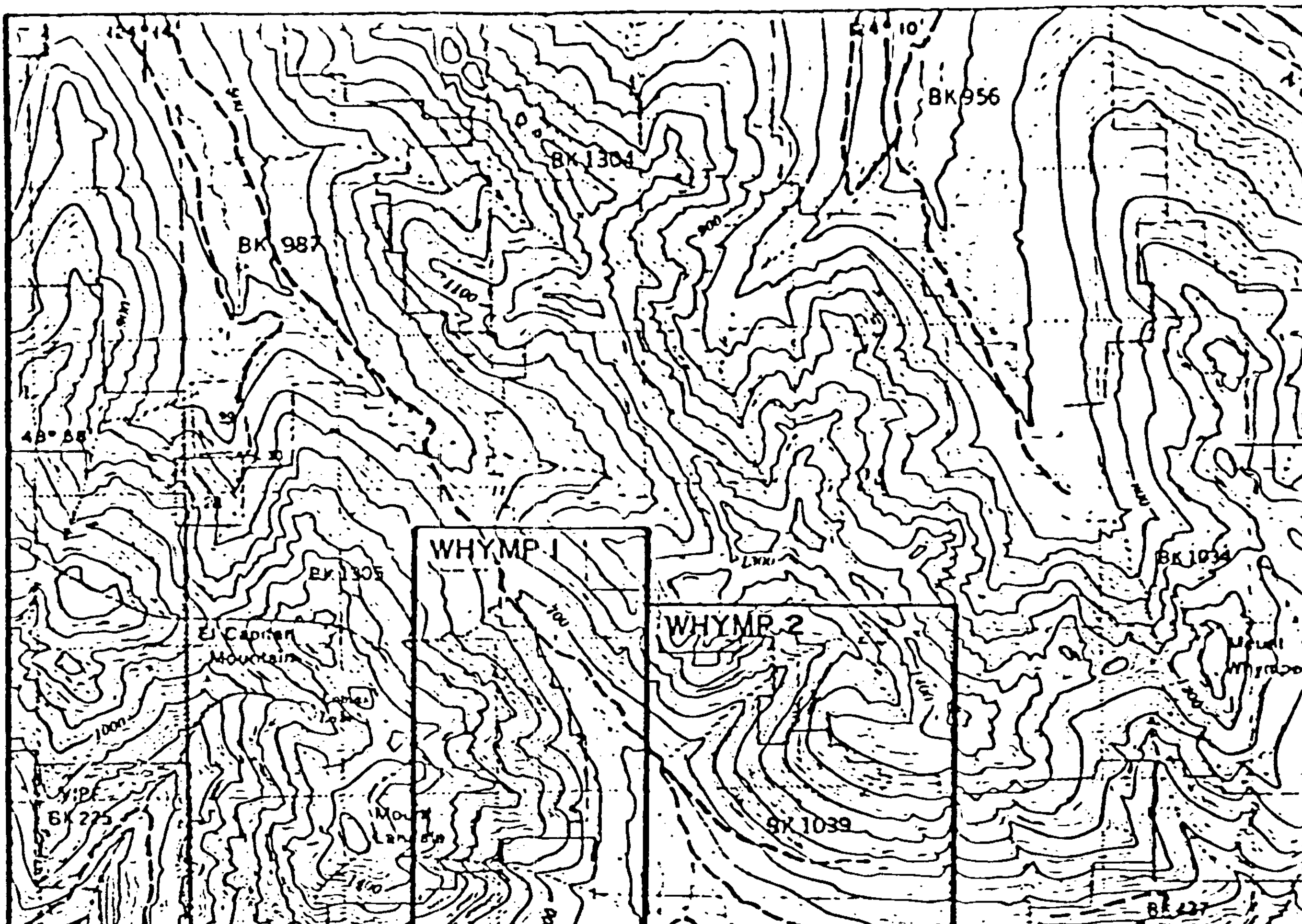
IMPERIAL METALS CORPORATION

MT. WHYMPER

FIGURE 1

LOCATION MAP

SCALE:	GEOLOGIST: A. CLARK
DATE: NOVEMBER 1984	DRAWN BY: S. HAWORTH



IMPERIAL METALS CORPORATION

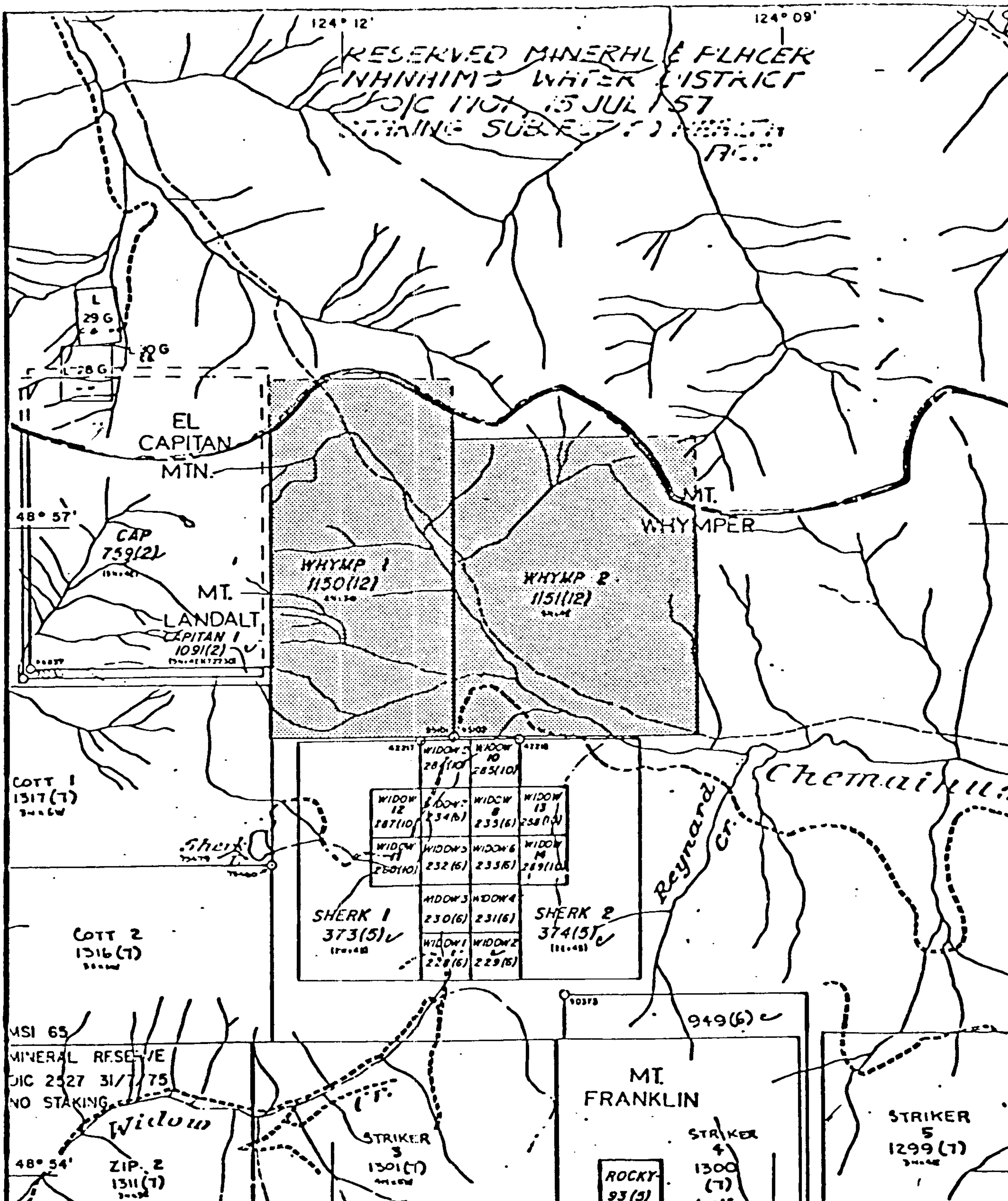
MT. WHYMPER

FIGURE 2 N.T.S. 92C/16E

TOPOGRAPHIC MAP

Km 1 0 1 2 Km

SCALE: 1:50 000	GEOLOGIST: A. CLARK
DATE: NOVEMBER 1984	DRAWN BY: S. HAWORTH



IMPERIAL METALS CORPORATION

MT. WHYMPER

FIGURE 3 N.T.S. 92C/16E

CLAIM MAP

Km 1 0 1 2 Km

SCALE: 1:50 000	GEOLOGIST: A. CLARK
DATE: NOVEMBER 1984	DRAWN BY: S. HAWORTH

Operations

The program was undertaken from Duncan on a daily basis from October 2 to October 13, 1985.

Physiography

Topography is steep and heavily wooded, except where logging has been completed. The claims extend from one ridge-crest across a valley to another ridge-crest, from about 550m to 1500m above sea level.

PREVIOUS WORK

Published

In 1977 Muller published an open-file report on the geology of Vancouver Island.

Assessment

A report by Imperial Metals Corporation covering assessment work (contour soil sampling) in 1984.

GEOLOGY

According to Muller the property is underlain by Middle Pennsylvanian Sicker Group sediments and Upper Triassic Karmutsen basaltic volcanics, intruded by the Jurassic Island intrusions of granodioritic to quartz dioritic composition. The property was not geologically mapped at the time of the soil sampling.

SAMPLE COLLECTION AND ANALYSIS

Samples of soil were collected from the B-horizon where this could be distinguished. The B-horizon was taken to be the first reddish soil horizon below the grey surficial horizon of soil. Locally, because of the steep terrain no soil horizons, as such, were developed, and soils had to be collected from "pore" spaces between boulders, at depths from surface (excluding the humic horizon) to about 40 cms depth. Soil sample descriptions are given in Appendix 1.

Analysis was by induction coupled plasma method for 30 elements, and by atomic absorption for gold. The method employed by the laboratory and the elements and results are given in Appendix 2. The elements considered of significance in this program (with their assumed anomalous thresholds) are:

Element	Thresholds
Copper	100 ppm
Lead	20 ppm
Zinc	100 ppm
Silver	1 ppm
Arsenic	25 ppm
Barium	200 ppm
Gold (AA)	15 ppb

Correlation co-efficients have been calculated for all 30 elements and histograms plotted for copper, zinc, silver, arsenic and gold based on the soil sample results from the grid (Appendix 3). These statistics are considered acceptable for interpretation of the contour samples as well. There is unexpectedly, practically no correlation among the elements, with even common pairs such as gold and arsenic having practically no correlation (Appendix 3).

DISCUSSION OF RESULTS

Contour Sampling

Soil samples were collected along traverses on both sides of the valley, covering areas not previously sampled (Figure 4). Because of cliffs and steepness of terrain some areas could not be adequately soil sampled.

Generally, 25 ppb has been used as the cut-off for anomalous gold values in soils, in which case only one sample is anomalous (Figure 5). However, the histogram of 5 ppb intervals (Appendix 3) suggests there may be a weak second "peak" developed about 10 to 20 ppb where the histogram bars appear to break from a smooth bell curve. If 15 ppb is taken as the anomalous threshold, then there are seven anomalous samples. These samples are not, however, located in any one area, but are scattered along the two hillsides and therefore are not considered to indicate an anomlous gold area for follow-up.

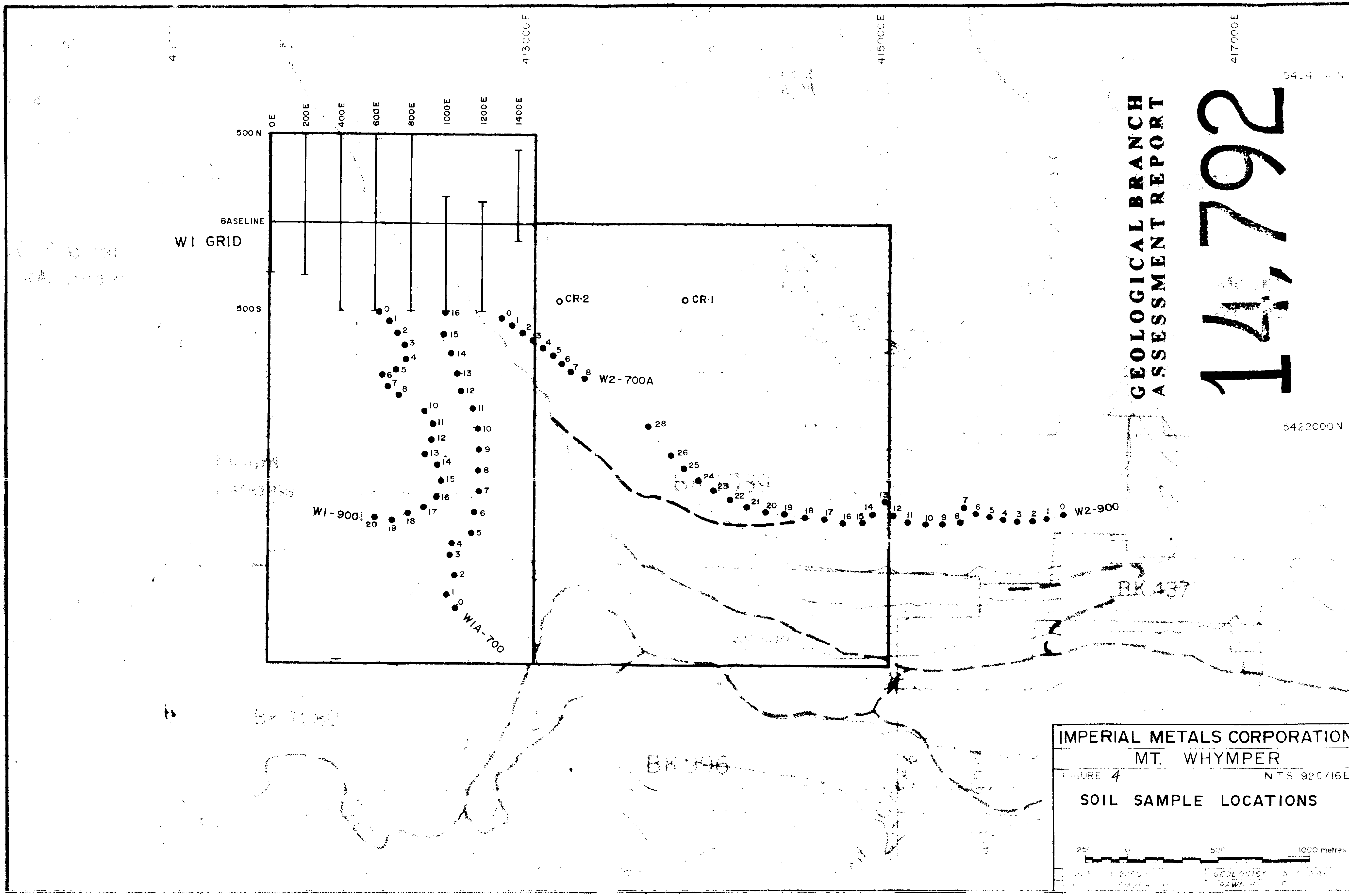
There are no anomalous silver samples.

Arsenic shows three anomalous samples, both associated with raised gold values, of which two are near one another which may indicate a similar source and should be checked in the field.

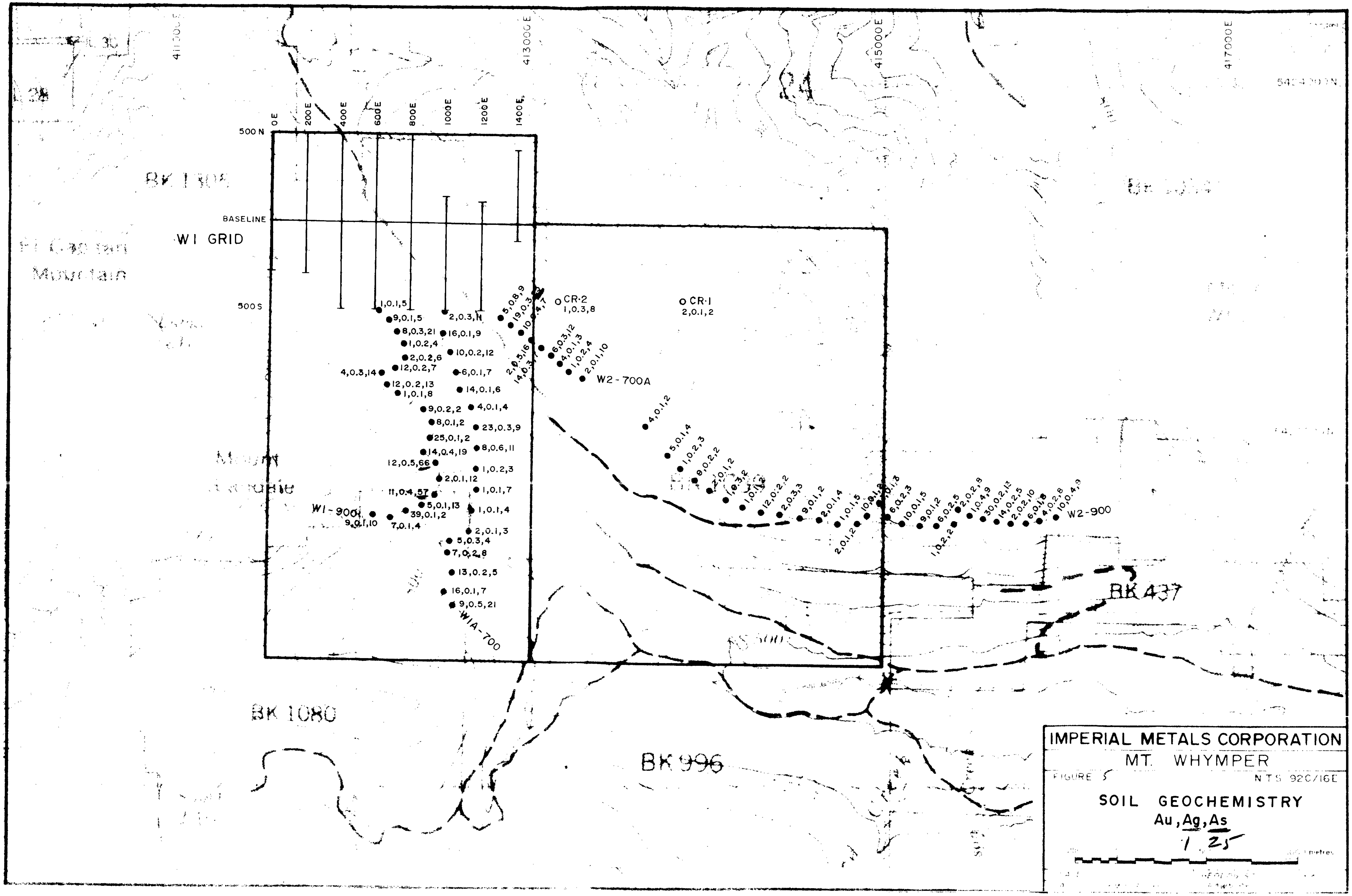
For Vancouver Island soil samples, 50 ppm or 100 ppm copper are usually considered anomalous. However, on this property there are many samples with greater than 100 ppm (Figure 6). These are not in a single localized area, and so do not appear to be due to a single anomalous (ore deposit) source, but rather due to rocks with high background copper (basic volcanics?). The highest values are from the W1-900 contour sample line and the area should be followed up with prospecting and rock sampling.

Anomalous lead values are considered to be those over about 20 ppm, of which there are only a few, mainly on the lower contour sample line on the west of the valley. A field check should be undertaken to determine whether these anomalies are originating lower down than the copper anomalies.

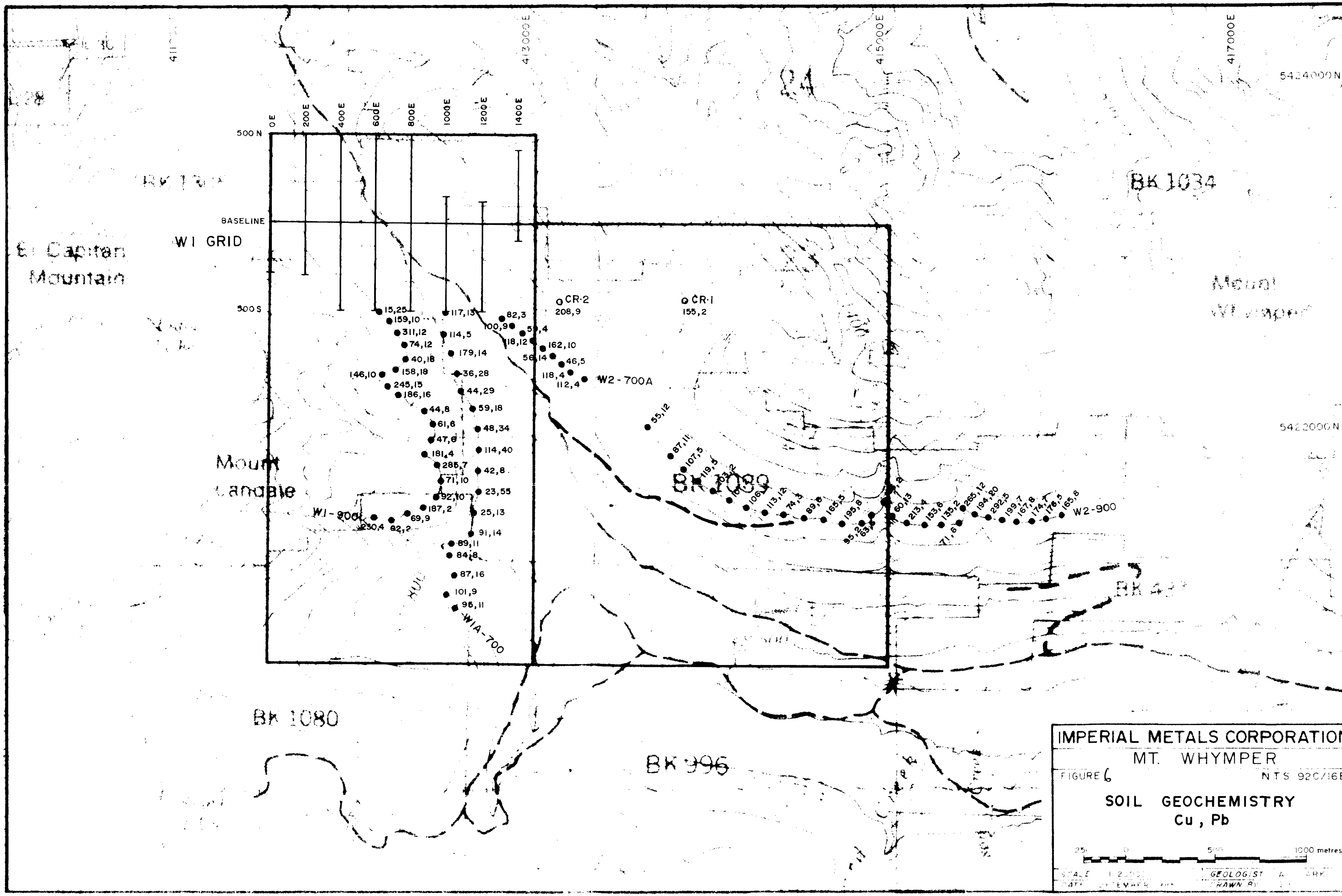
At 100 ppm threshold for anomalous zinc, there are several anomalous values, mainly on the eastern end of the property.

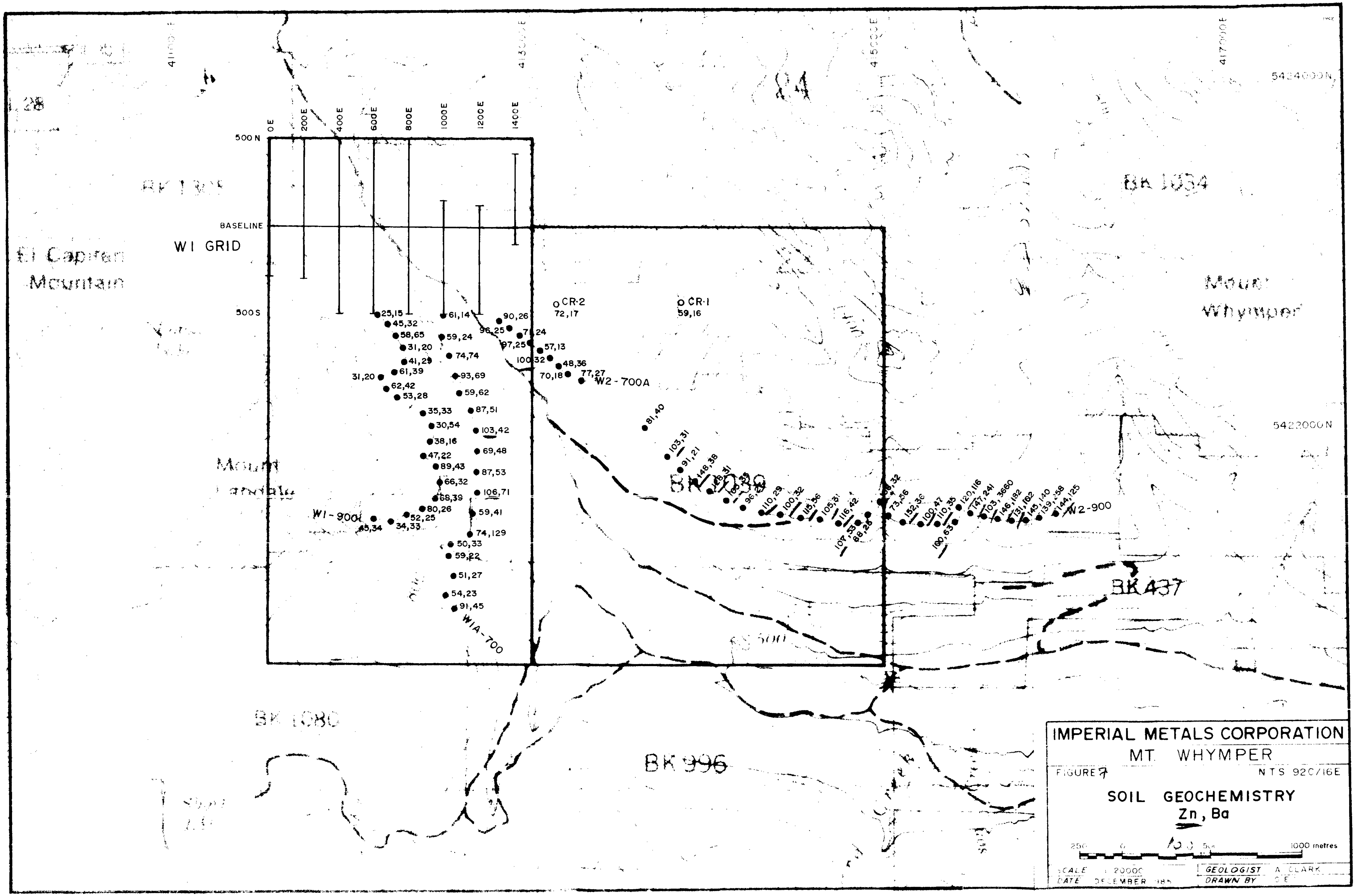


413000E
415000E
417000E
5422000N
0E
200E
400E
600E
800E
1000E
1200E
1400E
500 N
BASELINE
W1 GRID
500S
CR·2
CR·1
W2-700A
W2-900
W1-900
W1A-700
BK 437
BK 1196
GEOLOGICAL BRANCH
ASSESSMENT REPORT
14,792
IMPERIAL METALS CORPORATION
MT. WHYMPER
FIGURE 4
NTS 92C/16E
SOIL SAMPLE LOCATIONS
1000 metres
GEOLOGIST
DRAWN BY



IMPERIAL METALS CORPORATION
MT. WHYMPER
FIGURE 5
N.T.S. 92C/16E
SOIL GEOCHEMISTRY
Au, Ag, As
1:25
W1 GRID
BASELINE
500 N
500 S
0E
200E
400E
600E
800E
1000E
1200E
1400E
413000E
415000E
417000E
CR-2
1,0.3,8
CR-1
2,0.1,2
W2-700A
W2-900
W1-900
W1A-700
BK 1080
BK 996
BK 437


IMPERIAL METALS CORPORATION
MT. WHYMPER
FIGURE 6
NTS 92C/16E
SOIL GEOCHEMISTRY
Cu , Pb
1000 metres
W1 GRID
BASELINE
500 N
500 S
0E
200E
400E
600E
800E
1000E
1200E
1400E
413000E
415000E
417000E
5424000N
5422000N
BK 1034
BK 1089
BK 1080
BK 996
El Capitan Mountain
Mount Landale
Mount Whymper
CR-2
208,9
CR-1
155,2
W2-700A
W2-900
W1-900
W1A-700
15,25
159,10
311,12
74,12
40,18
158,18
146,10
245,15
186,16
44,8
61,6
47,6
181,4
285,7
71,10
92,10
187,2
69,9
230,4
82,2
117,13
114,5
179,14
36,28
44,29
59,18
48,34
114,40
42,8
23,55
25,13
91,14
89,11
84,8
87,16
101,9
96,11
82,3
100,9
118,12
162,10
46,5
118,4
112,4
55,12
87,11
107,5
119,5
113,12
74,3
89,6
165,5
195,8
95,2
60,13
213,4
153,8
135,2
265,12
194,20
292,5
199,7
167,8
174,7
176,5
165,6



IMPERIAL METALS CORPORATION
MT. WHYMPER
FIGURE 7 NTS 92C/16E
SOIL GEOCHEMISTRY
Zn, Ba
1000 metres
SCALE 1:20000
DATE DECEMBER 1985
GEOLOGIST A. CLARK

The normal barium anomalous soil threshold is taken at 200 ppm. In this property barium is everywhere lower than this.

Grid

A grid was flagged and soil samples collected at each accessible station. In addition a VLF-EM survey and an altimeter survey were undertaken.

In the initial contour soil sampling undertaken in 1984, soils in the area of the grid appeared to be predominantly enriched in gold on the western side and copper on the eastern side. The grid was placed to allow more detailed investigation of this.

Soil sample results from the grid (Figures 8 and 9) indicate that this apparent separation of base and precious metals values is not valid at a more detailed scale. High gold values occur in isolation, with only a weak grouping in the north-central part of the grid. Arsenic anomalies are not significantly associated with the gold. Copper anomalous values are widely spread, but more consistent in the southern part of the grid. Lead, zinc and barium only show weak patterns not repeated in adjacent lines, and of little significance.

A geological investigation of the grid may give more relevance to some of the results.

A VLF-EM survey was undertaken and both Dip Angle and Field Strength measured (Figure 10). The field strength shows little variation, though the southwest part of the grid has more field strength variability than elsewhere on the grid. Dip angle also shows little variability, though it is not as "smooth" as the field strength. Local broad anomalous parts, usually over 3 or 4 stations, should be checked against geology, and the major negative dip angle anomaly on line 10E should also be checked.

Altimeter readings were taken during the survey, and the results shown are Figure 11. Note that these are uncorrected results and the map is only to be used as a general guide to the topography.

CONCLUSIONS

Soil geochemical variations on the grid and on the contour sample lines should be checked in the field. In addition the VLF-EM weak anomalies and negative dip angle anomaly should also be checked.

REFERENCES

Muller, J.E., 1977. Geology of Vancouver Island. Geological Survey Canada, Open File No. 463.

Clark, A.M.S., 1984. Assessment Report, 1984 Field Work: Mt. Whymper Project (Imperial Metals Corporation). B.C. Assessment Report Files

CERTIFICATE

I, Anthony Miles Stapleton Clark, geologist, residing at 2988 Fleet Street, in the Municipality of Coquitlam, Province of British Columbia, hereby certify that:

1. I received a Bachelor of Science degree in geology from the University of Cape Town, Cape Town, South Africa, in 1963, and a Doctor of Philosophy degree in geology from the Memorial University of Newfoundland, St. John's, Newfoundland in 1974.

2. I have been practising my profession as an exploration geologist since 1963.

3. I am a registered Professional Geologist of the Association of Professional Engineers, Geologists and Geophysicists of Alberta.

4. I am a Fellow of the Geological Association of Canada and a Member of the Society of Economic Geologists.

5. I am employed by Imperial Metals Corporation of 1300 - 409 Granville Street, in the city of Vancouver, Province of British Columbia.

6. The work described in this report was undertaken under my direct supervision.

11th day of March, 1986

Vancouver, British Columbia

A.M.S. Clark, Ph.D., FGAC, MSEG
Geologist

APPENDIX 1

Soil Sample Descriptions

```
. ? northing    easting      soil description'
northing    easting      soil description
. list all northing,easting,soil for soil>' '
00001      -125        0 medium brown silt, 10% humic
00002      -100        0 medium brown silt, 10% humic
00003         0        0 dark brown silt, 10% humic
00007       325        0 missing due to yarding of logs
00011       375        0 missing due to yarding of logs
00014       425        0 destroyed by logging activity
00016       450        0 destroyed by logging activity
00018       475        0 destroyed by logging activity
00040         0       25 dark brown silt, 30% humic
00041         0       50 dark brown silt, 30% humic
00042         0       75 dark brown silt, 30% humic
00043         0      100 medium brown silt, 10% humic
00044         0      125 medium brown silt, 25% humic
00045         0      150 dark brown silt, 30% humic
00046         0      175 medium brown silt, 15% humic
00073        25      200 medium brown silt, 10% humic
00075        50      200 medium brown silt, 10% humic
00077        75      200 dark brown, humic material
00079       100      200 medium brown silt
00081       125      200 light brown silt
00083       150      200 light brown silt
00085       175      200 medium brown silt, 15% humic
00087       200      200 medium brown silt, 10% humic
00089       225      200 medium brown silt, 15% humic
00091       250      200 medium brown silt
00093       275      200 medium brown silt, 10% humic
00095       300      200 black humic material
00097       325      200 medium brown silt, 15% humic
00099       350      200 medium brown silt, 15% humic
00101       375      200 medium brown silt, 15% humic
00103       400      200 medium brown silt, 15% humic
00105       425      200 medium brown silt, 15% humic
00107       450      200 medium brown silt, 15% humic
00109       475      200 red silt, 10% humic
00111       500      200 medium brown silt, 10% humic
00114         0      275 dark brown humic material
00116         0      325 medium brown silt, 10% humic
00117         0      350 m brwn silt & sand, 10% humic
00119      -500      400 medium brown silt, 20% humic
00120      -475      400 dark brown silt - 30% humic
00121      -450      400 humic material - no soil
00122      -425      400 medium brown silt
00123      -400      400 dark brown silt, 30% humic
00124      -375      400 red silt
00125      -350      400 dark brown silt, 10% humic
00126      -325      400 dark brown silt, 10% humic
00127      -300      400 humic material -no soil
00128      -275      400 humic material - no soil
00129      -250      400 dark brown silt - 30% humic
00130      -225      400 humic material - no soil
00131      -200      400 gry m sand, o.c. shws carb. v
00132      -175      400 humic material - no soil
00133      -150      400 humic material - no soil
00134      -125      400 dark brown silt, 20% humic
00135      -100      400 medium brown silt
00136       -75      400 medium brown silt
00137       -50      400 dark brown silt, 10% humic
00138       -25      400 dark brown silt, 10% humic
00158       450      400 red brown silt
00159       475      400 red brown silt
00160       500      400 red brown silt
```

00208	0	700	medium brown silt
00209	100	700	light brown silt
00210	200	700	medium brown silt
00211	300	700	light brown silt
00212	400	700	light brown silt
00213	500	700	light brown silt
00214	600	700	light brown silt
00215	700	700	medium brown silt
00216	800	700	talus fines
00217	900	700	medium brown silt
00218	1000	700	medium brown silt
00219	1100	700	medium brown silt
00220	1200	700	medium brown silt
00221	1300	700	medium brown silt
00222	1400	700	grey silt
00223	1500	700	medium brown silt
00224	1600	700	medium brown silt
00289	0	825	light brown silt
00290	0	825	light brown silt
00291	0	850	light brown silt
00292	0	850	light brown silt
00293	0	875	light brown silt
00294	0	875	light brown silt
00295	0	900	light brown silt
00296	0	900	light brown silt
00297	0	925	orange silt
00298	0	950	orange silt
00299	0	975	orange silt
00319	0	1000	orange silt
00326	0	1025	orange silt
00327	0	1050	orange silt
00328	0	1075	light br silt, over outcrop
00329	0	1100	light brown silt, over outcrop
00330	0	1125	light brown silt, over outcrop
00331	0	1150	light brown silt, over outcrop
00332	0	1175	orange silt, over outcrop
00333	-500	1200	m. br silt, poss. dist by road
00334	-475	1200	red silt
00335	-450	1200	medium brown silt
00336	-425	1200	medium brown silt
00337	-400	1200	red silt
00338	-375	1200	red silt
00339	-350	1200	red silt
00340	-325	1200	red silt
00341	-300	1200	red silt
00342	-275	1200	red silt, poss. dist. by road
00343	-250	1200	red silt, poss. dist. by road
00344	-225	1200	red silt, poss. dist. by road
00345	-200	1200	dark brown silt, 10% humic
00346	-175	1200	red silt
00349	0	1200	med. brown silt, over outcrop
00350	25	1200	med. brown silt, over outcrop
00351	50	1200	med. brown silt, over outcrop
00352	75	1200	med. brown silt, over outcrop
00353	100	1200	med. brown silt, over outcrop
00354	125	1200	med. brwn silt, over outcrop

. set prinmt__t off

APPENDIX 2

Analytical Results

ACME ANALYTICAL LABORATORIES LTD. 852 E.HASTINGS ST.VANCOUVER B.C. V6A 1R6 PHONE 253-3158 DATA LINE 251-1011

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN.FE.CA.P.CR.MG.BA.TI.B.AL.NA.K.W.SI.ZR.CE.SN.Y.NB AND TA. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: SOILS -80 MESH AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: OCT 15 1985 DATE REPORT MAILED: Oct 21/85 ASSAYER. [signature] DEAN TOYE OR TOM SAUNDRY. CERTIFIED B.C. ASSAYER

IMPERIAL METALS CORPORATION PROJECT - 5008 FILE # 85-2811 PAGE 1

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
W1A 700-0	2	95	11	91	.5	25	15	298	3.98	21	5	ND	1	25	1	2	2	108	.90	.08	6	52	.56	45	.35	7	4.54	.06	.03	1	9
W1A 700-1	2	101	9	54	.1	29	14	295	4.48	7	5	ND	1	17	1	2	2	130	.47	.04	4	58	.79	23	.51	4	4.08	.03	.02	1	16
W1A 700-2	3	87	16	51	.2	27	14	306	4.10	5	5	ND	1	21	1	2	2	119	.54	.04	3	59	.74	27	.46	2	3.49	.03	.02	1	13
W1A 700-3	2	84	8	59	.2	19	9	221	5.46	8	5	ND	1	14	1	2	2	163	.51	.14	2	63	.53	22	.57	4	3.95	.03	.02	1	7
W1A 700-4	1	89	11	50	.3	17	8	258	3.10	4	5	ND	1	19	1	2	2	88	.53	.07	3	34	.47	33	.40	2	3.02	.03	.02	1	5
W1A 700-5	1	91	14	74	.1	24	20	781	3.21	3	5	ND	1	46	1	2	2	93	.92	.07	4	31	.69	129	.44	2	2.37	.03	.03	1	2
W1A 700-6	1	25	13	59	.1	12	8	835	2.27	4	5	ND	1	42	1	2	3	70	.63	.06	3	21	.36	41	.26	3	1.42	.02	.02	1	1
W1A 700-7	2	23	55	106	.1	34	21	2839	3.69	7	5	ND	1	25	1	2	2	119	.62	.15	3	52	1.78	71	.16	2	2.28	.01	.03	1	1
W1A 700-8	1	42	8	87	.2	11	7	2391	1.42	3	5	ND	1	27	1	2	2	33	.49	.11	3	13	.27	53	.12	3	1.26	.02	.02	1	1
W1A 700-9	1	114	40	69	.6	31	12	313	2.29	11	5	ND	1	37	1	2	2	58	1.21	.09	2	55	.79	48	.22	3	3.22	.12	.03	1	8
W1A 700-10	1	48	34	103	.3	17	12	839	3.98	9	5	ND	2	29	1	2	2	75	.56	.16	5	35	.77	42	.15	3	2.81	.02	.04	1	23
W1A 700-11	1	59	18	87	.1	19	16	736	3.88	4	5	ND	2	32	1	2	2	72	.59	.07	5	34	1.16	51	.16	2	2.59	.02	.04	1	4
W1A 700-12	1	44	29	59	.1	18	7	375	1.33	6	5	ND	1	43	1	2	2	33	1.22	.12	2	28	.42	62	.10	5	1.04	.04	.03	1	14
W1A 700-13	2	36	28	93	.1	10	14	2523	2.73	7	5	ND	1	47	1	2	2	50	.57	.11	5	19	.49	69	.10	4	1.86	.01	.05	1	6
W1A 700-14	2	179	14	74	.2	32	20	640	2.85	12	5	ND	2	48	1	2	2	69	1.31	.09	7	51	.95	74	.24	3	3.73	.05	.04	1	10
W1A 700-15	1	114	5	59	.1	24	12	288	4.08	9	5	ND	1	24	1	2	2	117	.61	.10	2	67	.72	24	.56	2	4.47	.03	.02	1	16
W1A 700-16	1	117	13	61	.3	26	13	330	5.28	11	5	ND	1	26	1	2	2	144	.57	.14	2	87	.80	14	.68	2	5.24	.03	.02	1	2
W2 700A-0	1	82	3	90	.8	23	13	631	4.57	9	5	ND	1	35	1	2	4	120	.68	.22	4	60	.65	26	.49	4	2.65	.02	.03	1	5
W2 700A-1	1	100	9	96	.3	33	23	984	5.62	25	5	ND	1	43	1	2	2	168	1.19	.12	5	74	1.19	25	.60	5	3.12	.03	.02	1	19
W2 700A-2	1	59	4	71	.4	21	11	409	4.46	7	5	ND	1	35	1	3	6	138	.75	.14	6	53	.68	24	.67	2	2.20	.02	.02	1	10
W2 700A-3	1	118	12	97	.5	36	15	469	7.15	16	5	ND	2	29	1	2	2	168	.50	.24	3	88	.96	25	.65	2	5.96	.02	.03	1	2
W2 700A-4	2	162	10	57	.3	29	18	404	4.38	7	5	ND	1	28	1	4	2	138	.70	.15	6	78	.89	13	.57	3	6.07	.02	.02	1	14
W2 700A-5	1	56	14	100	.3	27	29	1178	5.06	12	5	ND	1	51	1	2	2	144	1.36	.10	5	65	1.06	32	.54	2	3.02	.02	.03	1	6
W2 700A-6	1	46	5	48	.1	21	20	985	3.10	3	5	ND	1	40	1	2	3	104	.91	.07	4	42	.54	36	.52	4	1.64	.02	.03	1	4
W2 700A-7	1	118	4	70	.2	35	17	562	4.90	4	5	ND	1	40	1	2	2	148	.99	.06	5	66	1.30	18	.74	3	2.93	.03	.02	1	1
W2 700A-8	1	112	4	77	.1	44	24	634	5.05	10	5	ND	1	39	1	2	2	160	1.20	.05	4	77	1.20	27	.64	3	2.93	.03	.03	1	2
W1 900-0	1	15	25	25	.1	7	1	29	.17	5	5	ND	1	20	1	2	2	5	.65	.08	2	2	.12	15	.01	4	.21	.02	.02	1	1
W1 900-1	1	159	10	45	.1	27	22	368	3.61	5	5	ND	1	18	1	2	2	75	.45	.09	4	63	.34	32	.21	3	3.57	.02	.02	1	9
W1 900-2	2	311	12	58	.3	60	52	992	4.64	21	5	ND	1	53	1	2	2	92	1.57	.14	6	66	.64	65	.16	6	5.54	.04	.02	1	8
W1 900-3	1	74	12	31	.2	16	7	128	1.65	4	5	ND	1	16	1	2	2	43	.31	.08	2	32	.20	20	.12	2	1.04	.02	.02	1	1
W1 900-4	1	40	18	41	.2	16	6	197	2.12	6	5	ND	1	18	1	2	2	66	.51	.05	2	37	.38	29	.25	2	1.55	.03	.03	1	2
W1 900-5	1	158	18	61	.2	37	16	476	3.88	7	5	ND	1	22	1	2	2	103	.71	.07	2	86	.95	39	.35	2	4.40	.04	.03	1	12
W1 900-6	2	146	10	31	.3	20	10	208	2.01	14	5	ND	1	16	1	2	2	45	.40	.28	2	52	.45	20	.08	2	3.05	.02	.03	1	4
W1 900-7	1	245	15	62	.2	54	31	680	3.78	13	6	ND	1	48	1	2	2	91	1.45	.08	5	100	1.54	42	.27	5	4.84	.05	.03	1	12
W1 900-8	2	186	16	53	.1	43	19	488	3.21	8	5	ND	1	54	1	54	2	80	1.18	.12	4	97	1.17	28	.24	4	9.03	.02	.01	1	1
W1 900-10	1	44	8	35	.2	17	8	213	3.03	2	5	ND	1	19	1	2	3	102	.59	.03	2	48	.39	33	.37	3	1.71	.02	.01	1	9
STD C/AU-0.5	20	60	38	136	7.3	67	29	1164	3.95	37	18	7	35	50	16	15	21	59	.48	.15	38	57	.88	175	.08	37	1.71	.06	.10	12	500

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
W1 900-11	1	61	6	30	.1	17	13	963	2.02	2	5	ND	1	20	1	2	2	54	.47	.06	2	24	.27	54	.25	2	1.28	.02	.02	1	8
W1 900-12	1	47	6	38	.1	14	8	284	4.72	2	5	ND	1	10	1	2	2	97	.26	.07	2	28	.35	16	.34	5	1.39	.01	.01	1	25
W1 900-13	1	181	4	47	.4	42	22	443	3.29	19	5	ND	1	34	1	2	2	74	.91	.09	3	39	.64	22	.16	2	4.02	.02	.02	1	14
W1 900-14	1	285	7	89	.5	43	58	1226	3.18	66	5	ND	1	16	1	2	2	64	.40	.12	4	43	.53	43	.15	6	3.21	.02	.02	1	12
W1 900-15	2	71	10	66	.1	96	35	2450	3.31	12	5	ND	1	21	1	3	4	67	.50	.06	2	48	1.82	32	.15	2	2.32	.02	.02	1	2
W1 900-16	1	92	10	68	.4	21	12	347	4.84	57	5	ND	1	15	1	2	2	125	.46	.06	2	30	.29	39	.37	5	2.02	.01	.02	1	11
W1 900-17	2	187	2	80	.1	33	40	2243	3.73	13	5	ND	1	19	1	2	2	89	.47	.09	3	42	.58	26	.26	5	3.06	.02	.02	1	5
W1 900-18	2	69	9	52	.1	18	19	1981	3.79	2	5	ND	1	22	1	2	2	114	.44	.06	2	30	.44	25	.33	2	1.58	.01	.02	1	39
W1 900-19	2	92	2	34	.1	22	11	260	3.12	4	5	ND	1	20	1	2	3	82	.56	.04	2	37	.56	33	.32	2	2.20	.02	.01	1	7
W1 900-20	6	230	4	45	.1	38	20	356	4.08	10	5	ND	1	25	1	4	3	105	.63	.05	5	50	.77	34	.39	3	2.65	.02	.01	1	9
W2 900-0	2	165	8	144	.4	51	26	1142	6.14	9	5	ND	1	13	1	4	7	151	.23	.12	3	61	1.21	125	.40	7	4.53	.01	.03	1	10
W2 900-1	2	176	5	139	.2	65	30	767	6.37	8	5	ND	1	15	1	2	2	172	.23	.07	6	67	1.35	258	.41	3	4.92	.01	.02	1	4
W2 900-2	2	174	7	145	.1	57	28	899	6.02	8	5	ND	1	15	1	2	4	157	.23	.08	6	57	1.12	140	.36	5	4.19	.01	.03	1	6
W2 900-3	2	167	8	131	.2	57	27	1066	6.30	10	5	ND	1	16	1	3	4	162	.33	.10	8	64	1.36	102	.45	3	3.98	.01	.02	1	2
W2 900-4	1	199	7	146	.2	64	35	1421	7.03	5	5	ND	1	23	1	2	5	168	.27	.10	4	68	1.30	182	.28	2	4.44	.01	.03	1	14
W2 900-5	2	292	5	103	.2	66	40	1040	6.60	13	5	ND	1	173	1	2	3	161	.44	.05	8	67	2.71	3660	.27	3	6.11	.02	.02	1	30
W2 900-6	2	194	20	147	.4	61	31	896	6.59	9	5	ND	1	28	1	2	3	165	.23	.07	5	70	1.63	241	.35	3	4.56	.01	.02	1	1
W2 900-7	2	265	12	120	.2	67	34	1249	5.90	8	5	ND	1	50	1	2	5	131	.76	.16	3	113	1.60	116	.43	4	5.24	.01	.02	1	2
W2 900-8	1	71	6	100	.2	32	19	731	5.85	2	5	ND	1	14	1	2	2	153	.36	.08	2	56	.87	63	.43	3	2.67	.01	.02	1	1
W2 900-9	1	135	2	110	.2	60	25	846	5.92	5	5	ND	1	24	1	3	5	143	.44	.08	2	127	1.40	35	.57	2	4.02	.01	.02	1	6
W2 900-10	1	153	6	100	.1	53	22	841	5.35	2	5	ND	1	20	1	2	7	136	.33	.10	2	96	1.10	47	.48	6	4.55	.01	.03	1	9
W2 900-11	1	213	4	152	.1	68	34	1328	6.31	5	5	ND	1	33	1	3	7	163	.85	.09	7	110	1.56	36	.62	5	4.68	.03	.03	1	10
W2 900-12	1	60	13	73	.2	24	17	1746	3.71	3	5	ND	1	28	1	2	2	94	.61	.07	3	46	.63	56	.44	4	1.75	.01	.03	1	6
W2 900-13	1	155	2	106	.1	52	23	773	5.96	3	5	ND	1	23	1	2	2	152	.44	.09	3	95	1.21	32	.52	7	3.41	.01	.02	1	1
W2 900-14	1	63	6	88	.1	33	17	1190	4.51	2	5	ND	1	28	1	2	3	111	.57	.08	3	69	.79	25	.57	4	2.22	.01	.02	1	10
W2 900-15	1	95	2	107	.1	40	20	1942	4.77	2	5	ND	1	27	1	2	3	105	.40	.15	2	69	.82	53	.38	5	3.21	.01	.03	1	2
W2 900-16	1	195	8	116	.1	57	29	1124	5.79	5	5	ND	1	26	1	2	2	131	.40	.13	5	91	1.03	42	.43	6	4.40	.01	.03	1	1
W2 900-17	1	165	5	105	.1	52	22	628	5.68	4	5	ND	1	25	1	2	2	142	.39	.08	6	95	1.18	31	.58	3	4.36	.01	.03	1	2
W2 900-18	1	89	6	115	.1	57	30	4445	5.97	2	5	ND	1	28	1	2	2	141	.80	.10	4	125	1.51	56	.51	3	3.24	.02	.02	1	9
W2 900-19	1	74	3	100	.3	38	21	2918	5.03	3	5	ND	1	25	1	2	2	122	.48	.08	2	84	.78	32	.53	3	2.63	.01	.02	1	2
W2 900-20	1	113	12	110	.2	39	22	933	5.46	2	5	ND	1	25	1	2	4	125	.44	.08	5	83	.98	29	.54	9	3.10	.01	.02	1	12
W2 900-21	1	106	11	96	.1	47	21	785	5.55	2	5	ND	1	27	1	2	2	149	.44	.09	3	100	.78	27	.50	2	3.33	.01	.02	1	1
W2 900-22	1	107	2	105	.3	50	25	1430	6.05	2	5	ND	1	25	1	2	3	155	.46	.09	5	96	1.32	35	.50	3	3.48	.01	.02	1	1
W2 900-23	1	203	2	128	.1	48	23	1154	5.68	2	5	ND	1	40	1	2	2	133	.59	.20	3	76	1.01	31	.52	7	3.30	.01	.02	1	2
W2 900-24	1	119	5	148	.2	43	27	3017	5.89	2	5	ND	1	30	1	2	2	143	.54	.16	6	74	.87	38	.52	4	2.88	.01	.02	1	9
W2 900-25	1	107	5	91	.2	46	20	903	5.26	3	5	ND	1	29	1	2	3	130	.61	.10	9	93	1.45	21	.56	3	3.14	.02	.01	1	1
STD C/AU-0.5	20	58	40	135	7.5	69	28	1152	3.92	38	17	7	36	52	17	15	21	57	.48	.15	38	58	.88	173	.08	40	1.72	.06	.11	12	510

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au# PPB
W2 900-26	2	87	11	103	.1	44	23	1275	4.75	4	5	ND	2	42	1	2	7	108	.86	.14	2	80	1.24	31	.52	7	2.76	.02	.03	1	5
W2 900-28	1	55	12	81	.1	19	13	503	3.75	2	5	ND	1	26	1	2	2	92	.43	.05	4	42	.54	40	.45	7	2.04	.01	.02	1	4
W1 425E BL	3	83	6	22	.4	20	8	150	3.54	33	5	ND	1	10	1	2	2	79	.29	.09	3	88	.32	16	.30	5	4.76	.02	.01	1	7
W1 450E BL	2	39	18	35	.1	24	9	153	4.66	28	5	ND	1	14	1	2	7	165	.39	.07	2	68	.39	17	.58	7	1.81	.02	.02	1	9
W1 475E BL	2	136	12	35	.1	31	14	213	3.73	21	5	ND	1	15	1	2	2	89	.57	.05	2	89	.61	21	.31	4	2.93	.03	.02	1	20
W1 500E BL	4	157	4	24	.5	26	13	238	3.03	35	5	ND	1	12	1	2	2	58	.36	.10	4	73	.44	16	.22	4	5.70	.02	.02	1	1
W1 525E BL	3	89	15	40	.1	37	14	332	3.11	18	5	ND	1	27	1	2	2	66	.96	.09	2	78	.83	30	.22	4	2.59	.06	.03	1	4
W1 550E BL	2	171	14	25	.5	25	21	350	2.70	23	5	ND	1	18	1	2	2	47	.46	.21	3	58	.36	17	.11	2	3.86	.02	.03	1	6
W1 575E BL	3	88	8	32	.2	27	12	413	4.22	20	5	ND	1	11	1	2	3	97	.41	.11	3	72	.49	26	.27	2	2.29	.03	.02	1	2
W1 600E BL	2	50	11	21	.2	20	8	99	1.22	6	5	ND	1	24	1	2	2	23	.50	.15	3	29	.28	22	.05	4	1.63	.02	.02	1	1
W1 625E BL	3	100	10	56	.4	26	27	495	3.73	9	5	ND	1	15	1	2	2	66	.38	.13	3	49	.40	23	.24	5	3.70	.02	.02	1	38
W1 650E BL	4	122	3	64	.4	24	13	234	4.36	18	5	ND	1	11	1	2	2	63	.32	.11	2	75	.51	17	.26	4	6.02	.02	.02	1	7
W1 675E BL	5	103	2	114	.3	28	16	281	5.81	20	5	ND	1	11	1	2	2	117	.34	.09	2	83	.57	20	.43	8	6.35	.02	.02	1	3
W1 700E BL	4	111	2	48	.1	43	20	543	3.12	23	5	ND	1	40	1	2	2	65	1.86	.07	2	77	1.09	33	.24	2	2.90	.11	.03	1	8
W1 725E BL	3	90	8	57	.1	42	21	595	3.11	19	5	ND	1	42	1	2	4	73	1.79	.06	2	80	1.21	27	.27	6	2.64	.13	.03	1	1
W1 750E BL	5	122	14	44	.1	29	32	925	3.16	79	5	ND	1	17	1	2	2	66	.59	.16	3	67	.66	27	.15	4	3.89	.03	.02	1	4
W1 775E BL	4	160	2	45	.3	38	22	532	2.98	42	5	ND	1	33	1	4	2	63	1.41	.10	3	69	1.00	27	.19	6	3.07	.09	.03	1	2
W1 800E BL	5	131	19	81	.2	31	63	1492	5.29	141	5	ND	1	25	1	2	13	153	.85	.10	4	65	.82	24	.55	4	3.16	.02	.02	1	55
W1 800E-A BL	4	136	7	92	.4	37	45	1655	3.33	66	5	ND	1	30	1	2	2	76	1.35	.13	4	69	.83	30	.19	3	3.80	.04	.02	1	7
W1 825E BL	4	116	18	92	.2	30	37	1348	3.42	129	5	ND	1	48	1	2	2	82	1.88	.13	2	49	.90	22	.31	7	3.88	.02	.03	1	4
W1 850E BL	4	105	21	126	.2	32	38	1826	5.17	123	5	ND	1	29	1	2	2	128	1.01	.14	2	59	.85	31	.50	7	3.57	.02	.02	1	3
W1 875E BL	5	131	14	104	.6	33	25	569	5.27	89	5	ND	1	20	1	2	2	133	.56	.16	4	70	.92	19	.57	6	4.79	.02	.02	1	15
W1 900E BL	5	136	12	66	.3	39	21	555	4.72	81	5	ND	1	21	1	2	2	117	.70	.12	2	67	1.03	25	.53	6	5.87	.02	.02	1	6
W1 925E BL	4	94	14	70	.1	34	22	711	5.15	44	5	ND	1	24	1	2	2	146	.62	.10	2	59	.94	28	.63	4	3.71	.02	.02	1	34
W1 950E BL	3	72	20	120	.1	26	21	592	6.12	36	5	ND	1	27	1	2	19	187	.68	.07	2	63	.74	31	.82	7	2.53	.02	.03	1	15
W1 975E BL	4	144	15	63	.1	35	35	962	4.47	96	5	ND	1	25	1	3	2	113	1.06	.07	2	69	.90	17	.46	4	4.73	.02	.02	1	12
W1 1000E BL	5	133	3	59	.7	21	43	968	2.44	363	5	ND	1	16	1	3	2	56	.57	.12	6	70	.39	11	.18	2	7.27	.01	.02	1	1
W1 1025E BL	3	88	9	56	.4	23	25	556	3.68	190	5	ND	1	26	1	2	2	104	.58	.07	4	44	.51	24	.39	4	3.72	.01	.02	1	5
W1 1050E BL	3	103	13	79	.2	29	24	577	4.49	24	5	ND	1	31	1	2	2	121	.77	.07	2	56	.68	31	.51	6	3.45	.02	.02	1	20
W1 1075E BL	3	83	20	74	.3	33	34	3152	3.59	22	5	ND	1	33	1	3	2	94	.94	.11	3	68	.80	31	.32	5	2.50	.02	.02	1	7
W1 1100E BL	2	105	15	55	.2	22	14	429	5.29	15	5	ND	1	18	1	2	2	156	.46	.10	2	60	.70	17	.63	4	3.60	.02	.02	1	6
W1 1125E BL	2	94	17	56	.1	29	18	588	4.68	8	5	ND	1	25	1	2	2	124	.66	.06	4	60	.97	17	.55	2	2.66	.02	.02	1	12
W1 1150E BL	1	42	21	47	.1	26	12	365	4.28	6	5	ND	1	20	1	2	4	131	.60	.03	3	47	.86	14	.52	4	1.84	.03	.03	1	2
W1 1175E BL	2	96	30	73	.2	34	17	542	7.79	28	5	ND	2	18	1	2	2	189	.38	.07	9	73	1.20	11	.94	4	3.54	.02	.03	1	16
W1 1200E BL	2	76	29	54	.1	28	17	599	4.01	9	5	ND	1	23	1	2	2	107	.50	.08	5	42	.75	23	.44	2	2.20	.02	.02	1	135
W1 1225E BL	1	44	31	56	.1	21	18	1580	4.76	3	5	ND	1	18	1	2	2	153	.54	.06	3	38	.68	28	.44	3	2.06	.03	.02	1	4
STD C/AU-0.5	21	59	40	138	7.4	68	30	1191	3.97	39	19	8	36	49	16	15	22	57	.48	.15	40	58	.88	182	.08	39	1.72	.06	.11	13	490

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
W1 1250E BL	1	39	27	53	.2	22	16	1349	4.66	3	5	ND	1	22	1	2	8	155	.61	.06	6	38	.69	26	.41	19	2.06	.03	.03	1	8
W1 1275E BL	1	67	7	61	.1	30	20	980	3.92	2	5	ND	1	34	1	2	9	119	.74	.05	5	49	.78	32	.52	2	2.21	.02	.03	1	7
W1 1300E BL	1	51	25	52	.1	24	23	1191	3.58	3	5	ND	1	28	1	2	7	106	.56	.07	5	37	.65	26	.41	23	1.97	.02	.03	1	2
W1 1325E BL	1	52	2	67	.2	26	17	1223	4.74	5	5	ND	1	31	1	2	9	145	.63	.06	4	48	.81	26	.59	21	2.11	.02	.02	1	6
W1 1350E BL	1	106	16	78	.3	35	52	1751	3.66	38	5	ND	1	38	1	2	6	94	.99	.08	6	45	.83	31	.48	3	2.94	.02	.03	1	5
W1 1375E BL	1	135	3	49	.2	24	104	2325	3.14	26	5	ND	1	31	1	2	2	94	.55	.11	11	38	.51	27	.34	21	2.62	.02	.02	1	4
W1 1400E BL	1	158	5	50	.2	30	22	750	3.49	18	5	ND	1	22	1	2	2	93	.61	.08	6	64	.97	15	.47	22	4.17	.02	.01	1	16
W1 1425E BL	1	44	6	40	.2	14	8	296	3.33	23	5	ND	1	28	1	2	9	120	.45	.05	4	39	.40	23	.43	4	1.54	.01	.02	1	13
W1 1450E BL	1	159	3	76	.3	39	26	651	5.74	72	5	ND	1	28	1	2	6	142	.47	.11	5	80	1.25	17	.62	18	4.23	.02	.02	1	95
W1 1475E BL	1	157	5	72	.3	36	25	598	5.59	66	5	ND	1	33	1	2	2	139	.56	.09	5	66	.94	24	.46	19	4.37	.02	.02	1	190
W1 1500E BL	1	149	2	70	.3	36	19	517	7.38	38	5	ND	2	31	1	3	4	182	.47	.11	6	78	1.06	16	.60	19	4.12	.02	.03	1	9
W1 400E 25S	1	85	13	25	.3	17	8	172	5.23	28	5	ND	1	9	1	3	2	100	.29	.11	3	88	.43	13	.34	22	4.49	.02	.02	1	11
W1 400E 50S	1	102	8	24	.5	13	7	191	2.38	13	5	ND	1	9	1	2	2	41	.21	.17	2	49	.26	11	.12	28	4.37	.02	.02	1	1
W1 400E 75S	2	123	23	32	.1	23	18	755	3.36	40	5	ND	1	15	1	2	2	67	.47	.15	3	50	.49	19	.13	25	3.45	.03	.02	1	4
W1 400E 100S	1	105	5	29	.1	27	10	174	2.20	18	5	ND	1	15	1	2	2	57	.53	.10	3	55	.56	17	.16	24	3.05	.03	.02	1	82
W1 400E 125S	1	105	12	27	.5	25	10	221	4.52	20	5	ND	1	14	1	2	2	83	.33	.12	4	74	.47	16	.24	22	2.43	.02	.02	1	1
W1 400E 150S	1	15	18	14	.1	8	1	20	.23	4	5	ND	1	26	1	2	2	5	.33	.08	2	4	.11	21	.01	2	.22	.01	.02	1	1
W1 400E 175S	1	101	9	19	.5	17	9	215	2.69	31	5	ND	1	16	1	2	2	62	.47	.12	3	51	.33	17	.16	2	4.15	.02	.02	1	4
W1 400E 200S	1	167	21	45	.2	41	21	545	2.36	17	5	ND	1	155	1	2	2	61	5.18	.06	2	72	1.07	22	.14	2	6.45	.02	.03	1	2
W1 400E 225S	1	60	20	14	.2	12	5	90	.84	8	5	ND	1	15	1	2	2	19	.34	.18	2	21	.24	11	.03	23	2.84	.01	.02	1	1
W1 400E 250S	1	37	15	22	.1	10	3	27	.49	4	5	ND	1	26	1	2	2	11	.24	.12	2	9	.13	45	.03	4	.84	.01	.02	1	1
W1 400E 275S	1	54	14	27	.1	8	5	107	2.88	3	5	ND	1	15	1	2	2	65	.41	.08	3	28	.19	21	.13	17	1.24	.02	.02	1	22
W1 400E 300S	1	51	23	19	.3	12	4	44	.95	6	5	ND	1	13	1	2	2	18	.16	.19	2	14	.10	24	.03	22	1.49	.02	.03	1	4
W1 400E 325S	1	74	4	29	.4	22	9	233	3.65	5	5	ND	1	19	1	2	3	129	.72	.07	3	72	.50	17	.36	20	1.89	.04	.02	1	32
W1 400E 350S	1	35	6	35	.3	18	7	282	6.48	2	5	ND	2	25	1	2	8	244	.47	.05	3	90	.43	34	.64	15	1.66	.02	.02	1	8
W1 400E 375S	2	87	8	33	.3	23	33	882	2.50	27	5	ND	1	26	1	2	2	56	.66	.12	3	55	.44	28	.15	5	3.19	.02	.02	1	4
W1 400E 400S	1	47	30	32	.3	20	27	933	2.40	24	5	ND	1	31	1	2	2	48	1.24	.10	3	34	.35	28	.11	26	1.77	.02	.02	1	1
W1 400E 425S	1	51	2	32	.2	17	7	167	5.14	2	5	ND	1	10	1	2	5	140	.40	.06	3	46	.30	16	.43	4	1.71	.02	.02	1	12
W1 400E 450S	1	17	19	34	.1	8	2	29	.11	2	5	ND	1	19	1	2	2	3	.52	.07	2	2	.12	47	.01	24	.11	.02	.02	1	1
W1 400E 475S	2	193	9	29	.7	25	19	286	2.67	9	5	ND	1	13	1	2	2	59	.28	.11	3	36	.22	24	.16	19	3.11	.02	.02	1	1
W1 400E 500S	2	89	14	43	.2	26	22	372	3.04	13	5	ND	1	20	1	3	2	57	.50	.12	3	50	.45	38	.16	3	3.59	.02	.02	1	1
W1 1000E 150N	1	132	18	61	.1	40	35	1053	4.83	9	5	ND	1	34	1	2	4	132	1.19	.06	5	54	1.46	23	.51	20	3.60	.04	.03	1	8
W1 1000E 125N	1	86	14	60	.1	31	22	764	5.59	13	5	ND	1	41	1	2	5	152	.90	.07	7	55	1.00	24	.58	2	3.79	.02	.03	1	6
W1 1000E 100N	1	88	30	62	.2	24	51	1831	3.37	14	5	ND	1	35	1	2	3	88	.92	.13	4	34	.62	37	.34	2	2.53	.02	.02	1	4
W1 1000E 75N	1	59	14	54	.2	23	16	832	3.10	9	5	ND	1	40	1	2	4	89	1.04	.11	2	37	.52	33	.34	2	1.67	.02	.03	1	1
W1 1000E 50N	1	99	9	73	.5	30	25	739	5.18	76	5	ND	1	33	1	2	7	160	.72	.09	6	65	.95	24	.68	20	3.54	.03	.03	1	26
W1 1000E 25N	1	141	3	52	.4	31	20	589	3.92	44	5	ND	1	22	1	2	2	111	.63	.13	2	60	.99	16	.49	6	5.17	.02	.02	1	12
STD C/AU-0.5	20	59	41	135	7.5	67	28	1156	3.96	39	17	8	35	49	16	15	21	58	.46	.15	37	58	.88	174	.08	37	1.71	.06	.11	12	490

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
W1 1000E 25S	2	120	14	48	.7	31	24	430	4.58	224	5	ND	1	30	1	2	2	129	.67	.08	6	61	.77	21	.45	30	5.41	.02	.03	1	20
W1 1000E 50S	2	117	12	45	.3	32	24	512	4.61	52	5	ND	1	26	1	2	2	122	.72	.10	2	66	1.01	13	.57	28	6.15	.03	.02	1	21
W1 1000E 75S	1	113	14	53	.3	38	20	456	4.06	37	5	ND	1	25	1	2	2	116	.67	.07	4	68	1.01	16	.44	21	3.69	.03	.02	1	11
W1 1000E 100S	2	215	16	62	.4	50	27	621	5.08	30	5	ND	1	49	1	2	3	128	.64	.09	4	85	1.46	37	.35	23	5.02	.02	.03	1	23
W1 1000E 125S	2	196	8	51	.6	31	42	1509	4.58	25	5	ND	1	28	1	2	2	96	.59	.13	5	74	.80	19	.34	3	6.38	.02	.02	1	9
W1 1000E 150S	1	176	14	66	.4	41	22	587	4.36	36	5	ND	1	27	1	3	2	110	.66	.13	4	75	1.07	34	.40	22	4.86	.03	.02	1	4
W1 1000E 175S	2	205	4	71	.3	48	28	644	4.37	49	5	ND	2	31	1	2	2	110	.67	.13	5	75	1.30	44	.40	25	5.09	.03	.03	1	15
W1 1000E 200S	2	144	10	54	.5	28	24	674	4.81	28	5	ND	1	22	1	2	2	121	.51	.09	4	67	.73	28	.48	21	4.47	.02	.02	1	8
W1 1000E 225S	2	155	9	54	.6	45	24	570	4.56	32	5	ND	1	30	1	2	2	109	.62	.08	3	91	1.24	18	.45	2	6.08	.02	.02	1	16
W1 1000E 250S	2	111	7	59	.5	32	23	622	5.07	14	5	ND	1	21	1	2	4	130	.52	.08	4	68	.90	18	.57	26	4.09	.02	.02	1	7
W1 1000E 275S	2	91	15	52	.6	25	28	1138	7.03	26	5	ND	1	19	1	2	4	174	.46	.07	5	68	.58	21	.71	6	4.09	.02	.02	1	18
W1 1000E 300S	1	83	8	33	.5	18	9	239	5.34	17	5	ND	1	17	1	2	5	171	.57	.05	4	67	.50	16	.68	26	4.34	.03	.02	1	7
W1 1000E 325S	1	115	3	47	.4	25	15	389	3.82	16	5	ND	1	40	1	3	2	100	1.17	.09	4	68	.76	24	.39	27	5.64	.05	.03	1	13
W1 1000E 350S	1	107	6	37	.4	27	10	255	3.15	10	5	ND	1	16	1	3	2	81	.59	.08	2	63	.70	19	.41	29	6.19	.04	.02	1	9
W1 1000E 375S	1	99	11	50	.7	25	12	267	5.21	19	5	ND	1	19	1	2	3	145	.56	.09	2	79	.70	21	.55	25	4.83	.03	.02	1	3
W1 1000E 400S	2	125	9	39	.4	24	11	211	3.45	15	5	ND	1	13	1	3	2	76	.45	.09	2	65	.58	19	.33	24	6.97	.03	.02	1	18
W1 1000E 425S	2	178	9	43	.3	32	22	553	2.99	6	5	ND	1	28	1	2	2	78	1.05	.11	5	61	.82	34	.27	23	5.01	.06	.02	1	17
W1 1000E 450S	2	165	13	40	.4	31	15	362	2.98	12	5	ND	1	20	1	2	2	73	.76	.13	3	64	.77	32	.29	27	6.92	.04	.02	1	19
W1 1000E 475S	6	117	5	52	.4	22	12	296	4.34	7	5	ND	1	20	1	2	2	129	.61	.10	2	63	.56	29	.35	25	4.52	.03	.03	1	6
W1 1000E 500S	2	50	11	49	.3	15	7	270	3.41	2	5	ND	1	24	1	2	2	100	.50	.06	5	40	.37	29	.25	17	3.06	.03	.02	1	8
W1 1200E 125N	1	136	8	74	.6	26	28	791	4.59	8	5	ND	1	22	1	2	2	99	.45	.15	5	44	.61	18	.38	6	3.30	.02	.03	1	7
W1 1200E 100N	1	118	11	72	.3	30	18	460	5.78	7	5	ND	1	27	1	2	4	167	.60	.10	4	59	1.02	17	.76	21	4.14	.03	.03	1	9
W1 1200E 75N	1	48	14	56	.3	21	12	767	4.29	3	5	ND	1	35	1	2	2	132	.72	.06	4	40	.70	20	.58	20	2.12	.03	.02	1	50
W1 1200E 50N	1	82	19	71	.1	25	25	1084	3.26	2	5	ND	1	25	1	2	2	92	.49	.11	4	38	.55	27	.44	28	2.55	.02	.03	1	16
W1 1200E 25N	1	65	9	69	.4	26	20	871	4.90	3	5	ND	1	31	1	2	5	146	.61	.09	4	49	.87	16	.67	21	2.45	.03	.03	1	2
W1 1200E 125S	2	86	10	100	.1	26	58	5096	4.01	5	5	ND	1	30	1	2	2	99	.90	.11	3	45	.58	51	.34	26	2.64	.03	.03	1	10
W1 1200E 150S	1	74	10	77	.2	29	29	1291	4.57	2	5	ND	1	35	1	2	2	129	.88	.07	6	65	.60	30	.62	3	3.05	.02	.02	1	1
W1 1200E 175S	1	44	11	62	.2	20	17	1374	4.63	2	5	ND	1	35	1	2	2	134	.90	.07	5	54	.53	24	.61	25	2.23	.03	.02	1	16
W1 1200E 200S	1	68	12	80	.2	26	37	4485	3.41	5	5	ND	1	34	1	2	2	88	.82	.12	4	53	.53	29	.40	4	2.38	.02	.02	1	15
W1 1200E 225S	1	99	9	75	.2	33	18	684	5.59	4	5	ND	1	34	1	2	3	139	.85	.17	3	80	.86	28	.57	4	3.86	.03	.03	1	11
W1 1200E 250S	1	143	5	62	.3	33	16	446	4.66	7	5	ND	1	30	1	2	2	130	.72	.17	2	71	.94	20	.56	29	4.39	.03	.03	1	4
W1 1200E 275S	1	74	10	107	.3	32	46	2644	4.80	3	5	ND	1	28	1	2	2	106	.82	.19	3	81	.64	40	.56	5	3.07	.02	.03	1	3
W1 1200E 300S	1	100	11	65	.4	33	16	765	5.22	9	5	ND	1	41	1	2	2	155	1.02	.18	3	81	.96	33	.64	25	3.35	.03	.02	1	1
W1 1200E 325S	2	175	11	81	.6	41	22	540	5.60	4	5	ND	1	39	1	2	3	173	.81	.11	6	85	1.07	25	.73	2	4.35	.03	.03	1	24
W1 1200E 350S	2	128	2	64	.4	41	19	538	5.29	2	5	ND	1	44	1	2	3	165	.99	.06	4	87	1.19	17	.75	3	4.34	.03	.02	1	16
W1 1200E 375S	1	92	10	85	.3	42	21	776	5.41	7	5	ND	1	37	1	2	2	162	.92	.09	3	97	1.01	29	.66	5	3.62	.03	.03	1	26
STD C/AU-0.5	20	60	40	135	7.5	68	29	1155	3.95	37	18	7	35	49	16	15	21	58	.48	.15	38	58	.88	174	.08	38	1.71	.06	.11	13	490

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
W1 1200E 400S	1	95	2	74	.2	43	29	824	4.35	11	5	ND	1	34	1	5	3	123	.86	.09	4	101	.99	33	.53	21	3.71	.03	.02	1	6
W1 1200E 425S	1	63	14	86	.2	30	17	690	5.67	11	5	ND	1	39	1	4	9	176	.81	.15	4	94	.92	30	.79	19	2.85	.03	.03	1	5
W1 1200E 450S	1	153	9	66	.1	38	25	700	4.02	18	5	ND	1	40	1	2	2	111	1.13	.18	3	79	1.13	24	.51	23	4.96	.05	.02	1	4
W1 1200E 475S	1	141	23	85	.2	39	34	1353	3.90	12	5	ND	1	46	1	2	3	114	1.33	.13	5	74	1.13	40	.50	24	3.69	.05	.03	1	1
W1 1200E 500S	1	253	5	69	.4	49	49	1225	4.37	34	5	ND	1	39	1	2	2	126	1.00	.13	5	89	1.24	71	.55	21	5.26	.05	.03	1	14
W1 1400E 425N	1	32	19	45	.1	11	11	315	10.56	5	5	ND	1	19	1	5	14	430	.34	.11	2	86	.33	15	1.10	21	1.77	.02	.02	1	11
W1 1400E 400N	1	44	8	90	.1	43	23	1491	6.21	2	5	ND	1	35	1	2	8	190	1.13	.10	2	97	1.67	20	.74	20	2.72	.03	.03	1	5
W1 1400E 375N	2	53	50	53	.1	28	28	1826	3.22	6	5	ND	1	21	1	2	2	86	.49	.16	3	48	.63	32	.29	19	2.15	.02	.03	1	1
W1 1400E 350N	1	105	12	71	.3	26	17	528	5.72	7	5	ND	1	18	1	2	2	121	.33	.12	2	66	.90	17	.52	23	3.70	.02	.03	1	2
W1 1400E 325N	1	189	17	60	.2	35	24	763	4.27	5	5	ND	1	29	1	2	2	102	.46	.13	4	65	1.04	23	.35	29	3.43	.02	.03	1	6
W1 1400E 300N	1	125	9	69	.1	29	22	705	4.34	4	5	ND	1	41	1	3	2	110	.57	.10	7	50	.63	37	.35	6	2.49	.02	.04	1	84
W1 1400E 275N	1	89	17	62	.1	22	15	609	6.32	2	5	ND	1	37	1	2	2	159	.53	.07	2	56	.59	27	.48	22	2.48	.02	.03	1	13
W1 1400E 250N	1	57	9	61	.1	22	13	417	6.15	2	5	ND	1	40	1	3	2	172	.58	.07	5	70	.65	28	.57	22	2.58	.02	.03	1	11
W1 1400E 225N	1	134	13	94	.1	36	22	642	6.22	12	5	ND	2	39	1	3	8	174	.57	.10	6	81	1.20	28	.74	21	4.51	.02	.04	1	7
W1 1400E 200N	1	24	4	42	.1	13	8	333	3.13	2	5	ND	1	35	1	2	3	136	.69	.04	3	41	.43	31	.64	14	1.42	.02	.02	1	5
W1 1400E 175N	1	121	2	47	.1	20	14	283	3.61	3	5	ND	1	24	1	2	2	107	.37	.06	5	64	.42	41	.28	17	2.96	.02	.03	1	4
W1 1400E 150N	1	61	10	69	.1	25	14	491	3.77	6	5	ND	1	38	1	2	2	149	.58	.05	4	57	.65	27	.67	22	2.16	.02	.03	1	1
W1 1400E 125N	1	119	11	86	.1	38	36	1420	5.05	16	5	ND	1	46	1	2	2	144	.75	.08	4	72	.98	26	.57	19	2.75	.02	.03	1	52
W1 1400E 100N	1	187	8	99	.4	49	32	699	5.96	24	5	ND	2	41	1	6	2	162	.57	.09	7	84	1.20	31	.70	22	4.36	.02	.03	1	6
W1 1400E 75N	1	292	15	47	.1	25	87	1301	2.41	14	5	ND	1	33	1	2	2	70	.55	.08	12	33	.43	32	.31	22	2.41	.02	.03	1	8
W1 1400E 50N	1	218	14	133	.6	45	265	3506	4.83	28	5	ND	1	39	1	3	2	120	.74	.10	7	68	.75	45	.51	17	4.46	.02	.03	1	27
W1 1400E 25N	2	206	6	146	.4	55	259	5196	5.19	33	5	ND	1	42	1	3	4	127	.86	.11	7	74	.91	52	.55	24	3.99	.02	.04	1	65
W1 1400E 25S	2	148	6	72	.1	30	51	1078	3.68	24	5	ND	1	20	1	6	2	79	.44	.20	6	61	.60	22	.34	24	5.96	.02	.03	1	12
W1 1400E 50S	1	97	2	69	.1	29	24	781	4.93	10	5	ND	1	35	1	3	4	150	.77	.07	2	59	.87	27	.69	23	3.17	.03	.03	1	9
W1 1400E 75S	1	95	10	78	.1	21	30	1342	4.62	5	5	ND	1	31	1	3	4	135	.61	.08	4	51	.65	29	.53	24	2.76	.03	.03	1	7
W1 1400E 100S	1	132	2	59	.1	27	19	430	4.73	11	5	ND	1	26	1	6	4	149	.61	.15	3	67	.76	16	.64	5	4.15	.02	.03	1	16
EL 900 CR-1	1	155	2	72	.1	45	22	585	5.15	2	5	ND	1	35	1	2	3	157	.86	.06	2	88	1.15	17	.72	3	3.52	.03	.02	1	2
EL 900 CR-2	1	208	9	92	.3	46	27	682	4.77	8	5	ND	1	49	1	2	2	126	.98	.10	3	98	1.43	27	.60	20	4.17	.03	.02	1	1
STD C/AU-0.5	20	61	38	137	7.5	67	30	1183	3.98	38	18	8	35	49	16	15	22	57	.47	.15	38	60	.87	182	.08	36	1.72	.06	.11	13	500

TC. Mt. Whymper

ACME ANALYTICAL LABORATORIES LTD. 852 E.HASTINGS ST.VANCOUVER B.C. V6A 1R6 PHONE 253-3158 DATA LINE 251-1011

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN.FE.CA.P.CR.MG.BA.TI.B.AL.NA.K.W.SI.ZR.CE.SN.Y.NB AND TA. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: SOILS -80 MESH AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: OCT 9 1985 DATE REPORT MAILED: Oct 16/85 ASSAYER. D. Toye. DEAN TOYE OR TOM SAUNDRY. CERTIFIED B.C. ASSAYER

IMPERIAL METALS CORPORATION PROJECT - 5008 FILE # 85-2729 PAGE 1

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
W1 0E 500N	1	20	12	42	.1	13	1	135	2.62	4	5	ND	1	11	1	3	2	109	.40	.05	3	36	.24	23	.28	11	1.04	.02	.03	1	23
W1 0E 475N	2	98	13	56	.4	12	10	269	5.59	66	5	ND	1	8	1	5	2	90	.19	.09	7	38	.19	26	.16	6	3.06	.01	.02	1	21
W1 0E 450N	2	26	21	79	.1	12	12	498	3.83	319	5	ND	1	30	1	2	2	59	.72	.08	4	19	.29	34	.11	5	2.11	.01	.02	1	5
W1 0E 425N	2	54	11	37	.2	21	10	474	4.68	123	5	ND	1	15	1	3	2	86	.37	.07	8	42	.28	39	.19	7	2.37	.01	.02	1	440
W1 0E 400N	1	15	9	24	.1	6	1	99	1.79	15	5	ND	1	6	1	2	2	48	.22	.04	3	18	.21	11	.11	2	1.09	.01	.02	1	10
W1 0E 375N	2	84	12	43	.1	23	20	489	2.53	178	5	ND	1	22	1	2	2	44	.69	.08	4	34	.55	29	.09	3	2.51	.01	.03	1	2
W1 0E 350N	1	104	14	36	.2	19	3	175	2.88	13	5	ND	1	8	1	2	2	85	.30	.03	4	54	.28	22	.28	2	1.79	.01	.02	1	3
W1 0E 325N	1	33	9	34	.2	10	1	173	2.50	6	5	ND	1	6	1	2	2	101	.26	.03	3	34	.22	22	.23	2	1.24	.01	.02	1	18
W1 0E 300N	1	8	15	15	.1	2	1	41	.83	4	5	ND	1	4	1	2	2	61	.09	.03	3	11	.06	21	.16	2	.88	.01	.02	1	9
W1 0E 275N	2	94	8	42	.2	16	8	124	1.72	69	5	ND	1	9	1	2	2	45	.32	.07	2	29	.32	13	.12	2	2.39	.01	.02	1	1
W1 0E 250N	3	134	7	35	.8	9	1	64	2.28	28	5	ND	1	6	1	2	2	64	.13	.11	3	24	.15	14	.10	2	1.79	.01	.03	1	2
W1 0E 225N	2	109	27	41	.2	16	52	1265	2.07	101	5	ND	1	18	1	2	2	45	.53	.12	3	23	.26	16	.09	3	2.48	.01	.02	1	2
W1 0E 200N	2	120	17	44	.5	19	40	1235	2.29	181	5	ND	1	14	1	2	2	45	.38	.13	4	24	.20	15	.09	3	3.10	.01	.02	1	1
W1 0E 175N	1	64	42	28	.2	18	9	212	1.48	12	5	ND	1	22	1	2	2	31	.41	.13	3	16	.14	26	.07	2	1.88	.01	.04	1	28
W1 0E 150N	1	76	14	47	.2	16	3	81	1.97	29	5	ND	1	22	1	2	2	50	.40	.08	2	21	.15	34	.12	2	.92	.01	.03	2	6
W1 0E 125N	2	18	18	30	.3	10	1	76	2.25	27	5	ND	1	15	1	2	2	144	.26	.06	2	24	.13	27	.29	2	.50	.01	.03	1	2
W1 0E 100N	1	26	21	23	.2	10	1	63	1.25	8	5	ND	1	14	1	2	2	43	.22	.08	2	15	.14	24	.11	2	.54	.02	.03	1	1
W1 0E 75N	1	7	8	29	.1	4	1	24	.10	7	5	ND	1	20	1	2	2	2	.48	.07	2	2	.12	14	.01	2	.14	.01	.04	1	1
W1 0E 50N	1	14	22	26	.2	12	2	23	.29	7	5	ND	1	32	1	2	2	6	.69	.10	2	5	.10	54	.01	2	.36	.01	.04	1	2
W1 0E 25N	2	17	32	27	.1	8	4	106	1.29	54	5	ND	1	24	1	2	2	38	.92	.06	2	15	.14	28	.09	2	.61	.01	.03	1	1
W1 0E 25S	1	64	13	30	.3	14	1	147	3.05	11	5	ND	1	10	1	3	2	106	.28	.07	2	37	.20	20	.31	2	1.33	.02	.02	1	2
W1 0E 50S	1	73	12	31	.2	19	1	148	2.98	5	5	ND	1	9	1	2	2	95	.36	.06	2	48	.30	26	.29	2	1.43	.02	.02	1	21
W1 0E 75S	1	45	10	33	.1	17	1	150	4.11	14	5	ND	1	8	1	2	3	126	.22	.06	2	54	.29	21	.38	2	1.72	.01	.01	1	4
W1 0E 100S	1	70	14	28	.2	24	3	135	3.46	27	5	ND	1	14	1	2	2	93	.33	.05	2	72	.43	17	.26	2	2.42	.01	.01	1	5
W1 0E 125S	4	172	11	36	.2	34	7	224	3.55	35	9	ND	2	16	1	3	2	81	.37	.09	2	67	.59	26	.25	3	5.06	.02	.02	1	2
W1 0E 150S	1	161	15	35	.2	31	6	221	3.79	32	5	ND	1	11	1	2	3	76	.34	.11	2	59	.51	23	.20	2	4.03	.02	.02	1	3
W1 0E 175S	5	204	15	51	.5	34	8	533	3.88	36	5	ND	1	13	1	2	2	82	.36	.13	5	70	.56	34	.25	3	5.29	.02	.02	2	5
W1 0E 200S	1	109	10	42	.2	26	5	389	4.67	33	5	ND	1	9	1	2	2	97	.30	.07	2	65	.48	20	.30	2	3.24	.01	.02	1	6
W1 0E 225S	1	45	13	24	.3	18	3	161	2.19	26	5	ND	1	10	1	2	2	50	.28	.12	2	47	.25	27	.14	2	1.20	.01	.03	1	14
W1 0E 250S	2	134	11	39	.4	30	27	946	2.91	62	6	ND	1	21	1	2	2	59	.53	.16	2	52	.52	39	.10	2	2.88	.02	.03	1	6
W1 0E 275S	3	131	16	40	.6	36	12	992	4.89	16	5	ND	1	14	1	2	2	132	.35	.16	3	109	.79	19	.18	6	3.12	.01	.03	1	24
W1 0E 285S	1	170	11	79	.4	49	23	2036	3.72	11	5	ND	1	24	1	2	2	88	.68	.14	3	86	.53	72	.22	3	1.94	.02	.04	1	1
W1 200E 500N	1	28	13	57	.2	11	1	287	3.87	3	5	ND	2	15	1	4	2	145	.54	.05	2	33	.31	24	.41	2	1.20	.02	.03	1	2
W1 200E 475N	4	108	11	45	.1	16	1	164	3.37	43	5	ND	2	10	1	2	2	79	.24	.10	2	50	.37	14	.33	2	6.61	.01	.02	1	4
W1 200E 450N	4	70	11	63	.4	15	1	439	4.03	16	5	ND	2	14	1	2	2	114	.32	.10	2	48	.31	24	.34	3	3.17	.02	.03	1	1
W1 200E 425N	2	71	9	55	.2	16	2	185	4.46	15	5	ND	2	10	1	2	2	90	.28	.13	2	39	.37	20	.27	5	2.87	.02	.05	1	7
STD C/AU-0.5	21	61	41	132	6.9	70	25	1129	3.91	40	17	7	37	49	16	16	20	57	.48	.14	37	56	.88	183	.07	38	1.72	.05	.10	12	490

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
W1 200E 400N	1	32	10	36	.2	10	1	151	3.44	4	5	ND	1	8	1	3	2	109	.28	.05	4	37	.24	17	.34	3	1.31	.02	.03	1	8
W1 200E 375N	1	26	6	30	.1	9	1	144	3.29	2	5	ND	1	11	1	2	2	149	.25	.03	2	30	.16	16	.38	2	.90	.01	.01	1	4
W1 200E 350N	1	25	8	36	.1	7	1	139	7.11	5	5	ND	2	8	1	2	2	185	.30	.05	8	33	.31	15	.43	2	2.07	.01	.02	1	6
W1 200E 325N	1	52	6	66	.1	17	5	179	1.65	10	5	ND	1	17	1	2	2	54	.56	.12	2	49	.43	14	.18	4	1.36	.03	.03	1	10
W1 200E 300N	1	48	9	38	.3	15	5	177	1.61	10	5	ND	1	13	1	3	2	64	.41	.06	3	42	.44	19	.29	4	1.97	.02	.02	1	26
W1 200E 275N	1	19	11	31	.1	11	1	213	4.76	2	5	ND	1	7	1	2	2	191	.27	.05	5	54	.28	11	.51	5	1.10	.02	.02	1	4
W1 200E 250N	3	95	4	75	.4	20	118	3845	2.81	15	5	ND	1	11	1	3	2	95	.34	.11	2	64	.39	16	.23	4	5.04	.01	.02	1	78
W1 200E 225N	1	38	9	47	.1	12	3	173	2.45	3	5	ND	1	12	1	2	2	71	.25	.07	2	38	.17	18	.27	2	1.11	.02	.02	1	46
W1 200E 200N	1	42	10	49	.1	21	4	337	5.42	2	5	ND	1	14	1	2	3	129	.47	.06	3	68	.46	24	.43	3	2.21	.02	.03	1	16
W1 200E 175N	1	15	9	32	.1	14	1	161	2.52	2	5	ND	2	11	1	2	2	97	.49	.03	2	43	.34	15	.36	2	1.31	.02	.03	1	24
W1 200E 150N	1	18	6	29	.1	13	1	150	1.93	2	5	ND	1	10	1	2	2	92	.36	.03	2	36	.36	8	.45	2	.85	.02	.03	1	28
W1 200E 125N	1	19	13	40	.1	11	1	158	3.11	2	5	ND	1	10	1	2	2	125	.39	.04	2	45	.26	11	.37	3	1.22	.02	.02	1	6
W1 200E 100N	1	64	4	40	.3	16	3	128	3.12	5	5	ND	1	8	1	2	4	75	.28	.06	3	39	.29	15	.25	6	2.74	.01	.02	1	14
W1 200E 75N	1	15	37	73	.2	8	5	120	.22	11	5	ND	1	45	1	2	2	6	1.22	.06	2	4	.11	19	.01	2	.32	.01	.03	1	1
W1 200E 50N	2	38	15	36	.1	11	3	132	4.47	92	5	ND	1	8	1	2	3	130	.28	.04	2	44	.20	23	.30	3	1.74	.02	.02	1	10
W1 200E 25N	1	86	21	81	.2	16	17	1300	2.60	102	5	ND	1	23	1	2	2	78	1.04	.07	3	36	.19	31	.19	3	1.58	.01	.02	1	4
W1 200E 25S	1	31	9	32	.1	10	6	1068	1.26	79	5	ND	1	23	1	2	2	56	1.10	.05	2	36	.18	27	.15	3	.78	.01	.02	1	1
W1 200E 50S	1	14	9	29	.1	13	2	186	2.89	4	5	ND	1	10	1	2	4	107	.56	.03	2	52	.31	23	.32	3	.85	.03	.04	1	1
W1 200E 75S	1	96	5	11	.4	22	4	51	1.24	15	5	ND	1	25	1	2	2	29	.45	.06	3	26	.15	22	.10	2	1.07	.01	.02	1	4
W1 200E 100S	1	73	7	25	.4	12	4	89	2.88	23	5	ND	1	10	1	2	2	70	.20	.05	4	43	.22	17	.20	2	1.44	.01	.01	1	1
W1 200E 125S	1	199	3	30	.3	25	11	266	3.20	21	5	ND	1	13	1	2	2	64	.31	.08	2	53	.39	20	.22	2	4.10	.02	.02	1	4
W1 200E 150S	1	12	28	69	.2	7	3	50	.23	3	5	ND	1	42	1	2	2	6	.38	.08	2	4	.13	36	.01	4	.18	.01	.07	1	1
W1 200E 175S	1	34	20	49	.2	27	6	486	5.40	4	5	ND	1	25	1	2	2	139	.44	.06	6	88	.67	20	.42	2	2.21	.02	.02	1	24
W1 200E 200S	1	76	8	34	.3	20	3	99	2.14	8	5	ND	1	15	1	2	2	48	.28	.09	2	44	.20	12	.14	3	1.30	.02	.02	1	1
W1 200E 225S	4	100	8	31	.3	21	4	205	3.94	16	5	ND	1	13	1	2	2	102	.40	.09	5	80	.46	19	.28	5	2.51	.02	.01	1	16
W1 200E 250S	2	101	17	32	.5	23	6	193	3.03	3	5	ND	1	17	1	2	2	81	.44	.11	3	63	.45	24	.20	2	1.76	.02	.02	1	4
W1 200E 275S	1	69	9	22	.5	17	5	96	1.93	8	5	ND	1	16	1	2	2	36	.32	.12	2	39	.35	22	.09	3	1.52	.02	.03	1	1
W1 200E 300S	1	154	6	19	.2	14	13	783	2.22	19	5	ND	1	11	1	2	2	47	.29	.14	4	51	.34	15	.11	3	5.41	.01	.01	1	4
W1 400E 500N	2	94	7	63	.7	26	8	345	4.80	39	5	ND	2	20	1	2	2	129	.47	.12	2	74	.71	18	.58	2	5.15	.02	.02	1	80
W1 400E 475N	3	102	6	54	.3	13	3	156	5.25	36	5	ND	2	12	1	2	2	113	.26	.27	6	46	.35	15	.28	2	5.97	.01	.01	1	4
W1 400E 450N	1	135	4	53	.2	27	14	527	3.20	23	5	ND	1	32	1	2	2	90	.57	.10	2	52	.75	32	.34	2	3.82	.02	.02	1	6
W1 400E 425N	1	59	2	31	.4	13	1	236	6.15	10	5	ND	2	10	1	2	2	197	.28	.07	4	59	.35	15	.63	2	3.37	.01	.01	1	8
W1 400E 400N	1	66	4	32	.3	14	1	243	4.44	19	5	ND	1	13	1	3	2	110	.34	.08	2	43	.39	15	.48	2	3.06	.02	.01	1	28
W1 400E 375N	1	118	4	35	.3	18	4	240	3.50	12	5	ND	1	16	1	2	2	105	.52	.08	2	41	.54	12	.44	3	5.17	.02	.02	1	4
W1 400E 350N	3	83	8	45	.4	19	9	384	5.52	23	5	ND	1	15	1	3	2	149	.46	.07	6	46	.57	15	.60	3	3.82	.03	.02	1	1
W1 400E 325N	1	65	8	38	.4	17	1	230	5.48	9	5	ND	2	11	1	2	2	174	.45	.07	3	52	.49	13	.61	2	4.03	.03	.02	1	14
STD C/AU-0.5	20	59	38	139	7.0	67	28	1172	3.93	38	17	7	39	52	16	15	21	57	.48	.15	38	58	.88	177	.08	38	1.72	.06	.10	11	500

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Au*
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPB
WI 400E 300N	2	104	5	38	.3	20	1	258	4.03	3	10	ND	1	13	1	3	2	116	.39	.10	2	44	.55	12	.48	8	5.71	.02	.01	1	10
WI 400E 275S	1	109	2	30	.1	15	1	199	3.79	10	9	ND	1	14	1	2	3	103	.36	.13	2	43	.40	12	.36	4	6.40	.02	.02	1	36
WI 400E 250N	2	73	11	45	.5	15	5	502	4.88	6	12	ND	1	14	1	2	2	176	.51	.05	2	34	.43	22	.54	5	2.33	.02	.02	1	16
WI 400E 225N	2	72	7	58	.4	20	4	407	4.04	11	10	ND	1	13	1	5	2	115	.61	.12	2	39	.50	26	.40	9	4.02	.03	.02	1	10
WI 400E 200N	1	45	11	55	.2	14	1	272	3.30	10	8	ND	1	13	1	2	2	120	.33	.04	2	41	.31	32	.34	4	2.34	.02	.02	1	8
WI 400E 175N	1	51	5	32	.1	14	2	219	2.70	13	7	ND	1	15	2	6	2	57	.31	.09	2	45	.34	20	.20	5	5.13	.02	.02	1	6
WI 400E 150N	2	60	7	45	.4	16	1	191	4.59	62	12	ND	1	9	1	5	2	112	.32	.09	2	69	.34	16	.34	5	4.23	.03	.02	1	8
WI 400E 125N	4	87	10	76	.3	25	37	1140	5.14	69	13	ND	1	15	1	2	2	131	.49	.06	2	53	.36	37	.38	5	2.91	.03	.02	1	14
WI 400E 100N	1	72	2	53	.3	20	19	339	3.79	65	10	ND	1	8	1	2	2	84	.33	.07	2	55	.31	20	.28	4	5.37	.02	.01	1	1
WI 400E 75N	1	26	12	24	.2	9	3	78	.44	5	5	ND	1	33	2	4	2	10	.57	.06	2	9	.14	42	.03	4	.64	.01	.03	1	1
WI 400E 50N	1	12	16	9	.2	4	1	55	.40	5	5	ND	1	15	2	2	2	9	.32	.07	2	7	.06	14	.02	4	.44	.01	.02	1	1
WI 400E 25N	1	87	12	26	.3	16	1	137	3.73	29	9	ND	1	11	1	2	2	151	.45	.04	2	54	.33	13	.42	3	1.84	.02	.01	1	4
WI 600E 500N	4	85	68	209	.4	21	40	5264	4.05	43	10	ND	1	27	2	2	2	114	.60	.07	2	26	.42	85	.37	2	1.83	.01	.02	1	12
WI 600E 475N	2	90	26	145	.5	19	17	744	4.77	87	10	ND	1	19	1	2	2	124	.36	.06	2	33	.64	30	.44	4	2.44	.01	.01	1	8
WI 600E 450N	1	31	40	96	.2	23	17	1084	3.68	19	9	ND	1	28	1	2	2	105	.80	.08	2	26	1.20	23	.31	4	1.79	.02	.04	1	4
WI 600E 425N	1	130	42	179	.2	30	75	1910	3.01	73	7	ND	1	21	2	2	4	69	.63	.11	2	30	.54	41	.22	4	4.02	.01	.03	1	6
WI 600E 400N	5	131	25	171	.8	36	15	592	5.60	63	14	ND	2	26	1	3	2	157	.66	.11	2	42	.93	26	.52	5	3.46	.02	.03	1	10
WI 600E 375N	3	80	17	101	.6	22	6	609	5.06	23	12	ND	1	21	1	2	2	151	.44	.10	2	38	.75	26	.53	5	3.31	.02	.02	1	2
WI 600E 350N	3	77	21	107	.4	17	19	924	3.49	25	9	ND	1	26	2	2	2	110	.75	.09	2	25	.50	25	.40	5	1.71	.01	.03	1	4
WI 600E 325N	3	112	21	109	.3	35	27	1684	4.53	23	11	ND	1	33	1	5	2	128	.90	.12	2	45	1.12	33	.43	4	2.63	.02	.03	1	1
WI 600E 300N	3	54	20	83	.3	23	3	910	4.61	14	11	ND	1	30	1	2	2	130	.68	.12	2	40	.80	37	.58	3	2.25	.02	.02	1	1
WI 600E 275N	2	41	18	86	.3	20	10	590	4.30	34	11	ND	1	30	1	2	2	136	.77	.09	2	39	.64	32	.53	2	1.74	.02	.03	1	1
WI 600E 250N	1	5	9	50	.5	2	1	14	.10	6	5	ND	1	20	2	2	2	2	.45	.06	2	1	.04	28	.01	3	.09	.01	.03	1	1
WI 600E 225N	1	43	9	39	.3	11	1	144	5.70	326	14	ND	1	13	1	2	2	232	.39	.04	2	50	.35	19	.68	2	2.05	.01	.02	1	4
WI 600E 200N	2	77	3	60	.4	19	1	225	4.94	115	13	ND	1	15	1	2	2	149	.45	.08	2	61	.63	10	.44	2	3.59	.02	.02	1	6
WI 600E 175N	4	49	6	54	.3	14	1	203	6.01	220	16	ND	1	14	1	2	2	228	.49	.06	2	51	.45	15	.68	2	2.42	.03	.03	1	8
WI 600E 150N	1	147	4	52	.2	29	7	274	2.83	194	7	ND	1	18	2	7	2	73	.68	.07	2	57	.69	15	.24	4	5.58	.03	.01	1	34
WI 600E 125N	1	112	2	36	.4	13	3	137	2.25	61	6	ND	1	9	2	3	2	42	.25	.10	2	50	.26	9	.15	2	5.70	.01	.01	1	12
WI 600E 100N	3	308	11	38	1.2	20	3	148	3.57	32	9	ND	1	9	2	2	2	79	.22	.09	2	60	.33	13	.27	2	4.27	.01	.01	1	6
WI 600E 75N	2	122	16	64	.4	34	18	672	2.31	41	6	ND	1	29	2	2	3	55	.87	.11	2	60	.68	23	.12	3	3.24	.04	.02	1	4
WI 600E 50N	3	67	9	56	.5	24	3	318	5.54	23	14	ND	1	11	1	2	2	143	.35	.08	2	74	.60	20	.42	2	2.29	.02	.03	1	16
WI 600E 25N	6	70	7	45	.3	21	1	275	6.85	23	17	ND	1	9	1	2	3	176	.32	.07	2	88	.48	16	.44	3	2.70	.02	.02	1	8
WI 600E 25S	2	43	15	52	.4	23	1	159	5.55	8	14	ND	1	24	1	2	2	174	.53	.08	2	61	.37	34	.50	3	1.54	.02	.03	1	1
WI 600E 50S	2	74	2	52	.5	23	3	226	3.14	12	9	ND	1	10	2	5	2	75	.40	.08	2	58	.49	16	.28	2	5.39	.02	.02	1	1
WI 600E 75S	2	94	2	50	.5	23	3	1411	3.45	4	10	ND	1	9	1	4	2	83	.35	.14	2	63	.47	22	.32	4	6.80	.03	.02	1	4
WI 600E 100S	2	83	3	47	.4	16	6	447	3.45	8	9	ND	1	8	2	3	2	67	.29	.16	2	64	.31	14	.22	4	5.92	.02	.02	1	1
STD C/AU-0.5	20	60	41	135	7.1	68	26	1148	3.92	40	17	7	36	50	17	15	21	59	.48	.15	37	57	.88	169	.08	38	1.72	.06	.10	12	510

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
W1 600E 125S	1	65	2	42	.1	16	6	376	2.82	2	5	ND	1	9	1	2	2	51	.24	.11	3	57	.32	17	.21	6	6.20	.01	.01	1	6
W1 600E 150S	1	70	6	49	.2	22	2	399	4.99	18	5	ND	1	9	1	3	2	106	.45	.14	4	86	.52	16	.37	9	4.60	.03	.02	1	1
W1 600E 175S	1	65	15	48	.2	21	4	412	4.33	9	5	ND	2	13	1	4	2	118	.45	.08	2	62	.35	29	.33	8	2.39	.02	.03	1	2
W1 600E 200S	1	129	2	39	.3	16	67	2323	3.12	2	5	ND	1	8	1	6	2	57	.15	.17	4	59	.16	24	.13	6	7.07	.01	.01	1	2
W1 600E 225S	1	100	7	38	.2	21	1	184	4.11	7	5	ND	1	13	1	5	2	97	.33	.07	4	46	.34	26	.35	10	2.82	.02	.01	1	65
W1 600E 250S	1	122	5	78	.2	18	32	2347	3.67	19	5	ND	1	13	1	6	2	84	.26	.12	4	48	.43	39	.13	8	5.35	.01	.01	1	2
W1 600E 275S	1	121	4	60	.2	21	12	578	4.46	7	5	ND	1	18	1	2	2	99	.41	.08	2	71	.40	50	.27	6	3.77	.01	.02	1	1
W1 600E 300S	1	88	5	57	.2	20	7	386	5.04	8	5	ND	2	13	1	2	2	115	.32	.07	2	83	.41	27	.37	6	4.04	.01	.02	1	2
W1 600E 325S	1	57	8	69	.3	23	1	447	4.44	2	5	ND	1	18	1	2	2	149	.49	.06	4	90	.38	29	.47	7	2.14	.02	.02	1	2
W1 600E 350S	1	149	8	74	.2	37	29	1867	3.07	5	5	ND	1	35	2	3	2	73	.81	.13	2	69	.76	37	.14	8	2.93	.02	.02	1	8
W1 600E 375S	1	135	10	52	.2	37	13	630	4.08	2	5	ND	1	20	1	7	2	101	.64	.07	3	77	.84	29	.31	5	4.98	.03	.02	1	10
W1 600E 400S	1	77	7	70	.2	39	13	672	4.25	4	5	ND	1	31	1	2	2	85	.73	.11	4	83	.85	26	.26	8	2.74	.02	.03	1	1
W1 600E 425S	1	127	16	43	.2	24	94	1670	2.76	6	5	ND	1	20	2	5	2	36	.33	.15	3	35	.22	44	.06	7	4.06	.01	.02	1	1
W1 600E 450S	1	54	6	37	.3	21	3	298	4.13	6	5	ND	1	12	1	2	2	128	.41	.08	3	61	.38	23	.31	6	2.66	.02	.02	1	9
W1 600E 475S	1	66	7	14	.2	10	26	594	.58	2	5	ND	1	18	2	4	2	13	.34	.16	5	7	.08	24	.02	4	3.90	.01	.02	1	1
W1 600E 500S	1	12	7	37	.1	6	1	12	.15	3	5	ND	1	20	1	2	3	3	.88	.08	2	3	.07	16	.01	3	.20	.01	.03	2	1
W1 800E 500N	1	31	3	35	.1	17	1	281	2.76	12	5	ND	1	16	1	2	2	137	.38	.06	2	43	.48	21	.49	7	1.12	.02	.02	1	32
W1 800E 475N	1	21	14	56	.1	24	6	632	6.54	10	5	ND	2	26	1	2	2	219	.44	.06	2	57	.97	18	.67	6	2.02	.01	.02	1	34
W1 800E 450N	1	64	12	96	.4	34	7	1370	7.03	37	5	ND	2	17	1	2	2	187	.27	.08	2	62	1.45	29	.58	4	3.24	.01	.03	1	19
W1 800E 425N	1	67	13	96	.2	34	35	651	7.25	80	5	ND	2	16	1	2	2	170	.32	.09	2	52	.97	19	.51	3	4.17	.01	.03	1	6
W1 800E 400N	1	68	18	129	.1	44	23	1441	6.17	48	5	ND	2	23	1	2	2	161	.51	.05	5	63	1.46	42	.53	4	3.03	.02	.04	1	10
W1 800E 375N	1	21	11	36	.2	16	1	269	4.25	11	5	ND	1	15	1	4	2	128	.48	.02	3	39	.57	13	.36	5	1.78	.02	.02	2	1
W1 800E 325N	2	132	16	110	.3	40	39	1788	5.80	149	5	ND	1	38	1	6	2	145	.77	.07	6	45	1.15	38	.37	9	4.36	.03	.03	1	37
W1 800E 300N	2	165	19	114	.7	42	29	970	5.67	119	5	ND	2	30	1	5	2	147	.71	.08	2	46	1.13	34	.45	9	3.52	.02	.03	1	150
W1 800E 275N	1	99	16	98	.4	32	17	1008	5.10	49	5	ND	1	34	1	3	2	146	.97	.10	2	43	1.03	35	.47	7	3.24	.02	.03	1	1
W1 800E 250N	1	68	44	72	.3	17	98	2278	1.10	19	5	ND	1	36	2	2	2	21	1.13	.21	3	9	.20	38	.03	5	2.75	.02	.03	1	2
W1 800E 225N	1	47	39	73	.2	13	7	562	1.52	26	5	ND	1	34	1	2	4	36	.91	.14	2	12	.26	35	.11	4	.84	.01	.04	1	24
W1 800E 200N	1	89	20	111	.1	50	126	2335	4.03	75	5	ND	1	49	1	2	3	97	1.27	.40	2	43	1.09	42	.17	3	4.41	.01	.03	1	110
W1 800E 175N	2	161	13	92	.1	54	54	786	5.03	39	5	ND	1	32	1	2	2	133	1.97	.08	3	54	1.87	16	.51	7	3.30	.06	.04	1	2
W1 800E 150N	1	88	13	66	.6	27	11	416	4.26	36	5	ND	1	28	1	2	3	128	.89	.07	2	40	.88	19	.41	6	2.44	.02	.04	1	30
W1 800E 125N	1	174	12	68	.4	37	20	628	4.66	37	7	ND	2	25	1	2	2	127	.88	.08	3	51	1.10	18	.47	6	4.26	.03	.03	1	15
W1 800E 100N	1	66	8	75	.4	20	7	547	4.49	23	5	ND	1	21	1	2	2	128	.48	.07	2	40	.59	24	.48	2	2.48	.02	.02	1	1
W1 800E 75N	2	101	12	89	.5	29	13	493	5.27	58	5	ND	2	24	1	2	2	146	.54	.08	2	52	.83	25	.56	4	3.66	.02	.03	1	8
W1 800E 50N	2	150	7	62	.5	34	19	722	3.84	59	5	ND	1	69	1	6	2	96	1.50	.13	3	62	1.01	18	.32	7	5.18	.03	.03	1	7
W1 800E 25N	2	74	10	65	.3	19	2	374	5.53	63	5	ND	1	20	1	2	2	177	.53	.09	2	52	.50	30	.62	4	2.69	.02	.02	1	1
W1 800E 25S	1	120	5	48	.2	34	18	565	2.98	73	5	ND	1	25	1	2	2	69	.82	.08	2	67	.81	27	.19	5	3.99	.04	.02	1	2
STD C/AU-0.5	21	58	39	134	6.9	68	26	1152	3.94	38	17	7	37	51	17	15	21	58	.48	.15	39	57	.88	172	.08	40	1.73	.06	.10	12	500

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
W1 800E 50S	1	124	2	43	.4	30	13	438	3.63	72	5	ND	1	14	1	2	2	83	.44	.07	2	72	.57	20	.24	2	4.44	.02	.02	1	8
W1 800E 75S	2	128	2	43	.5	32	18	625	2.71	50	5	ND	1	13	1	2	2	87	.40	.08	4	56	.49	17	.22	2	4.36	.02	.02	1	9
W1 800E 100S	1	116	2	59	.1	31	14	428	2.97	12	5	ND	1	38	1	2	2	77	1.22	.07	3	51	.94	22	.26	4	3.65	.04	.02	1	6
W1 800E 125S	1	64	10	33	.4	14	1	304	4.18	8	5	ND	1	11	1	4	2	130	.32	.07	2	47	.33	18	.43	2	2.98	.02	.02	1	2
W1 800E 150S	2	146	6	65	.3	34	17	1794	4.75	4	5	ND	1	15	1	2	2	110	.38	.15	7	86	.68	37	.35	2	5.56	.02	.02	1	1
W1 800E 175S	1	102	4	61	.3	31	13	1208	3.21	2	5	ND	1	23	1	2	2	77	.66	.07	2	67	.61	37	.24	2	3.52	.02	.02	1	7
W1 800E 200S	1	101	8	84	.3	27	12	980	5.05	2	5	ND	1	25	1	2	2	117	.60	.09	3	81	.61	32	.36	2	3.64	.01	.02	1	24
W1 800E 225S	1	88	2	43	.3	20	1	199	3.71	2	5	ND	1	10	1	2	2	72	.29	.10	2	75	.42	18	.26	3	6.26	.02	.02	1	1
W1 800E 250S	1	103	2	47	.3	21	3	303	3.40	2	5	ND	2	9	1	2	2	80	.29	.11	3	66	.45	20	.26	3	5.84	.02	.02	1	2
W1 800E 275S	2	153	3	73	.2	34	30	1089	3.38	2	5	ND	1	18	1	2	2	68	.46	.14	4	65	.69	30	.18	3	4.43	.02	.02	1	12
W1 800E 300S	2	89	2	34	.4	22	4	261	3.43	8	5	ND	1	11	1	2	2	73	.30	.08	3	62	.48	35	.22	3	3.42	.01	.02	1	7
W1 800E 325S	2	112	12	42	.4	22	21	1203	2.56	2	5	ND	1	23	1	2	2	60	.52	.08	4	37	.38	49	.17	3	2.46	.02	.03	1	2
W1 800E 350S	1	53	6	52	.3	22	5	330	3.04	2	5	ND	1	22	1	2	2	81	.43	.05	2	62	.52	61	.19	2	1.68	.01	.02	1	1
W1 800E 375S	2	387	8	44	.8	25	8	405	3.49	2	5	ND	1	18	1	2	2	94	.57	.06	3	58	.51	29	.26	3	1.99	.02	.03	1	30
W1 800E 400S	2	323	8	36	.4	30	32	1033	2.11	11	5	ND	1	32	1	2	2	45	1.06	.12	3	43	.48	30	.10	3	3.96	.03	.02	1	1
W1 800E 425S	1	111	21	53	.2	13	23	816	1.01	4	5	ND	1	36	1	2	2	22	1.37	.08	2	21	.15	31	.04	4	.79	.01	.04	1	2
W1 800E 450S	1	10	16	19	.1	6	1	33	.11	7	5	ND	1	14	1	2	2	2	.55	.08	2	4	.05	10	.01	3	.10	.02	.03	1	1
W1 800E 475S	1	115	8	30	.1	26	10	201	2.16	2	5	ND	1	21	1	2	2	45	.51	.08	3	49	.37	38	.11	3	4.19	.02	.02	1	2
W1 800E 500S	1	149	9	35	.3	30	6	215	2.44	6	5	ND	1	24	1	2	2	55	.71	.09	2	52	.64	23	.12	3	3.15	.02	.02	1	28
W1 BL 0E	1	70	18	40	.3	25	5	492	3.07	6	5	ND	1	12	1	3	2	89	.40	.09	2	49	.27	19	.20	3	1.67	.03	.03	1	9
W1 BL 25E	1	92	9	21	.4	15	1	80	1.81	4	5	ND	1	9	1	2	2	84	.19	.06	2	46	.16	16	.21	3	1.37	.02	.02	1	6
W1 BL 50E	1	67	9	33	.3	15	1	115	2.78	30	5	ND	1	11	1	2	2	78	.23	.07	2	27	.17	21	.21	3	1.50	.02	.02	1	2
W1 BL 75E	1	30	16	27	.1	9	1	131	1.78	8	5	ND	1	18	1	2	2	53	.32	.08	2	18	.13	20	.14	2	.75	.01	.03	1	1
W1 BL 100E	1	42	8	32	.3	15	1	127	2.77	25	5	ND	1	13	1	3	2	102	.29	.06	2	37	.26	13	.29	2	.97	.02	.02	1	2
W1 BL 125E	3	52	13	51	.4	16	35	1205	1.73	651	5	ND	1	19	1	2	2	47	.68	.09	5	57	.19	29	.12	3	3.46	.02	.03	1	1
W1 BL 150E	2	24	11	36	.2	9	5	141	1.37	222	5	ND	1	19	1	2	2	41	.36	.08	2	27	.10	32	.10	3	1.38	.02	.02	1	1
W1 BL 175E	2	38	13	42	.4	13	7	423	3.09	418	5	ND	1	41	1	4	2	83	2.14	.05	4	38	.22	33	.21	5	1.95	.01	.03	1	1
W1 BL 200E	2	37	6	39	.3	13	6	194	2.97	427	5	ND	1	14	1	2	2	69	.35	.05	2	32	.25	20	.17	3	2.26	.02	.03	1	6
W1 BL 225E	1	19	40	30	.2	10	3	132	.82	28	5	ND	1	25	1	2	2	23	1.09	.06	2	13	.14	24	.06	4	.48	.02	.04	1	1
W1 BL 250E	2	44	10	45	.2	13	17	331	3.77	325	5	ND	1	12	1	2	2	88	.23	.05	3	33	.24	29	.19	2	2.34	.01	.03	1	2
W1 BL 275E	1	17	13	34	.1	10	2	46	.75	22	5	ND	1	19	1	2	2	20	.66	.08	2	9	.11	20	.05	5	.49	.02	.03	1	1
W1 BL 300E	3	18	12	27	.1	18	1	151	2.68	144	5	ND	1	23	1	2	2	82	.56	.04	2	50	.43	40	.25	3	.98	.03	.02	1	2
W1 BL 325E	2	75	11	54	.2	24	28	933	2.21	280	5	ND	1	16	1	2	2	53	.59	.09	3	44	.41	32	.14	4	3.91	.02	.03	1	1
W1 BL 350E	2	73	8	62	.4	41	41	1385	3.79	95	5	ND	1	24	1	2	2	92	1.02	.05	4	80	1.06	32	.24	5	3.09	.08	.03	1	1
W1 BL 375E	1	18	10	31	.6	16	1	172	4.43	26	5	ND	1	11	1	6	2	213	.42	.05	4	63	.39	18	.64	4	1.08	.03	.03	2	8
W1 BL 400E	1	103	6	30	.2	33	7	233	2.95	19	5	ND	1	14	1	4	3	81	.64	.06	4	82	.68	20	.24	5	3.92	.03	.02	1	1
STD C/AU-0.5	20	60	40	136	7.0	69	26	1162	3.95	37	19	7	37	50	16	15	21	59	.48	.15	39	57	.88	171	.08	41	1.73	.06	.11	12	500

APPENDIX 3

Statistical Calculations

[illegible]

STRUCTURE FOR FILE: B:[illegible].DBF
NUMBER OF RECORDS: 00313
DATE OF LAST UPDATE: 08/31/84
PRIMARY USE DATABASE

FLD	NAME	TYPE	WIDTH	DEC
001	MOPPM	N	005	
002	CUPPM	N	005	
003	PBPPM	N	005	
004	ZNPPM	N	005	
005	AGPPM	N	005	001
006	NIPPM	N	005	
007	COPPM	N	005	
008	MNPPM	N	005	
009	FEPCT	N	005	002
010	ASPPM	N	005	
011	UPPM	N	005	
012	AUPPM	N	005	
013	THPPM	N	005	
014	SRPPM	N	005	
015	CDPPM	N	005	
016	SBPPM	N	005	
017	BIPPM	N	005	
018	VPPM	N	005	
019	CAPCT	N	005	002
020	PPCT	N	005	002
021	LAPPM	N	005	
022	CRPPM	N	005	
023	MGPCT	N	005	002
024	BAPPM	N	005	
025	TIPCT	N	005	002
026	BPPM	N	005	
027	ALPCT	N	005	002
028	NAPCT	N	005	002
029	KPCT	N	005	002
030	WPPM	N	005	
031	AUPPB	N	005	
** TOTAL **			00156	

. SET PRINT OFF

COL A	MEAN	STD DEV	COL B	COVARIANCE	CORRELATION
1	1.670927	1.051716	2	12.55177	.2204132
			3	.3126202	3.497774E-02
			4	6.636078	.2308426
			5	.0470424	.2686224
			6	1.907032	.1769424
			7	2.068184	.0736287
			8	79.95581	9.965298E-02
			9	.2601619	.1595082
			10	21.17103	.2845727
			11	.6762448	.308479
			12	-.2307363	-.1592425
			13	5.750799E-02	.1343677
			14	.6955376	4.957567E-02
			15	-.2209883	-.1472355
			16	2.340508E-02	2.309511E-02
			17	-.0107789	-6.311578E-03
			18	9.447434	.1735037
			19	-9.092689E-02	-6.375431E-02
			20	-.2012653	-.1266506
			21	-.1199975	-6.846617E-02
			22	7.451233	.2965534
			23	-.1289061	-8.684548E-02
			24	1.475117	.1264283
			25	-.170634	-.123065
			26	-.6540537	-8.582164E-02
			27	.4285503	.2317361
			28	-.2221881	-.13125
			29	-.1216063	-.1547645
			30	-8.489418E-02	-.1416404
			31	.617981	1.859943E-02
2	92.22044	54.31987	3	-84.48407	-.1830162
			4	335.2144	.2257704
			5	3.817431	.42205
			6	352.5628	.6333595
			7	558.139	.384716
			8	10074.42	.2431086
			9	16.08377	.190927
			10	-165.5901	-4.309488E-02
			11	-5.934815	-5.241658E-02
			12	13.34295	.1782931
			13	-2.849838	-.1289219
			14	61.48377	8.484931E-02
			15	10.44086	.1346852
			16	-1.081894	-2.066972E-02
			17	-3.043427	-3.450373E-02
			18	-226.0435	-8.037605E-02
			19	10.22981	.1388752
			20	10.13027	.1234239
			21	14.66235	.1619748
			22	341.7149	.2633168
			23	19.36977	.2526609
			24	-29.25977	-4.855441E-02
			25	7.159027	9.996841E-02

COL A	MEAN	STD DEV	COL B	COVARIANCE	CORRELATION
			26	46.29566	.1176152
			27	50.21335	.5257159
			28	13.94058	.1594407
			29	7.599776	.1872646
			30	5.73053	.1851159
			31	61.8263	3.602779E-02
3	11.86262	8.525432	4	71.4577	.3066448
			5	-.1775799	-.1250918
			6	-5.842011	-6.686801E-02
			7	25.31862	.1111937
			8	1630.44	.2506844
			9	-1.64769	-.1246227
			10	12.94104	2.145867E-02
			11	1.468277	8.262506E-02
			12	-.1825576	-1.554265E-02
			13	-4.153347E-02	-1.197146E-02
			14	24.62407	.216516
			15	.1859779	1.528576E-02
			16	-.8498707	-.1034535
			17	.4083252	2.949522E-02
			18	-34.34119	-7.780227E-02
			19	.419672	3.630024E-02
			20	.143321	1.112578E-02
			21	-.7882385	-5.548093E-02
			22	-63.76074	-.3130475
			23	.2657919	.0220901
			24	26.65424	.2818164
			25	-.4856558	-4.320954E-02
			26	-1.907555	-3.087753E-02
			27	-3.655533	-.2438512
			28	-.1131592	-8.246137E-03
			29	-.1131077	-1.775781E-02
			30	-6.168175E-02	-1.269545E-02
			31	-1.122376	-4.167205E-03
4	54.68051	27.42122	5	.5200682	.1139003
			6	147.4742	.5248098
			7	349.6944	.4774837
			8	12843.14	.6139365
			9	19.12146	.4496477
			10	142.626	7.352953E-02
			11	8.450989	.1478567
			12	8.151863	.2157803
			13	-.6453667	-5.783425E-02
			14	69.31726	.1894965
			15	7.206711	.1841587
			16	-1.905563	-7.211825E-02
			17	7.131119	.1601522
			18	251.1196	.1768835
			19	7.576691	.2037552
			20	7.324723	.1767833
			21	1.967835	.043063
			22	5.329834	.0081358
			23	10.81744	.2795181

COL A	MEAN	STD DEV	COL B	COVARIANCE	CORRELATION
			24	69.0785	.2270767
			25	7.545647	.2087263
			26	-4.01944	-2.022836E-02
			27	8.921371	.1850272
			28	9.488146	.214967
			29	4.193851	.2047104
			30	3.469299	.222005
			31	44.30316	5.114122E-02
5	.2817891	.1670469	6	.2594233	.1515455
			7	.304996	6.836163E-02
			8	2.593918	2.035433E-02
			9	.0393101	.1517413
			10	1.453179	.122979
			11	8.709001E-02	.250121
			12	-4.355457E-02	-.1892505
			13	1.118216E-02	.164495
			14	8.241368E-02	3.698345E-02
			15	-2.124944E-02	-8.913558E-02
			16	2.222657E-02	.1380838
			17	-3.283364E-02	-.1210438
			18	1.907417	.2205468
			19	-4.011069E-02	-.177067
			20	-4.605659E-02	-.1824695
			21	-8.417904E-03	-3.023905E-02
			22	1.22824	.3077643
			23	-2.053995E-02	-8.712311E-02
			24	4.146814E-02	2.237653E-02
			25	-3.524317E-02	-.160031
			26	.1210796	.1000264
			27	.0750646	.2555568
			28	-4.281049E-02	-.1592169
			29	-2.094644E-02	-.1678362
			30	-1.559168E-02	-.1637805
			31	.1221101	2.313857E-02
6	23.82428	10.28057	7	125.2225	.4560598
			8	3155.57	.4023458
			9	7.302765	.458045
			10	-35.82837	-4.926741E-02
			11	-2.228165	-.1039801
			12	3.331768	.2352335
			13	-.5367413	-.128296
			14	38.89139	.2835847
			15	2.267525	.1545527
			16	-.7538147	-7.609496E-02
			17	1.866352	.1117991
			18	65.36988	.1228157
			19	3.452856	.2476721
			20	2.909224	.1872823
			21	3.275757	.191204
			22	96.24512	.3918635
			23	5.719252	.3941797
			24	7.333435	6.429936E-02
			25	2.191618	.1617019

COL A	MEAN	STD DEV	COL B	COVARIANCE	CORRELATION
			26	11.33675	.1521785
			27	7.806412	.4318419
			28	3.619681	.218741
			29	1.996193	.2598955
			30	1.357317	.231671
			31	34.3573	.1057852
7	17.99361	26.79373	8	14955.19	.7316403
			9	4.36348	.1050118
			10	93.79449	4.948734E-02
			11	-5.166123	-9.250214E-02
			12	11.18476	.3029948
			13	-2.900959	-.2660564
			14	24.14679	6.755738E-02
			15	9.117426	.238441
			16	-2.426483	-9.398373E-02
			17	4.316487	9.921084E-02
			18	-230.6217	-.1662495
			19	8.255435	.2272075
			20	10.50519	.2594822
			21	4.237503	9.490288E-02
			22	-65.64014	-.1025439
			23	12.68939	.3355673
			24	1.733002	5.830185E-03
			25	6.498059	.1839577
			26	6.957115	3.583258E-02
			27	11.69049	.2481361
			28	14.43232	.3346417
			29	5.05299	.252423
			30	5.023508	.3289892
			31	35.28548	4.168559E-02
8	665.8755	765.3338	9	187.2556	.1577692
			10	826.7305	1.527084E-02
			11	-30.10034	-1.886865E-02
			12	185.8664	.1762754
			13	-52.77637	-.1694548
			14	1525.772	.1494463
			15	132.5166	.1213281
			16	-9.051392	-1.227363E-02
			17	71.64429	5.764912E-02
			18	-1047.965	-2.644778E-02
			19	188.2687	.1814024
			20	177.9689	.153897
			21	159.6792	.1251987
			22	-209.3516	-1.144982E-02
			23	237.0224	.2194374
			24	2380.511	.2803727
			25	102.9159	.1019997
			26	200.2612	3.611004E-02
			27	238.7234	.1773925
			28	247.7986	.2011524
			29	91.68216	.1603421
			30	83.21081	.1907817
			31	604.5391	2.500326E-02

COL A	MEAN	STD DEV.	COL B	COVARIANCE	CORRELATION
9	3.741758	1.555793	10	-1.621689	-1.473553E-02
			11	.437294	.1348473
			12	.46189	.2154907
			13	3.632617E-02	5.737639E-02
			14	-1.500946	-7.232026E-02
			15	.4179649	.1882479
			16	-.0838337	-5.592108E-02
			17	.607853	.2406073
			18	49.08789	.6094193
			19	.1828241	8.665582E-02
			20	.3784616	.160993
			21	.6341095	.2445767
			22	14.06998	.3785429
			23	.6617716	.3013899
			24	-2.608765	-.1511471
			25	.6553173	.3194975
			26	1.252031	.1110569
			27	.8155375	.2981143
			28	.527891	.2107996
			29	.2127857	.1830646
			30	.1637106	.184643
			31	6.252377	.1272086
10	36.84984	70.76429	11	18.12004	.122501
			12	-13.65968	-.1397148
			13	2.23003	7.722114E-02
			14	78.17005	8.257472E-02
			15	-10.81559	-.1067954
			16	6.645401	9.718291E-02
			17	-5.028992	-4.364184E-02
			18	237.8914	6.474888E-02
			19	-6.099028	-6.337773E-02
			20	-13.20489	-.1231492
			21	4.626061	3.911776E-02
			22	77.97803	4.599449E-02
			23	-11.43988	-.1142231
			24	77.1905	9.804838E-02
			25	-10.89362	-.1164393
			26	-39.09557	-7.602731E-02
			27	6.770241	5.425689E-02
			28	-14.06367	-.1231224
			29	-6.882021	-.1298045
			30	-5.602528	-.1385326
			31	156.3559	6.974253E-02
11	5.501598	2.091075	12	-.7354877	-.255298
			13	.1533547	.1802157
			14	.4113846	1.474773E-02
			15	-.5181737	-.1736392
			16	.3510294	.1742138
			17	-.3746491	-.1103359
			18	37.5636	.3469693
			19	-.6738253	-.2376258
			20	-.7243811	-.2292632
			21	-.8836574	-.2535811

COL A	MEAN	STD DEV	COL B	COVARIANCE	CORRELATION
			22	7.294983	.1460253
			23	-.4359465	-.1477188
			24	2.733688	.1178409
			25	-.3912957	-.1419394
			26	-1.798386	-.1186848
			27	.0982666	2.672557E-02
			28	-.772773	-.2295935
			29	-.3746764	-.2398283
			30	-.3069949	-.2576139
			31	-1.588142	-2.404047E-02
12	.4153355	1.382128	13	-.4153355	-.7384416
			14	-7.640479	-.4143993
			15	1.456838	.7385929
			16	-.5214916	-.3915684
			17	.2110361	9.403088E-02
			18	-36.12724	-.5048706
			19	1.271156	.6782137
			20	1.825505	.8741211
			21	.5207259	.2260807
			22	-17.92955	-.5429935
			23	1.506288	.772204
			24	-7.837173	-.5111258
			25	1.39911	.7678408
			26	-.9827089	-9.812026E-02
			27	.3509916	.144424
			28	1.969264	.8851826
			29	.9577912	.9275479
			30	.7403873	.9399798
			31	-4.643	-.1063344
13	1	.4082484	14	1.392971	.2557786
			15	-.3226837	-.5538529
			16	.115016	.2923764
			17	-.0607028	-9.156851E-02
			18	11.73163	.5550438
			19	-.2895212	-.5229641
			20	-.3983076	-.6457002
			21	-9.584665E-02	-.1408818
			22	4.434502	.4546673
			23	-.3145687	-.545963
			24	1.568691	.3463614
			25	-.2929071	-.544218
			26	.1054316	3.563921E-02
			27	-2.923322E-02	-4.072328E-02
			28	-.4298084	-.654075
			29	-.2086888	-.6842083
			30	-.1629393	-.7003403
			31	1.380192	.1070134
14	19.47284	13.38268	15	-5.877939	-.3077682
			16	1.703426	.1320957
			17	1.503223	.0691739
			18	145.9755	.2106833
			19	-.8709202	-4.799003E-02
			20	-7.255241	-.3587942

COL A	MEAN	STD DEV.	COL B	COVARIANCE	CORRELATION
			21	-.4251175	-1.906199E-02
			22	87.94648	.2750734
			23	-4.263199	-.2257172
			24	66.00986	.4446129
			25	-5.409497	-.3066063
			26	15.64284	.1613074
			27	-6.289673E-02	-2.672855E-03
			28	-7.879354	-.3657839
			29	-3.817945	-.3818564
			30	-3.046259	-.3994214
			31	29.27643	6.924653E-02
15	1.376997	1.431686	16	-.3487532	-.2528011
			17	8.120966E-02	3.493186E-02
			18	-29.91136	-.4035355
			19	.9877703	.5087729
			20	1.201487	.555403
			21	7.354403E-02	3.082492E-02
			22	-14.63923	-.4279998
			23	1.412167	.6988926
			24	-5.669159	-.3569334
			25	1.08715	.5759822
			26	-.8917513	-8.595632E-02
			27	.3109245	.1235088
			28	1.316499	.5712808
			29	.7346226	.6867996
			30	.5619431	.688735
			31	-3.946044	-8.724432E-02
16	2.255591	.9666766	17	-.2090359	-.1331685
			18	9.779159	.1953951
			19	-.3528822	-.2691934
			20	-.4992956	-.3418325
			21	-.1103721	-6.851418E-02
			22	5.374382	.232713
			23	-.410977	-.3012372
			24	2.20686	.2057832
			25	-.3920442	-.3076248
			26	.1050119	1.499131E-02
			27	.2079754	.1223549
			28	-.5387688	-.3462569
			29	-.2629741	-.3641207
			30	-.1894987	-.3439796
			31	3.257784	.1066754
17	2.530352	1.629026	18	15.62129	.1852177
			19	.217639	9.852007E-02
			20	.1581335	6.424405E-02
			21	.3606758	.1328592
			22	.6563416	1.686458E-02
			23	.1731916	7.533054E-02
			24	-.660698	-3.655877E-02
			25	.240997	.1122151
			26	1.198093	.101495
			27	-.1727042	-6.029284E-02
			28	.2439494	9.303559E-02

COL A	MEAN	STD DEV	COL B	COVARIANCE	CORRELATION
			29	.0830431	.0682322
			30	.0712471	7.674446E-02
			31	1.109585	2.156035E-02
18	90.21406	51.93933	19	-24.84775	-.3527821
			20	-35.13403	-.4476807
			21	2.688995	3.106678E-02
			22	774.5313	.6241888
			23	-21.8798	-.2984827
			24	103.5498	.1797088
			25	-19.34453	-.2825071
			26	55.31671	.1469745
			27	2.492432	2.729088E-02
			28	-37.41382	-.4475204
			29	-18.18394	-.4686033
			30	-14.07664	-.4755654
			31	237.5049	.1447436
19	.8625244	1.360423	20	1.161041	.5648205
			21	.4043632	.1783611
			22	-11.10502	-.3416795
			23	1.016414	.5293819
			24	-4.54955	-.301447
			25	.8717166	.4860365
			26	-.138195	-1.401847E-02
			27	.4000189	.1672235
			28	1.448782	.6416165
			29	.6148727	.6049577
			30	.5087495	.6562024
			31	-3.460199	-8.051008E-02
20	.4893619	1.515839	21	.5594343	.2214617
			22	-17.04568	-.4706897
			23	1.268091	.5927475
			24	-7.530776	-.4478198
			25	1.378358	.6897258
			26	-.7493108	-6.821675E-02
			27	.4080395	.1530875
			28	1.867363	.7653376
			29	.8147625	.7194353
			30	.7187061	.831967
			31	-4.408491	-.0920577
21	3.169329	1.671812	22	2.841187E-02	7.11354E-04
			23	.4890876	.2072868
			24	-1.875176	-.1011046
			25	.4973731	.2256641
			26	2.093212	.1727858
			27	.4602185	.1565551
			28	.5225569	.1941885
			29	.2903012	.2324209
			30	.1518133	.159342
			31	8.024018	.1519245
22	47.32269	23.96715	23	-10.8623	-.3211276
			24	62.60608	.2354597
			25	-11.48314	-.3634223
			26	32.67825	.1881587

COL A	MEAN	STD DEV	COL B	COVARIANCE	CORRELATION
			27	14.88319	.3531591
			28	-18.31213	-.4746785
			29	-9.060904	-.5060213
			30	-7.124829	-.5216338
			31	77.41828	.1022469
23	.8733225	1.415851	24	-5.873645	-.3739441
			25	1.052584	.5639058
			26	-.1612449	-.0157163
			27	.4700861	.1888211
			28	1.612249	.7074433
			29	.83785	.7920678
			30	.5585755	.6922645
			31	-2.498996	-5.586903E-02
24	22.71566	11.12944	25	-5.839222	-.3979689
			26	4.007141	4.968706E-02
			27	-3.546562	-.1812278
			28	-8.075998	-.4508168
			29	-3.906094	-.4697677
			30	-3.10248	-.4891515
			31	32.44064	9.226549E-02
25	.6313735	1.322581	26	-.3833838	-4.000307E-02
			27	.2358024	.101395
			28	1.507984	.708356
			29	.633377	.6409935
			30	.568764	.7546011
			31	-2.909603	-6.963612E-02
26	6.789138	7.269555	27	2.527487	.1977296
			28	-.8873444	-7.583358E-02
			29	-.5456533	-.1004668
			30	-.406363	-9.808759E-02
			31	19.93549	8.680452E-02
27	3.15492	1.764003	28	.4458766	.1570336
			29	.1250676	9.489849E-02
			30	.1360848	.1353687
			31	1.385185	2.485603E-02
28	.4509266	1.614777	29	1.026671	.8510055
			30	.7918131	.8604344
			31	-4.820104	-9.448588E-02
29	.2323949	.7495078	30	.3613946	.8460834
			31	-2.346867	-9.911411E-02
30	1.178914	.5717183	31	-1.948943	-.1079047
31	12.17891	31.69324			

OF ROWS = 313

```
 LOW LIMIT     ( DX = 40     SCALE = 2:1 )

                 |====*====*====*====*====*
 0               |::::*::::*::::*::::*::::* <15.9%>
                 |====*====*====*====*====*====*====*====*===
 40              |::::*::::*::::*::::*::::*::::*::::*::::*::: <27.7%>
                 |====*====*====*====*====*====*====*====*====*=
 80              M:::*::::*::::*::::*::::*::::*::::*::::*::::*: <29.3%>
                 |====*====*====*====*====*====*====*====*====*=
 120             |::::*::::*::::*::::*::::*::: <17.8%>
                 |====*====*====*====*====*===
 160             |::::*:::: <5.7%>
                 |====*====
 200             |:: <1.5%>
                 |==
 240             | <.3%>
                 |=
 280             |: <.6%>
                 |=
 320             | <.3%>
                 |
 360             | <.3%>
                 |
```


FROM	TO BELOW	FREQ	%	CUMUL	%	
0	40	50	15.9	50	15.9	
40	80	87	27.7	137	43.7	
80	120	92	29.3	229	73.1	*MEDIAN*
120	160	56	17.8	285	91	
160	200	18	5.7	303	96.8	
200	240	5	1.5	308	98.4	
240	280	1	.3	309	98.7	
280	320	2	.6	311	99.3	
320	360	1	.3	312	99.6	
360	400	1	.3	313	100	

MEAN: 93.22684   S-SQUARED: 3077.447   S: 55.47475   SKEWNESS: 1.231649
S.D. OF MEAN: 3.135618

Low Outliers = 0
High Outliers = 0

```
 LOW LIMIT    { DX = 7    SCALE = 4:1 }
 ---------

             |====*====*====*====
 0           |::::*::::*::::*:::: <24.9%>
             |====*====*====*====*====*====*====
 7           M::::*::::*::::*::::*::::*::::*:::: <43.4%>
             |====*====*====*====*====*====*====
 14          |::::*::::*::::*: <20.7%>
             |====*====*====*=
 21          |:::: <5.7%>
             |====
 28          |: <2.2%>
             |=
 35          |: <1.2%>
             |=
 42          | <.9%>
             |
 49          | <.3%>
             |
 56          | <0%>
             |
 63          | <.3%>
             |
```


FROM	TO BELOW	FREQ	%	CUMUL	%	
0	7	78	24.9	78	24.9	
7	14	136	43.4	214	68.3	*MEDIAN*
14	21	65	20.7	279	89.1	
21	28	18	5.7	297	94.8	
28	35	7	2.2	304	97.1	
35	42	4	1.2	308	98.4	
42	49	3	.9	311	99.3	
49	56	1	.3	312	99.6	
56	63	0	0	312	99.6	
63	70	1	.3	313	100	

MEAN: 12.49042   S-SQUARED: 76.97434   S: 8.773502   SKEWNESS: 2.032191
S.D. OF MEAN: .4959077

Low Outliers = 0
High Outliers = 0

LOW LIMIT (DX = 20 SCALE = 2:1)

```
                    |====*
  0                 |::::* <3.1%>
                    |====*====*====*====*====*====*====*====*====*=
 20                 |::::*::::*::::*::::*::::*::::*::::*::::*::::*: <29.7%>
                    |====*====*====*====*====*====*====*====*====*====*
 40                 M::::*::::*::::*::::*::::*::::*::::*::::*::::*::::* <31.9%>
                    |====*====*====*====*====*====*====*====*====*====*
 60                 |::::*::::*::::*::::*::::*::::*:::: <22%>
                    |====*====*====*====*====*====*====
 80                 |::::*::::*: <7%>
                    |====*====*=
100                 |::::* <3.1%>
                    |====*
120                 |:: <1.2%>
                    |==
140                 |: <.6%>
                    |=
160                 |: <.6%>
                    |=
180                 | <0%>
                    |
200                 | <.3%>
                    |
```

----> FREHIST (B:TEMPACME.DAT): PAGE 1

FROM	TO BELOW	FREQ	%	CUMUL	%	
0	20	10	3.1	10	3.1	
20	40	93	29.7	103	32.9	
40	60	100	31.9	203	64.8	*MEDIAN*
60	80	69	22	272	86.9	
80	100	22	7	294	93.9	
100	120	10	3.1	304	97.1	
120	140	4	1.2	308	98.4	
140	160	2	.6	310	99	
160	180	2	.6	312	99.6	
180	200	0	0	312	99.6	
200	220	1	.3	313	100	

MEAN: 54.85623 S-SQUARED: 781.5288 S: 27.95584 SKEWNESS: 1.569985
S.D. OF MEAN: 1.580157

Low Outliers = 0
High Outliers = 0

LOW LIMIT (DX = .15 SCALE = 2:1)

```
        |====*====*====*====*====*====*====*====
0       |::::*::::*::::*::::*::::*::::*::::*:::: <24.9%>
        |====*====*====*====*====*====*====*====
.15     |::::*::::*::::*::::*::::*::::*::::*:::: <24.9%>
        |====*====*====*====*====*====*====*====*====*====*====*==
.3      M::::*::::*::::*::::*::::*::::*::::*::::*::::*::::*::::*:: <36.4%>
        |====*====*====*====*====*====*====*====*====*====*====*==
.45     |::::*::::*: <7%>
        |====*====*=
.6      |::::*::: <5.4%>
        |====*===
.75     |: <.9%>
        |=
.9      | <0%>
        |
1.05    | <0%>
        |
1.2     | <.3%>
        |
1.35    | <0%>
        |
```

---> FREHIST (B:TEMPACME.DAT):

PAGE 1

FROM	TO BELOW	FREQ	%	CUMUL	%	
0	.15	78	24.9	78	24.9	
.15	.3	78	24.9	156	49.8	
.3	.45	114	36.4	270	86.2	*MEDIAN*
.45	.6	22	7	292	93.2	
.6	.75	17	5.4	309	98.7	
.75	.9	3	.9	312	99.6	
.9	1.05	0	0	312	99.6	
1.05	1.2	0	0	312	99.6	
1.2	1.35	1	.3	313	100	
1.35	1.5	0	0	313	100	

EAN: .296885 S-SQUARED: 3.293159E-02 S: .1814706 SKEWNESS: .9254641
D. OF MEAN: 1.025733E-02

ow Outliers = 0
igh Outliers = 0

```
LOW LIMIT    { DX = 70    SCALE = 6:1 }
----------

             |=====*=====*=====*=====*=====*=====*=====
 0           M::::*::::*::::*::::*::::*::::*:::: <87.2%>
             |=====*=====*=====*=====*=====*=====*=====
 70          |:: <7%>
             |==
 140         | <2.2%>
             |
 210         | <.9%>
             |
 280         | <1.2%>
             |
 350         | <.6%>
             |
 420         | <.3%>
             |
 490         | <0%>
             |
 560         | <0%>
             |
 630         | <.3%>
             |
```

---> FREHIST (B:TEMPACME.DAT):

FROM	TO BELOW	FREQ	%	CUMUL	%	
0	70	273	87.2	273	87.2	*MEDIAN*
70	140	22	7	295	94.2	
140	210	7	2.2	302	96.4	
210	280	3	.9	305	97.4	
280	350	4	1.2	309	98.7	
350	420	2	.6	311	99.3	
420	490	1	.3	312	99.6	
490	560	0	0	312	99.6	
560	630	0	0	312	99.6	
630	700	1	.3	313	100	

MEAN: 54.23323   S-SQUARED: 4451.809   S: 66.72188   SKEWNESS: 5.051055
S.D. OF MEAN: 3.771344

Low Outliers = 0
High Outliers = 0

---> FREHIST (A:CHEMONLY.DAT): MT WHYMPER W1-GRID SOIL SAMPLES ARSENIC HISTOGRAM


```
LOW LIMIT   ( DX = 10    SCALE = 4:1 )
---------

               |====*====*====*====*====*====*===
0              |::::*::::*::::*::::*::::*::::*::: (44.2%)
               |====*====*====*====*====*====*===
10             M::::*::::*::: (17.7%)
               |====*====*===
20             |::::*:::: (13%)
               |====*====
30             |::::* (7.7%)
               |====*
40             |:: (3.3%)
               |==
50             |: (1.6%)
               |==
60             |:: (3.6%)
               |==
70             |:: (2.6%)
               |==
80             |: (1.3%)
               |=
90             | (1%)
               |
100            | (.6%)
               |
110            | (.6%)
               |
120            | (1%)
               |
130            | (0%)
               |
140            | (1%)
               |
```

---> FREHIST (A:CHEMONLY.DAT):

FROM	TO BELOW	FREQ	%	CUMUL	%	
0	10	132	44.2	132	44.2	
10	20	53	17.7	185	62	*MEDIAN*
20	30	39	13	224	75.1	
30	40	23	7.7	247	82.8	
40	50	10	3.3	257	86.2	
50	60	5	1.6	262	87.9	
60	70	11	3.6	273	91.6	
70	80	8	2.6	281	94.2	
80	90	4	1.3	285	95.6	
90	100	3	1	288	96.6	
100	110	2	.6	290	97.3	
110	120	2	.6	292	97.9	
120	130	3	1	295	98.9	
130	140	0	0	295	98.9	
140	150	3	1	298	100	

MEAN: 23.99329 S-SQUARED: 796.9731 S: 28.23071 SKEWNESS: 2.10442
S.D. OF MEAN: 1.595694

Low Outliers = 0
High Outliers = 15

```
---> FREHIST (A:CHEMONLY.DAT): MT WHYMPER  W1-GRID  SOIL SAMPLES   ARSENIC HISTO
GRAM                                                                 PAGE  1

 LOW LIMIT    { DX = 5    SCALE = 2:1 }
 ---------

              |====*====*====*====*====*====*====*
 0            |::::*::::*::::*::::*::::*::::*::::* <27%>
              |====*====*====*====*====*====*====*
 5            M::::*::::*::::*::::*::::*::::* <23.2%>
              |====*====*====*====*====*====*
 10           |::::*::::*:::: <10.6%>
              |====*====*====
 15           |::::*::::*:: <9.5%>
              |====*====*==
 20           |::::*::::* <7.6%>
              |====*====*
 25           |::::*:::: <7.2%>
              |====*====
 30           |:::: <3.4%>
              |====*==
 35           |::::*:: <5.3%>
              |====*==
 40           |::: <2.6%>
              |===
 45           |: <1.1%>
              |=
 50           |: <1.1%>
              |=
 55           |: <.7%>
              |=
```

```
---> FREHIST (A:CHEMONLY.DAT):                                       PAGE  1
```

FROM	TO BELOW	FREQ	%	CUMUL	%	
0	5	71	27	71	27	
5	10	61	23.2	132	50.3	*MEDIAN*
10	15	28	10.6	160	61	
15	20	25	9.5	185	70.6	
20	25	20	7.6	205	78.2	
25	30	19	7.2	224	85.4	
30	35	9	3.4	233	88.9	
35	40	14	5.3	247	94.2	
40	45	7	2.6	254	96.9	
45	50	3	1.1	257	98	
50	55	3	1.1	260	99.2	
55	60	2	.7	262	100	

MEAN: 14.98092   S-SQUARED: 172.0893   S: 13.11828   SKEWNESS: 1.10179
S.D. OF MEAN: .7414892

Low Outliers = 0
High Outliers = 51

---> FREHIST (a:chemonly.dat): MT WHYMPER   W1 GRID   SOIL SAMPLES   BARIUM HISTOGRAM


```
LOW LIMIT     { DX = 9    SCALE = 2:1 }
---------

                |====*====*==
   0            |::::*::::*:: <7.9%>
                |====*====*====*====*====*====*====*====
   9            |::::*::::*::::*::::*::::*::::*::::*:::: <25.2%>
                |====*====*====*====*====*====*====*====*====*====*====
  18            M::::*::::*::::*::::*::::*::::*::::*::::*::::*::::*:::: <34.5%>
                |====*====*====*====*====*====*====*====*====*====*====
  27            |::::*::::*::::*::::*::::*::::*:::: <22%>
                |====*====*====*====*====*====*====
  36            |::::*::::*: <7.3%>
                |====*====*=
  45            |:: <1.5%>
                |==
  54            |: <.6%>
                |=
  63            | <0%>
                |
  72            | <.3%>
                |
  81            | <.3%>
                |
```

---> FREHIST (a:chemonly.dat):

FROM	TO BELOW	FREQ	%	CUMUL	%	
0	9	25	7.9	25	7.9	
9	18	79	25.2	104	33.2	
18	27	108	34.5	212	67.7	*MEDIAN*
27	36	69	22	281	89.7	
36	45	23	7.3	304	97.1	
45	54	5	1.5	309	98.7	
54	63	2	.6	311	99.3	
63	72	0	0	311	99.3	
72	81	1	.3	312	99.6	
81	90	1	.3	313	100	

MEAN: 23.13259   S-SQUARED: 129.5104   S: 11.38027   SKEWNESS: 1.090947
S.D. OF MEAN: .6432506

Low Outliers = 0
High Outliers = 0

LOW LIMIT { DX = 50 SCALE = 8:1 }

```
                |=====*=====*=====*=====*=====*=====*=====*==
0               M::::*:::::*:::::*:::::*:::::*:::::*:::::*:: <96.1%>
                |=====*=====*=====*=====*=====*=====*=====*==
50              | <2.2%>
                |
100             | <.6%>
                |
150             | <.6%>
                |
200             | <0%>
                |
250             | <0%>
                |
300             | <0%>
                |
350             | <0%>
                |
400             | <.3%>
                |
450             | <0%>
                |
```

---> FREHIST (B:TEMPACME.DAT):

FROM	TO BELOW	FREQ	%	CUMUL	%	
0	50	301	96.1	301	96.1	*MEDIAN*
50	100	7	2.2	308	98.4	
100	150	2	.6	310	99	
150	200	2	.6	312	99.6	
200	250	0	0	312	99.6	
250	300	0	0	312	99.6	
300	350	0	0	312	99.6	
350	400	0	0	312	99.6	
400	450	1	.3	313	100	
450	500	0	0	313	100	

MEAN: 28.99361 S-SQUARED: 758.8115 S: 27.54653 SKEWNESS: 10.81533
S.D. OF MEAN: 1.557022

Low Outliers = 0
High Outliers = 0

```
---> FREHIST (B:CHEMONLY.DAT): MT WHYMPER   W1-GRID   SOIL SAMPLES    AU(PPB) HI
STOGRAM
                                                                      PAGE  1

 LOW LIMIT    { DX = 10     SCALE = 4:1 }
 ---------

               |====*====*====*====*====*====*====*====*====*====*=====*
   0           M::::*::::*::::*::::*::::*::::*::::*::::*::::*::::*::::* <71.8%>
               |====*====*====*====*====*====*====*====*====*====*=====*
  10           |::::*::::*: <14.8%>
               |====*====*=
  20           |::::* <7.1%>
               |====*
  30           |:: <3.2%>
               |==
  40           | <.3%>
               |
  50           | <.6%>
               |
  60           | <.3%>
               |
  70           | <.3%>
               |
  80           | <.6%>
               |
  90           | <.3%>
               |
 100           | <0%>
               |
 110           | <.3%>
               |
```

---> FREHIST (B:CHEMONLY.DAT): PAGE 1

FROM	TO BELOW	FREQ	%	CUMUL	%	
0	10	222	71.8	222	71.8	*MEDIAN*
10	20	46	14.8	268	86.7	
20	30	22	7.1	290	93.8	
30	40	10	3.2	300	97	
40	50	1	.3	301	97.4	
50	60	2	.6	303	98	
60	70	1	.3	304	98.3	
70	80	1	.3	305	98.7	
80	90	2	.6	307	99.3	
90	100	1	.3	308	99.6	
100	110	0	0	308	99.6	
110	120	1	.3	309	100	

MEAN: 10.92233   S-SQUARED: 193.0814   S: 13.89537   SKEWNESS: 4.01048
S.D. OF MEAN: .7854129

Low Outliers = 0
High Outliers = 4

---> FREHIST (B:CHEMONLY.DAT): MT WHYMPER W1-GRID SOIL SAMPLES AU(PPB) HISTOGRAM


```
LOW LIMIT   { DX = 5    SCALE = 4:1 }
---------

                 |====*====*====*====*====*====*====*====
 0               M::::*::::*::::*::::*::::*::::*::::*:::: <52.1%>
                 |====*====*====*====*====*====*====*====
 5               |::::*::::*::::*: <21.1%>
                 |====*====*====*=
 10              |::::*: <8.2%>
                 |====*=
 15              |::::* <6.9%>
                 |====*
 20              |::: <4.9%>
                 |===
 25              |: <2.3%>
                 |=
 30              |: <2.3%>
                 |=
 35              | <.9%>
                 |
 40              | <0%>
                 |
 45              | <.3%>
                 |
 50              | <.3%>
                 |
 55              | <.3%>
                 |
```

---> FREHIST (B:CHEMONLY.DAT):

FROM	TO BELOW	FREQ	%	CUMUL	%	
0	5	158	52.1	158	52.1	*MEDIAN*
5	10	64	21.1	222	73.2	
10	15	25	8.2	247	81.5	
15	20	21	6.9	268	88.4	
20	25	15	4.9	283	93.3	
25	30	7	2.3	290	95.7	
30	35	7	2.3	297	98	
35	40	3	.9	300	99	
40	45	0	0	300	99	
45	50	1	.3	301	99.3	
50	55	1	.3	302	99.6	
55	60	1	.3	303	100	

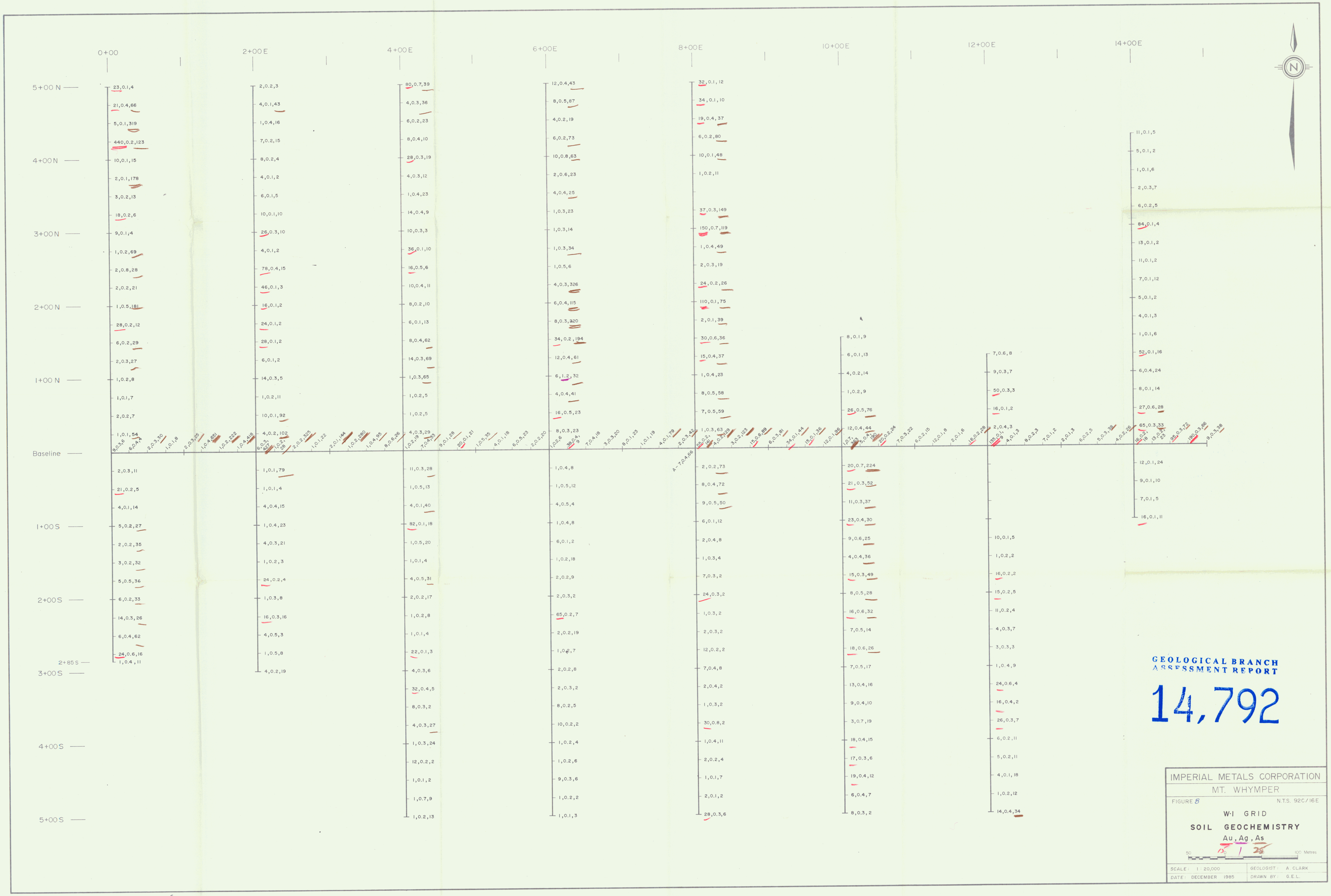
MEAN: 8.523102   S-SQUARED: 84.92685   S: 9.215576   SKEWNESS: 2.117683
S.D. OF MEAN: .5208952

Low Outliers = 0
High Outliers = 10

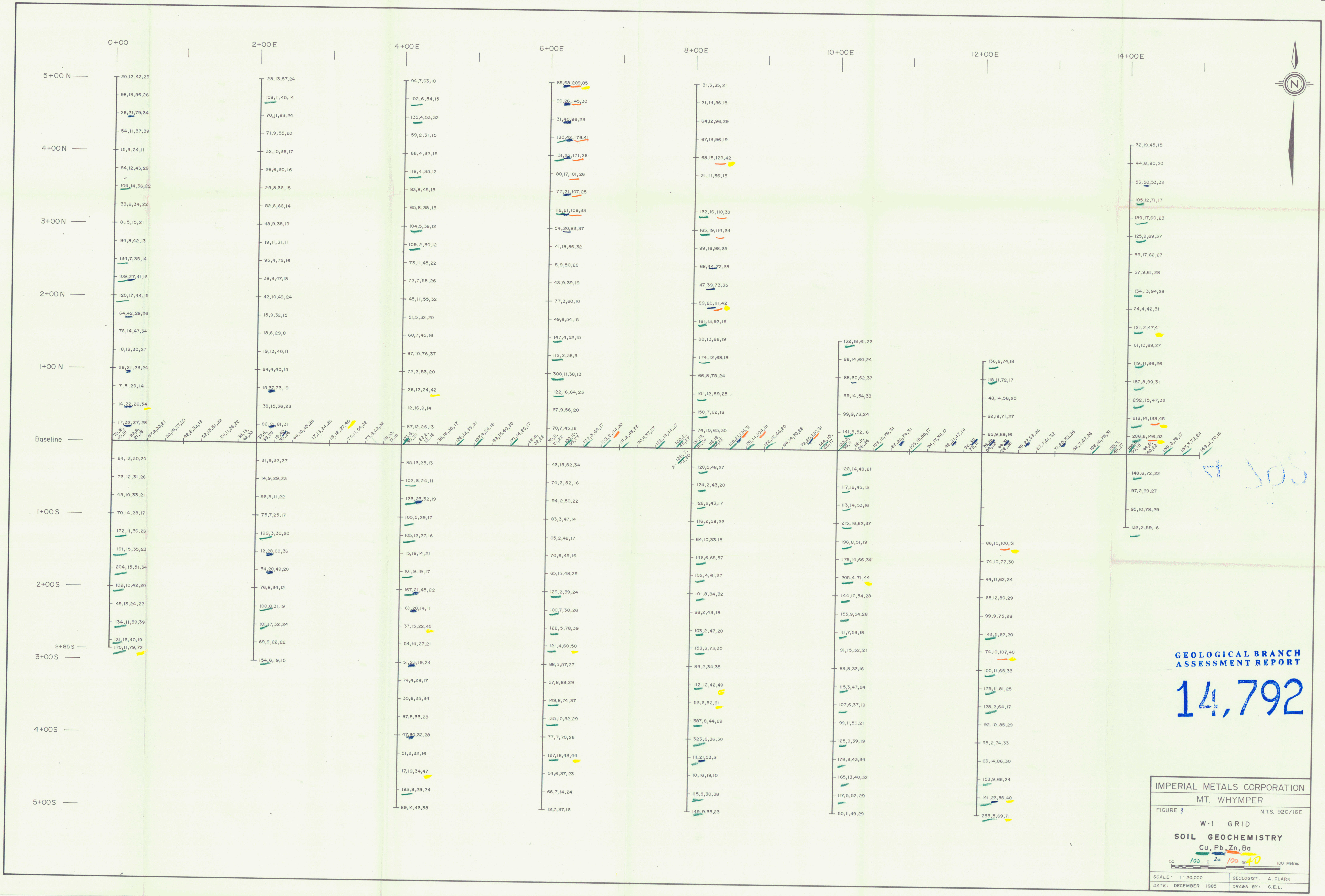
SUMMARY OF FIELD COSTS

MT. WHYMPER PROJECT - 1985

Field Crew	12 days @ $175/man-day	$ 2,100.00
Supervisor	2 days @ $250/day	500.00
Board and Lodging	26 man days @ $75/man-day	1,950.00
Truck	14 truck-days @ $100/day	1,400.00
Mob/Demob		100.00
Equipment		500.00
Samples		2,700.00
Geophysical Equipment Rental/Month		350.00
Drafting		500.00
Report		200.00
		$10,300.00



0+00
2+00E
4+00E
6+00E
8+00E
10+00E
12+00E
14+00E
5+00 N
4+00 N
3+00 N
2+00 N
1+00 N
Baseline
1+00 S
2+00 S
2+85S
3+00 S
4+00 S
5+00 S
N
GEOLOGICAL BRANCH
ASSESSMENT REPORT
14,792
IMPERIAL METALS CORPORATION
MT. WHYMPER
FIGURE 8
N.T.S. 92C/16E
W-1 GRID
SOIL GEOCHEMISTRY
Au, Ag, As
SCALE 1:20,000
GEOLOGIST: A. CLARK
DATE: DECEMBER 1985
DRAWN BY: G.E.L.



GEOLOGICAL BRANCH
ASSESSMENT REPORT

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IMPERIAL METALS CORPORATION

MT. WHYMPER

FIGURE 5

N.T.S. 92C/16E

W-1 GRID

SOIL GEOCHEMISTRY

Cu, Pb, Zn, Ba

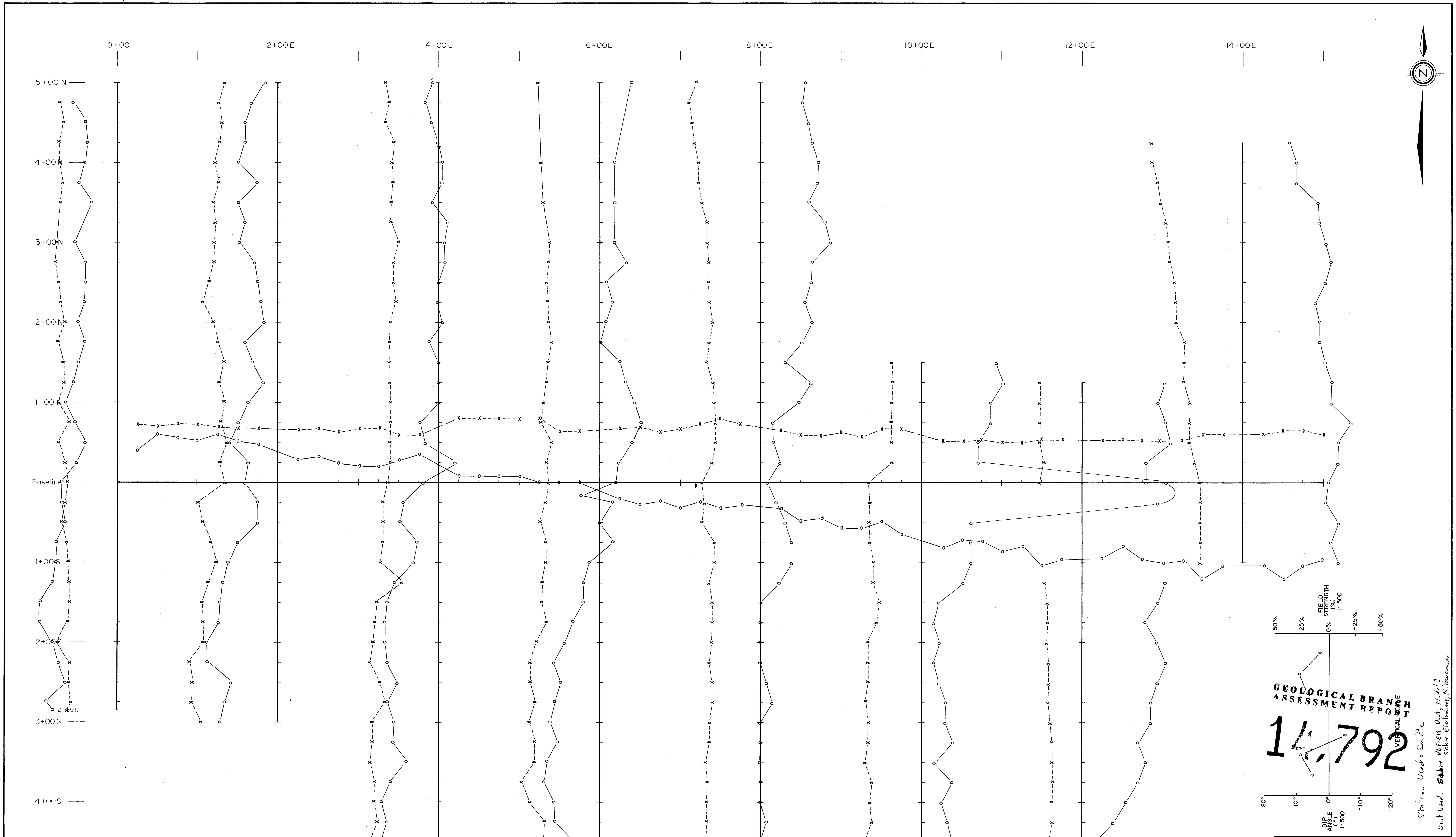
100 20 100 40

SCALE: 1:20,000

GEOLOGIST: A. CLARK

DATE: DECEMBER 1985

DRAWN BY: G.E.L.



IMPERIAL METALS CORPORATION

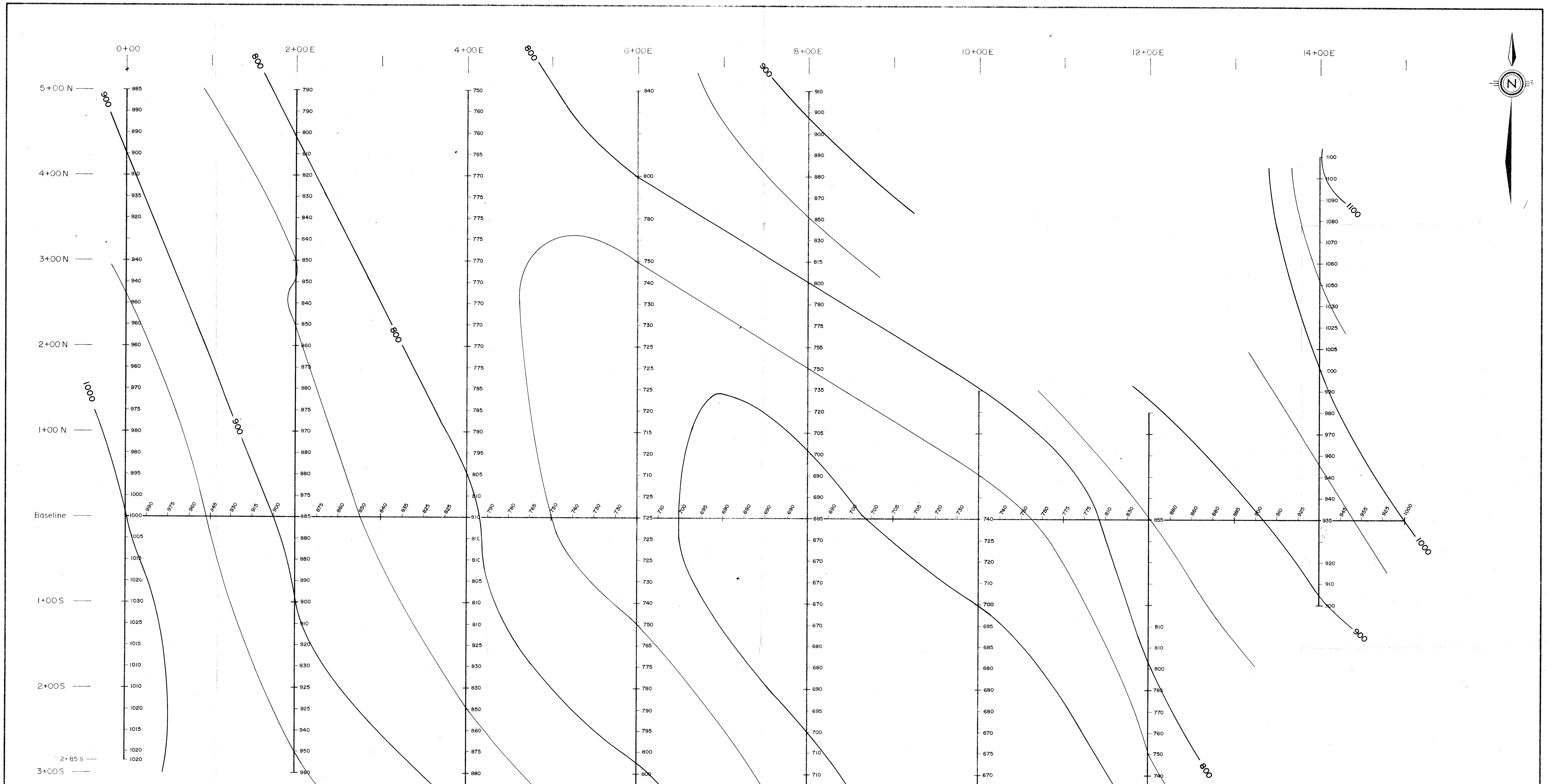
MT. WHYMPER

FIGURE 10 N.T.S. 92C/16E

VLF-EM SURVEY

50 0 50 100 Metres

SCALE 1 20,000	GEOLOGIST: A. CLARK
DATE: DECEMBER 1985	DRAWN BY: G.E.L.



NOTE: PLOTTED FROM UNCORRECTED ALTIMETER READINGS.

GEOLOGICAL BRANCH
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IMPERIAL METALS CORPORATION

MT. WHYMPER

FIGURE 11 N.T.S. 92C/16E

TOPOGRAPHY

50 0 50 100 Metres

SCALE: 1 : 20,000	GEOLOGIST: A. CLARK
DATE: DECEMBER 1985	DRAWN BY: G.E.L.