

RIVER PLANTATION MUNICIPAL UTILITY DISTRICT

NOTICE OF PUBLIC MEETING

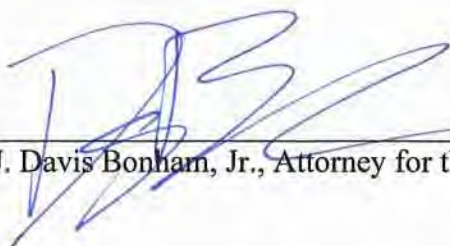
Notice is hereby given to all interested members of the public that the Board of Directors of the captioned district will hold a public meeting at **610 River Plantation Drive, Conroe, Texas 77302.**

The meeting will be held at **6:30 p.m. on Thursday, March 28, 2024.**

The subject of the meeting is to consider and act on the following:

1. Minutes of the meeting of Board of Director(s)
2. Receive comments from the Public
3. Agreement to Lease Administration Building to Montgomery County ESD No. 9
4. Financial and bookkeeping matters including:
 - a. Bookkeeper's report
 - b. Tax Assessor-Collectors' report
 - c. Review of investments
 - d. Payment of District bills
5. Order Establishing Drought Contingency Plan
6. Order Adopting Water Conservation Plan
7. Resolution to Adopt the Verity Voting 2.5 System for use in May 4, 2024 Directors Election
8. Park Rules; Penalty for Operation of Prohibited Motor Vehicle
9. Park maintenance matters
10. Operator's Report
11. Engineer's Report
12. Executive (closed) Session Pursuant to Texas Government Code §§ 551.071, 551.072, and 551.076 as necessary
13. Pending business





J. Davis Bonham, Jr., Attorney for the District

River Plantation MUD
Cash Analysis
March 28, 2024

GENERAL OPERATING FUND - First Financial Bank

| | | |
|--------------------------------------------------------------------------------------------------------------------|----|------------|
| Ending Balance from last meeting | \$ | 86,750.01 |
| Add in voided check #23882 written to All Seasons Lawn Maintenance, lost in mail | + | 11,625.00 |
| <u>Receipts</u> | | |
| Transfer from General Operating - Online Fund | + | 60,000.00 |
| Transfer from Capital Projects Fund - Texas Class, Series 2022 | + | 37,445.63 |
| Interest earned on account | + | 24.46 |
| <u>Withdrawals</u> | | |
| Payment to Centerpoint Energy, utility expense | - | 221.21 |
| Payment to Energy, utility expense | - | 5,295.35 |
| Bank charges/fees | - | 25.00 |
| Checks previously approved | | |
| 24017 - Centerpoint Energy, blank check for utility expense, holding | | |
| 24018 - Consolidated Communications, blank check for telephone expenses, holding | | |
| 24019 - Entergy, utility expense | - | 2,441.75 |
| 24021 - Synaptic Integration's, surveillance | - | 1,271.44 |
| Checks presented for signatures on March 28, 2024 | | |
| 24022 - Association of Water Board Directors, AWBD Annual Conference - Director Gilmer | - | 435.00 |
| 24023 - Consolidated Communications, telephone expenses | - | 332.31 |
| 24024 - Entergy, utility expense | - | 4,851.95 |
| 24025 - L & S District Services, LLC., bookkeeping fees & expenses for February | - | 4,319.64 |
| 24026 - Municipal Operations & Consulting, Inc., maintenance & operations for February | - | 39,627.98 |
| 24027 - Prepared Publications, Inc., operations admin | - | 210.00 |
| 24028 - River Plantation MUD - Joint Drainage, joint drainage expenses | - | 833.11 |
| 24029 - River Plantation MUD - STP, February billing & January supplement | - | 39,167.20 |
| 24030 - Smith, Murdaugh, Little & Bonham, LLP., legal fees | - | 14,383.59 |
| 24031 - The Radich Law Firm, PLLC., legal fees | - | 8,508.50 |
| 24032 - Vogler & Spencer Engineering, general engineering fees - \$3,110.00, Emergency Preparedness Plan - \$20.00 | - | 3,130.00 |
| 24033 - First Financial Bank, NA., safe deposit box rental | - | 65.00 |
| 24034 - Heidi & Luke Lawler, refund | - | 21.78 |
| 24035 - Charles H. Meyer Jr., refund | - | 80.96 |
| 24036 - Josue Garcia, refund | - | 198.01 |
| 24037 - Johnathan Johnson, refund | - | 94.14 |
| 24038 - Dee Ginn, refund | - | 65.95 |
| 24039 - Entergy, blank check for utility expense | | |
| Total Disbursements | \$ | 125,579.87 |
| Ending Balance at March 28, 2024 | \$ | 70,265.23 |

GENERAL OPERATING FUND - ONLINE - First Financial

| | | |
|--------------------------------------|----|--------------|
| Ending Balance from last meeting | \$ | 40,025.42 |
| <u>Receipts</u> | | |
| Accounts Receivable | + | 63,074.42 |
| Interest earned on account | + | 31.88 |
| <u>Withdrawals</u> | | |
| Transfer to General Operating Fund | - | 60,000.00 |
| Customer returned NSF items | - | 106.82 |
| Total Disbursements | \$ | 60,106.82 |
| Ending Balance at March 28, 2024 | \$ | 43,024.90 |
| <u>Investments</u> | | |
| General Operating Fund - Texas Class | \$ | 1,551,201.24 |
| Total Operating Funds | \$ | 1,664,491.37 |

TAX DEPOSIT ACCOUNT - First Financial Bank

| | | |
|-------------------------------------------------------------|----|------------|
| Ending Balance from last meeting | \$ | 291,917.65 |
| <u>Receipts</u> | | |
| Tax Collections | + | 220,591.13 |
| Interest earned on account | + | 92.71 |
| <u>Withdrawals</u> | | |
| Transfer to General Operating Fund - Texas Class | - | 305,643.78 |
| Transfer to Debt Service Fund - Park | - | 30,830.03 |
| Transfer to Debt Service Fund | - | 161,857.66 |
| Total Disbursements | \$ | 498,331.47 |
| Ending Balance at March 28, 2024 | \$ | 14,270.02 |
| 2023 Levy - \$1,448,345.17 (90.78% collected as of 2/29/24) | | |
| All Outstanding - \$173,466.59 | | |

CAPITAL PROJECTS FUND - First Financial Bank

| | | |
|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|----|--------------|
| Ending Balance from last meeting | \$ | 6,244.20 |
| <u>Receipts</u> | | |
| Transfer from Texas Class - Series 2022 WSD | + | 10,000.00 |
| Transfer from Texas Class - Series 2022 Park | + | 76.51 |
| Interest earned on account | + | 3.28 |
| <u>Withdrawals</u> | | |
| Bank charges/fees | - | 0.84 |
| Checks presented for signatures on March 28, 2024 | | |
| 2003 - River Plantation MUD - STP, Wastewater Treatment Facility Rehab Phase 1 | - | 3,970.38 |
| 2004 - Vogler & Spencer Engineering, Water Plant No. 2 Electrical Controls - \$1,786.76, Sanitary Sewer Rehab Phase 2 - \$1,161.60, Storm Sewer Rehab Phase 1 - \$3,321.73 | - | 6,270.09 |
| Total Disbursements | \$ | 10,241.31 |
| Ending Balance at March 28, 2024 | \$ | 6,082.68 |
| <u>Investments</u> | | |
| Texas Class - Series 2022 WSD | \$ | 3,630,335.48 |
| Total Capital Projects Funds | \$ | 3,636,418.16 |

DEBT SERVICE FUND - Texas Class

| | | |
|----------------------------------------------------------------|----|------------|
| Ending Balance from last meeting | \$ | 624,544.84 |
| <u>Receipts</u> | | |
| Transfer from Tax Fund | + | 161,857.66 |
| Interest earned on account | + | 2,627.51 |
| <u>Withdrawals</u> | | |
| Wire to Bank of New York Mellon, 3/1/24 debt service payment | - | 150,206.25 |
| Wire to Bank of New York Mellon, paying agent fee | - | 750.00 |
| Total Disbursements | \$ | 150,956.25 |
| Ending Balance at March 28, 2024 | \$ | 638,073.76 |
| Next Debt Service payment due September 1, 2024 - \$265,206.25 | | |

DEBT SERVICE FUND - PARK - Texas Class

| | | |
|--------------------------------------------------------------------|----|-----------|
| Ending Balance from last meeting | \$ | 52,201.89 |
| <u>Receipts</u> | | |
| Transfer from Tax Fund | + | 30,830.03 |
| Interest earned on account | + | 210.91 |
| <u>Withdrawals</u> | | |
| Wire to Bank of New York Mellon, 3/1/24 debt service payment | - | 23,990.63 |
| Wire to Bank of New York Mellon, paying agent fee | - | 750.00 |
| Total Disbursements | \$ | 24,740.63 |
| Ending Balance at March 28, 2024 | \$ | 58,502.20 |
| Next Park Debt Service payment due September 1, 2024 - \$53,990.63 | | |

SEWER TREATMENT PLANT FUND - First Financial Bank

| | | |
|---------------------------------------------------------------------------------------------------------------------------------------------------------------------|----|-----------|
| Ending Balance from last meeting | \$ | 14,344.72 |
| <u>Receipts</u> | | |
| Accounts Receivable - River Plantation MUD | + | 45,784.50 |
| Accounts Receivable - East Plantation UD | + | 14,097.55 |
| Interest earned on account | + | 18.34 |
| <u>Withdrawals</u> | | |
| Payment to Entergy, utility expense | - | 8,724.38 |
| Bank service charges | - | 5.21 |
| Checks previously approved | | |
| 2005 - Entergy, blank check for utility expense, holding | | |
| 2006 - Republic Services, garbage expense | - | 200.51 |
| Checks presented for signatures on March 28, 2024 | | |
| 2007 - GFL Environmental, sludge removal | - | 1,824.00 |
| 2008 - L & S District Services, LLC., bookkeeping fees & expenses for February | - | 590.18 |
| 2009 - Municipal Operations & Consulting, operations & maintenance | - | 51,774.10 |
| 2010 - Republic Services, garbage expense | - | 202.72 |
| 2011 - Vogler & Spencer Engineering, Wastewater Treatment Facility Rehab Phase 1 - \$6,566.40, Wastewater Discharge Permit - \$371.25, WWTF General - \$1,102.50 | - | 8,040.15 |
| 2012 - Republic Services, blank check for garbage expense | | |
| Total Disbursements | \$ | 71,361.25 |
| Ending Balance at March 28, 2024 | \$ | 2,883.86 |

JOINT DRAINAGE FUND - First Financial Bank

| | | |
|--------------------------------------------------------------------------------------------------------------------------------------|----|-----------|
| Ending Balance from last meeting | \$ | 15,992.76 |
| <u>Receipts</u> | | |
| Transfer from Capital Projects Fund - Series 2022, reimburse payment to Vogler & Spencer, Existing Conditions Drainage Assessment | + | 11,327.50 |
| Accounts Receivable - River Plantation MUD | + | 275.45 |
| <u>Withdrawals</u> | | |
| Payment to Entergy, utility expense | - | 32.82 |
| Bank service charges | - | 2.16 |
| Checks presented for signatures on March 28, 2024 | | |
| 2006 - L & S District Services, LLC., bookkeeping fees & expenses for February | - | 441.23 |
| 2007 - Vogler & Spencer Engineering, 711 Holly Springs Storm Sewer Replacement | - | 1,190.00 |
| 2008 - Entergy, blank check for utility expense | | |
| Total Disbursements | \$ | 1,666.21 |
| Ending Balance at March 28, 2024 | \$ | 25,929.50 |

**River Plantation MUD General Operating Fund
Profit & Loss Budget Performance
February 2024**

| | Feb 24 | Budget | Oct '23 - Feb 24 | YTD Budget | Annual Budget |
|----------------------------------------|------------|------------|------------------|--------------|---------------|
| Ordinary Income/Expense | | | | | |
| Income | | | | | |
| Water Revenue | | | | | |
| 4100 · Customer Service Fees - Water | 23,967.18 | 40,390.00 | 131,520.27 | 201,959.00 | 484,689.00 |
| 4110 · Water Tap Connection Fees | 0.00 | 0.00 | 4,120.00 | 0.00 | 0.00 |
| 4150 · LSGCD Fees | 500.72 | 1,083.00 | 3,033.29 | 5,419.00 | 13,000.00 |
| Total Water Revenue | 24,467.90 | 41,473.00 | 138,673.56 | 207,378.00 | 497,689.00 |
| Sewer Revenue | | | | | |
| 4200 · Customer Service Fees - Sewer | 34,290.54 | 35,416.00 | 174,523.41 | 177,088.00 | 425,000.00 |
| Total Sewer Revenue | 34,290.54 | 35,416.00 | 174,523.41 | 177,088.00 | 425,000.00 |
| Other Revenues | | | | | |
| 4320 · Maintenance Taxes | 303,721.02 | 304,000.00 | 820,948.93 | 822,000.00 | 855,828.00 |
| 4330 · Penalties and Interest | 867.89 | 1,000.00 | 4,124.76 | 5,000.00 | 12,000.00 |
| 4380 · Termination/Reconnection/NSF Fe | 2,176.21 | 1,083.00 | 14,331.31 | 5,419.00 | 13,000.00 |
| 4400 · Transfer/Connection Fees | 150.00 | 83.00 | 977.95 | 419.00 | 1,000.00 |
| 4600 · TCEQ Assessment Fees | 291.12 | 333.00 | 1,249.14 | 1,669.00 | 4,000.00 |
| 4800 · Customer Service Inspections | 0.00 | 166.00 | 0.00 | 838.00 | 2,000.00 |
| 5380 · Miscellaneous Income | 200.00 | 83.00 | 200.00 | 419.00 | 1,000.00 |
| 5385 · Bank Fees | 0.00 | 4.00 | 0.00 | 22.00 | 50.00 |
| 5386 · Interest Temp Investments | 0.00 | 66.00 | 0.00 | 338.00 | 800.00 |
| 5391 · Interest Income | 5,549.17 | 1,666.00 | 22,589.41 | 8,338.00 | 20,000.00 |
| Total Other Revenues | 312,955.41 | 308,484.00 | 864,421.50 | 844,462.00 | 909,678.00 |
| Total Income | 371,713.85 | 385,373.00 | 1,177,618.47 | 1,228,928.00 | 1,832,367.00 |
| Expense | | | | | |
| Water Expenses | | | | | |
| 6124 · Laboratory Expense | 507.50 | 2,200.00 | 3,992.79 | 11,000.00 | 26,400.00 |
| 6126 · Permit Fees | 0.00 | 0.00 | 6,113.90 | 3,500.00 | 3,500.00 |
| 6127 · LSGWCD Fees | 0.00 | 1,708.00 | 19,198.81 | 8,544.00 | 20,500.00 |
| 6130 · TCEQ Regulatory - Water | 0.00 | 0.00 | 0.00 | 0.00 | 1,750.00 |
| 6132 · Operator Fees | 7,844.40 | 52,850.00 | 47,237.38 | 264,250.00 | 634,200.00 |
| 6135 · Repairs & Maintenance | 25,983.26 | 16,250.00 | 125,275.68 | 81,250.00 | 195,000.00 |
| 6136 · Landscape Services - Water | 0.00 | 6,824.00 | 17,375.00 | 34,122.00 | 81,890.00 |
| 6142 · Chemicals | 0.00 | 1,250.00 | 445.50 | 6,250.00 | 15,000.00 |
| 6152 · Utilities | 5,586.10 | 5,833.00 | 22,466.09 | 29,169.00 | 70,000.00 |
| 6170 · Tap Connection Expense | 0.00 | 166.00 | 4,845.00 | 838.00 | 2,000.00 |
| Total Water Expenses | 39,921.26 | 87,081.00 | 246,950.15 | 438,923.00 | 1,050,240.00 |

**River Plantation MUD General Operating Fund
Profit & Loss Budget Performance
February 2024**

| | Feb 24 | Budget | Oct '23 - Feb 24 | YTD Budget | Annual Budget |
|----------------------------------------|-------------------|-------------------|-------------------|-------------------|---------------------|
| Sewer Expenses | | | | | |
| 6201 · Purchased Sewer Service | 36,404.05 | 14,718.00 | 104,529.43 | 73,596.00 | 176,622.00 |
| 6224 · Laboratory Expense | 0.00 | 166.00 | 0.00 | 838.00 | 2,000.00 |
| 6230 · TCEQ Regulatory - Wastewater | 0.00 | 0.00 | 0.00 | 0.00 | 2,000.00 |
| 6232 · Operator Fees | 3,665.40 | 2,291.00 | 22,848.36 | 11,463.00 | 27,500.00 |
| 6235 · Repair and Maintenance | 1,404.67 | 6,250.00 | 19,340.90 | 31,250.00 | 75,000.00 |
| 6236 · Landscape Services - Wastewater | 0.00 | 0.00 | 17,375.00 | 0.00 | 0.00 |
| 6240 · Purchased Drainage | 833.11 | 833.00 | 13,223.28 | 4,169.00 | 10,000.00 |
| 6242 · Chemicals | 222.75 | 0.00 | 222.75 | 0.00 | 0.00 |
| 6252 · Utilities | 99.20 | 83.00 | 479.78 | 419.00 | 1,000.00 |
| 6271 · Tap Connection - Wastewater | 0.00 | 416.00 | 2,200.00 | 2,088.00 | 5,000.00 |
| 6276 · Maintenance & Repairs - Park | 0.00 | 3,333.00 | 33,152.86 | 16,669.00 | 40,000.00 |
| Total Sewer Expenses | 42,629.18 | 28,090.00 | 213,372.36 | 140,492.00 | 339,122.00 |
| Other Expenses | | | | | |
| 6310 · Director Fees | 0.00 | 937.00 | 9,750.00 | 4,691.00 | 11,250.00 |
| 6314 · Payroll Taxes | 0.00 | 93.00 | 745.89 | 474.00 | 1,125.00 |
| 6320 · Legal Fees | 22,892.09 | 16,666.00 | 69,549.52 | 83,338.00 | 200,000.00 |
| 6321 · Auditing Fees | 0.00 | 0.00 | 0.00 | 0.00 | 10,000.00 |
| 6322 · Engineering Fees | 3,130.00 | 6,250.00 | 28,851.25 | 31,250.00 | 75,000.00 |
| 6326 · TCEQ Assessment Fees | 0.00 | 0.00 | 4,076.88 | 0.00 | 0.00 |
| 6330 · Appraisal District Fees | 0.00 | 375.00 | 3,610.00 | 1,875.00 | 4,500.00 |
| 6333 · Bookkeeping Fees | 4,319.64 | 6,833.00 | 33,123.49 | 34,169.00 | 82,000.00 |
| 6335 · M&R - Park | 2,350.00 | 0.00 | 2,350.00 | 0.00 | 0.00 |
| 6337 · Tax Assessor/Collector | 0.00 | 66.00 | 0.00 | 338.00 | 800.00 |
| 6338 · Legal Notices/Other Publication | 0.00 | 0.00 | 0.00 | 0.00 | 1,000.00 |
| 6340 · Office Expense | 0.00 | 833.00 | 36.80 | 4,169.00 | 10,000.00 |
| 6341 · Delivery Expense | 0.00 | 41.00 | 94.15 | 213.00 | 500.00 |
| 6350 · Postage | 0.00 | 375.00 | 0.00 | 1,875.00 | 4,500.00 |
| 6353 · Insurance | 0.00 | 0.00 | 34,156.92 | 32,000.00 | 32,000.00 |
| 6354 · Travel Expense | 0.00 | 175.00 | 1,745.06 | 875.00 | 2,100.00 |
| 6356 · Registration/Membership Fees | 435.00 | 0.00 | 965.00 | 30.00 | 30.00 |
| 6359 · Other Expenses | 660.72 | 625.00 | 1,989.96 | 3,125.00 | 7,500.00 |
| 6360 · AWBD Expense | 0.00 | 58.00 | 0.00 | 294.00 | 700.00 |
| Total Other Expenses | 33,787.45 | 33,327.00 | 191,044.92 | 198,716.00 | 443,005.00 |
| Total Expense | 116,337.89 | 148,498.00 | 651,367.43 | 778,131.00 | 1,832,367.00 |
| Net Ordinary Income | 255,375.96 | 236,875.00 | 526,251.04 | 450,797.00 | 0.00 |
| Net Income | 255,375.96 | 236,875.00 | 526,251.04 | 450,797.00 | 0.00 |

River Plantation MUD STP Fund
Profit & Loss Budget Performance
February 2024

| | Feb 24 | Budget | Oct '23 - Feb 24 | YTD Budget | Annual Budget |
|--------------------------------|------------------|------------------|-------------------|-------------------|-------------------|
| Ordinary Income/Expense | | | | | |
| Income | | | | | |
| 4203 · RP MUD Revenue | 36,404.05 | 14,718.00 | 104,529.43 | 73,596.00 | 176,622.00 |
| 4204 · EPUD Revenue | 26,398.66 | 9,812.00 | 86,806.75 | 49,064.00 | 117,748.00 |
| 4205 · RP CPF Revenue | 3,970.38 | 0.00 | 28,233.81 | 0.00 | 0.00 |
| 5380 · Miscellaneous Income | 0.00 | 0.00 | 3,730.50 | 0.00 | 0.00 |
| 5391 · Interest earned | 7.47 | 4.00 | 56.90 | 22.00 | 50.00 |
| Total Income | 66,780.56 | 24,534.00 | 223,357.39 | 122,682.00 | 294,420.00 |
| Expense | | | | | |
| 6236 · Mowing - Wastewater | 0.00 | 75.00 | 0.00 | 375.00 | 900.00 |
| 6397 · Garbage Expense | 202.72 | 66.00 | 880.09 | 338.00 | 800.00 |
| 6224 · Laboratory Expense | 222.75 | 1,083.00 | 5,116.65 | 5,419.00 | 13,000.00 |
| 6226 · Permit Fees | 0.00 | 0.00 | 0.00 | 0.00 | 34,000.00 |
| 6232 · Operator Fees | 1,500.00 | 2,083.00 | 6,093.27 | 10,419.00 | 25,000.00 |
| 6235 · Repair and Maintenance | 49,265.01 | 5,833.00 | 94,157.29 | 29,169.00 | 70,000.00 |
| 6237 · Sludge Removal | 1,824.00 | 2,500.00 | 10,032.00 | 12,500.00 | 30,000.00 |
| 6242 · Chemicals | 786.34 | 583.00 | 5,281.56 | 2,919.00 | 7,000.00 |
| 6251 · Telephone | 0.00 | 60.00 | 0.00 | 300.00 | 720.00 |
| 6252 · Utilities | 4,347.15 | 3,750.00 | 21,079.21 | 18,750.00 | 45,000.00 |
| 6322 · Engineering Fees | 8,040.15 | 4,100.00 | 74,021.65 | 21,300.00 | 50,000.00 |
| 6333 · Bookkeeping Fees | 590.18 | 833.00 | 6,686.02 | 4,169.00 | 10,000.00 |
| 6353 · Insurance | 0.00 | 0.00 | 0.00 | 0.00 | 5,000.00 |
| 6359 · Other Expenses | 2.26 | 0.00 | 9.65 | 0.00 | 0.00 |
| 6395 · Security Service | 0.00 | 250.00 | 0.00 | 1,250.00 | 3,000.00 |
| Total Expense | 66,780.56 | 21,216.00 | 223,357.39 | 106,908.00 | 294,420.00 |
| Net Ordinary Income | 0.00 | 3,318.00 | 0.00 | 15,774.00 | 0.00 |
| Net Income | 0.00 | 3,318.00 | 0.00 | 15,774.00 | 0.00 |

River Plantation MUD Joint Drainage Fund
Profit & Loss Budget Performance
February 2024

| | <u>Feb 24</u> | <u>Budget</u> | <u>Oct '23 - Feb 24</u> | <u>YTD Budget</u> | <u>Annual Budget</u> |
|------------------------------------|--------------------|---------------------|-------------------------|----------------------|----------------------|
| Ordinary Income/Expense | | | | | |
| Income | | | | | |
| 4203 · RP MUD Revenue | 833.10 | 833.00 | 13,133.27 | 4,169.00 | 10,000.00 |
| 4204 · EPUD Revenue | 833.11 | 833.00 | 13,133.29 | 4,169.00 | 10,000.00 |
| 4205 · RP CPF Revenue | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 5391 · Interest Earned on Checking | 0.00 | 4.00 | 0.00 | 22.00 | 50.00 |
| Total Income | <u>1,666.21</u> | <u>1,670.00</u> | <u>26,266.56</u> | <u>8,360.00</u> | <u>20,050.00</u> |
| Expense | | | | | |
| 6235 · Repair and Maintenance | 0.00 | 301.00 | 6,500.00 | 1,509.00 | 3,616.00 |
| 6252 · Utilities | 32.82 | 29.00 | 145.31 | 147.00 | 350.00 |
| 6315 · Mowing | 0.00 | 410.00 | 0.00 | 2,130.00 | 5,000.00 |
| 6322 · Engineering Fees | 1,190.00 | 410.00 | 14,622.75 | 2,130.00 | 5,000.00 |
| 6333 · Bookkeeping Fees | 441.23 | 500.00 | 4,962.05 | 2,500.00 | 6,000.00 |
| 6359 · Other Expenses | 2.16 | 7.00 | 36.45 | 35.00 | 84.00 |
| Total Expense | <u>1,666.21</u> | <u>1,657.00</u> | <u>26,266.56</u> | <u>8,451.00</u> | <u>20,050.00</u> |
| Net Ordinary Income | <u>0.00</u> | <u>13.00</u> | <u>0.00</u> | <u>-91.00</u> | <u>0.00</u> |
| Net Income | <u><u>0.00</u></u> | <u><u>13.00</u></u> | <u><u>0.00</u></u> | <u><u>-91.00</u></u> | <u><u>0.00</u></u> |

**River Plantation MUD
Comparison of TCEQ Approved Estimates
with Actual Costs - Series 2022 Bonds
March 28, 2024**

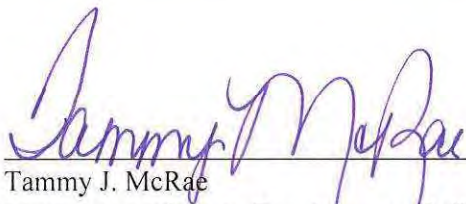
| <u>CONSTRUCTION COSTS</u> | <u>Approved Estimates</u> | <u>District Expenditure</u> | <u>Over Under</u> |
|-----------------------------------------|-------------------------------|---------------------------------|-----------------------|
| District Items | | | |
| WWTF Rehab Phase 1 | \$ 625,000 | \$ 33,748.23 | (591,251.77) |
| WWTF Electrical Upgrades | 615,000 | 24,282.71 | (590,717.29) |
| WP No. 3 Electrical Upgrades | 72,500 | 71,888.90 | (611.10) |
| WP No. 2 Recoating | 178,500 | 110,604.56 | (67,895.44) |
| Fire Hydrant & Valve Survey | 50,757 | 0.00 | (50,757.00) |
| Fire Hydrant & Valve Rehab | 152,500 | 0.00 | (152,500.00) |
| Sanitary Clean & Televis | 326,177 | 156,698.73 | (169,478.27) |
| Sanitary Sewer Rehab Phase 1 | 382,896 | 940,558.68 | 557,662.68 |
| Sanitary Sewer Rehab Phase 2 | 367,898 | 524,334.73 | 156,436.73 |
| Sanitary Sewer Rehab Phase 3 | 366,682 | 0.00 | (366,682.00) |
| Sanitary Manhole Rehab Phase 1 | 390,785 | 22,616.88 | (368,168.12) |
| Storm Sewer Clean & Televis | 28,538 | 90,686.10 | 62,148.10 |
| Channel Survey & Evaluation | 50,000 | 0.00 | (50,000.00) |
| Storm Sewer Rehab Phase 1 | 389,889 | 378,971.64 | (10,917.36) |
| Storm Sewer Rehab Phase 2 | 390,847 | 77,841.00 | (313,006.00) |
| Mosswood Ditch Rehab Phase 1 | 559,825 | 97,049.79 | (462,775.21) |
| Contingency | 954,015 | 70,945.25 | (883,069.75) |
| <u>NON-CONSTRUCTION COSTS</u> | | | |
| Legal Fees | 238,500 | 208,500.00 | (30,000.00) |
| Financial Advisory Fee | 139,000 | 139,000.00 | 0.00 |
| Capitalized Interest | 347,500 | 302,225.00 | (45,275.00) |
| Bond Discount | 208,500 | 130,578.50 | (77,921.50) |
| Bond Issuance Expense | 35,366 | 102,596.41 | 67,230.41 |
| Bond Application Report Costs | 55,000 | 55,000.00 | 0.00 |
| Attorney General | 6,950 | 6,950.00 | 0.00 |
| TCEQ Bond Issuance Fee | 17,375 | 17,375.00 | 0.00 |
| Contingency | 0 | 0.00 | 0.00 |
| TOTAL | \$ 6,950,000 | \$ 3,562,452.11 | (3,387,547.89) |
| Proceeds from Bond Sale | \$ 6,950,000.00 | | |
| Transfer to GOF, 1/25/24 | (164,489.49) | | |
| Interest income/bank service charges | 413,359.76 | | |
| Expenditures | <u>(3,562,452.11)</u> | | |
| Total funds remaining - Series 2022 | \$ 3,636,418.16 | | |

Tammy J. McRae
Montgomery County
Tax Assessor-Collector

Monthly Tax Collection Report
For the month of February 2024


River Plantation MUD

| | <u>MTD</u> | <u>YTD</u> |
|------------------------------------------------|----------------------|------------------------|
| 2023 Base Tax | \$ 110,663.02 | \$ 1,322,767.61 |
| 2023 Penalty & Interest | 1,147.90 | 1,147.90 |
| Prior Years Base Tax | 1,160.47 | 18,421.79 |
| Prior Years Penalty & Interest | 280.20 | 4,435.39 |
| Reversals (Refunds, Returned Items, Transfers) | (1,152.71) | (9,158.46) |
| Collection Fee | - | (472.00) |
| 5% Rendition Fee | - | (0.36) |
| | | |
| Total Collections | <u>\$ 112,098.88</u> | <u>\$ 1,337,141.87</u> |

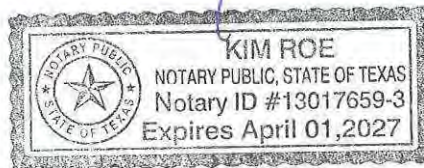


Tammy J. McRae
Montgomery County Tax Assessor-Collector

Sworn to and subscribed before me on the 4th day of March, 2024.



Notary Public in and for the State of Texas



| YEAR | FUND | TAX RATE | LEVY PAID | DISCOUNT GIVEN | PENALTY INTEREST | TIF AMOUNT | DISBURSE TOTAL | ATTORNEY | OTHER FEES | REFUND AMOUNT | PAYMENT AMOUNT |
|------|-------|----------|------------|----------------|------------------|------------|----------------|----------|------------|---------------|----------------|
| 2023 | M & O | .400000 | 67,390.84 | .00 | 706.40 | .00 | 68,097.24 | .00 | .00 | .00 | 68,097.24 |
| | I & S | .250000 | 42,119.47 | .00 | 441.50 | .00 | 42,560.97 | .00 | .00 | .00 | 42,560.97 |
| | TOTAL | .650000 | 109,510.31 | .00 | 1,147.90 | .00 | 110,658.21 | .00 | .00 | .00 | 110,658.21 |
| 2022 | M & O | .270000 | 602.56 | .00 | 145.48 | .00 | 748.04 | 288.14 | .00 | .00 | 1,036.18 |
| | I & S | .250000 | 557.91 | .00 | 134.72 | .00 | 692.63 | .00 | .00 | .00 | 692.63 |
| | TOTAL | .520000 | 1,160.47 | .00 | 280.20 | .00 | 1,440.67 | 288.14 | .00 | .00 | 1,728.81 |
| ALL | M & O | | 67,993.40 | .00 | 851.88 | .00 | 68,845.28 | 288.14 | .00 | .00 | 69,133.42 |
| ALL | I & S | | 42,677.38 | .00 | 576.22 | .00 | 43,253.60 | .00 | .00 | .00 | 43,253.60 |
| ALL | TOTAL | | 110,670.78 | .00 | 1,428.10 | .00 | 112,098.88 | 288.14 | .00 | .00 | 112,387.02 |
| DLO | M & O | | 602.56 | .00 | 145.48 | .00 | 748.04 | 288.14 | .00 | .00 | 1,036.18 |
| DLO | I & S | | 557.91 | .00 | 134.72 | .00 | 692.63 | .00 | .00 | .00 | 692.63 |
| DLO | TOTAL | | 1,160.47 | .00 | 280.20 | .00 | 1,440.67 | 288.14 | .00 | .00 | 1,728.81 |
| CURR | M & O | | 67,390.84 | .00 | 706.40 | .00 | 68,097.24 | .00 | .00 | .00 | 68,097.24 |
| CURR | I & S | | 42,119.47 | .00 | 441.50 | .00 | 42,560.97 | .00 | .00 | .00 | 42,560.97 |
| CURR | TOTAL | | 109,510.31 | .00 | 1,147.90 | .00 | 110,658.21 | .00 | .00 | .00 | 110,658.21 |

TAX COLLECTION SYSTEM
DEPOSIT DISTRIBUTION
SUMMARY OF PAYMENTS AND REVERSALS
FROM: 02/01/2024 THRU 02/29/2024
JURISDICTION: 412 RIVER PLANTATION MUD

| YEAR DEPOSIT | ACCOUNT NUMBER | EFF YR/MO | LEVY PAID | DISCOUNT GIVEN | PENALTY INTEREST | ATTORNEY CAUSE /REV | REFUND AMOUNT | PAYMENT AMOUNT |
|--------------|-----------------|--------------|--------------|-------------------|---------------------|---------------------|------------------|-------------------|
| | 2022 TOTAL | | 1,160.47 | 0.00 | 280.20 | 288.14 | 0.00 | 1,728.81 |
| | 2023 TOTAL | | 110,663.02 | 0.00 | 1,147.90 | 0.00 | 0.00 | 111,810.92 |
| | TOTAL PAYMENTS | | 111,823.49 | 0.00 | 1,428.10 | 288.14 | 0.00 | 113,539.73 |
| | 2023 TOTAL | | 1,152.71- | 0.00 | 0.00 | 0.00 | 0.00 | 1,152.71- |
| | TOTAL REVERSALS | | 1,152.71- | 0.00 | 0.00 | 0.00 | 0.00 | 1,152.71- |
| | TOTAL FOR UNIT | | 110,670.78 | 0.00 | 1,428.10 | 288.14 | 0.00 | 112,387.02 |

TAX COLLECTION SYSTEM
 TAX COLLECTOR MONTHLY REPORT
 FROM 02/01/2024 TO 02/29/2024

FISCAL START: 10/01/2023 END: 09/30/2024 JURISDICTION: 0412 RIVER PLANTATION MUD

| | CERT TAXABLE VALUE | ADJUSTMENTS | ADJ TAX VALUE | TAX RATE | TAX LEVY | PAID ACCTS |
|--------------|--------------------|-------------|---------------|-------------|--------------|------------|
| | ----- | ----- | ----- | ----- | ----- | ----- |
| CURRENT YEAR | 200,831,428 | 21,988,594 | 222,820,022 | 0 00.650000 | 1,448,345.17 | 1,137 |
| | ----- | ----- | ----- | ----- | ----- | ----- |

| YEAR | TAXES DUE | MONTH ADJ | ADJUSTMENT YTD | LEVY PAID | PAID YTD | BALANCE | COLL % | YTD UNCOLL |
|------|--------------|-----------|----------------|------------|--------------|------------|--------|------------|
| | ----- | ----- | ----- | ----- | ----- | ----- | ----- | ----- |
| 2023 | 1,305,419.11 | .00 | 142,926.06 | 109,510.31 | 1,314,840.33 | 133,504.84 | 90.78 | 0.00 |
| 2022 | 37,688.59 | .00 | 913.12- | 1,160.47 | 12,916.38 | 23,859.09 | 35.12 | 0.00 |
| 2021 | 7,260.07 | .00 | 0.00 | 0.00 | 1,885.51 | 5,374.56 | 25.97 | 0.00 |
| 2020 | 4,311.66 | .00 | 0.00 | 0.00 | 1,250.33 | 3,061.33 | 29.00 | 0.00 |
| 2019 | 2,559.29 | .00 | 0.00 | 0.00 | 509.28 | 2,050.01 | 19.90 | 0.00 |
| 2018 | 2,211.85 | .00 | 0.00 | 0.00 | 509.28 | 1,702.57 | 23.03 | 0.00 |
| 2017 | 1,556.87 | .00 | 0.00 | 0.00 | 140.97 | 1,415.90 | 9.05 | 0.00 |
| 2016 | 1,136.95 | .00 | 0.00 | 0.00 | 0.00 | 1,136.95 | | 0.00 |
| 2015 | 662.76 | .00 | 0.00 | 0.00 | 0.00 | 662.76 | | 0.00 |
| 2014 | 304.19 | .00 | 0.00 | 0.00 | 0.00 | 304.19 | | 0.00 |
| 2013 | 282.53 | 17.60- | 17.60- | 0.00 | 0.00 | 264.93 | | 0.00 |
| 2012 | 12.80 | .00 | 0.00 | 0.00 | 0.00 | 12.80 | | 0.00 |
| 2011 | 16.00 | .00 | 0.00 | 0.00 | 0.00 | 16.00 | | 0.00 |
| 2010 | 12.40 | .00 | 0.00 | 0.00 | 0.00 | 12.40 | | 0.00 |
| 2009 | 12.40 | .00 | 0.00 | 0.00 | 0.00 | 12.40 | | 0.00 |
| 2008 | 12.44 | .00 | 0.00 | 0.00 | 0.00 | 12.44 | | 0.00 |
| 2007 | 12.62 | .00 | 0.00 | 0.00 | 0.00 | 12.62 | | 0.00 |
| 2006 | 13.54 | .00 | 0.00 | 0.00 | 0.00 | 13.54 | | 0.00 |
| 2005 | 18.02 | .00 | 0.00 | 0.00 | 0.00 | 18.02 | | 0.00 |
| 2004 | 19.24 | .00 | 0.00 | 0.00 | 0.00 | 19.24 | | 0.00 |
| 2003 | 67.70 | 67.70- | 67.70- | 0.00 | 0.00 | 0.00 | | 0.00 |
| 2002 | 0.00 | .00 | 0.00 | 0.00 | 0.00 | 0.00 | | 0.00 |
| **** | 1,363,591.03 | 85.30- | 141,927.64 | 110,670.78 | 1,332,052.08 | 173,466.59 | | 0.00 |
| CURR | 1,305,419.11 | .00 | 142,926.06 | 109,510.31 | 1,314,840.33 | 133,504.84 | | 0.00 |
| DELO | 58,171.92 | 85.30- | 998.42- | 1,160.47 | 17,211.75 | 39,961.75 | | 0.00 |

RIVER PLANTATION MUNICIPAL UTILITY DISTRICT

**RESOLUTION FOR ADOPTION OF ORDER
FOR DROUGHT CONTINGENCY PLAN**

The board of directors of River Plantation Municipal Utility District (“District”) met at its regular meeting place on March 28, 2024, with a quorum of directors present, as follows:

Julie Gilmer, President
Timothy Goodman, Vice President
Betty Brown, Secretary
Karl Sakocius, Assistant Secretary
Thomas Vandever, Treasurer

and the following absent:

None

when the following business was transacted:

The order set out below was introduced for consideration of the board. It was duly moved and seconded that said order be adopted; and, after due discussion, said motion carried by the following vote:

Ayes: All directors present.

Noes: None.

The order thus adopted is as follows:

Any order and amendments thereto, heretofore adopted by the board of directors, providing for a drought contingency plan for customers within the District, is hereby revoked upon the effective date of this order.

The order hereinafter set forth shall become effective on May 1, 2024.

**ORDER ESTABLISHING DROUGHT CONTINGENCY PLAN
FOR
RIVER PLANTATION MUNICIPAL UTILITY DISTRICT**

WHEREAS, the board of directors (“Board”) of River Plantation Municipal Utility District (“District”) owns a water and sewer system designed to serve present and future inhabitants within the District and recognizes that the amount of water available to the District and its water utility customers may be limited and subject to depletion during periods of extended drought;

WHEREAS, the Board recognizes that natural limitations due to drought conditions and other acts of God occur, and the District cannot guarantee an uninterrupted water supply for all purposes;

WHEREAS, Section 11.1272 of the Texas Water Code, as amended, and applicable rules of the Texas Commission on Environmental Quality require all public water supply systems in Texas, such as the District, to prepare a drought contingency plan;

WHEREAS, the San Jacinto River Authority has required the District to adopt a drought contingency plan that meets or exceeds the minimum requirements adopted by the San Jacinto River Authority; and

WHEREAS, as authorized under law, and in the best interests of the customers of the District, the Board deems it expedient and necessary to establish certain rules and policies for the orderly and efficient management of limited water supplies during drought and other water supply emergencies; therefore,

BE IT ORDERED BY THE BOARD OF DIRECTORS OF RIVER PLANTATION MUNICIPAL UTILITY DISTRICT THAT:

Section I: Declaration of Policy, Purpose, and Intent

In order to conserve the available water supply and protect the integrity of water supply facilities, with particular regard for domestic water use, sanitation, and fire protection, and to protect and preserve public health, welfare, and safety and minimize the adverse impacts of water supply

shortage or other water supply emergency conditions, the District hereby adopts the following regulations and restrictions on the delivery and consumption of water.

Water uses regulated or prohibited under this Drought Contingency Plan (“Plan”) are considered to be non-essential water use and continuation of such uses during times of water shortage or other emergency water supply condition are deemed to constitute a waste of water which subjects the offender(s) to penalties as defined in Section XI of this Plan.

Section II: Public Involvement

Opportunity for the public to provide input into the preparation of the Plan was provided by the District by means of scheduling and providing public notice of a public meeting to accept input on the Plan.

Section III: Public Education

The District will periodically provide the public with information about the Plan, including information about the conditions under which each stage of the Plan is to be initiated or terminated and the Drought Response Measures to be implemented in each stage. This information will be provided by means of utility bill inserts, signs posted in the subdivision, or other method reasonably calculated to provide notice to District customers.

Section IV: Coordination with Regional Water Planning Groups

The service area of the District is located within the Texas Water Development Board Region H Regional Water Planning Group and the District has provided a copy of this Plan to the Region H Regional Water Planning Group. The District has a Groundwater Reduction Planning, Alternative Water Supply, and Related Goods and Services contract with San Jacinto River Authority (“SJRA”) and has provided a copy of this Plan to them.

Section V: Authorization

The Board of Directors of the District or its designee is hereby authorized and directed to implement the applicable provisions of this Plan upon determination that such implementation is necessary to protect public health, safety, and welfare. The Board of Directors of the District or its designee shall have the authority to initiate or terminate drought or other water supply emergency response measures as described in this Plan.

Section VI: Application

The provisions of this Plan shall apply to all persons, customers, and property utilizing water provided by the District. The terms “person” and “customer” as used in the Plan include individuals, corporations, partnerships, associations, and all other legal entities.

Section VII: Definitions

For the purposes of this Plan, the following definitions shall apply:

Aesthetic water use: water use for ornamental, scenic or decorative purposes such as fountains, reflecting pools, and water gardens.

Commercial and institutional water use: water use which is integral to the operations of commercial and non-profit establishments and governmental entities such as retail establishments, hotels and motels, restaurants, and office buildings.

Conservation: those practices, techniques, and technologies that reduce the consumption of water, reduce the loss or waste of water, improve the efficiency in the use of water or increase the recycling and reuse of water so that a supply is conserved and made available for future or alternative uses.

Customer: any person, company, or organization using water supplied by the District.

Domestic water use: water use for personal needs or for household or sanitary purposes such as drinking, bathing, heating, cooking, sanitation, or for cleaning a residence, business, industry, or institution.

Even numbered address: street addresses, box numbers, or rural postal route numbers ending in 0, 2, 4, 6, or 8 and locations without addresses.

Industrial water use: the use of water in processes designed to convert materials of lower value into forms having greater usability and value.

Landscape irrigation use: water used for the irrigation and maintenance of landscaped areas, whether publicly or privately owned, including residential and commercial lawns, gardens, golf courses, parks, athletic fields, and rights-of-way and medians.

Non-essential water use: water uses that are not essential nor required for the protection of public, health, safety, and welfare, including:

- (a) landscape irrigation use, except otherwise provided under this Plan;
- (b) use of water to wash any motor vehicle, motorbike, boat, trailer, airplane or other vehicle;
- (c) use of water to wash down any sidewalks, walkways, driveways, parking lots, tennis courts, or other hard-surfaced areas;
- (d) use of water to wash down buildings or structures for purposes other than immediate fire protection;
- (e) flushing gutters or permitting water to run or accumulate in any gutter or street;
- (f) use of water to fill, refill, or add to any indoor or outdoor swimming pools or jacuzzi-type pools;
- (g) use of water in a fountain or pond for aesthetic water use except where necessary to support aquatic life;
- (h) failure to repair a controllable leak(s) within a reasonable period after having been given notice directing the repair of such leak(s); and
- (i) use of water from hydrants for construction purposes or any other purposes other than firefighting.

Odd numbered address: street addresses, box numbers, or rural postal route numbers ending in 1, 3, 5, 7, or 9.

Section VIII: Trigger Conditions for Initiation and Termination of Drought Response Stages

The Board or its designee, shall monitor water supply and/or demand conditions on a regular basis and shall determine when conditions warrant initiation or termination of each stage of the Plan. Notwithstanding any of the Trigger Conditions described herein, upon receipt of a notice of a declaration of a state of disaster due to drought conditions pursuant to Sections 418.014 or 418.108 of the Texas Gov't Code, the District shall implement the appropriate stage of this Plan. Public notification of the initiation or termination of drought response stages shall be in accordance with Subsection (f).

The triggering conditions (“Trigger Conditions”) described below are based on the District’s anticipated ability to provide water to its customers based the District’s historical experience of operations in drought conditions.

A. Stage 1 - Mild Drought Conditions

This condition (herein “Mild Drought Condition”) exists when any of the following conditions exist: (1) demand on the District’s water supply reaches or exceeds 70% of the production capacity of such facilities for five (5) consecutive days, as determined by the District’s operator; (2) the SJRA Lake Conroe Division initiates Stage 1 of its Drought Contingency Plan; or (3) the General Manager or designated representative of SJRA designates Stage 1 of the GRP Division’s Drought Contingency Plan due to water demands/weather forecasts or equipment, pipeline or sample failure.

B. Stage 2 - Moderate Drought Conditions

This condition (herein “Moderate Drought Condition”) exists when any of the following conditions exist: (1) demand on the District’s water supply reaches or exceeds 80% of the production capacity of such facilities for three (3) consecutive days, as determined by the District’s operator; (2) the SJRA Lake Conroe Division initiates Stage 2 of its Drought Contingency Plan; or (3) the General Manager or designated representative of the SJRA designates Stage 2 of the GRP Division’s Drought Contingency Plan due to water demands/weather forecasts or equipment, pipeline or sample failure.

C. Stage 3 - Advanced Drought Conditions

This condition (herein “Advanced Drought Condition”) exists when any of the following conditions exist: (1) demand on the District’s water supply reaches or exceeds 90% of the production capacity of such facilities for five (5) consecutive days, as determined by the District’s operator; (2) the SJRA Lake Conroe Division initiates Stage 3 of its Drought Contingency Plan; or (3) the General Manager or designated representative of the SJRA designates Stage 3 of the GRP Division’s Drought Contingency Plan due to water demands/weather forecasts or equipment, pipeline or sample failure.

D. Stage 4 – Severe Drought Conditions

This condition (herein “Severe Drought Condition”) exists when any of the following conditions exist: (1) demand on the District’s water supply reaches 100% of the production capacity of such facilities for five (5) consecutive days, as determined by the District’s operator ; (2) the SJRA Lake Conroe Division initiates Stage 4 of its Drought Contingency Plan; or (3) the General Manager or designated representative of the SJRA designates Stage 4 of the GRP Division’s Drought Contingency Plan due to water demands/weather forecasts or equipment, pipeline or sample failure.

E. Stage 5 – Emergency Water Shortage Conditions

This condition (herein “Emergency Water Shortage Condition”) exists when any of the following exist:

1. The SJRA Lake Conroe initiates an Emergency Water Supply Condition under its Drought Contingency Plan;
2. The General Manager or designated representative of the SJRA designates an Emergency Water Supply Condition pursuant to the GRP Division’s Drought Contingency Plan due to anticipation of a drought condition beyond historical level of severity, system failure in the GRP Division system, contamination, equipment, pipeline or sample failure, or other factors at the General Manager’s discretion.
3. Major water line breaks or pump or system failures of the District or the SJRA GRP Division occur, which cause unprecedented loss of capability to provide water service;
4. Natural or man-made contamination of the water supply source(s) occurs; or
5. An emergency water supply condition has been enacted by another governmental official or agency with jurisdiction.

E. Notice

Once one of the Trigger Conditions has occurred, Customers will be notified that such Trigger Condition has occurred and of the Drought Response Measures (as defined below) to be taken. The process for notifying Customers may include any of the following:

1. Mailing, prior to the commencement of the required Drought Response Measures, a written notice to each Customer;
2. Posting of signs at the entrances to the District;
3. Posting of notices at public places in the District;
4. Placing door-hangers at all residences and places of commercial water use;
5. Dissemination of press releases to the local news media and/or
6. Other means as may be appropriate.

The Board of Directors or its designee shall notify directly the following individuals and entities:

Texas Water Development Board Region H Regional Water Planning Group;
Texas Commission on Environmental Quality (Stages 2 – 5 only);
Fire chief(s);

Homeowners or property owners association(s);
County Emergency Management Coordinator; and
Critical water users (hospitals, schools, etc.).

Any notice issued shall contain (i) the date the Drought Response Measures will begin, (ii) the date the Drought Response Measures will terminate, if known, (iii) a list or summary of Drought Response Measures to be implemented, and (iv) an explanation of penalties for violations of such Drought Response Measures.

Section IX: Drought Response Stages and Drought Response Measures

The Board of Directors of the District or its designee, shall monitor water supply and/or demand conditions on a regular basis and, in accordance with the Trigger Conditions set forth in Section VIII of the Plan, shall determine that a mild, moderate, advanced, severe, or emergency condition exists and shall implement the following actions upon prior notification to District customers:

A. Stage 1 - Mild Drought Condition Measures

Target: Achieve a voluntary 5% reduction in daily water demand.

1. Water Customers will be asked to voluntarily reduce water use and will be informed of specific steps that can be taken to reduce water use.
2. All non-essential water use shall be limited to even-numbered days for Customers with even-numbered addresses, and odd-numbered days for water Customers with odd-numbered addresses, and outdoor water use shall be prohibited between the hours of 10:00 a.m. and 9:00 p.m. In the event no street address exists, only Customers living on the north and west side of a street may use water outdoors on even-numbered days and only Customers on the south and east side of a street may use water outdoors on odd-numbered days.

B. Stage 2 - Moderate Drought Condition Measures

Target: Achieve a 5% reduction in daily water demand (October through March).
Achieve a 10% reduction in daily water demand (April through September).

1. The Drought Response Measures established for Mild Drought Conditions shall continue to be implemented on a mandatory basis.

C. Stage 3 - Advanced Drought Condition Measures

Target: Achieve a 10% reduction in daily water demand (October through March).
Achieve a 20% reduction in daily water demand (April through September).

1. All non-essential water use must be conducted with a hand-held hose with a manual on-off nozzle.
2. The District shall recommend that the following public waer uses not essential for public health and safety be curtailed:

- (a) Street washing;
- (b) Fire hydrant flushing; and
- (c) Filling of swimming pools.

D. Stage 4 - Severe Drought Condition Measures

Target: Achieve a 15% reduction in daily water demand (October through March).
Achieve a 30% reduction in daily water demand (April through September).

1. All non-essential water use shall be prohibited.
2. A surcharge equal to 200% of the applicable rate for all water used in excess of 10,000 gallons/month shall be imposed on all Customers.
3. The Board of Directors may prohibit water use by certain industrial or commercial Customers which water uses are not essential to the health and safety of the community so that remaining water is available for essential health and safety related uses.

E. Stage 5 – Emergency Water Shortage Conditions

See Section X of this Plan

F. Termination of Trigger Conditions Notification.

When a Trigger Condition based upon demand on the District’s water supply occurs the District shall enforce the Drought Response Measures applicable to such Trigger Condition for a minimum of five (5) days after the last day the demand on the District’s water supply facilities reaches or exceeds the limits of such Trigger Condition. After such five (5) day period, the Drought Response Measures prescribed may, in the discretion of the Board or its designee, be continued for an additional five (5) day period. After the expiration of ten (10) days, and assuming no other Trigger Conditions have occurred, the Drought Response Measures prescribed shall terminate and the District shall cease implementation and enforcement of such measures.

When a Trigger Condition occurs due to an Emergency Water Shortage Condition or due to receipt of notification by a third party, such as the SJRA Lake Conroe Division, the SJRA GRP Division, or other governmental entity with jurisdiction, the District shall enforce the Drought Response Measure applicable to the Trigger Condition until the emergency is over or until receipt of notification from the third party that restrictions have been lifted.

The District will notify Customers of the termination of the particular Drought Response Measures and may utilize the same manner of notification used to inform Customers of the occurrence of the Trigger Condition and implementation of the Drought Response Measures.

Section X: Emergency Contingency Plan

In the event of Stage 5 Water Shortage Conditions or a fire, flood, hurricane, lightning strike, tornado, windstorm, or any other act of God, riot, terrorist act, or any other act of civil disobedience, or any other similar occurrence which results in the inability of the District to provide potable water to Customers (or the likelihood thereof), the Board, in its discretion, may,

without prior notice, invoke all of any of the Drought Response Measures set forth in this Plan as “Emergency Response Measures.” The Board may establish any of the penalties set forth in Section XI for violations of the Emergency Response Measures.

Section XI: Enforcement

The following penalties shall apply to any person, entity or customer violating the terms of this Plan or the Drought Response Measures or Emergency Response Measures adopted pursuant hereto:

- A. **First Violation.** Any person, entity or customer who violates this Plan shall receive written notification of such violation, which notice shall set forth (i) the date of the violation, (ii) the nature of the violation, (iii) the Drought Response Measures then in effect, and (iv) the penalties applicable for any further violations of this Plan; provided, however, that if such person, entity or customer has ever previously violated this Plan, the penalties set forth in Section B below, may, in the discretion of the Board, be imposed.

- B. **Subsequent Violations.**
 - 1. **Disconnection for Noncompliance.** If any person, entity or customer violates any provision of this Plan more than one time (which violation shall constitute an unauthorized use of District services and/or facilities), then in addition to any other remedies, penalties, sanctions and enforcement procedures provided for herein, the District shall have the right to terminate water service to such person, entity or customer after notice and any other procedural requirements in the District’s rate order are satisfied.

 - 2. **Monetary Penalties for Noncompliance.** If any person, entity or customer violates any provision of this Plan more than one time (which violation shall constitute an unauthorized use of District services and/or facilities), then, in addition to disconnection as provided in Subsection B1 of this Section, the Board of the District, after providing any legally required notice, may impose a penalty of up to the maximum amount permitted under Texas Water Code Ch. 49.004 for each violation of this Plan. Each day that a breach of any provision of this Plan continues shall be considered a separate violation. This penalty shall be in addition to any other legal rights and remedies of the District as may be allowed by law.

Section XII: Variances

The Board of Directors or its designee may, in writing, grant temporary variance for existing water uses otherwise prohibited under this Plan if it is determined that failure to grant such variance would cause an emergency condition adversely affecting the health, sanitation, or fire protection for the public or the person requesting such variance and if one or more of the following conditions are met:

- (a) Compliance with this Plan cannot be technically accomplished during the duration of the water supply shortage or other condition for which the Plan is in effect.

- (b) Alternative methods can be implemented which will achieve the same level of reduction in water use.

Persons requesting an exemption from the provisions of this Plan shall file a petition for variance with the District. All petitions for variances shall be reviewed by the Board of Directors or its designee and shall include the following:

- (a) Name and address of the petitioner(s).
- (b) Purpose of water use.
- (c) Specific provision(s) of the Plan from which the petitioner is requesting relief.
- (d) Detailed statement as to how the specific provision of the Plan adversely affects the petitioner or what damage or harm will occur to the petitioner or others if petitioner complies with this Plan.
- (e) Description of the relief requested.
- (f) Period of time for which the variance is sought.
- (g) Alternative water use restrictions or other measures the petitioner is taking or proposes to take to meet the intent of this Plan and the compliance date.
- (h) Other pertinent information.

Variances granted by the Board of Directors shall be subject to the following conditions, unless waived or modified by the Board of Directors or its designee:

- (a) Variances granted shall include a timetable for compliance.
- (b) Variances granted shall expire when the Plan is no longer in effect unless the petitioner has failed to meet specified requirements.

No variance shall justify any violation of this Plan occurring prior to the issuance of the variance.

Section XIII: Severability

It is hereby declared to be the intention of the Board of Directors that the sections, paragraphs, sentences, clauses, and phrases of this Plan are severable and, if any phrase, clause, sentence, paragraph, or section of this Plan shall be declared unconstitutional by the valid judgment or decree of any court of competent jurisdiction, such unconstitutionality shall not affect any of the remaining phrases, clauses, sentences, paragraphs, and sections of this Plan, since the same would not have been enacted by the Board of Directors without the incorporation into this Plan of any such unconstitutional phrase, clause, sentence, paragraph, or section.

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The President or Vice President is authorized to execute, and the Secretary or Assistant Secretary is authorized to attest this Order on behalf of the Board of Directors of the District.

JULIE GILMER

President

ATTEST:

BETTY BROWN

Secretary

I, the undersigned secretary of the board of directors of River Plantation Municipal Utility District, hereby certify that the foregoing is a true and correct copy of the order amending a drought contingency plan, adopted by said board at its regular meeting of March 28, 2024, together with excerpts from the minutes of said board's meeting on that date showing the adoption of said order, as same appear of record in the official minutes of the board, on file in the District's office.

I further certify that said meeting was open to the public, and that notice thereof was posted in compliance with the provisions of Tex. Gov't. Code Ann. § 551.001 et seq.

Witness my hand and the official seal of said District this March 28, 2024.

Secretary



RIVER PLANTATION MUNICIPAL UTILITY DISTRICT

ORDER ADOPTING WATER CONSERVATION PLAN; PROVIDING FOR IMPLEMENTATION AND ENFORCEMENT THEREOF; AND CONTAINING OTHER PROVISIONS RELATED TO THE SUBJECT

The Board of Directors (“Board”) of River Plantation Municipal Utility District (“District”) met at the Board’s regular meeting place on March 28, 2024, with a quorum of Directors present, as follows:

Julie Gilmer, President
Timothy Goodman, Vice President
Betty Brown, Secretary
Karl Sakocius, Assistant Secretary
Thomas Vandever, Treasurer

and the following absent:

None

when the following business was transacted:

The order set out below was introduced and considered by the Board. It was then moved, seconded and unanimously carried that the following order be adopted:

WHEREAS, water conservation includes those practices, techniques and technologies that reduce the consumption of water, reduce the loss or waste of water, improve efficiency in the use of water, or increase recycling and reuse of water so that a water supply is made available for future or alternative uses;

WHEREAS, the District has previously adopted a Water Conservation Plan which is required to be reviewed and updated at regular intervals;

WHEREAS, the District desires to comply with the Texas Water Code and applicable rules of the Texas Commission on Environmental Quality;

WHEREAS, as authorized under law, and in the best interests of the customers of the District, the Board deems it expedient and necessary to establish certain rules and policies for the conservation of water;

WHEREAS, the Board of Directors of River Plantation Municipal Utility District has carefully considered the current water conditions in the District and area-wide and has determined that the adoption of this Water Conservation Plan (the “Plan”) by the District is necessary to ensure that an adequate supply of water is maintained; and

WHEREAS, the Board of Directors of the District desires to evidence its approval of this Plan and to adopt such Plan as the official policy of the District;

NOW, THEREFORE, BE IT ORDERED BY THE BOARD OF DIRECTORS OF RIVER PLANTATION MUNICIPAL UTILITY DISTRICT THAT:

Section 1. Approval of the Plan. The Board of Directors of the District hereby approves and adopts this Plan as set forth in this Order, and the provisions of such Plan shall be implemented immediately and enforced as rules of the District.

Section 2. Declaration of Policy, Purpose and Intent. The purpose of the Plan is to promote the efficient and responsible use of water by (1) implementing structural programs that result in quantifiable water conservation results, (2) developing, maintaining and enforcing water conservation policies, (3) adhering to all applicable rules of the Texas Commission on Environmental Quality and/or the Texas Water Development Board and (4) supporting public education programs that educate customers about water and wastewater facilities operations, water quantity and quality, water conservation and non-point source protection.

Section 3. Service Area. The District’s Utility Profile includes data on the District’s service area, including population and customer data, water use data, water supply system data and

wastewater data. The District's operator will make any necessary updates to the District's Utility Profile and will submit the updated Utility Profile to the Texas Water Development Board's online portal by May 1, 2024. The District will instruct the District's operator to make any necessary updates to the District's Utility Profile at least once every five years.

Section 4. Five-year and Ten-year Targets. The District shall use reasonable efforts to reduce water loss and municipal use of water. In doing so, the District has identified the following goals for water savings:

A. Five-year Target: Within five (5) years of the date hereof, the District shall attempt to reduce the average daily municipal use of water in the District's service area by 10 gallons per day ("gpd") per connection and to keep the unaccounted water in the system below 10% annually.

B. Ten-year Target: Within ten (10) years of the date hereof, the District shall attempt to reduce the average municipal use of water in the District's service area by 40 gpd per connection and to keep the unaccounted water in the system below 10% annually.

C. Require customers to limit landscape irrigation during summer months (May through September) to early mornings or late evenings to reduce evaporation from sprinkler heads that causes water waste.

Notwithstanding the targets identified above, the District shall not be obligated to achieve any water savings in its service area, and the District's failure to do so shall not subject the District to any liability whatsoever.

Section 5. Metering Devices. The District will implement a plan of universal metering of all water delivered by the District, and all such metering devices will be calibrated regularly to ensure reasonable accuracy and replaced as needed.

Section 6. Unaccounted Water Usage. The District authorizes the District's operator to implement any reasonable program to determine unaccounted uses of water and to make recommendations to the District regarding measures to control such unaccounted uses of water. Such measures may include periodic visual inspections along distribution lines, annual or monthly audits of the water system to determine illegal connections, and investigation of abandoned service connections. The District's operator shall also establish a program of leak detection, repair, and water loss accounting for the water storage, delivery and distribution system in order to control unaccounted uses of water.

Section 7. Continuing Public Education and Information. The District hereby institutes an educational program, to be implemented immediately, to promote the Plan by the general public which may include any of the following:

- A. Publications of articles in a newspaper or newsletter of general circulation in the District's service area, providing information regarding water conservation;
- B. Direct distributions to all customers of the District of educational and informational material regarding water conservation; and
- C. Additional educational activities consisting of: (i) conducting an informational school program in a school attended by students within the District's service area, or (ii) conducting an educational program for Users at a public place within or accessible to residents within the service area of the District, or (iii) conducting or engaging in such other informational or educational activity designed to further water conservation measures as, in the discretion of the Board of Directors, may be consistent with the purposes and policies of this Plan, or (iv) any combination of the foregoing.

Section 8. Cost-based Rate Structure. The District hereby acknowledges that it has

adopted an increasing block water rate structure, as reflected in its Order for Adoption of Schedule of Water and Sewer Fees and Rates adopted September 7, 2023, 2024 (attached hereto as Appendix “A”), that is intended to encourage water conservation and discourage excessive use and waste of water.

Section 9. Reservoir Systems Operations Plan. The District does not own any reservoirs within a common watershed or river basin and is not required to establish a reservoir systems operation plan.

Section 10. Implementation and Enforcement. Without limitation to specific actions stated in this Plan to be taken by the District’s operator, the District’s operator will administer and enforce this Plan, and will oversee and be responsible for the execution and implementation of all elements of this Plan. The operator shall report to the Board of the District, at meetings of the Board, regarding actions taken and actions that need to be taken under this Plan.

Section 11. Record Management. The District authorizes the District’s operator and/or general manager to establish a record management system to record water pumped, water delivery, water sales, and water losses, and which allows for the segregation of water sales and uses into residential, commercial, public and institutional, industrial, agricultural, and wholesale user classes.

Section 12. Wholesale Water Customers. The District shall require that each successive wholesale customer develop and implement a water conservation plan or water conservation measures in compliance with all applicable rules of the Texas Commission on Environmental Quality. This requirement will also extend to each successive wholesale customer in the resale of water.

Section 13. Five-year Review. The District shall review and update the Plan every five

years, or more frequently, as appropriate, based on an assessment of previous five-year and ten-year targets and any other new or updated information.

Section 14. Coordination with Regional Water Planning Group. The service area of the District is located within the Region H Regional Water Planning Group of the Texas Water Development Board, and the District has provided or will provide a copy of this water conservation plan to the San Jacinto River Authority.

Section 15. Effective Date. This Order shall become effective on May 1, 2024 and as further provided herein.

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Passed, ordered and approved, this March 28, 2024.

President

ATTEST:

Secretary

Appendix "A"
 [Excerpt of the District's Order for Adoption of Schedule of
 Water and Sewer Fees and Rates Adopted September 7, 2023]

| | | |
|------------------------------------------------------------------|---------------------------------------------------------------------------|---------------------------------------------------------------------------------------------------------------|
| Section 4.1 <u>Monthly rates for water service</u> | <u>Residential Consumers</u> First 3,000 gallons of water used | Minimum \$15.00 for 3/4" meter \$19.50 for 1" meter \$25.35 for 1 1/2" meter \$30.85 for 2" meter |
| | 3,001 to 10,000 gallons | \$3.35/1,000 gallons |
| | 10,001 to 20,000 gallons | \$3.70/1,000 gallons |
| | 20,001 to 30,000 gallons | \$4.18/1,000 gallons |
| | 30,001 to 40,000 gallons | \$4.70/1,000 gallons |
| | 40,001 to 50,000 gallons | \$5.59/1,000 gallons |
| | over 50,001 gallons | \$7.06/1,000 gallons |
| | Monthly Fee for additional tap (e.g. sprinklers, swimming pools, etc.) | \$9.80 |
| | Monthly fee for swimming pool backwash or overflow line | \$21.00 |
| | <u>Apartments</u> | Same rates as Residential Consumers |
| <u>Commercial Consumers and Nontaxable Entities</u> | Same rates as Residential Consumers | |

I, the undersigned Secretary of the board of directors of River Plantation Municipal Utility District, hereby certify that the foregoing is a true and correct copy of the order adopting water conservation plan and minute entry showing its adoption at the Board's regular meeting held on March 28, 2024, the originals of which order and minute entry are on file in the minute book of the Board in the District's office.

I further certify that said meeting was open to the public and that notice thereof was posted in compliance with the provisions of Tex. Gov't. Code Ann. § 551.001 et seq.

Witness my hand and the seal of said District, this March 28, 2024.

Secretary



RIVER PLANTATION MUNICIPAL UTILITY DISTRICT

Resolution to Adopt the Verity Voting 2.5 System

At a meeting of the board of directors (the “Board”) of River Plantation Municipal Utility District (the “District”) held on March 28, 2024, at which a quorum of said Board was present, as follows:

Julie Gilmer, President
Timothy Goodman, Vice President
Betty Brown, Secretary
Karl Sakocius, Assistant Secretary
Thomas Vandever, Treasurer

and the following absent:

None

the following business was transacted:

It was duly moved, seconded and unanimously carried that the resolution set out below be passed and adopted, all directors present voting “aye” and no one voting “no.” The resolution thus adopted is as follows:

WHEREAS, the Verity Voting 2.5 system by Hart InterCivic Inc. is an updated version of the Verity Voting 2.4 system, which the Office of the Texas Secretary of State certified in June 2020 for use in Texas elections. The updated version includes enhancements to the existing hardware and software components of the Verity voting system; and

WHEREAS, Section 123.035 of the Texas Election Code requires that use of new voting equipment must be approved by the Elections Division of the office of the Texas Secretary of State; and

WHEREAS, the Texas Secretary of State certified the Verity Voting 2.5 system for use in Texas elections as described in correspondence dated October 28, 2021; and

WHEREAS, the Montgomery County Office of Elections Administration has purchased the new ADA-compliant Verity Voting 2.5 system to be used for early and regular election day voting by Montgomery County for the May 4, 2024 election and all subsequent elections; and

WHEREAS, River Plantation Municipal Utility District will use Montgomery County's Verity Voting 2.5 system and pursuant to Section 123.001 (b) of the Texas Election Code must formally adopt said voting system.

NOW, THEREFORE, be it resolved by the Board of Directors of River Plantation Municipal Utility District that:

River Plantation Municipal Utility District does hereby adopt the Verity Voting 2.5 system, as certified by the State of Texas, to be used for early and regular election day voting by Montgomery County for the May 4, 2024 election and all subsequent elections.

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Passed, approved and adopted by the Board of Directors of River Plantation Municipal Utility District on this March 28, 2024.

JULIE GILMER

President

ATTEST:

BETTY BROWN

Secretary

I, the undersigned secretary of the board of directors of River Plantation Municipal Utility District, hereby certify that the foregoing is a true and correct copy of the Resolution to Adopt the Verity Voting 2.5 system adopted by said Board at its regular meeting on March 28, 2024, and a minute entry of that date showing the adoption thereof, the original of which resolution appears in the minute book of said Board, on file in an office and meeting place of the District.

I further certify that said meeting was open to the public, and that notice was given in compliance with the provisions of Tex. Gov't. Code Ann. § 551.001 et seq. as adopted.

Witness my hand and the official seal of said District, on this March 28, 2024.

Secretary



RIVER PLANTATION MUNICIPAL UTILITY DISTRICT

Order Adopting Rules and Regulations for District Parks, Recreational Areas
and District Property, Facilities, Easements and Rights-of-Way

On March 28, 2024, the Board of Directors (“Board”) of River Plantation Municipal Utility District (“District”) met at its regular meeting place, with a quorum of directors present, as follows:

Julie Gilmer, President
Timothy Goodman, Vice President
Betty Brown, Secretary
Karl Sakocius, Assistant Secretary
Thomas Vandever, Treasurer

and the following were absent:

None

when the following business was transacted:

The order set out below was introduced for the Board’s consideration. It was duly moved and seconded that said order be adopted, and after due discussion, said motion carried by the following vote:

Ayes: All directors present

Noes: None

The order thus adopted is as follows:

The order hereinafter set forth shall become effective on March 28, 2024.

RIVER PLANTATION MUNICIPAL UTILITY DISTRICT
RULES AND REGULATIONS FOR
DISTRICT PARKS, LAKES, RECREATIONAL AREAS AND
DISTRICT PROPERTY, FACILITIES, EASEMENTS AND RIGHTS-OF-WAY

MISSION STATEMENT

In pursuit of an enhanced quality of life through a greater opportunity for recreational activity, River Plantation Municipal Utility District seeks to develop and maintain versatile parks and recreational facilities for its residents and further seeks to preserve the health and well-being of its residents.

RULES

Section 1: **AUTHORITY.** These rules and regulations (“Rules”) have been adopted under the authority of Section 54.205 of the Texas Water Code and previous orders of the Board of Directors of River Plantation Municipal Utility District.

Section 2: **ADMINISTRATION.** The Board of Directors of River Plantation Municipal Utility District, along with the Montgomery County Sheriff, the Montgomery County Precinct 2 Constable and their respective deputies, shall enforce these Rules.

Section 3: **AREA COVERED.** These Rules apply to all existing and future parks and recreational facilities of the District, including the property comprising the former Charleston course, and related areas developed and maintained pursuant to the Texas Water Code, together with such additional land as may be designated as parks and recreational facilities by the District, and to all District property, facilities, easements and rights-of-way.

Section 4: **DEFINITIONS.** As used in these Rules:

- a. “Alcoholic Beverage” means any beverage containing more than one-half of one percent (.5%) of alcohol by volume, which is suitable for use as a beverage, either alone or diluted;
- b. “Board” means the Board of Directors of River Plantation Municipal Utility District;
- c. “Cart Paths” means the asphalt or concrete paths approximately five feet in width within the Recreational Facilities and constructed for the purpose of the operation of a Golf Cart.
- d. “County” means Montgomery County, Texas;
- e. “District” means River Plantation Municipal Utility District;
- f. “District Property” means any water plant site, wastewater treatment plant site, lift station site, detention pond, drainage facility, easement or right-of-way owned or used by the District in performing its responsibilities as a Texas municipal utility district, including facilities and improvements located thereon;

g. “Explosives” means any chemical compound or mixture that is commonly used or intended for the purpose of producing an explosion;

h. “Golf Cart” means a small motorized vehicle designed for the purpose of transporting golfers and their golf equipment with a dry weight of less than 1,000 pounds.

i. “Parks” means all existing and future park and recreational facilities of the District, including the property comprising the former Charleston course, and related areas and developed and maintained pursuant to the Texas Water Code, together with such additional land as may be designated as parks and recreational facilities by the District;

j. “Peace Officers” means sheriffs and their deputies, constables and deputy constables, and all other peace officers as defined in Article 2.12 of the Texas Code of Criminal Procedure, as amended;

k. “Pet” means a domesticated animal kept for pleasure rather than utility;

l. “Recreational Areas” means any Parks or other areas, whether within or outside the District’s boundaries, that have been designated by the District for recreational use by residents of the District and the public;

m. “Road” means any road maintained or controlled by the County or other entity for the public passage of vehicles;

n. “Special Event” means an organized activity intended for more than twenty five (25) persons to share a common purpose as a group;

o. “Vehicle” means every motor-driven device in, upon, or by which any person or property is or may transported or drawn upon a road except devices moved by human power;

p. “Weapon” means a rifle, handgun, pistol, bow and arrow, shotgun, gas gun or gas pistol, BB gun or BB pistol, pellet gun or pellet pistol, sling or sling shot; and

q. “Wildlife” means living things that are neither human nor domesticated.

Section 5: HOURS OPEN. Unless otherwise posted, the Recreational Areas shall be open from sunrise to sundown. No person shall enter into or remain within the Recreational Areas at any other time without prior written approval of the Board.

Section 6: MOTORIZED VEHICLES AND GOLF CARTS.

a. No person shall operate a Vehicle, other than a Golf Cart in the manner permitted herein, within the Recreational Areas or District Property except on any Road or associated parking lots. Operation of a Vehicle on the shoulder of a Road will be limited to driving thereon for the purpose of parking on the shoulder of the Road or driving a parked Vehicle from the shoulder of the Road to the paved portion of the Road. This provision does not apply to any Vehicle making deliveries of material, supplies and equipment purchased or rented by the District;

b. No person shall operate or cause or participate in the operation of a Vehicle other than a Golf Cart on a Cart Path within the Recreational Facilities other than on a designated Road or within designated Parking Areas.

c. No person shall operate or cause or participate in the operation of a Vehicle including a Golf Cart at a speed in excess of ten (10) miles per hour.

d. No person shall operate or cause or participate in the operation of a Vehicle including a Golf Cart in a manner which causes damage to District facilities or improvements.

e. No person shall operate or cause or participate in the operation of a Vehicle including a Golf Cart in a manner which is unsafe, reckless, or may cause harm to themselves or to others who are present on District property.

f. No person shall cause a Vehicle to be parked within the Recreational Areas except in a designated parking area. Vehicles parked on the shoulder of a Road in designated areas must be parked parallel to the Road. This provision does not apply to any Vehicle making deliveries of materials, supplies and equipment purchased or rented by the District; and

g. No person shall cause a Vehicle to remain within the Recreational Areas after hours unless one of the officers named in Section 2 above is notified; provided, however, that in no event shall any person cause a Vehicle to remain within the Recreational Areas in excess of twenty-four (24) hours at any given time. Vehicles remaining within the Recreational Areas for which notification has not been received will be towed and placed in storage by Peace Officers at the owner's expense.

h. No person shall operate a Vehicle including a Golf Cart within the Recreational Facilities who does not hold a valid driver's license, or learner's permit if accompanied by a licensed driver at least twenty-one (21) years of age.

i. The operation of a Golf Cart is permitted within the Recreational Facilities on Cart Paths only. Operation of a Golf Cart outside of the Cart Paths is prohibited. The operation of a Golf Cart within the Recreational Facilities is subject to all rules and regulations herein, including but not limited to Section 6 (a)-(h).

Section 7: GOLFING. No person shall play golf or otherwise strike a golf ball with a golf club within the Recreational Areas.

Section 8: WILDLIFE. No person shall willfully feed, harm, harass, trap, confine, catch, or possess any Wildlife within the Recreational Areas.

Section 9: PLANT LIFE. No person shall willfully destroy or remove any tree, shrub, vine, wildflower, grass, fern, moss, leaves, cones, or dead or downed wood within the Recreational Areas except with prior written approval of the Board.

Section 10: FIRES. No person may light, build or maintain a fire within the Recreational Areas other than within a camp stove and/or barbecue pit. If a burn ban has been enacted by the District, fire is prohibited in all areas.

Section 11: **SMOKING.** No person shall light, burn or smoke any cigar, pipe, cigarette, electronic cigarette (e-cigarette) or other device used for smoking or delivering tobacco or nicotine or any other legal substance within the Recreational Areas.

Section 12: **WEAPONS.** No person other than a Peace Officer or a person duly licensed by the State of Texas may carry or possess a weapon within the Recreational Areas. The unlawful possession or discharge of weapons within the Recreational Areas is prohibited.

Section 13: **EXPLOSIVES.** No person may possess gun powder or other combustibles, explosives or fireworks within the Recreational Areas. Provided, however, that this provision does not apply to gasoline and other petroleum products in fuel tanks of Vehicles or to petroleum products intended to be used as fuel for cooking.

Section 14: **ANIMALS.** No person may bring into or possess in the Recreational Areas any Pet or other animal other than a dog or domestic cat, except in areas clearly marked “off-leash.” Any person bringing a dog or domestic cat into the Recreational Areas shall keep such dog or domestic cat confined to a vehicle or secured by a leash not exceeding fifteen (15) feet in length. Each person who brings a Pet or other animal of any kind into the Recreational Areas is responsible for the prompt clean up and disposal of any Pet or animal waste in an appropriate trash receptacle.

Section 15: **GLASS BEVERAGE CONTAINERS.** No person shall use any glass beverage containers in the Recreational Areas. This provision shall not apply to baby bottles, baby food jars, glass lined thermos bottles and glass lined picnic beverage coolers.

Section 16: **ALCOHOLIC BEVERAGES.** No person shall consume an Alcoholic Beverage in the Recreational Areas.

Section 17: **USE OF LOUDSPEAKERS.** No person shall use any loudspeaker, public address system or amplifier within the Recreational Areas without prior written permission from the Board.

Section 18: **DUMPING AND LITTERING.** All persons shall dispose of trash associated with use of the Recreational Areas in an appropriate trash receptacle. No person shall bring into the Recreational Areas or District Property any trash, refuse or waste material. Disposal of household or commercial waste, trash or refuse using any of the District’s trash receptacles is prohibited.

Section 19: **ADVERTISING.** No person shall place, erect or attach any structure, sign, bulletin board, post, pole or advertising device of any kind whatsoever, or attach any notice, bill, poster, sign, wire, rod or cord to any tree, shrub, fence, railing, post or structure, in the Recreational Areas.

Section 20: **SOLICITING AND SALES.** No person shall solicit funds or donations, or sell or offer to sell services or goods or distribute circulars in the Recreational Areas. This rule does not apply to the following:

- a. Persons soliciting donations or conducting fund-raising events for and on behalf of non-profit organizations who have secured prior written permission from the Board;

b. Concessionaires and persons employed by concessionaires when selling goods or services, or charging for amusements, pursuant to written authority of the Board; and

c. Fees, including reasonable security deposits, for the use of specific Recreational Areas as may be established by the Board from time to time.

Section 21: **CAMPING.** No person shall engage in overnight camping in the Recreational Areas except with prior written approval of the Board.

Section 22: **SUPERVISION OF CHILDREN.** Children under 13 years of age must be supervised by an adult at all times.

Section 23: **NUISANCE:** No person shall use profanity or vulgar language within the Recreational Areas. No person shall use any threatening, abusive, or insulting language or language otherwise constituting “fighting words.” No person shall commit any obscene, lewd or indecent act or create a nuisance of any kind. No person shall disturb in any manner any picnic, meeting, service, concert, exercise or exhibition.

Section 24: **SPECIAL EVENTS.** No person or organization shall solicit for, hold or sponsor a Special Event in the Recreational Areas without submitting a completed Application for Use for Special Event form and the prior written permission of the Board, who may require the providing of liability insurance in the amounts of \$100,000 for each person, \$300,000 for each single occurrence for bodily injury or death and \$100,000 for each single occurrence for injury to or destruction of property, naming the District as insured, and the furnishing of one or more Peace Officers. The opinion of the Board as to whether or not insurance will be required and as to the required number of Peace Officers shall be final and binding.

Section 25: **EMERGENCY BURN BAN.** The Board may, at its sole discretion, find and determine that drought conditions exist in the District, or in the vicinity of the District, and that such drought conditions create an elevated danger of fire in the Recreational Areas or District Property that constitutes a hazard to public health and safety and an emergency.

After making such findings, the Board may impose a temporary emergency burn ban to prohibit charcoal fires, open fires, fireworks, outdoor use of inflammable materials and other conduct that could result in a fire, such burn ban to be applicable to and effective on all Recreational Areas and District Property.

Imposition of a burn ban by the Board shall have the effect of an immediate, temporary suspension of any and all authority for fires, fireworks and use of combustible materials as provided in Sections 10, 11 and 13 of these Rules until termination of the burn ban by the Board.

Notice of a District emergency burn ban shall be provided by signs, flyers, public service announcements and any other means necessary to call public attention to the burn ban, the conditions that constitute an emergency, and penalties that may result from violations of the burn ban. Notice of termination of a burn ban shall be provided by the same means.

Section 26: **VIOLATIONS; REWARDS.** No person shall use any portion of the Recreational Areas or District Property for any purpose other than the purpose for which it was

designed or designated. The District will pay a reward of up to \$1,000 for information leading to the arrest of persons responsible for vandalism or destruction of any portion of the Recreational Areas or District Property.

Section 27: PENALTIES. Compliance with these Rules and state and federal law is a condition of the use of the Recreational Areas. Pursuant to the authority granted by Sections 49.004 and 54.205 of the Texas Water Code, as amended, the Board may seek reasonable penalties for the failure of any person to comply with these Rules and laws, which penalties shall not exceed the jurisdiction of a justice court as provided in Section 27.031 of the Texas Government Code, as amended, currently up to \$20,000.00. Such penalties may be sought for each violation of these Rules and for each day of a continuing violation and shall be in addition to any other penalties provided by state or federal law and may be enforced by complaints filed in the appropriate court of jurisdiction in the County. In any suit to enforce these Rules, the District shall seek to recover reasonable fees for attorneys and expert witnesses and other costs incurred by the District. The Board may adopt a schedule of penalties solely for its own use and guidance in levying penalties prescribed herein.

Section 28: SANCTIONS. Compliance with these Rules and state and federal laws is a condition to the use of the Recreational Areas.

a. The authorities designated in Section 2 above to enforce these Rules are hereby authorized to notify any person who fails or refuses to comply with these Rules or applicable state or federal laws to depart from the Recreational Areas.

b. Any person who fails to depart upon such notification shall be subject to prosecution under Section 30.05 of the Texas Penal Code for criminal trespass, in addition to other punishment or prosecution for any other crime.

c. A person who fails to comply with these Rules is subject to civil penalties of currently up to \$20,000, for each violation and for each day of a continuing violation, together with attorneys' fees, expert witness fees and costs, as provided in Section 49.004 of the Texas Water Code, as amended. These penalties shall be in addition to any other penalties provided by state or federal law and may be enforced by complaints filed in the appropriate court of jurisdiction in the County.

d. In the event of a violation of these Rules, a violation notice shall be issued to the person responsible for the violation, and the Board shall conduct a hearing on the violation and imposition of a penalty.

e. Any person witnessing any concerning action or discovery of any concerning situation should immediately notify a District constable or any other Peace Officers on duty, the District's General Manager or a member of the Board.

Section 29: APPLICABILITY AND WAIVER. The Board may, at its sole discretion, waive any portion of the Rules, for any reason, including but not limited to as necessary to perform District functions including for work being performed on behalf of the District by employees, contractors, or subcontractors of the District.

Section 30: EFFECT ON EXISTING LAW. These Rules are in addition to, and not in lieu of, all state and federal laws and other rules and regulations applicable within the Recreational Areas and District Property.

Section 31: SEVERABILITY. The provisions of these Rules are severable. If any word, phrase, clause, sentence, section, provision or part of these Rules should be held invalid or unconstitutional, it shall not affect the validity of the remaining provisions, and it is hereby declared to be the intent of the Board that these Rules would have been adopted as to the remaining portions, regardless of the invalidity of any part.

Section 32: AMENDMENTS. These Rules may be reviewed and amended from time to time by the Board.

Section 33: POSTING: A summary of these Rules shall be conspicuously posted at or near the entrances to the Recreational Areas, and a copy or an excerpt of these Rules shall be provided to any person who requests a copy and to any person who submits an Application for Use for Special Event of the Recreational Areas.

Section 34: EFFECTIVE DATE: These Rules shall become effective and enforceable five days after the first publication of the notice of adoption or any amendment of these Rules, as provided in Sections 54.207 and 54.208 of the Texas Water Code.

The President or any Vice President is authorized to execute and the Secretary or Assistant Secretary is authorized to attest this order on behalf of the Board and the District.

Passed and adopted this 28th day of March, 2024.

JULIE GILMER

President

ATTEST:

BETTY BROWN

Secretary

I, the undersigned secretary of the Board of Directors of River Plantation Municipal Utility District, hereby certify that the foregoing is a true and correct copy of the Order Adopting Rules and Regulations for District Parks, Recreational Areas and District Property, Facilities, Easements and Rights-of-Way adopted by said Board at its meeting of March 28, 2024, and a minute entry of that date showing the adoption thereof, the original of which resolution appears in the minute book of said Board, on file in the District's office.

I further certify that said meeting was open to the public, and that notice thereof was posted in compliance with the provisions of Tex. Gov't. Code Ann. § 551.001 et seq.

Witness my hand and seal of said District this 28th day of March, 2024.

Secretary





MONTHLY OPERATIONS REPORT FOR RIVER PLANTATION MUD

February, 2024

Connections: 977
Vacant: 11

| REVENUE: | Water | LSGCD | Sewer | TCEQ | Taps | Deposits | Penalty | Misc. | TOTAL |
|--------------|--------------|--------------|--------------|------------|--------|-------------|-----------|-------------|--------------|
| | \$ 21,112.14 | \$ 465.58 | \$ 33,116.32 | \$ 274.59 | \$ - | \$ 1,150.00 | \$ 794.66 | \$ 6,121.48 | \$ 63,034.77 |
| BILLED CONS: | Residential | Builder/Temp | Multi Family | Irrigation | STP/LS | Commercial | Total | | |
| | 5,798,000 | 0 | 0 | 58,000 | 60,000 | 44,000 | 5,960,000 | | |

| WATER: | 01/18/24 - 02/19/24 | LSGCD - Well Permit | |
|-------------------------------|---------------------|--------------------------|-------------|
| Gallons pumped from Well No.2 | 4,672,000 | Permit Expires: | 12/31/2024 |
| Gallons pumped from Well No.3 | 1,978,000 | Permitted Authorization: | 225,868,339 |
| Total Pumpage | 6,650,000 | February Withdrawal: | 6,289,000 |
| Total Gallons Billed | 5,960,000 | Y-T-D Withdrawal: | 13,145,000 |
| Leaks, Construction, Flushing | 200,000 | Amount Remaining: | 212,723,339 |
| Pumped vs. Billed | 90% | | |
| Pumped vs. Accounted | 93% | | |
| Leaks repaired in District | 3 | | |
| Bacteriological samples: | 6 | Good | |

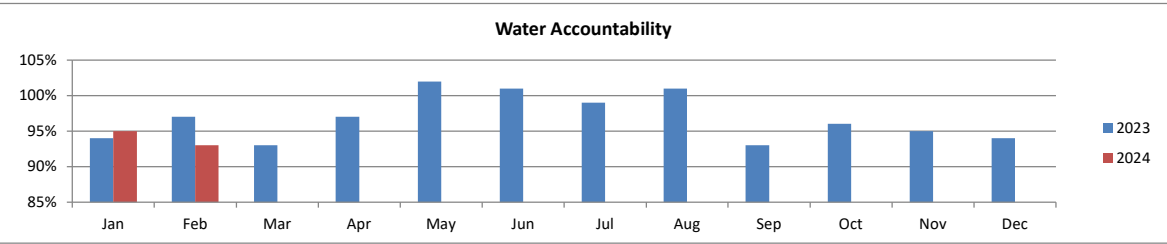
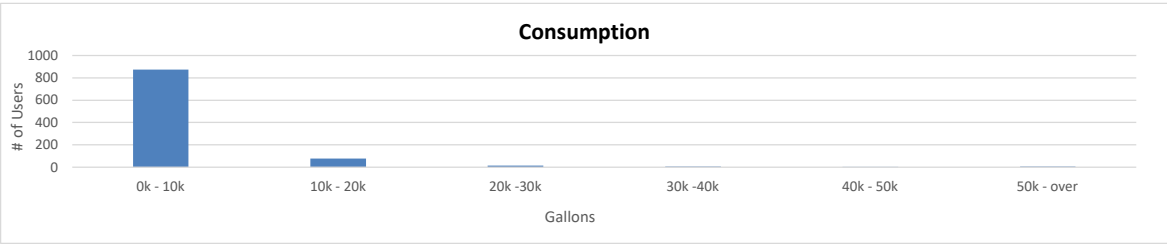
WASTEWATER TREATMENT PLANT
T.C.E.Q. Permit Number: WQ0010978001
Permit expiration date: January 2, 2029

| February, 2024 | | | Measured by: |
|--------------------------------|---------|-----------------------------------|----------------------|
| Average daily flow | 407,000 | Permitted Daily Flow | 600,000 gal.per day |
| Average CBOD | 2.10 | Permitted CBOD | 10 mg/l |
| Average Total Suspended Solids | 1.43 | Permitted T.S.S. | 15 mg/l |
| Average Ammonia Nitrogen | 0.85 | Permitted Ammonia Nitrogen | 3 mg/l |
| Average PH | 7.29 | Permitted PH | 6.00 - 9.00 STD UNIT |
| Average Dissolved Oxygen | 9.09 | Permitted Dissolved Oxygen (Min.) | 6.0 mg/l |
| Maximum Chlorine Residual | 3.89 | Permitted Chlorine Maximum | 4.0 mg/l |
| Minimum Chlorine Residual | 1.59 | Permitted Chlorine Minimum | 1.0 mg/l |
| Average E. coli | 10.21 | Permitted E. coli | 63.0 mpn/100 ml |
| Total Rainfall | 1.35" | | |

Sewer Treatment plant is currently operating at 68% of the permitted capacity.

Total gallons of Reuse for the month of February - 0.000 MG

| Aged Receivables: | Current | 30 day | 60 day | 90 day | 120 day | Total |
|-------------------|--------------|-------------|-----------|-----------|-----------|--------------|
| | \$ 59,882.00 | \$ (514.20) | \$ 950.18 | \$ 148.62 | \$ 335.00 | \$ 60,801.60 |



| Parameter | | NODI | Quantity or Loading | | | Quality or Concentration | | | | # of Ex. | Freq. of Analysis | Smpl. Type |
|--------------------|------------------------------------------|------|-----------------------|-----------------------|-------------------------|--------------------------|------------------------|--------------------------------------|-------|----------|-------------------|------------|
| Code | Name | | Value 1 | Value 2 | Units | Value 1 | Value 2 | Value 3 | Units | | | |
| 50050 | Flow, in conduit or thru treatment plant | | = 0.407 | = 0.75 | MGD | | | | | 0 | 99/99 | TM |
| 1 - Effluent Gross | | | | | | | | | | | | |
| Season: 0 | | Req. | <= 0.6 Daily Average | Req Mon Daily Maximum | Million Gallons per Day | | | | | | Continuous | TOTALZ |
| NODI: | | NODI | | | | | | | | | | |
| 50060 | Chlorine, total residual | | | | | = 1.59 | = 3.89 | mg/L | | 0 | 01/01 | GR |
| 1 - Effluent Gross | | | | | | | | | | | | |
| Season: 0 | | Req. | | | | >= 1.0 Monthly Minimum | <= 4.0 Monthly Maximum | Milligrams per Liter | | | Daily | GRAB |
| NODI: | | NODI | | | | | | | | | | |
| 51040 | E. coli | | | | | = 10.213 | = 104.3 | MPN/100mL | | 0 | 02/30 | GR |
| 1 - Effluent Gross | | | | | | | | | | | | |
| Season: 0 | | Req. | | | | <= 63.0 Daily Average | <= 200.0 Daily Maximum | Most Probable Number (MPN) per 100ml | | | Twice Per Month | GRAB |
| NODI: | | NODI | | | | | | | | | | |
| 80082 | BOD, carbonaceous [5 day, 20 C] | | = 3.86 | | lb/d | = 2.1 | = 2.4 | mg/L | | 0 | 01/07 | CS |
| 1 - Effluent Gross | | | | | | | | | | | | |
| Season: 0 | | Req. | <= 50.0 Daily Average | | Pounds per Day | <= 10.0 Daily Average | <= 25.0 Daily Maximum | Milligrams per Liter | | | Weekly | COMPOS |
| NODI: | | NODI | | | | | | | | | | |

Edit Check Errors

No results.

DMR Comments

Comments

Attachments

No results.

Report Last Saved By

User: deena@nwdls.com
 Name: Deena Higginbotham
 E-Mail: deena@nwdls.com
 Date/Time: 03/14/24 4:31 CDT

**RIVER PLANTATION MUNICIPAL UTILITY DISTRICT
ENGINEER'S REPORT
VSE Project No. 32000-000-0-DST
March 28, 2024, 6:30 p.m.**

Engineering Representative: Taylor J. Reed, P.E.

**Directors: Julie Gilmer, President
Tim Goodman, Vice President
Tom Vandever, Treasurer
Betty Brown, Secretary
Karl Sakocius, Asst. Secretary**

11. Items for Discussion:

I. Permits

- A. WWTF Discharge Permit Renewal (Expires September 2028)**
 - 1. No update

- B. Storm Water Quality Management Plan – MS4 Permit (Expires January 2024)**
 - 1. Finalizing the 2023 annual report and will be submitting on April 5, 2024

- C. Water Plant No. 1 – Water Well No. 1 Testing**
 - 1. Testing and Inspection due January 12, 2026

- D. Emergency Operation Information**
 - 1. Update as necessary

II. Design Projects

- A. Joint Projects**
 - 1. East Ditch FEMA Work**
 - a)** Under review with FEMA. We continue to receive updates that it is progressing through the system. Quarterly report has been submitted as required.



2. East Ditch Maintenance

a) No update. The next maintenance will be scheduled for April.

3. WWTP Rehabilitation and Electrical Upgrades

a) Project has been advertised. Expected bids on 4/5/2024. We will present bids at the April meeting.

4. Holly Springs Drainage Issue

a) We received 3 bids. AR TurnKee was the low bidder in the amount of \$87,165. We recommend awarding the contract to them and proceeding with the work.

B. District Projects

1. District Wide Drainage Study

a) We have identified 3 areas within the District that become heavily inundated during rain events. Attached is the entire study performed. We will discuss it during the meeting.

2. Sanitary Sewer Rehabilitation Phase 2

a) We received 4 bids. Insituform Technologies was the low bidder in the amount of \$692,620.00. Attached is our Recommendation of Award and bid tab.

3. Sanitary Sewer Manhole Rehabilitation Phase 1

a) After review of the manholes, we find the interiors to be in acceptable condition. From the initial videos. We are conducting more inspections with the Sanitary Sewer Rehabilitation Phase 2 project.

C. Charleston Park Irrigation

1. We are waiting for the maintenance proposal from the contractor for the irrigation system. The sprinkler heads were marked in anticipation for a site walk with directors. The site walk was rescheduled to 4/1/24 due to weather. The I spoke with the mowing contractor, and they are going to avoid them and ensure they do not get destroyed and the surveyor will be out next week to survey all the head locations.
2. They provided a proposal in the amount of \$15,600 for maintenance of the irrigation system. This includes 24 visits per year, checking for leaks, coverage, reprogram as needed, minor repairs and adjustments.
3. Received the attached proposal for 20 additional sprinkler heads to keep in storage along with necessary fittings.

D. Storm Sewer Phase 1 Rehabilitation

1. A site walk was performed with the contractor. Attached is change order no. 3 for performing pipe on a 54" where the pipe repair goes underneath an existing driveway and too close to the house to safely work on.

E. Water Plant No. 2 Electrical Upgrades

1. Construction underway. The contractor is waiting on the Motor Control Center to be delivered. They have been working on the conduits and new service connection. No pay application this month.

F. Plantation Village Drainage Improvements

1. Using the drainage study, we were able to put together an exhibit and size a potential swale to capture the flow of the property, channelize it and direct it to the front of the lots. Attached is an exhibit of the proposed plan and cost estimate.

III. Other Matters

A. 10 Year CIP

1. I have shared the new 10-year CIP with the FA and we are discussing the next bond issue for more District repairs.

IV. Questions/Answers

A. 592 Stone Wall Jackson Bend

1. MOC is filling in the hole, and we are working to address the underlying cause in the storm sewer located next to the problem area.

B. Stonewall Jackson Manhole Sinkhole

1. MOC has prepared a price to replace the manhole.

- C. Robert E. Lee Dr. Storm Sewer Issue
 - 1. MOC has prepared a price to fix the area.



777 North Eldridge Parkway, Suite 500
Houston, TX 77079
713.782.0042 | Fax 713.782.5337
info@vs-eng.com
vs-eng.com



March 27, 2024

River Plantation Municipal Utility District
c/o Smith, Murdaugh, Little, & Bonham, LLP
2727 Allen Parkway, Suite 1100
Houston, TX 77019

Re: Recommendation of Award
711 Holly Springs Storm Sewer Replacement
Within River Plantation Municipal Utility District
VSE Project No.: 32000-812-1-UTL (c&e)

Dear Directors:

Enclosed please find the Bid Tabulation of bids received for construction of the above referenced project. A total of **Three (3)** bids were received.

We recommend that a construction contract be awarded to **AR TurnKee** based on their low bid of **Eighty-Seven Thousand, One Hundred Sixty-Five and 00/100 Dollars (\$87,165.00)**

Sincerely,

A handwritten signature in black ink, appearing to read "Taylor J. Reed".

Taylor J. Reed, P.E.
Project Manager
Vogler & Spencer Engineering, Inc.
Texas Registered Engineering Firm No. F-148

Enclosure

TJR;amw

xc: AR TurnKee
File

BID TABULATION
711 HOLLY SPRINGS STORM SEWER REPLACEMENT
WITHIN RIVER PLANTATION MUNICIPAL UTILITY DISTRICT
Bid Date: Wednesday, March 27, 2024
VSE Project No.: 32000-501-1-STP (c&e)

| | | | | 1. AR TurnKee | | 2. Wright Solutions | | 3. ICS LLC. | |
|--------------------------------------|----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|------|----------|--------------------|-------------|------------------------|-------------|---------------------|--------------|
| ITEM No. | DESCRIPTION | UNIT | BID QTY. | UNIT PRICE | AMOUNT | UNIT PRICE | AMOUNT | UNIT PRICE | AMOUNT |
| STORM SEWER REPLACEMENT ITEMS | | | | | | | | | |
| 1. | MOBILIZATION Including Bonds, Insurance, Move-In/Move-Out (Max 3% of total cost) | LS | 1 | \$7,000.00 | \$7,000.00 | \$3,250.00 | \$3,250.00 | \$9,500.00 | \$9,500.00 |
| 2. | REMOVE & DISPOSE 36" ACMP (includes excavation and disposal of debris and pipe) | LF | 200 | \$40.00 | \$8,000.00 | \$50.00 | \$10,000.00 | \$45.00 | \$9,000.00 |
| 3. | INSTALL 36" HDPE (includes excavation, disposal of debris, finishing of pipe, installation, backfilling, cement stabilized sand, and site restoration) | LF | 180 | \$173.00 | \$31,140.00 | \$225.00 | \$40,500.00 | \$285.00 | \$51,300.00 |
| 4. | REMOVE AND DISPOSE TYPE E-INLET AND MANHOLE (2). REPLACE w/ 36" CONCRETE HEADWALL w/ FLARED WINGWALLS STRUCTURE (w/ 30° SKEW) (includes excavation, disposal of debris and structures, furnishing of structure, installation, backfilling, cement stabilized sand, and site restoration) | EA | 1 | \$11,000.00 | \$11,000.00 | \$15,500.00 | \$15,500.00 | \$16,500.00 | \$16,500.00 |
| 5. | CLEARING (includes removal and disposal of debris and trees) | LS | 1 | \$7,500.00 | \$7,500.00 | \$8,500.00 | \$8,500.00 | \$12,650.00 | \$12,650.00 |
| 6. | REMOVE & DISPOSE (2) MANHOLES. REPLACE w/ 8'X5' JB w/ E-INLET TOP & TIE IN EXIST. 36" CMP & 24" RCP (includes excavation, removal, disposal of debris and structures, furnishing of junction box, installation, existing pipe and swale tie-ins, backfill, cement stabilized sand, and site restoration) | EA | 1 | \$9,000.00 | \$9,000.00 | \$9,800.00 | \$9,800.00 | \$9,500.00 | \$9,500.00 |
| 7. | TYPE "C" MANHOLE w/ PRECAST BASE (includes excavation, backfill, cement stabilized sand, furnishing of manhole, installation, and site restoration) | EA | 1 | \$5,000.00 | \$5,000.00 | \$7,000.00 | \$7,000.00 | \$6,500.00 | \$6,500.00 |
| 8. | DRIVEWAY REPLACEMENT (includes removal, disposal, backfilling, grading, forming, and concrete, and placement)(to be used only with Engineer's approval) | SY | 25 | \$101.00 | \$2,525.00 | \$300.00 | \$7,500.00 | \$175.00 | \$4,375.00 |
| 9. | 36" CMP STORM SEWER POINT REPAIR W/ HDPE UNDER TURF - ALL DEPTHS (includes excavation, furnishing of material, concrete collar, backfill, cement stabilized sand, site restoration, and post repair video) | EA | 1 | \$6,000.00 | \$6,000.00 | \$12,500.00 | \$12,500.00 | \$6,750.00 | \$6,750.00 |
| TOTAL PROJECT BID | | | | \$87,165.00 | | \$114,550.00 | | \$126,075.00 | |
| ALTERNATE BID ITEMS | | | | | | | | | |
| A1 | INSTALL 42" HDPE (includes excavation, disposal of debris, finishing of pipe, installation, backfilling, cement stabilized sand, and site restoration) (in lieu of 36" HDPE) | LF | 180 | \$195.00 | \$35,100.00 | \$250.00 | \$45,000.00 | \$350.00 | \$63,000.00 |
| A2 | REMOVE AND DISPOSE TYPE E-INLET AND MANHOLE (2). REPLACE w/ 42" CONCRETE HEADWALL w/ FLARED WINGWALLS STRUCTURE (w/ 30° SKEW) (includes excavation, disposal of debris and structures, furnishing of structure, installation, backfilling, cement stabilized sand, and site restoration) (in lieu of 36" HDPE) | EA | 1 | \$12,000.00 | \$12,000.00 | \$17,500.00 | \$17,500.00 | \$22,500.00 | \$22,500.00 |
| A3 | INSTALL 2' X 4' RCB (includes excavation, disposal of debris, finishing of pipe, installation, backfilling, cement stabilized sand, and site restoration) (in lieu of 36" HDPE) | LF | 180 | \$475.00 | \$85,500.00 | \$420.00 | \$75,600.00 | \$850.00 | \$153,000.00 |

| | | | |
|------------------------------|---------------------------|-----------------|-------------|
| Hank | Additional Bidders | Base Bid | Days |
| NO ADDITIONAL BIDDERS | | | |



777 North Eldridge Parkway, Suite 500
Houston, TX 77079
713.782.0042 | Fax 713.782.5337
info@vs-eng.com
vs-eng.com



February 23, 2024

River Plantation Municipal Utility District
c/o Smith, Murdaugh, Little, & Bonham, LLP.
2727 Allen Parkway, Suite 1100
Houston, TX 77019

Re: Recommendation of Award
Sanitary Sewer Rehabilitation Phase No. 2
Within River Plantation Municipal Utility District
VSE Project No.: 32000-808-2-UTL (c&e)

Dear Directors:

Enclosed please find the Bid Tabulation of bids received for construction of the above referenced project. A total of **Four (4)** bids were received.

We recommend that a construction contract be awarded to **Insituform Technologies, LLC.** based on their low bid of **Six Hundred Ninety-Two Thousand, Six Hundred Twenty and 00/100 Dollars (\$692,620.00)** with a contract time of **One Hundred Eighty (180) calendar days to Substantial Completion and an additional Thirty (30) calendar days to Final Completion.**

Sincerely,

A handwritten signature in blue ink, appearing to read 'Peitao Long'.

Peitao Long, E.I.T.
Engineer in Training
Vogler & Spencer Engineering, Inc.
Texas Registered Engineering Firm No. F-148

Enclosure

PL;amw

xc: Insituform Technologies, LLC
File

BID TABULATION
Vogler & Spencer Engineering, Inc.
SANITARY SEWER REHABILITATION PHASE No. 2
WITHIN RIVER PLANTATION MUNICIPAL UTILITY DISTRICT
MONTGOMERY COUNTY, TEXAS
Bid Date: Friday, February 23, 2024
VSE Project No.: 32000-808-2-UTL (c&e)

| ITEM No. | DESCRIPTION | UNIT | BID QTY. | 1. Insituform Technologies, LLC | | 2. Texas Pride Utilities, LLC | | 3. Cruz Tec | |
|-------------------------------------------------------------|-----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|------|----------|---------------------------------|----------------------|-------------------------------|----------------------|-------------|----------------------|
| | | | | UNIT PRICE | AMOUNT | UNIT PRICE | AMOUNT | UNIT PRICE | AMOUNT |
| A) GENERAL ITEMS | | | | | | | | | |
| 1. | Mobilization/Demobilization/Payment/Performance Bonds/Permits & Fees (Refer to the Special Conditions Part A for insurance requirements. Requirements must be strictly adhered to - this includes the Contractor's Pollution Liability (CPL) Insurance in the amount of \$1,000,000.00 (I.L.C.vi - page 5). (Maximum amount not to exceed 3% of the Base Bid amount). | LS | 1 | \$20,000.00 | \$20,000.00 | \$22,000.00 | \$22,000.00 | \$45,000.00 | \$45,000.00 |
| A. GENERAL ITEMS SUBTOTAL | | | | | \$ 20,000.00 | | \$ 22,000.00 | | \$ 45,000.00 |
| B) CIVIL SITE WORK | | | | | | | | | |
| 1. | Temporary Traffic Control Plan | LS | 1 | \$5,000.00 | \$5,000.00 | \$8,800.00 | \$8,800.00 | \$5,000.00 | \$5,000.00 |
| 2. | Manhole Cleaning & Inspections (Including GPS location of all Manholes) | EA | 225 | \$425.00 | \$95,625.00 | \$400.00 | \$90,000.00 | \$700.00 | \$157,500.00 |
| 3. | Relocate Unknown Pipe (Coordinate w/ Local Dry Utility to Safely Relocate Unknown Protruding Piping.) | EA | 2 | \$3,250.00 | \$6,500.00 | \$4,000.00 | \$8,000.00 | \$7,500.00 | \$15,000.00 |
| 4. | Obstruction Removal At Service Lead by Remote Cutting Application | EA | 4 | \$315.00 | \$1,260.00 | \$400.00 | \$1,600.00 | \$850.00 | \$3,400.00 |
| 5. | Sanitary Sewer Point Repair - all Depths (Includes Excavation, Backfill, Landscape Repairs, and Provide Post Repair Videos) | EA | 4 | \$3,000.00 | \$12,000.00 | \$3,200.00 | \$12,800.00 | \$3,250.00 | \$13,000.00 |
| 6. | Obstruction Removal Within Sanitary Sewer Mains (To Differentiate From Service Lead Obstruction Removals). | EA | 4 | \$315.00 | \$1,260.00 | \$600.00 | \$2,400.00 | \$1,200.00 | \$4,800.00 |
| 7. | Heavy Grease Removal and Cleaning at Designated Locations | EA | 12 | \$315.00 | \$3,780.00 | \$200.00 | \$2,400.00 | \$150.00 | \$1,800.00 |
| 8. | 8" Cured-In-Place-Pipe Sanitary Sewer Rehab. | LF | 11,873 | \$35.00 | \$415,555.00 | \$36.00 | \$427,428.00 | \$32.50 | \$385,872.50 |
| 9. | 15" Cured-In-Place-Pipe Sanitary Sewer Rehab. | LF | 1,135 | \$63.00 | \$71,505.00 | \$84.00 | \$95,340.00 | \$70.00 | \$79,450.00 |
| 10. | Remove and Replace Exist. 8" Sanitary Sewer w/ SDR 26 PVC Pipes (Includes Excavation, Backfill, & Provide Post Repair Videos) | LF | 40 | \$85.00 | \$3,400.00 | \$100.00 | \$4,000.00 | \$150.00 | \$6,000.00 |
| 11. | OSHA Trench Safety System (All Depths) | LF | 40 | \$11.50 | \$460.00 | \$100.00 | \$4,000.00 | \$25.00 | \$1,000.00 |
| 12. | Site Restoration to Equal or Better Condition (Includes Fence Replacement and Sodding) | LS | 1 | \$5,000.00 | \$5,000.00 | \$6,000.00 | \$6,000.00 | \$15,000.00 | \$15,000.00 |
| 13. | All Necessary Bypass Pumping for the Duration of the Project. | LS | 1 | \$5,000.00 | \$5,000.00 | \$18,000.00 | \$18,000.00 | \$15,000.00 | \$15,000.00 |
| 14. | Post Cleaning and Televising of all Repaired and CIPP Sanitary Sewer Lines for Verification of Work. | LS | 1 | \$1,000.00 | \$1,000.00 | \$26,016.00 | \$26,016.00 | \$30,000.00 | \$30,000.00 |
| B. CIVIL SITE WORK SUBTOTAL | | | | | \$ 627,345.00 | | \$706,784.00 | | \$ 732,822.50 |
| C) ADDITIONAL WORK ITEMS (AS AUTHORIZED BY ENGINEER) | | | | | | | | | |
| 1. | Extra Length of Point Repair for 8" Pipe | LF | 50 | \$160.00 | \$8,000.00 | \$100.00 | \$5,000.00 | \$65.00 | \$3,250.00 |
| 2. | Extra 8" Sanitary Sewer Replacement | LF | 50 | \$85.00 | \$4,250.00 | \$240.00 | \$12,000.00 | \$150.00 | \$7,500.00 |
| 3. | Remove & Replace Cleanouts. | EA | 5 | \$2,000.00 | \$10,000.00 | \$400.00 | \$2,000.00 | \$1,500.00 | \$7,500.00 |
| 4. | External Service Reconnection. | EA | 5 | \$950.00 | \$4,750.00 | \$1,200.00 | \$6,000.00 | \$2,800.00 | \$14,000.00 |
| 5. | Extra Cement Stabilized Sand. | CY | 50 | \$68.00 | \$3,400.00 | \$40.00 | \$2,000.00 | \$85.00 | \$4,250.00 |
| 6. | Extra Manhole Cleaning & Inspections (Including GPS location of all Manholes) | EA | 35 | \$425.00 | \$14,875.00 | \$400.00 | \$14,000.00 | \$700.00 | \$24,500.00 |
| C. ADDITIONAL WORK ITEMS SUBTOTAL | | | | | \$ 45,275.00 | | \$41,000.00 | | \$ 61,000.00 |
| TOTAL BASE BID (A-C) | | | | | \$ 692,620.00 | | \$ 769,784.00 | | \$ 838,822.50 |
| SUBSTANTIAL COMPLETION CALENDAR DAYS | | | | | 180 | | 240 | | 270 |
| FINAL COMPLETION CALENDAR DAYS | | | | | 30 | | 10 | | 45 |
| Rank | Additional Bidders | | | Base Bid | | | Days | | |
| 4. | AR TurnKey Construction Company, Inc. | | | \$1,499,012.00 | | | 180/30 | | |

River Plantation M.UD.
Annual Maintenance
Total Bid Package Summary Sheet

| Facility | UNIT | NUMBER OF MOWS | UNIT PRICE | AMOUNT |
|-----------------------------------------------------------------------------------------------------------------------------------------------|------|----------------------|-------------------------------------|---------------------------|
| <u>RP MUD Park - 71.45 acres</u> | | | | |
| Park Maintenance (Mowing, edging, trimming, including blowing along the trail/walkway)(Bi-monthly April - October, Monthly November - March.) | LS | 19 | <u>\$3,720.00</u> | <u>\$70,680.00</u> |
| | | | RP MUD Park Subtotal | <u>\$70,680.00</u> |
| <u>District Facilities</u> | | | | |
| Water Plant No. 1 - 0.34 Acres (Mowing, edging, trimming, etc) (Bi-monthly April - October, Monthly November - March.) | LS | 19 | <u>\$100.00</u> | <u>\$1,900.00</u> |
| Water Plant No. 2 - 0.73 Acres (Mowing, edging, trimming, etc) (Bi-monthly April - October, Monthly November - March.) | LS | 19 | <u>\$125.00</u> | <u>\$2,375.00</u> |
| Water Plant No. 3 - 0.46 Acres (Mowing, edging, trimming, etc) (Bi-monthly April - October, Monthly November - March.) | LS | 19 | <u>\$110.00</u> | <u>\$2,090.00</u> |
| WWTP - 3.64 Acres (Mowing, edging, trimming, etc) | LS | 19 | <u>\$225.00</u> | <u>\$4,275.00</u> |
| District Administration Building - 4.93 Acres (Mowing, edging, trimming, etc) (Bi-monthly April - October, Monthly November - March.) | LS | 19 | <u>\$275.00</u> | <u>\$5,225.00</u> |
| | | | District Facilities Subtotal | <u>\$15,865.00</u> |
| <u>Drainage Facilities</u> | | | | |
| North Ditch - 1.41 Acres (Mowing, edging, trimming, etc.) | LS | 4 | <u>\$600.00</u> | <u>\$2,400.00</u> |
| Mosswood Easement - 1.41 Acres (Mowing, edging, trimming, etc.) | LS | 6 | <u>\$500.00</u> | <u>\$3,000.00</u> |

| | |
|-------------------------------------|--------------------|
| Drainage Facilities Subtotal | \$5,400.00 |
| Annual Maintenance Total | \$91,945.00 |

Extra Work Items (not included as part of total bid amount)

| | | | | |
|-----------------------------------------------------------------------------------------------------------------------------------------|----|---|--------------------|---------------------|
| East Concrete Ditch - 7000LF (Debris removal and minor desilting)(to be performed at direction of the Board of Directors) | LS | 1 | <u>Bid / Quote</u> | <u>Upon Request</u> |
| Mosswood Ditch - 1.82 acres (Mowing, edging trimming, and minor clearing, etc)(to be performed at direction of the Board of Directors) | LS | 4 | <u>\$1,800.00</u> | <u>\$7,200.00</u> |
| Annual Overseading (to be performed at direction of the Board of Directors) | LS | 1 | <u>Bid / Quote</u> | <u>Upon Request</u> |
| Annual Wildflower Planting (to be performed at direction of the Board of Directors) | LS | 1 | <u>Bid / Quote</u> | <u>Upon Request</u> |

Irrigation System Maintenance Quote

24 Visits per year at \$650.00 per visit \$15,600.00

Includes: run through entire system. Check for leaks. Check coverage. Reprogram controllers as needed. Minor repairs and head adjustments. Monthly updates. Quotes provided for equipment replacements or repairs.



TEXAS IRRIGATION SUPPLY CON
 501 Hickerson, Building #1
 Conroe, TX 77301
 Phone 936-494-0046
 Fax 936-494-2276



Quotation

| | |
|-------------------------------------------------------------------------------------------------------------------------|--------------|
| EXPIRATION DATE | QUOTE NUMBER |
| 03/25/2024 | S5362326 |
| TEXAS IRRIGATION SUPPLY CON 501 Hickerson, Building #1 Conroe, TX 77301 Phone 936-494-0046 Fax 936-494-2276 | PAGE NO. |
| | 1 of 1 |

QUOTE TO:

SHIP TO:

HANSEN LANDSCAPE CONSTRUCTION, INC
 9240 LANTERN CREEK COURT
 CONROE, TX 77303

CHARLESTON PARK RIVER PLN GOLF CLUB
 550 COUNTRY CLUB DRIVE
 CONROE, TX 77302

| CUSTOMER NUMBER | CUSTOMER PO NUMBER | JOB NAME / RELEASE NUMBER | SALESPERSON | |
|-----------------|--------------------------------------------------------------------------------------------------------------------------|---------------------------|--------------|-----------------|
| 52690 | CHARLESTON PARK | | ANDREW BAKER | |
| WRITER | SHIP VIA | TERMS | SHIP DATE | FREIGHT ALLOWED |
| ANDREW BAKER | PK PICK-UP TX | Net Due 60 Days | 03/26/2024 | No |
| ORDER QTY | DESCRIPTION | | UNIT PRICE | EXT PRICE |
| 20ea | D70E5080A 1 1/4 IN FULL CIRCLE ROTOR ELECTRIC VIH #50-BLACK NOZZLE 80 PSI WEATHERMATIC SPECIAL ORDER - NON-RETURNABLE | | 245.950/ea | 4919.00 |
| 20ea | ADPT150N INLET BUSHING ADAPTER - 1-1/4 IN MALE ACME X 1-1/2 IN IN FEMALE NPT WEATHERMATIC SPECIAL ORDER - NON-RETURNABLE | | 18.917/ea | 378.33 |

The pricing on this bid is good for 30 days from the date generated.
 Taxes are not included in totals.

| | |
|-------------|---------|
| Subtotal | 5297.33 |
| S&H Charges | 0.00 |
| Amount Due | 5297.33 |

Change Order

2058-CO3

2/28/2023

From: **AR TurnKee Construction Company Inc.**
PO Box 925985
Houston, TX 77292
713-469-5952

To: **River Plantation Municipal Utility District**
c/o Vogler & Spencer Engineering, Inc
777 North Eldridge Parkway , Suite 500
Houston, TX 77079

Re: Westlawn and Highland Drainage Improvements

AR TurnKee Construction Company proposes the following work to be performed for the above referenced job:

| <u>Change Order:</u> | <u>Unit</u> | <u>Quantity</u> | <u>Price\$</u> | <u>Total Price</u> |
|------------------------------------------------------|-------------|-----------------|----------------|--------------------|
| * Inspect, prep, clean, and televise 54" storm sewer | LS | 1 | \$5,000.00 | \$ 5,000.00 |
| * Geopolymer lining of 54" storm sewer | LF | 185 | \$369.00 | \$ 68,265.00 |
| * Post tv of lines | LF | 185 | \$7.00 | \$ 1,295.00 |

Total Cost for Work This Proposal

\$ 74,560.00

Includes:

- * All material, equipment, and labor necessary to complete proposed work

Excludes:

- * Any demolition or removal of debris not shown on plans or mentioned in proposal
- * Handling of any hazardous waste encountered
- * Haul off of material not mentioned in proposal
- * Import of fill
- * Extra work caused by obstructions not shown on plans

Thanks for your consideration.

Adam Turner
AR TurnKee Construction Company

**PRELIMINARY COST ESTIMATE
 PLANTATION VILLAGE DRAINAGE IMPROVEMENTS
 WITHIN RIVER PLANTATION
 MUNICIPAL UTILITY DISTRICT
 PROJECT NO. 32000-813-1-UTL**

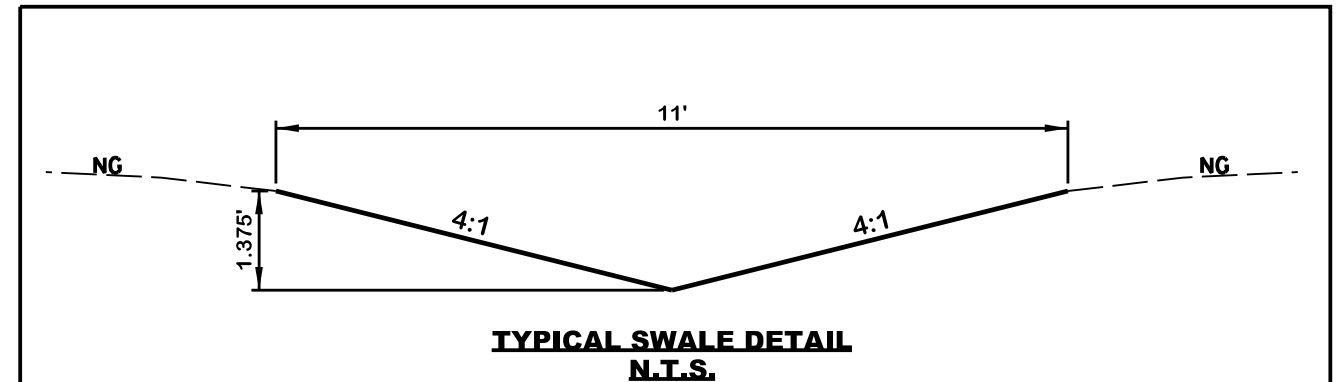
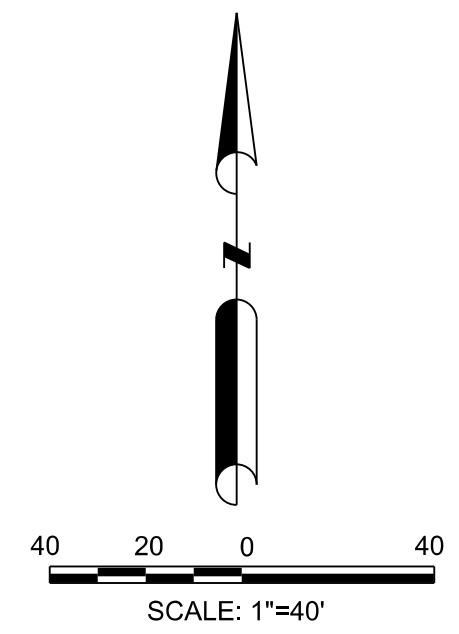
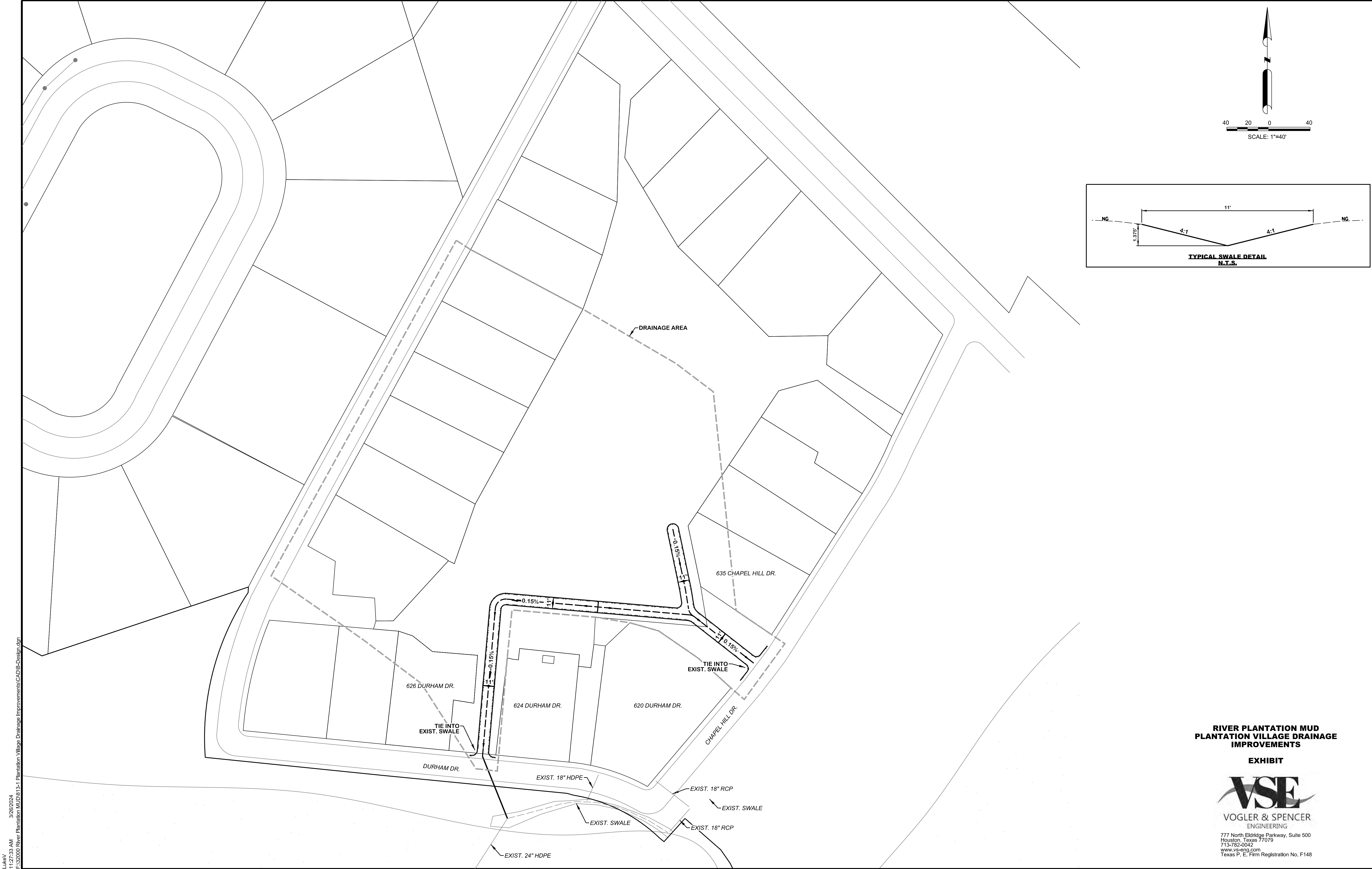
| ITEM NO. | DESCRIPTION | UNIT | ESTIMATED QUANTITY | UNIT PRICE | AMOUNT |
|------------------------------------|---------------------------------------------------------------------------------------------------------------------------------------------------------|------|-----------------------|---------------|----------------------------|
| <u>STORM SEWER ITEMS</u> | | | | | |
| 1. | MOBILIZATION Including Bonds, Insurance, Move-In/Move-Out (Max 3% of total cost) | LS | 1 | \$ 3,000.00 | \$ 3,000.00 |
| 1. | EXCAVATION AND GRADING OF PROPOSED SWALES (includes excavation, haul off & disposal of spoils, grading as specified within plans, and site restoration) | LF | 500 | \$ 20.00 | \$ 10,000.00 |
| 2. | INSTALL 24" HDPE (includes excavation, disposal of debris, finishing of pipe, installation, backfilling, cement stabilized sand, and site restoration) | LF | 65 | \$ 200.00 | \$ 13,000.00 |
| STORM SEWER ITEMS SUB-TOTAL | | | | | <u>\$ 26,000.00</u> |

CIVIL SITE ITEMS

| | | | | | |
|----|-------------------------------------------------------------------------------------------------------------------|----|---|-------------|-------------|
| 3. | CLEARING (includes removal, haul off and disposal, and site restoration) TO BE USED ONLY WITH ENGINEER'S APPROVAL | EA | 2 | \$ 4,000.00 | \$ 8,000.00 |
|----|-------------------------------------------------------------------------------------------------------------------|----|---|-------------|-------------|

**PRELIMINARY COST ESTIMATE
PLANTATION VILLAGE DRAINAGE IMPROVEMENTS
WITHIN RIVER PLANTATION
MUNICIPAL UTILITY DISTRICT
PROJECT NO. 32000-813-1-UTL**

| ITEM NO. | DESCRIPTION | UNIT | ESTIMATED QUANTITY | UNIT PRICE | AMOUNT |
|------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|------|-----------------------|---------------|----------------------------|
| 4. | FULL DEPTH REMOVE AND REPLACE ASPHALT PAVEMENT (includes sawcut, removal, haul off and disposal, excavation, subgrade, backfilling, cement stabilized sand, compaction, testing, furnishing, bituminous concrete base course, 1 1/2" bituminous concrete surface course, and site restoration) | SY | 30 | \$ 200.00 | \$ 6,000.00 |
| CIVIL SITE ITEMS SUB-TOTAL | | | | | <u>\$ 14,000.00</u> |
| <u>STORMWATER POLLUTION PREVENTION ITEMS</u> | | | | | |
| 1. | Reinforced Filter Fabric Fence (includes disposal upon project completion) | LF | 425 | \$ 2.00 | \$ 850.00 |
| 2. | ROCK FILTER DAM (includes disposal upon project completion) | EA | 2 | \$ 300.00 | \$ 600.00 |
| STORMWATER POLLUTION PREVENTION ITEMS SUB-TOTAL | | | | | <u>\$ 1,450.00</u> |
| TOTAL PROJECT COST (Storm Sewer Items, Civil Site Items, & SWPPP) | | | | | <u>\$ 41,450.00</u> |
| CONTINGENCY (20%) | | | | | <u>\$ 8,290.00</u> |
| TOTAL COST ESTIMATE | | | | | <u>\$ 49,740.00</u> |



**RIVER PLANTATION MUD
PLANTATION VILLAGE DRAINAGE
IMPROVEMENTS**

EXHIBIT






**VOGLER & SPENCER
ENGINEERING**

777 North Eldridge Parkway, Suite 500
Houston, Texas 77079
713-782-0042
www.vse-eng.com
Texas P. E. Firm Registration No. F148

Luke V 3/26/2024 11:27:33 AM
 F:\32000 River Plantation MUD\3-1 Plantation Village Drainage Improvements\CAD\E-Design.dgn



777 North Eldridge Parkway, Suite 500 
Houston, TX 77079
713.782.0042 | Fax 713.782.5337 
info@vs-eng.com 
vs-eng.com

RIVER PLANTATION MUD EXISTING CONDITONS

DRAINAGE ASSESSMENT

Prepared By:
Vogler & Spencer Engineering, Inc.
Consulting Engineers
Firm Registration No. F-148

February 2024

VSE Project No. 32000-607-1-RPT

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List of Exhibits

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- Exhibit 2 – Project Location
- Exhibit 3 – FEMA FIRMs
- Exhibit 4 – Overall Existing Drainage Area Map
- Exhibit 5 – Existing Storm Sewer Layout (1 of 3)
- Exhibit 6 – Existing Storm Sewer Layout (2 of 3)
- Exhibit 7 – Existing Storm Sewer Layout (3 of 3)
- Exhibit 8 – Local Storm 10% AEP Inundation Layout
- Exhibit 9 – Local Storm 1% AEP Inundation Layout
- Exhibit 10 – Local Storm 0.2% AEP Inundation Layout
- Exhibit 11 – Regional Storm 10% AEP Inundation Layout
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- Exhibit 14 – XPSWMM/XPSTORM Model Layout Area 1
- Exhibit 15 – XPSWMM/XPSTORM Model Layout Area 2
- Exhibit 16 – XPSWMM/XPSTORM Model Layout Area 3
- Exhibit 17 – Ponding Area 1 Improvement Investigation Areas
- Exhibit 18 – Ponding Area 2 Improvement Investigation Areas
- Exhibit 19 – Ponding Area 3 Improvement Investigation Areas

List of Appendices

- Appendix A – Peak Runoff Rate Calculations

EXECUTIVE SUMMARY

River Plantation Municipal Utility District (The District) contracted Vogler & Spencer Engineering, Inc. (VSE) to analyze the existing drainage conditions and ponding levels for the River Plantation Development using the Atlas 14 rainfall values for the 10%, 1%, and 0.2% annual exceedance probability (AEP) rain events. The report includes three (3) annual exceedance probability model analysis for the entire District boundary (Exhibit 2) up to the project limits at the West Fork San Jacinto River. The report does not include assessments for regional storm events.

The District drainage assessment addresses the existing hydrologic and hydraulic conditions during specific storm events. The purpose of this evaluation is to develop an independent unsteady 1D/2D integrated hydrologic and hydraulic existing conditions model to identify the current storm sewer system inadequacies, natural depressions, and the resulting impacted areas during localized storms.

River Plantation experiences local and regional flooding during extreme rain events. This drainage analysis report provides a detailed description of the existing drainage conditions, based on the performed modeling using LiDAR 2018 data, site visits, and historic drawings. VSE analyzed all 10, 100, and 500-year extreme rain events, as per the Drainage Criteria Manual for Montgomery County, using 1D/2D integrated hydraulic models to identify natural depressions and analyze the existing drainage system.

SECTION 1.0 – INTRODUCTION

1.1 Project Name & Purpose

The District boundary includes approximately 894 acres of land, presently platted into single family residential lots, and includes an 18-hole golf course, club house, recreational facilities, and municipal facilities. Three main drainage channels run through The District from north to south; the East Ditch, Mosswood Ditch, and Stewarts Creek. Running along the southern boundary of The District is the West Fork San Jacinto River. Since East Ditch is an un-studied channel, the tailwater condition was set as a free outfall. It is noted that during regional extreme rain events, the West Fork San Jacinto River water surface elevations tend to surpass its existing banks, causing regional flooding within The District.

1.2 Project Limits

The District is located within Montgomery County, Texas, just South of the City of Conroe. The District is bounded by I-45 to the West, Sunset Heights Lane to the North, the East Plantation Municipal Utility District and a power transmission right of way to the East, and the West Fork San Jacinto River to the South, as shown in Exhibits 1 & 2.

1.3 Project Objectives

The District contracted with VSE to perform a hydrologic and hydraulic study analysis of The District's drainage to determine the existing drainage conditions and to further analyze areas with high ponding potential. This analysis will establish the current conditions within the study area for the 10, 100, and 500-year storm events.

1.4 Assumptions and Constraints

The modeling performed considered the area's topography using 2018 LiDAR, the existing drainage system by use of record drawings and field visits. Initially a 2-dimensional (2D) grid surface was developed to highlight flooded areas and street ponding due to overland runoff only. The District's overland flow characteristics were then analyzed to manually delineate drainage sub-areas for the overall drainage boundary. The existing storm sewer location and flowlines were estimated based on field visits and record drawings. The regional flooding within The District due to the West Fork San Jacinto River water surface levels during extreme rain events is not part of this study's scope of work for analyzation or proposed solutions, but is depicted in Exhibits 11, 12, & 13 to provide a full assessment of The District's flooding issues.

1.5 Project Datum

The project vertical datum is tied to the North American Vertical Datum (NAVD) 1988, 2001 Adjustment.

SECTION 2.0 – EXISTING CONDITIONS

The existing drainage system, as per record drawings and field visits, consists of grate inlets, type “E” inlets, and drainage swales (including roadside ditches) connecting to reinforced concrete pipe (RCP) and/or corrugated metal pipe (CMP), ranging from 18" to 60" in diameter, as shown in Exhibits 5, 6, & 7. The natural drainage pattern conveys stormwater from the Northeast through the East Ditch of River Plantation, which outfalls to the West Fork San Jacinto River; from the central region of the district towards the West through Mosswood Ditch which outfalls to the West Fork San Jacinto River; and from the Northwest through Stewart’s Creek and Mosswood Ditch, which outfalls to the West Fork San Jacinto River. The overall drainage sub-areas are shown in Exhibit 4. After modeling the overall drainage sub-areas over the terrain using XPSTORM/XPSWMM, three (3) high ponding areas were observed.

Ponding Area 1:

The area deemed as “Ponding Area 1” is located in the Northwestern region of The District, as shown in Exhibits 8, 9, & 10. This area was analyzed by further delineating sub-areas corresponding to the existing inlets and culverts of the existing drainage system described by the record drawings and site visits. The existing storm sewer layout for Ponding Area 1 is shown in Exhibit 5. Modeling reveals that various storm sewer components in the system are undersized, resulting in a high risk of potential localized flooding in Ponding Area 1. Inundations for the 10%, 1%, and 0.2% events are shown in Exhibits 8, 9, & 10.

Ponding Area 2:

The area deemed as “Ponding Area 2” is located in the central region of The District, as shown in Exhibits 8, 9, & 10. As with Ponding Area 1, Ponding Area 2 was analyzed by further delineating sub-areas corresponding to the existing inlets and culverts of the existing drainage system described by the record drawings and site visits. The existing storm sewer layout for Ponding Area 2 is shown in Exhibit 6. Modeling revealed that most of the localized flooding was a result of water backing up and spilling out of the inlets and culverts at various points within the area. It can be observed that the existing storm sewer layout is deficiently conveying stormwater runoff resulting in a high risk of potentially flooding during local storm events. Inundations for the 10%, 1%, and 0.2% events are shown in Exhibits 8, 9, & 10.

Ponding Area 3:

The area deemed as “Ponding Area 3” is located in the Eastern region of The District, as shown in Exhibits 8, 9, & 10. As with Ponding areas 1 and 2, Ponding Area 3 was analyzed by further delineating sub-areas corresponding to the existing inlets and culverts of the existing drainage system described by the record drawings and site visits. The existing storm sewer layout for Ponding Area 3 is shown in Exhibit 7. Stormwater overwhelms the existing storm sewer system causing localized flooding in the area. Results reveal that various residential lots

pose a high potential risk of localized flooding. Inundations for the 10%, 1%, and 0.2% events are shown in Exhibits 8, 9, & 10.

In all areas previously mentioned, the existing drainage system performs as needed to convey the 2-year storm event flows within The District. However, during the 10-year event and more severe events, overland flow overwhelms the existing system due to its limited conveyance capacity and the lack of detention basins. As a result, the severe rain events cause localized flooding conditions within natural depressions, especially in the specified areas of the Northwestern, Central, and Eastern regions of the River Plantation District. Exhibits 8, 9, & 10 show the inundations within the River Plantation District for the 10%, 1% and 0.2% AEP events, respectively.

The primary flooding concern for The District is due to regional flooding caused by the limited capacity of West Fork Jacinto River and the low natural ground elevations along its banks and within The District. During the extreme events, the West Fork San Jacinto River backs into its tributaries, including the East Ditch, Mosswood Ditch, and Stewart's Creek, causing overtopping of their banks. Exhibits 11, 12, & 13 show the inundations The District during regional 10%, 1%, and 0.2% AEP events, respectively.

2.1 Land Use

The existing land use within The District boundary consist of roadways/major thoroughfares, single-family residential homes, open space characterization, heavily wooded areas, recreational areas, municipal facilities, and water bodies.

2.2 Right-of ways, Pipelines, and Utilities

Various private and public utilities conflicting with the existing storm sewer system are located throughout The District boundary both within and outside the right-of-way. Some of the utilities located outside of the right-of-way do not have an easement.

2.3 FEMA Floodplain Information

The West Fork San Jacinto River watershed has studied limits to establish flood hazard zones due to riverine flooding by the Federal Emergency Management Agency (FEMA). The floodplain limits are described within the Flood Insurance Rate Maps (FIRMs) for the area. The District lies partially within the Federal Emergency Management Agency (FEMA) Zone AE (base flood elevations determined). The floodplain is shown on the FEMA FIRMs below:

- 48339C0390G dated 08/18/2014.
- 48339C0395G dated 08/18/2014.
- 48339C0530G dated 08/18/2014.
- 48339C0535G dated 08/14/2014.

The FEMA FIRMs were merged and are shown in Exhibit 3.

SECTION 3.0 – HYDROLOGY & HYDRAULICS

3.1 Analysis Objective

This report aims to document existing conditions during the 10-year, 100-year, and 500-year local rain events to identify natural depressions, storm sewer deficiencies, and conveyance capacities.

3.2 Digital Terrain Model (DTM)

The same Digital Terrain Model (DTM) was used to model the various storm event scenarios. The DTM developed utilized 2018 LiDAR.

3.3 Subsurface (1D) Model

The physical subsurface model (1D) was developed using the available record drawings for The District and field visits to verify some pipe sizes at particular locations. The flowlines provided were estimated based on multiple field visits, the DTM elevations, and record drawings.

3.4 Drainage Areas

The drainage area map included in this study was delineated manually using an overall Rain-On Grid model integrated with the developed DTM. The drainage area includes the entire District boundary and off-site drainage areas, as shown on Exhibit 4.

3.5 Hydrologic and Hydraulic Methodologies

Peak runoff rate and runoff hydrograph computations of existing conditions for the 10%, 1%, and 0.2% exceedance probability events (AEPs) used the Rational Method based on runoff coefficients, intensity, and sub-area acreages, as per the Montgomery County Drainage Criteria Manual.

3.5.1 Runoff Coefficient

The runoff coefficient represents the existing conditions per drainage sub-area and was obtained by using table 3.5.1 Runoff Coefficients from the Montgomery Country Drainage Criteria Manual.

TABLE 2.2 Rational Method Runoff Coefficients for 5-10 Year Frequency Storms

| Description of Area | Basin Slope < 1% | Basin Slope 1%-3.5% | Basin Slope 3.5%-5.5% |
|--------------------------------------------|---------------------|------------------------|--------------------------|
| Single-Family Residential Districts | | | |
| Lots greater than 1/2 acre | 0.30 | 0.35 | 0.40 |
| Lots 1/4 - 1/2 acre | 0.40 | 0.45 | 0.50 |
| Lots less than 1/4 acre | 0.50 | 0.55 | 0.60 |
| Multi-Family Residential Districts | 0.60 | 0.65 | 0.70 |
| Apartment Dwelling Areas | 0.75 | 0.80 | 0.85 |
| Business Districts | | | |
| Downtown | 0.85 | 0.87 | 0.90 |
| Neighborhood | 0.75 | 0.80 | 0.85 |
| Industrial Districts | | | |
| Light | 0.50 | 0.65 | 0.80 |
| Heavy | 0.60 | 0.75 | 0.90 |
| Railroad Yard Areas | 0.20 | 0.30 | 0.40 |
| Cemeteries | 0.10 | 0.18 | 0.25 |
| Playgrounds | 0.20 | 0.28 | 0.35 |
| Streets | | | |
| Asphalt | 0.80 | 0.80 | 0.80 |
| Concrete | 0.85 | 0.85 | 0.85 |
| Concrete Drives and Walks | 0.85 | 0.85 | 0.85 |
| Roofs | 0.85 | 0.85 | 0.85 |
| Lawn Areas | | | |
| Sandy Soil | 0.05 | 0.08 | 0.12 |
| Clay Soil | 0.15 | 0.18 | 0.22 |
| Woodlands | | | |
| Sandy Soil | 0.15 | 0.18 | 0.25 |
| Clay Soil | 0.18 | 0.20 | 0.30 |
| Pasture | | | |
| Sandy Soil | 0.25 | 0.35 | 0.40 |
| Clay Soil | 0.30 | 0.40 | 0.50 |
| Cultivated | | | |
| Sandy Soil | 0.30 | 0.55 | 0.70 |
| Clay Soil | 0.35 | 0.60 | 0.80 |

Table 3.5.1 Runoff Coefficients

3.5.2 Time of Concentration

The time of concentration was calculated for each sub-drainage area using the combination of the inlet time and the travel time in a conduit, channel, or overland as per the Montgomery County Drainage Criteria Manual. The components in calculating the time of concentration are the longest flow path, land use, slope, and velocity. The 2-year, 24-hour duration, precipitation depth (4.89in), as seen in the National Oceanic and Atmospheric Administration Atlas 14 (NOAA Atlas 14) table 3.5.4, which specifies precipitation depth for the subject region of study, was utilized when calculating the time of concentration, as per equation 2.3 of the Montgomery County Drainage Criteria Manual.

3.5.3 Intensity

As per the Montgomery County Drainage Criteria Manual, intensity duration frequency (IDF curves) were used to obtain rainfall intensity per sub-area (Figures 3.5.3 & 3.5.3.1). The design rainfall duration was set equal to the time of concentration for all portions of the drainage sub-areas under consideration that contribute flow to the point of interest. The IDF curves did not include the 0.2% AEP event, therefore, NOAA Atlas 14 precipitation intensity values were utilized or interpolated based on the sub-areas' time of concentration (Figure 3.5.3.2).

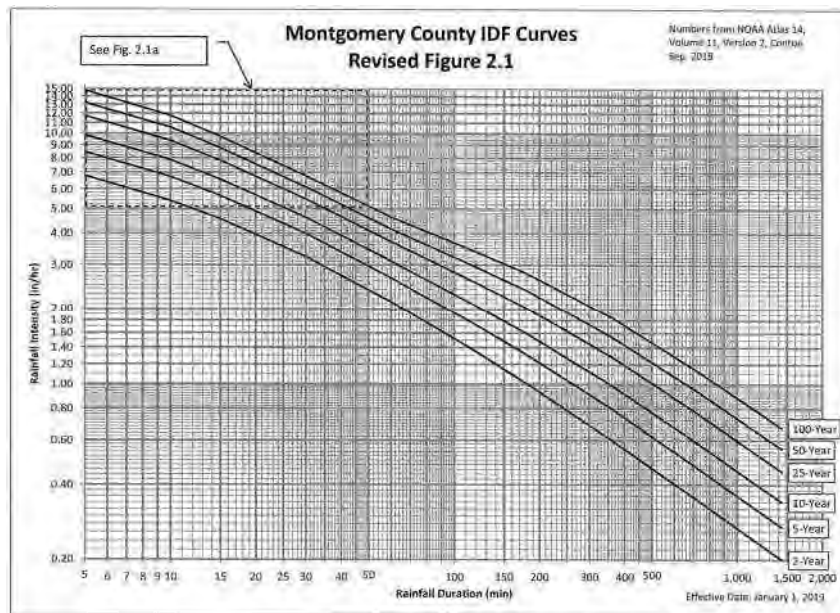


Table 3.5.3

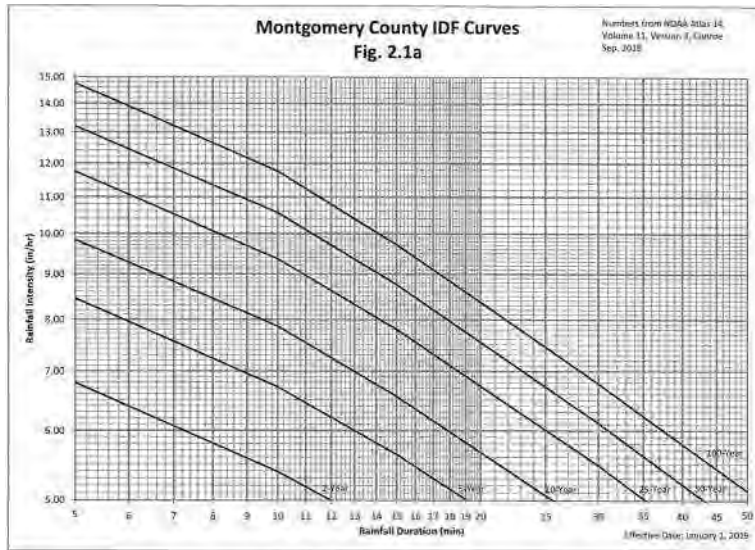


Table 3.5.3.1

NOAA Atlas 14, Volume 11, Version 2
Location name: Conroe, Texas, USA*
Latitude: 30.2536°, Longitude: -95.4413°
Elevation: 120 ft**
*source: ESRI Mapx
**source: USGS

POINT PRECIPITATION FREQUENCY ESTIMATES

Sergio Parica, Sandra Pavlovic, Michael St. Laurent, Carl Tryppel, Dale Ulrich, Citlar White
NOAA, National Weather Service, Silver Spring, Maryland
[PF_tutorial](#) | [PF_graphical](#) | [Maps_4_gisusers](#)

PF tabular

PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches/hour)¹



| Duration | Average recurrence interval (years) | | | | | | | | | |
|----------|-------------------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|
| | 1 | 2 | 5 | 10 | 25 | 50 | 100 | 200 | 500 | 1000 |
| 5-min | 5.83 (4.42-7.70) | 6.88 (5.24-9.16) | 8.54 (6.80-11.2) | 9.95 (7.46-13.2) | 11.9 (8.61-16.3) | 13.4 (9.46-18.9) | 14.9 (10.9-21.6) | 16.5 (11.1-24.6) | 18.7 (12.1-28.8) | 20.4 (12.9-32.9) |
| 10-min | 4.62 (3.50-6.10) | 5.45 (4.15-7.32) | 6.80 (5.16-8.93) | 7.93 (5.95-10.6) | 9.49 (6.91-13.0) | 10.7 (7.68-15.1) | 11.9 (8.21-17.3) | 13.1 (8.81-19.5) | 14.7 (9.55-22.6) | 15.9 (10.0-26.1) |
| 15-min | 3.92 (2.96-5.18) | 4.60 (3.51-6.01) | 5.70 (4.34-7.49) | 6.62 (4.97-8.82) | 7.89 (5.75-10.8) | 8.88 (6.29-12.5) | 9.84 (6.79-14.3) | 10.9 (7.32-16.2) | 12.3 (8.06-19.0) | 13.4 (8.50-21.2) |
| 30-min | 2.80 (2.12-3.70) | 3.27 (2.50-4.28) | 4.04 (3.06-5.31) | 4.67 (3.50-6.22) | 5.53 (4.01-7.57) | 6.18 (4.36-8.70) | 6.88 (4.73-9.94) | 7.61 (5.12-11.3) | 8.70 (5.62-13.4) | 9.59 (6.07-15.2) |
| 60-min | 1.84 (1.39-2.43) | 2.17 (1.66-2.83) | 2.70 (2.06-3.54) | 3.14 (2.36-4.16) | 3.75 (2.72-5.18) | 4.21 (2.97-5.92) | 4.70 (3.24-6.62) | 5.27 (3.55-7.86) | 6.12 (3.96-9.46) | 6.84 (4.33-10.8) |
| 2-hr | 1.11 (0.847-1.46) | 1.36 (1.03-1.78) | 1.74 (1.33-2.27) | 2.08 (1.57-2.79) | 2.57 (1.88-3.51) | 2.97 (2.11-4.19) | 3.42 (2.36-4.93) | 3.94 (2.65-5.83) | 4.72 (3.07-7.25) | 5.38 (3.42-8.47) |
| 3-hr | 0.811 (0.618-1.06) | 1.02 (0.768-1.29) | 1.33 (1.01-1.72) | 1.61 (1.22-2.13) | 2.04 (1.50-2.79) | 2.40 (1.71-3.37) | 2.81 (1.95-4.05) | 3.29 (2.22-4.86) | 4.01 (2.62-6.14) | 4.62 (2.94-7.25) |
| 6-hr | 0.466 (0.356-0.611) | 0.611 (0.453-0.794) | 0.811 (0.607-1.04) | 1.01 (0.768-1.32) | 1.31 (0.985-1.78) | 1.67 (1.13-2.20) | 1.87 (1.31-2.65) | 2.22 (1.51-3.27) | 2.75 (1.80-4.20) | 3.20 (2.04-5.00) |
| 12-hr | 0.265 (0.204-0.345) | 0.353 (0.269-0.430) | 0.474 (0.364-0.606) | 0.596 (0.454-0.780) | 0.783 (0.582-1.07) | 0.952 (0.688-1.33) | 1.16 (0.803-1.64) | 1.37 (0.932-2.01) | 1.71 (1.12-2.60) | 1.99 (1.26-3.10) |
| 24-hr | 0.150 (0.116-0.194) | 0.203 (0.151-0.244) | 0.275 (0.212-0.350) | 0.348 (0.266-0.454) | 0.462 (0.346-0.625) | 0.666 (0.412-0.992) | 0.887 (0.465-0.978) | 0.822 (0.561-1.20) | 1.02 (0.673-1.54) | 1.19 (0.764-1.84) |
| 2-day | 0.082 (0.064-0.108) | 0.114 (0.084-0.125) | 0.166 (0.121-0.197) | 0.199 (0.153-0.250) | 0.267 (0.202-0.384) | 0.331 (0.243-0.462) | 0.403 (0.284-0.572) | 0.480 (0.328-0.695) | 0.588 (0.396-0.884) | 0.674 (0.436-1.04) |
| 3-day | 0.059 (0.046-0.076) | 0.082 (0.061-0.097) | 0.112 (0.087-0.142) | 0.143 (0.111-0.186) | 0.192 (0.136-0.261) | 0.238 (0.175-0.332) | 0.289 (0.204-0.409) | 0.342 (0.234-0.495) | 0.415 (0.273-0.625) | 0.474 (0.306-0.731) |
| 4-day | 0.048 (0.037-0.061) | 0.065 (0.049-0.078) | 0.089 (0.070-0.113) | 0.114 (0.088-0.147) | 0.151 (0.115-0.205) | 0.186 (0.137-0.253) | 0.225 (0.159-0.311) | 0.265 (0.180-0.382) | 0.320 (0.212-0.485) | 0.364 (0.238-0.561) |
| 7-day | 0.032 (0.025-0.041) | 0.043 (0.033-0.052) | 0.068 (0.046-0.073) | 0.072 (0.055-0.093) | 0.094 (0.071-0.127) | 0.114 (0.084-0.157) | 0.136 (0.096-0.191) | 0.158 (0.103-0.228) | 0.190 (0.126-0.284) | 0.215 (0.146-0.321) |
| 10-day | 0.026 (0.020-0.032) | 0.033 (0.025-0.040) | 0.044 (0.034-0.055) | 0.054 (0.042-0.076) | 0.070 (0.053-0.094) | 0.084 (0.062-0.115) | 0.099 (0.073-0.156) | 0.115 (0.079-0.165) | 0.137 (0.091-0.204) | 0.164 (0.104-0.237) |
| 20-day | 0.017 (0.013-0.021) | 0.021 (0.016-0.026) | 0.027 (0.021-0.034) | 0.032 (0.023-0.042) | 0.041 (0.031-0.054) | 0.047 (0.036-0.065) | 0.054 (0.039-0.076) | 0.062 (0.043-0.089) | 0.073 (0.049-0.109) | 0.082 (0.053-0.123) |
| 30-day | 0.013 (0.010-0.017) | 0.016 (0.013-0.020) | 0.021 (0.016-0.026) | 0.024 (0.019-0.032) | 0.030 (0.023-0.040) | 0.034 (0.026-0.047) | 0.039 (0.029-0.055) | 0.044 (0.031-0.063) | 0.051 (0.034-0.076) | 0.057 (0.037-0.087) |
| 45-day | 0.011 (0.009-0.014) | 0.013 (0.010-0.016) | 0.016 (0.013-0.021) | 0.019 (0.015-0.025) | 0.023 (0.017-0.030) | 0.026 (0.019-0.035) | 0.029 (0.021-0.041) | 0.032 (0.022-0.046) | 0.037 (0.025-0.054) | 0.040 (0.029-0.058) |
| 60-day | 0.010 (0.009-0.012) | 0.011 (0.009-0.014) | 0.014 (0.011-0.018) | 0.016 (0.013-0.021) | 0.019 (0.014-0.026) | 0.022 (0.016-0.030) | 0.024 (0.017-0.033) | 0.027 (0.019-0.037) | 0.029 (0.020-0.043) | 0.031 (0.020-0.048) |

¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS). Numbers in parentheses are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

Table 3.5.3.2

3.5.4 Precipitation

To reflect the most up to date Atlas 14 data, the precipitation was considered for each sub-area using the NOAA Atlas 14 database. Table 3.5.4 summarizes the point rainfall depths for various AEP events. These depths were utilized to obtain volumes per rain event per drainage sub-area.

NOAA Atlas 14, Volume 11, Version 2
Location name: Conroe, Texas, USA*
Latitude: 30.2536°, Longitude: -95.4413°
Elevation: m/ft**
* source: ESRI Maps
 ** source: USGS

POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sandra Pavlovic, Michael St. Laurent, Carl Tryppaluk, Dale Ururah, Orlan Wihle
 NOAA, National Weather Service, Silver Spring, Maryland

[PF tabular](#) | [PF graphical](#) | [Maps & aerials](#)

PF tabular

| Duration | Average recurrence interval (years) | | | | | | | | | |
|----------|-------------------------------------|------------------------|------------------------|-----------------------|-----------------------|----------------------|----------------------|----------------------|---------------------|---------------------|
| | 1 | 2 | 5 | 10 | 25 | 50 | 100 | 200 | 500 | 1000 |
| 5-min | 0.486 (0.368-0.642) | 0.672 (0.437-0.747) | 0.712 (0.542-0.935) | 0.829 (0.622-1.10) | 0.990 (0.719-1.36) | 1.11 (0.788-1.57) | 1.24 (0.655-1.80) | 1.37 (0.924-2.05) | 1.56 (1.01-2.40) | 1.70 (1.08-2.69) |
| 10-min | 0.770 (0.583-1.02) | 0.908 (0.693-1.19) | 1.13 (0.863-1.49) | 1.32 (0.991-1.75) | 1.58 (1.15-2.17) | 1.78 (1.26-2.52) | 1.99 (1.37-2.88) | 2.19 (1.47-3.25) | 2.45 (1.59-3.77) | 2.64 (1.67-4.18) |
| 15-min | 0.979 (0.741-1.29) | 1.15 (0.876-1.50) | 1.43 (1.09-1.87) | 1.66 (1.24-2.21) | 1.97 (1.43-2.70) | 2.21 (1.57-3.12) | 2.46 (1.70-3.57) | 2.72 (1.83-4.05) | 3.08 (2.00-4.74) | 3.36 (2.12-5.30) |
| 30-min | 1.40 (1.06-1.85) | 1.64 (1.25-2.14) | 2.02 (1.54-2.65) | 2.34 (1.75-3.11) | 2.77 (2.00-3.78) | 3.09 (2.18-4.35) | 3.43 (2.36-4.97) | 3.81 (2.53-5.67) | 4.35 (2.83-6.71) | 4.80 (3.04-7.58) |
| 60-min | 1.84 (1.39-2.43) | 2.17 (1.66-2.83) | 2.70 (2.06-3.54) | 3.14 (2.36-4.18) | 3.75 (2.72-5.13) | 4.21 (2.97-5.92) | 4.70 (3.24-6.82) | 5.27 (3.50-7.56) | 6.12 (3.98-9.46) | 6.84 (4.33-10.8) |
| 2-hr | 2.23 (1.70-2.93) | 2.73 (2.07-3.49) | 3.49 (2.66-4.54) | 4.16 (3.14-5.52) | 5.15 (3.75-7.03) | 5.94 (4.22-8.35) | 6.83 (4.73-9.85) | 7.87 (5.31-11.7) | 9.43 (6.15-14.5) | 10.8 (6.84-16.9) |
| 3-hr | 2.44 (1.86-3.29) | 3.07 (2.31-3.87) | 3.99 (3.04-5.17) | 4.85 (3.66-6.41) | 6.13 (4.49-8.37) | 7.21 (5.14-10.1) | 8.44 (5.86-12.2) | 9.87 (6.57-14.6) | 12.0 (7.55-18.5) | 13.9 (8.63-21.8) |
| 6-hr | 2.80 (2.15-3.66) | 3.66 (2.73-4.82) | 4.86 (3.72-6.25) | 6.03 (4.58-7.94) | 7.82 (5.78-10.7) | 9.40 (6.76-13.2) | 11.2 (7.82-16.1) | 13.3 (9.02-19.6) | 16.5 (10.6-25.2) | 19.2 (12.2-30.0) |
| 12-hr | 3.20 (2.46-4.16) | 4.26 (3.17-5.19) | 5.72 (4.40-7.31) | 7.17 (5.47-9.40) | 9.44 (7.02-12.9) | 11.5 (8.30-16.1) | 13.8 (9.68-19.8) | 16.5 (11.2-24.2) | 20.6 (13.5-31.3) | 24.0 (15.4-37.4) |
| 24-hr | 3.61 (2.79-4.67) | 4.89 (3.63-5.88) | 6.61 (5.10-8.40) | 8.38 (6.40-10.9) | 11.1 (8.32-15.1) | 13.6 (9.90-19.0) | 16.5 (11.6-23.5) | 19.7 (13.5-28.8) | 24.5 (15.2-37.1) | 28.5 (18.3-44.2) |
| 2-day | 3.98 (3.09-5.13) | 5.50 (4.08-6.53) | 7.51 (5.82-9.49) | 9.68 (7.37-12.4) | 12.9 (9.72-17.5) | 15.9 (11.7-22.2) | 19.4 (13.7-27.5) | 23.1 (15.8-33.4) | 28.2 (18.7-42.5) | 32.4 (20.9-50.1) |
| 3-day | 4.29 (3.34-5.61) | 5.93 (4.42-7.04) | 8.13 (6.31-10.2) | 10.4 (8.00-13.4) | 13.9 (10.5-18.9) | 17.2 (12.6-23.9) | 20.9 (14.8-29.5) | 24.7 (16.9-35.6) | 29.9 (19.8-44.9) | 34.1 (22.1-52.7) |
| 4-day | 4.62 (3.60-5.91) | 6.32 (4.74-7.53) | 8.64 (6.73-10.9) | 11.0 (8.47-14.2) | 14.6 (11.1-19.7) | 17.9 (13.2-24.9) | 21.6 (15.3-30.5) | 25.5 (17.5-36.7) | 30.8 (20.4-46.1) | 35.0 (22.7-53.9) |
| 7-day | 5.51 (4.32-7.03) | 7.28 (5.56-6.78) | 9.78 (7.66-12.3) | 12.2 (9.46-15.7) | 15.9 (12.1-21.4) | 19.2 (14.1-26.5) | 22.9 (16.3-32.1) | 26.7 (18.4-38.4) | 32.0 (21.3-47.8) | 36.2 (23.6-55.6) |
| 10-day | 6.24 (4.90-7.95) | 8.07 (6.21-9.86) | 10.7 (8.40-13.4) | 13.2 (10.2-16.9) | 16.9 (12.8-22.6) | 20.2 (14.9-27.8) | 23.8 (17.0-33.4) | 27.6 (19.1-39.7) | 32.9 (22.3-48.1) | 37.2 (24.2-56.9) |
| 20-day | 8.27 (6.52-10.5) | 10.2 (8.01-12.6) | 13.2 (10.4-16.5) | 15.8 (12.4-20.2) | 19.7 (14.9-26.1) | 22.9 (16.9-31.2) | 26.4 (18.9-36.9) | 30.1 (20.9-43.1) | 35.3 (23.7-52.5) | 39.5 (25.9-60.3) |
| 30-day | 9.96 (7.87-12.6) | 12.0 (9.51-14.9) | 15.2 (12.1-19.1) | 18.0 (14.1-22.9) | 22.0 (16.7-28.9) | 25.2 (18.5-34.1) | 28.5 (20.4-39.7) | 32.2 (22.4-46.0) | 37.2 (25.1-53.2) | 41.3 (27.1-62.9) |
| 45-day | 12.5 (9.50-15.7) | 14.7 (11.8-18.3) | 18.3 (14.6-23.0) | 21.3 (16.8-27.1) | 25.5 (19.4-33.4) | 28.7 (21.2-38.7) | 32.0 (23.0-44.4) | 35.4 (24.8-50.5) | 40.1 (27.0-55.3) | 43.7 (28.7-66.4) |
| 60-day | 14.8 (11.7-18.6) | 17.2 (13.6-21.3) | 21.2 (17.0-26.5) | 24.2 (19.2-31.0) | 28.8 (21.9-37.6) | 32.0 (23.7-43.1) | 35.2 (25.3-48.7) | 38.4 (26.9-54.7) | 42.6 (28.6-62.9) | 45.8 (30.1-69.4) |

1 Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS). Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.
 Please refer to NOAA Atlas 14 document for more information.

Table 3.5.4

3.5.5 Small Watershed Hydrograph Development

The Malcom, H.R Small Watershed Hydrograph Method was used to develop curvilinear design hydrographs for each drainage sub-area within the study limits. The assigned hydrograph peaks at a designated flow rate, obtained using the rational formula, and contains a runoff volume consistent with the design rainfall as updated by NOAA Atlas 14. The precipitation depths for the 10-year, 100-year, and 500-year, 24-hour duration, AEP storm events are provided in Table 3.5.4.

3.6 Hydrologic and Hydraulic Analysis

3.6.1 Hydrologic Analysis

Th District's overall drainage area was divided into smaller subareas based on overland drainage patterns and offsite flow. Each sub-area represents the area contributing flow at a specific point of interest and are shown in Exhibit 4. Each subarea was then assigned a specific hydrograph (Appendix A) to model the existing overland conditions more accurately. Once the drainage patterns were analyzed, VSE focused on areas portraying a high potential flood risk. A more detailed model consisting of an integrated 1D subsurface network with a 2D DTM was created and analyzed for the high ponding areas.

3.6.2 Hydraulic Analysis

A XPSTORM/XPSWMM 1D/2D integrated model was developed to analyze The District. The storm sewer pipes are modeled as links while manholes and inlets are modeled as nodes. The District's network consists of inlets, storm sewer pipes, and drainage swales. The DTM acknowledged the drainage swales and were therefore integrated in the 2D portion of the model. The elevations used in the model are obtained from the 2018 LiDAR DTM and record drawings. The overall drainage pattern for Th District was first modeled using a rain-on-grid method, which involves directly applying a rainfall hydrograph to the DTM, which resulted in obtaining the overland flow pattern of The District. The District drainage boundary was then delineated into sub-drainage areas allowing for rain and area-specific hydrographs to be developed and applied as rain-on-grid over each drainage sub-areas for a more accurate representation of drainage within The District. Once the high ponding areas were identified, separate 1D/2D integrated models were created for each high ponding area. These models further broke down each high ponding area by applying rain and area-specific hydrographs to inlets which allowed for the models to account for infiltration and dynamically connect the

underground stormwater drainage network and the DTM. The integrated 1D/2D models were utilized to portray the most accurate representation of local inundation within each of the designated high ponding areas and can be observed in Exhibits 8, 9, & 10.

SECTION 4.0 – SUMMARY & CONCLUSION

In general, the lack of conveyance capacity, whether due to undersized storm sewers or the condition of the existing storm sewers plus the lack of detention, are some of the factors that cause localized flooding within The District. VSE's analysis concludes that the following designated high ponding areas are the main areas of concern for local storm event flooding within The District.

Ponding Area 1:

This area is located in the Northwestern region of The District. After analyzing the area, modeling by use of XPSTORM/XPSWMM revealed that the existing storm sewer system lacks the capacity to convey the contributing stormwater runoff, as seen in Exhibits 8, 9, & 10. The first step in possibly resolving the local flooding issues of this area would be to explore the possibility of implementing a detention pond in place of the existing amenity pond within the abandoned portion of the golf course and upsizing various storm sewer pipes. The potential areas to be explored for improvements are highlighted in Exhibit 17. This recommendation should not be utilized for anything other than preliminary design discussions.

Ponding Area 2:

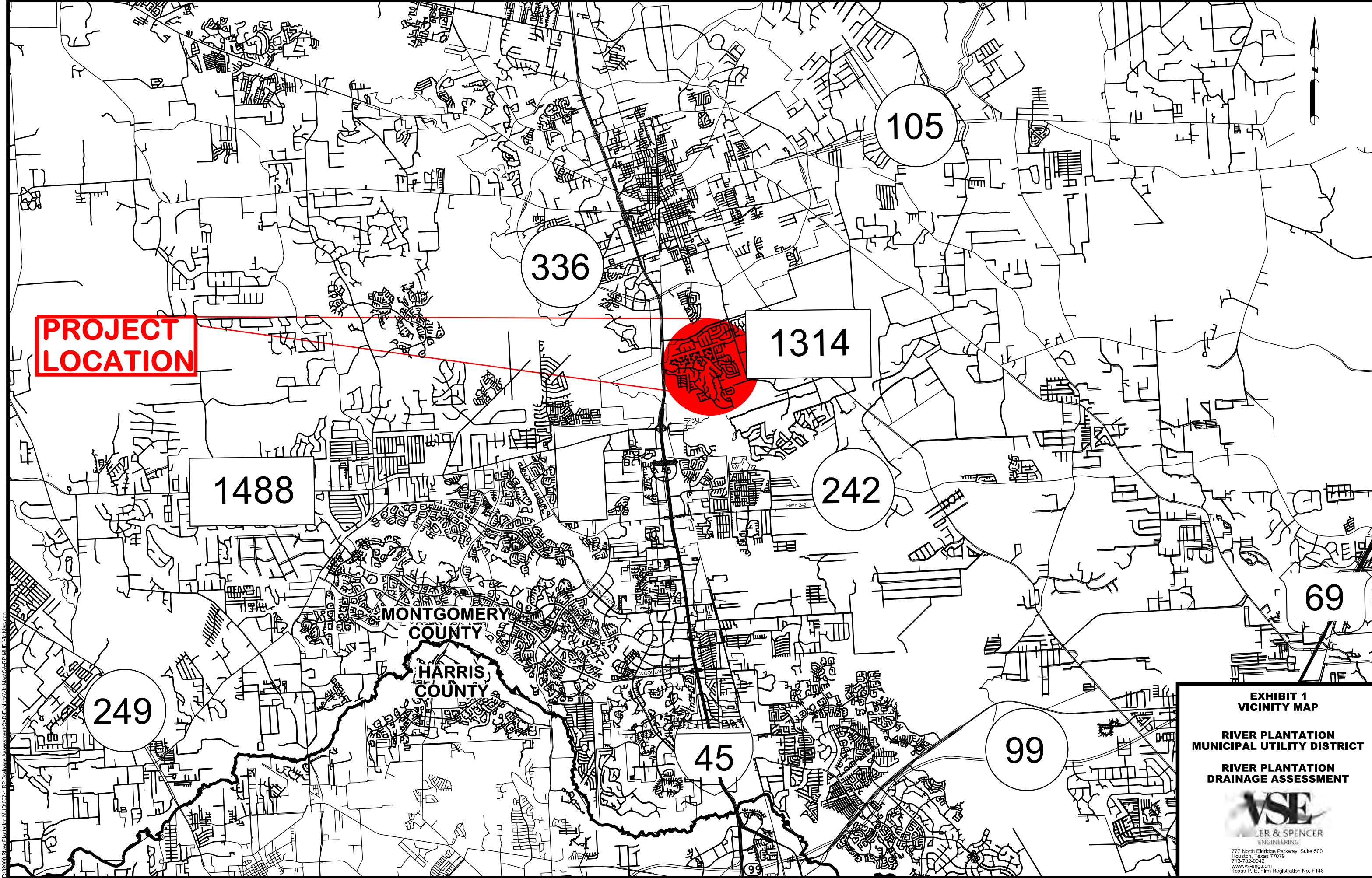
The subject area is located in the central region of The District. Upon analyzing the area, assumptions were made regarding the existing storm sewer network's pipe sizes and swale slopes. The most conservative approach was taken. Modeling by use of XPSMM/XPSTORM revealed that the upstream portions of the network within the area lack the capacity to convey runoff efficiently, causing localized flooding in the area, seen in Exhibits 8, 9, & 10. A potential solution would be to investigate utilizing the existing wooded areas on both sides of River Plantation Drive, just South and Southeast of the intersection of River Plantation Drive and Robert E. Lee Drive, for detention purposes during the localized extreme rain events. The potential detention basin locations are highlighted in Exhibit 18. Exploration of this solution would be to determine if the overwhelming runoff could be routed to the potential detention basins and if the potential detention basin areas would provide enough storage to achieve a positive impact to the localized flooding within the subject region. This recommendation should not be utilized for anything other than preliminary design discussions.

Ponding Area 3:

The area is located in the Eastern region of the District. It can be observed that the existing drainage network is overwhelmed, and the existing amenity pond overtops its banks causing localized flooding in the area, as seen in Exhibits 8, 9, & 10. After analyzing the drainage network, it was determined that the existing weir structure does not provide enough capacity to restrict the amenity pond's water surface to reside within its banks. Potential solutions to positively impact the localized flooding would be to further analyze the existing weir structure and investigate reconstruction to increase its capacity, increasing the outlet's pipe size, or excavation of an extreme event overflow swale that routes the overflow safely and provides temporary detention during the localized extreme rain events. The areas of potential improvements are highlighted in Exhibit 19. This recommendation should not be utilized for anything other than preliminary design discussions.

EXHIBITS

EXHIBIT 1
Vicinity Map



**PROJECT
LOCATION**

336

105

1314

1488

242

69

MONTGOMERY
COUNTY
HARRIS
COUNTY

249

45

99

**EXHIBIT 1
VICINITY MAP**

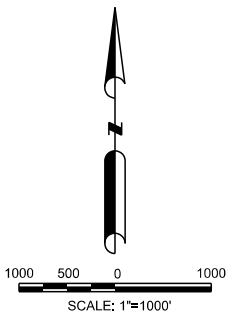
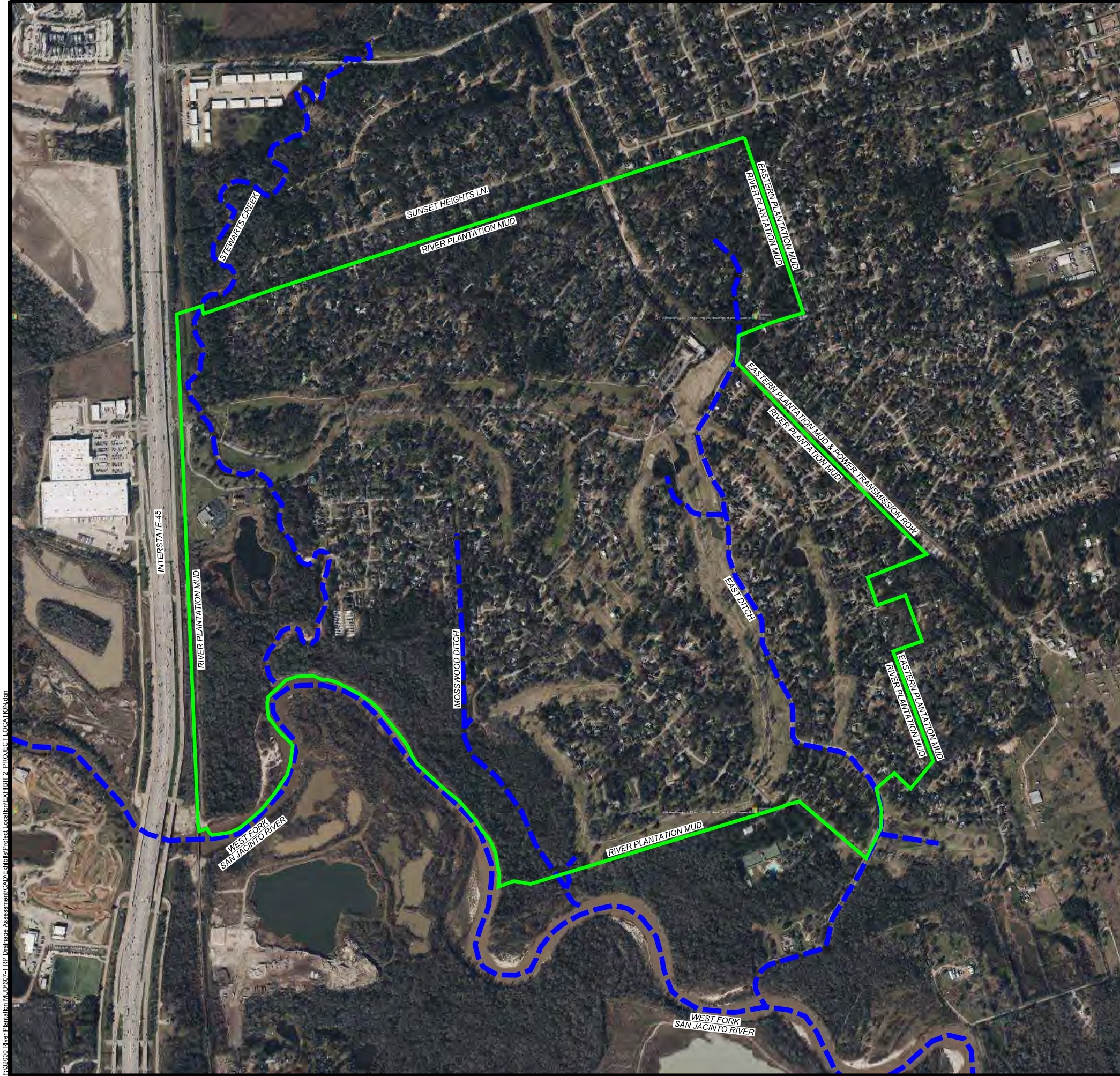
**RIVER PLANTATION
MUNICIPAL UTILITY DISTRICT**

**RIVER PLANTATION
DRAINAGE ASSESSMENT**



777 North Eldridge Parkway, Suite 500
Houston, Texas 77079
713-782-0042
www.vse-eng.com
Texas P. E. Firm Registration No. F148

EXHIBIT 2
Project Location



LEGEND

- MUD BOUNDARY
- - - CHANNEL FLOWLINE

**EXHIBIT 2
PROJECT LOCATION**

**RIVER PLANTATION
MUNICIPAL UTILITY DISTRICT**

**RIVER PLANTATION
DRAINAGE ASSESSMENT**



777 North Eldridge Parkway, Suite 500
Houston, Texas 77079
713-782-0042
www.vse-eng.com
Texas P. E. Firm Registration No. F148

2/1/2024 9:58:40 AM
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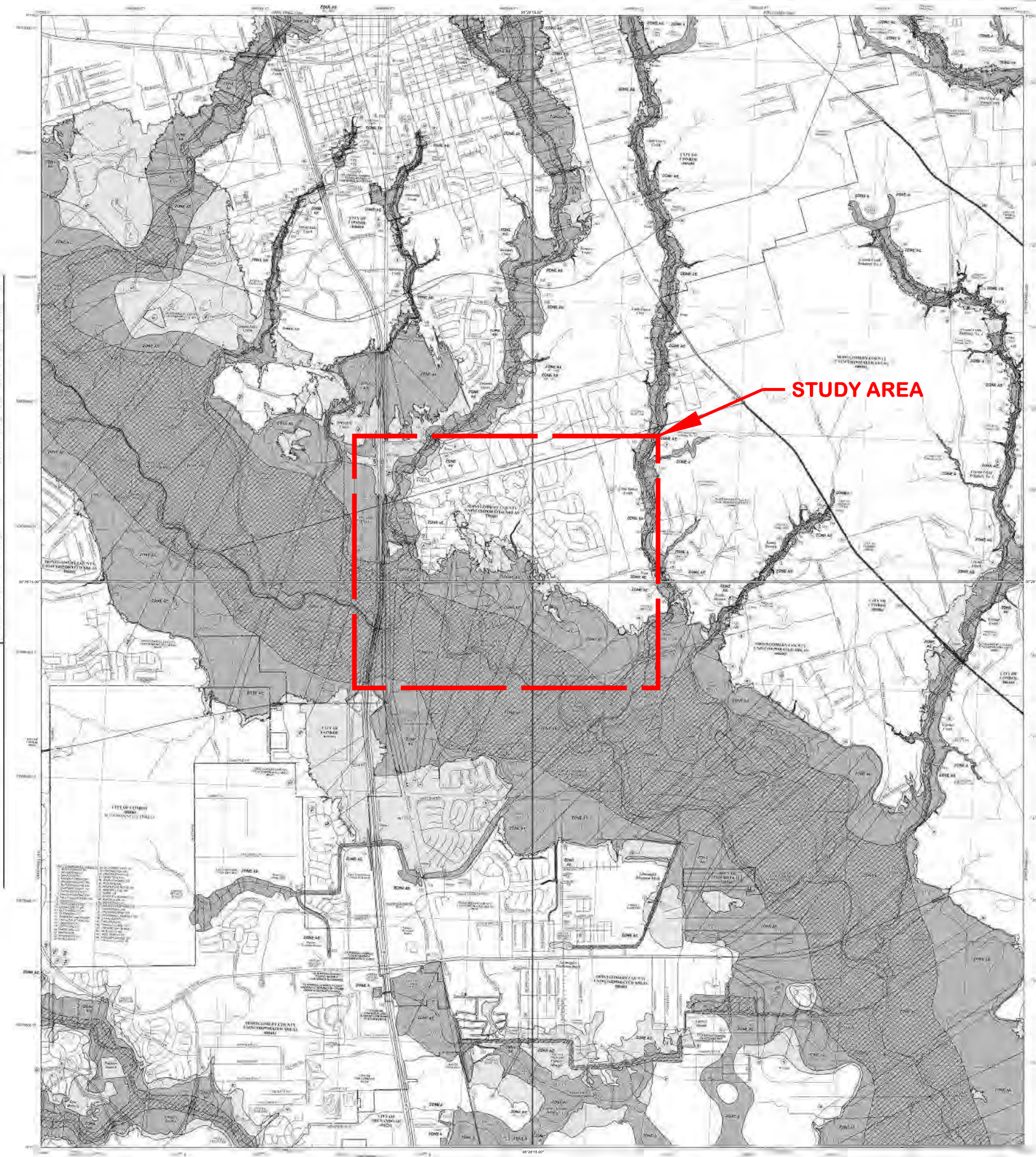
EXHIBIT 3
FEMA FIRMS



NOTES TO USERS

This map was prepared for the purpose of determining flood insurance rates for the River Plantation Municipal Utility District. The map is based on the best available data and is not intended to be used for any other purpose. The map is not a warranty of any kind and does not constitute an offer of insurance. The map is subject to change without notice and is not to be used as a basis for any legal action.

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STUDY AREA

LEGEND

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|----------|-----------|
| [Symbol] | Zone A1 |
| [Symbol] | Zone A2 |
| [Symbol] | Zone A3 |
| [Symbol] | Zone A4 |
| [Symbol] | Zone A5 |
| [Symbol] | Zone A6 |
| [Symbol] | Zone A7 |
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| [Symbol] | Zone A9 |
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| [Symbol] | Zone A11 |
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| [Symbol] | Zone A98 |
| [Symbol] | Zone A99 |
| [Symbol] | Zone A100 |

FIRM
FLOOD INSURANCE RATE MAP
MONTGOMERY COUNTY
TEXAS
ANFVCS08080501A.FIRM

PANEL 0000

MAP NUMBER: 401000000
 MAP REVISED: AUGUST 18, 2014

12/28/2023 11:23:15 AM ER20000 River Plantation MUD 6/7/21 RE: Drainage Assessment CAD/John Smith/FEMA FIRM/EXHIBIT 3 - FEMA FIRM/Revision

EXHIBIT 3
FEMA FIRMs

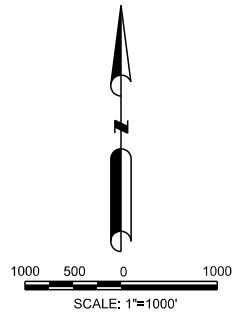
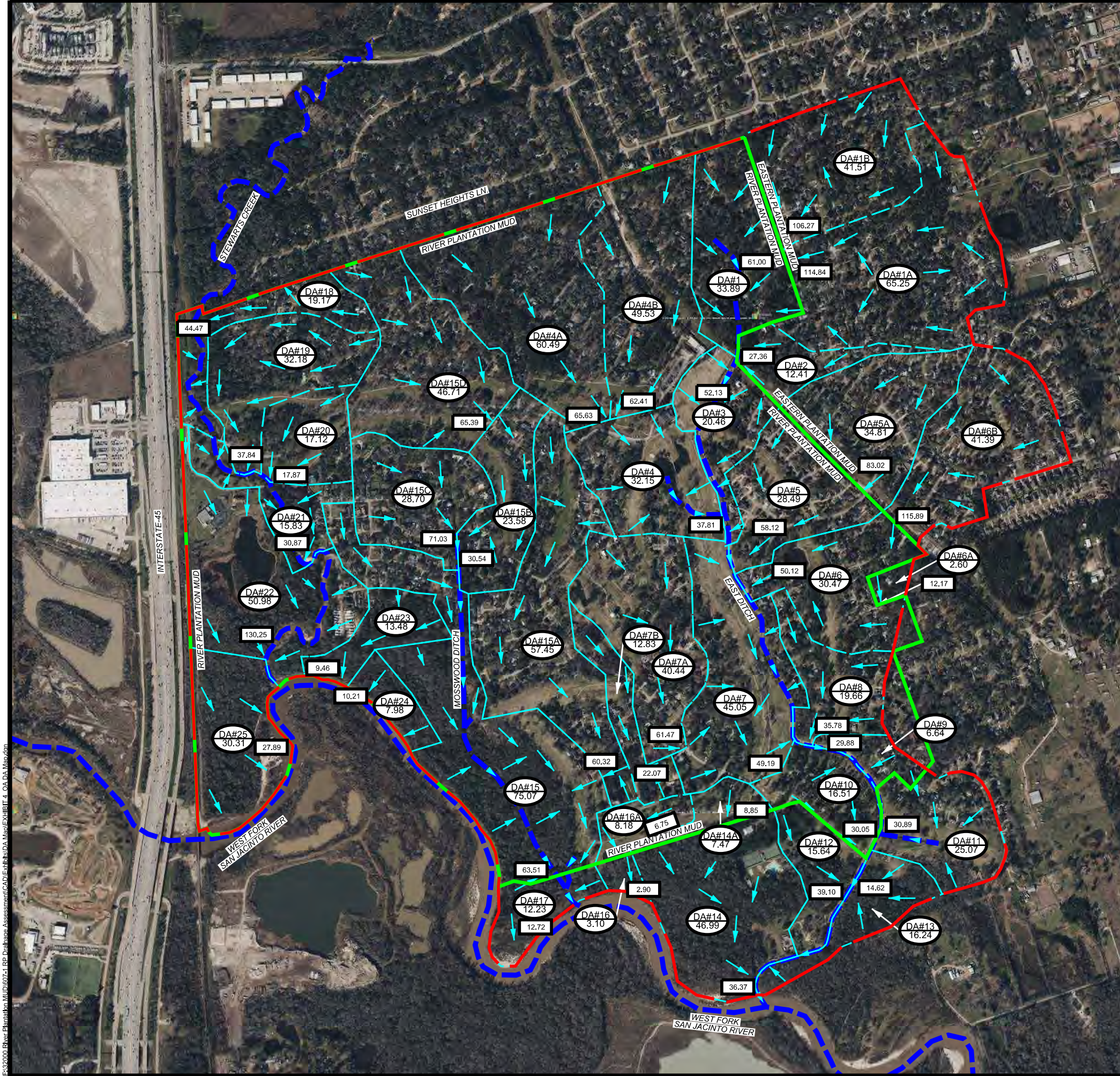
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EXHIBIT 4
Overall Existing Drainage Area Map



LEGEND

- 96 EXIST. CONTOUR LINE
- DRAINAGE AREA LIMITS
- DRAINAGE SUBAREA ID
DRAINAGE SUBAREA (AC)
- DRAINAGE AREA'S PEAK
100-YR FLOW RATE (CFS)
- SHEET FLOW
- MUD BOUNDARY
- CHANNEL FLOWLINE
- OVERALL DRAINAGE AREA

**EXHIBIT 4
OVERALL EXISTING DRAINAGE
AREA MAP**

**RIVER PLANTATION
MUNICIPAL UTILITY DISTRICT**

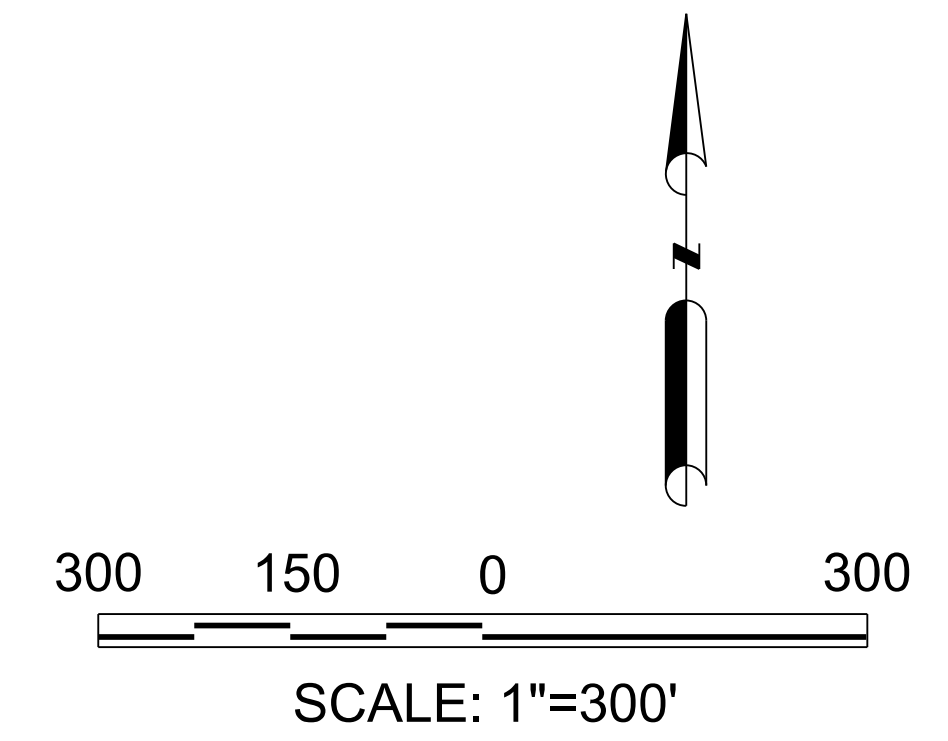
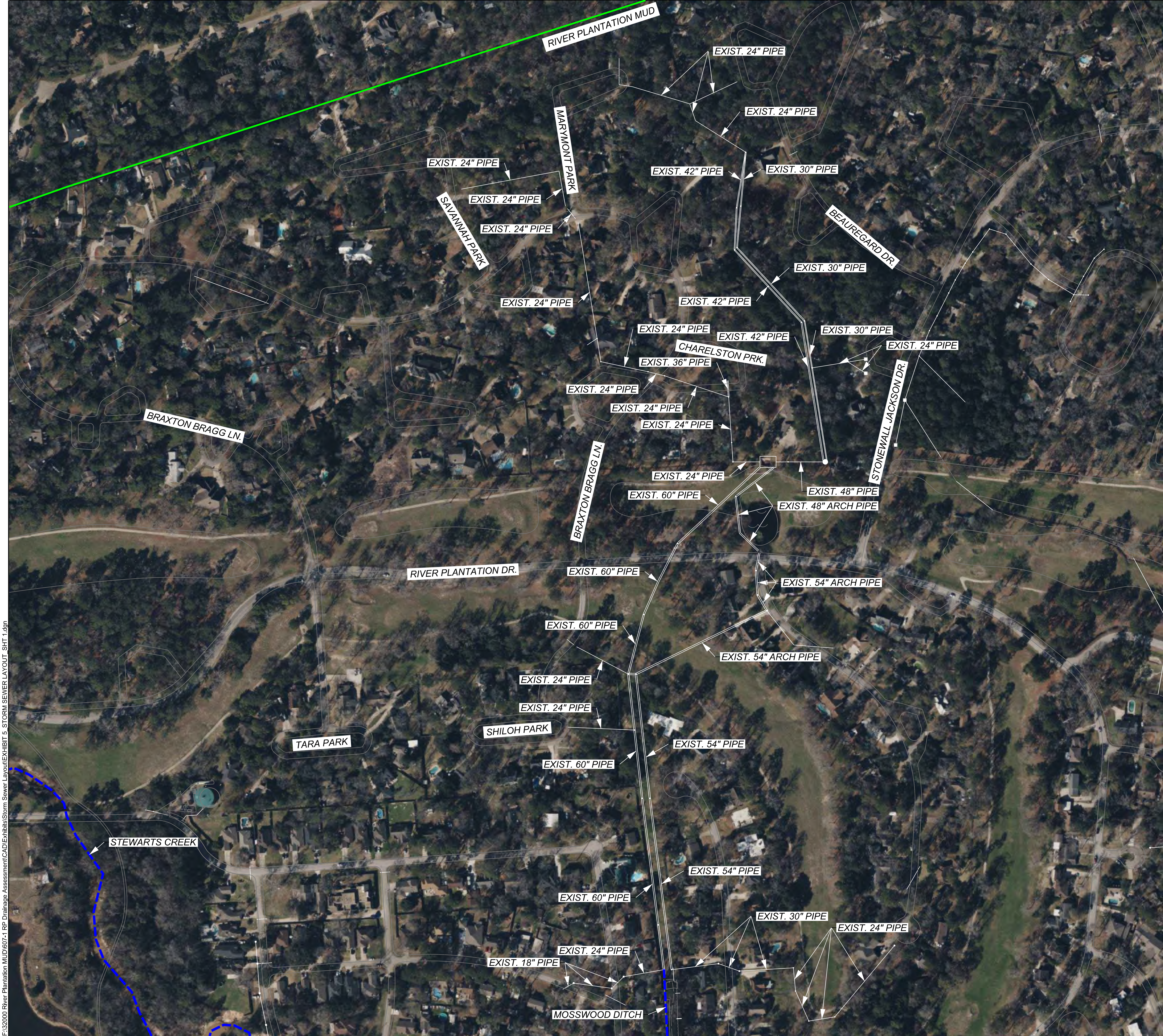
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 FR320000 River Plantation MUD 06/21 RE Drainage Assessment CAD/Exhibit 4 OA DA Map.dwg
 LukeV

EXHIBIT 5
Existing Storm Sewer Layout (1 of 3)



LEGEND

-  96 EXIST.CONTOUR LINE
-  MUD BOUNDARY
-  OVERALL DRAINAGE AREA
-  EXIST.STORM SEWER, MANHOLE & INLETS
-  CHANNEL FLOWLINE

**EXHIBIT 5
EXISTING STORM SEWER LAYOUT
(1 OF 3)**

**RIVER PLANTATION
MUNICIPAL UTILITY DISTRICT**

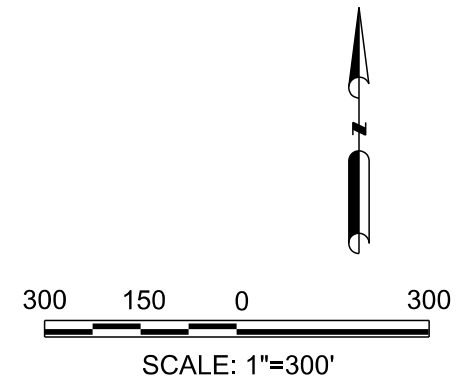
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Luke V 2/1/2024 10:14:49 AM F:\32000 River Plantation MUD\607-1 RP Drainage Assessment\CAD\Exhibits\Storm Sewer Layout\EXHIBIT 5 STORM SEWER LAYOUT_SHT1.dgn

EXHIBIT 6
Existing Storm Sewer Layout (2 of 3)



LEGEND

-  96 EXIST.CONTOUR LINE
-  MUD BOUNDARY
-  OVERALL DRAINAGE AREA
-  EXIST.STORM SEWER, MANHOLE & INLETS
-  CHANNEL FLOWLINE

**EXHIBIT 6
EXISTING STORM SEWER LAYOUT
(2 OF 3)**

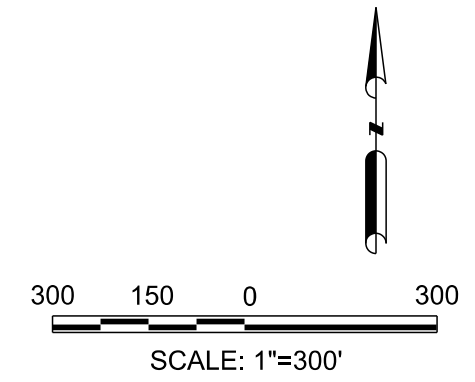
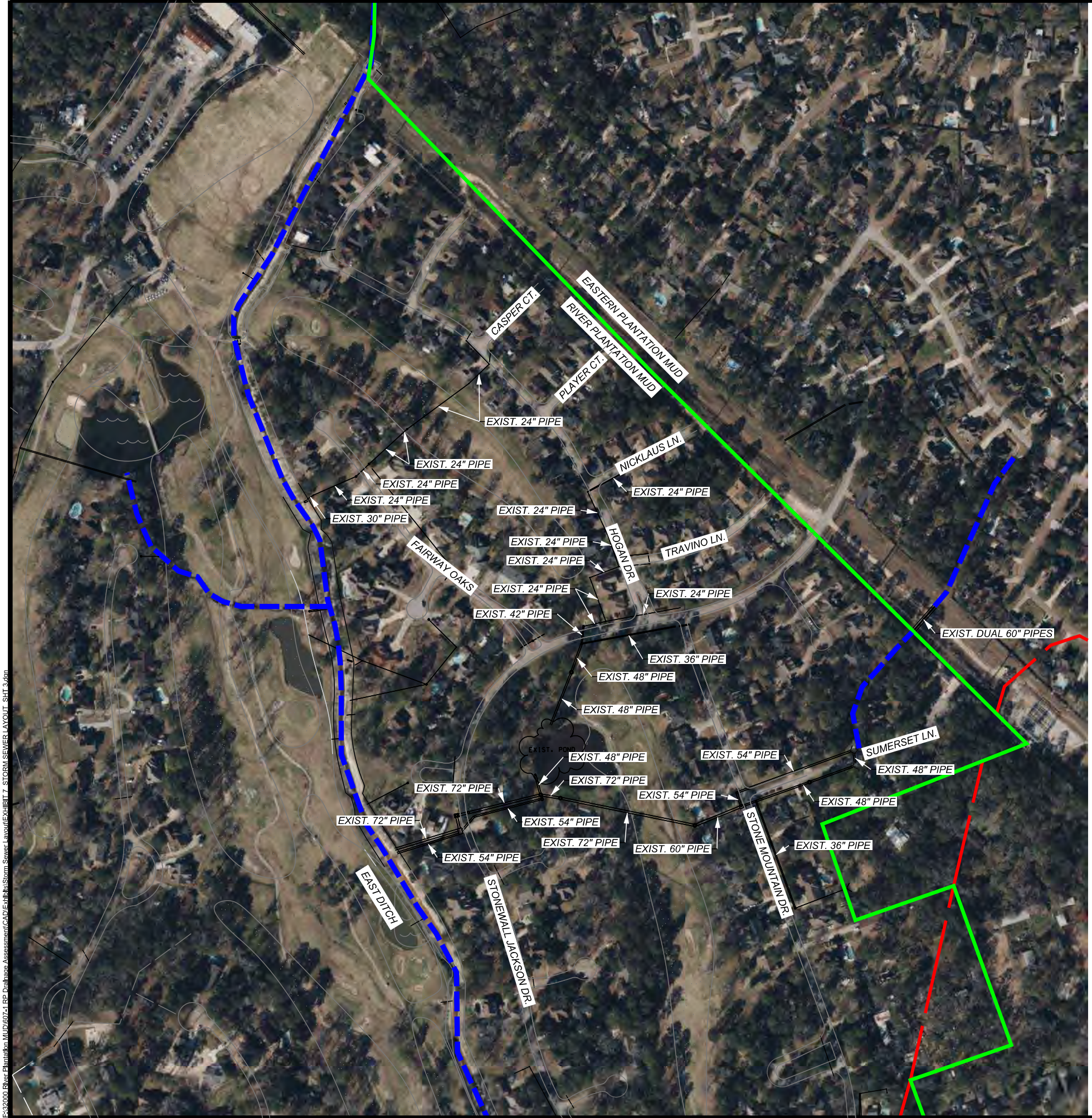
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DRAINAGE ASSESSMENT**








Luke V 2/16/2024 4:57:23 PM E:\202000 River Plantation MUD\61721 R2 Prelim Assessment\CAD\Exhibits\Storm Sewer Layout\EXHIBIT 6 STORM SEWER LAYOUT_SHT 2.dwg

EXHIBIT 7
Existing Storm Sewer Layout (3 of 3)



LEGEND

-  96 EXIST.CONTOUR LINE
-  MUD BOUNDARY
-  OVERALL DRAINAGE AREA
-  EXIST.STORM SEWER, MANHOLE & INLETS
-  CHANNEL FLOWLINE

**EXHIBIT 7
EXISTING STORM SEWER LAYOUT
(3 OF 3)
RIVER PLANTATION
MUNICIPAL UTILITY DISTRICT
RIVER PLANTATION
DRAINAGE ASSESSMENT**

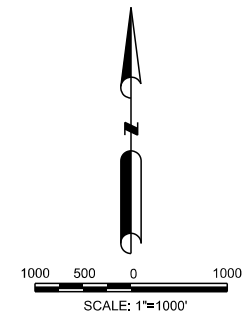
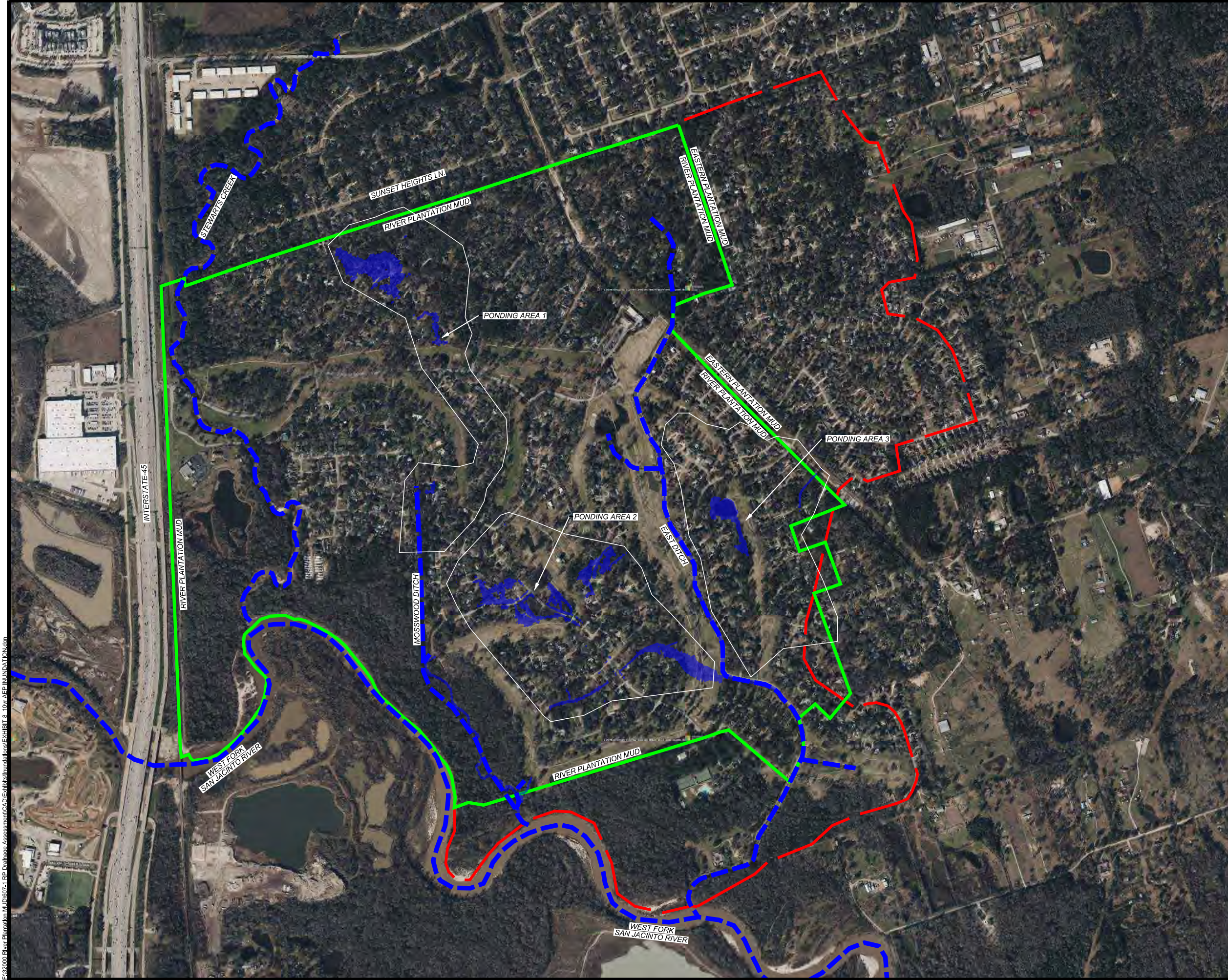


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LukeV 2/1/2024 10:23:33 AM
 EX:20000 River Plantation MUD\61721 LR Prelim Assessment\CAD\Initial\Storm Sewer Layout\EXHIBIT 7 STORM SEWER LAYOUT_SHT_3.dwg

EXHIBIT 8

Local Storm 10% AEP Inundation Layout



LEGEND

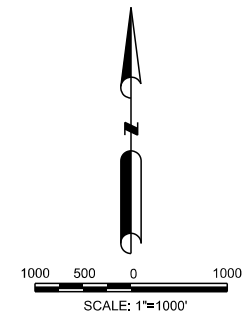
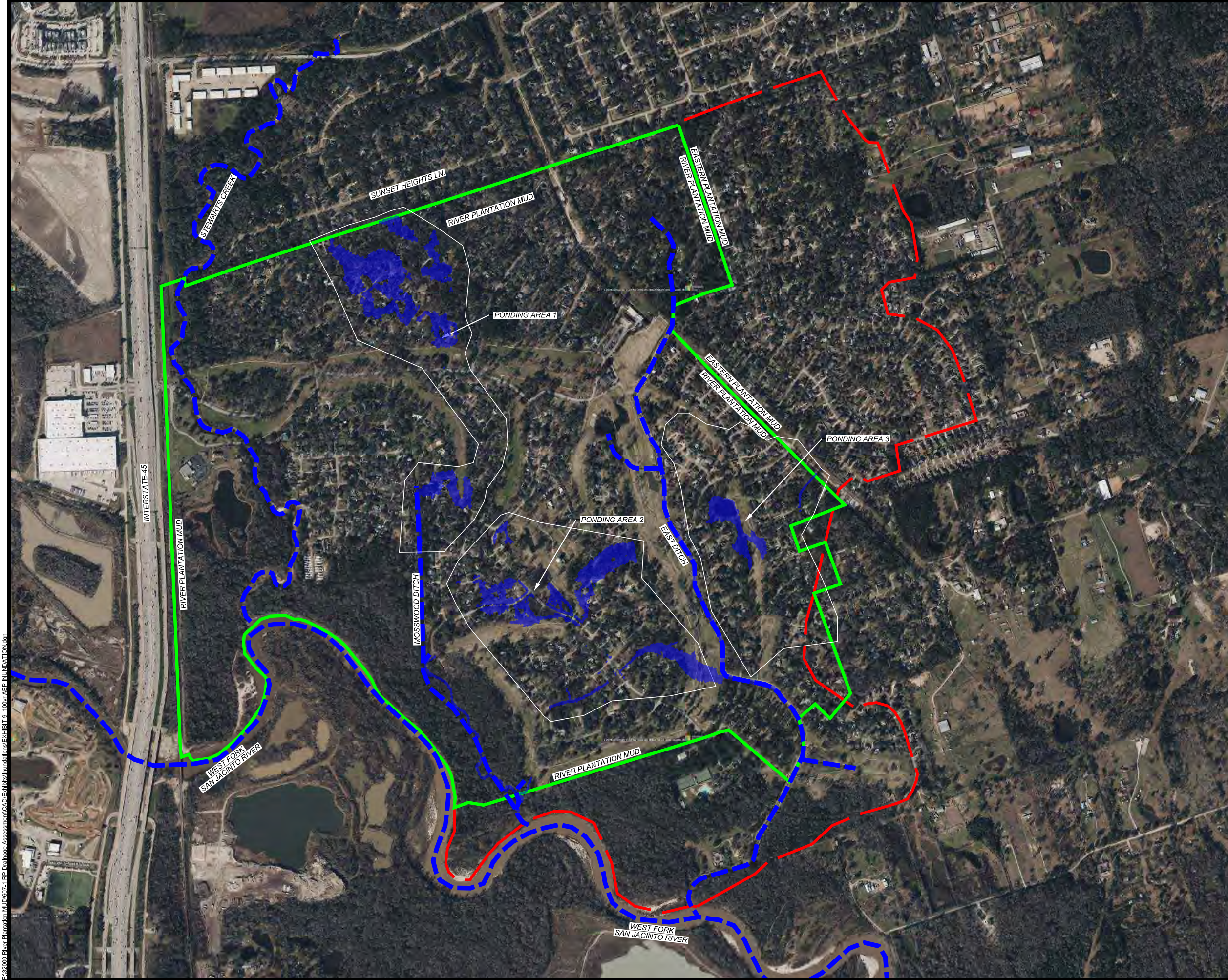
- MUD BOUNDARY
- - - CHANNEL FLOWLINE
- OVERALL DRAINAGE AREA
- 10% AEP LOCAL INUNDATION

**EXHIBIT 8
EXIST. 10% AEP LOCAL
INUNDATION
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EXHIBIT 9
Local Storm 1% AEP Inundation Layout



LEGEND

- MUD BOUNDARY
- - - CHANNEL FLOWLINE
- OVERALL DRAINAGE AREA
- 1% AEP LOCAL INUNDATION

**EXHIBIT 9
EXIST. 1% AEP LOCAL
INUNDATION
RIVER PLANTATION
MUNICIPAL UTILITY DISTRICT
RIVER PLANTATION
DRAINAGE ASSESSMENT**

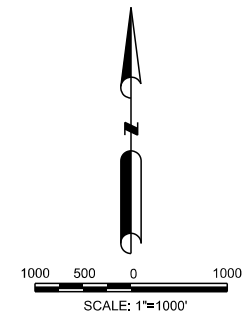
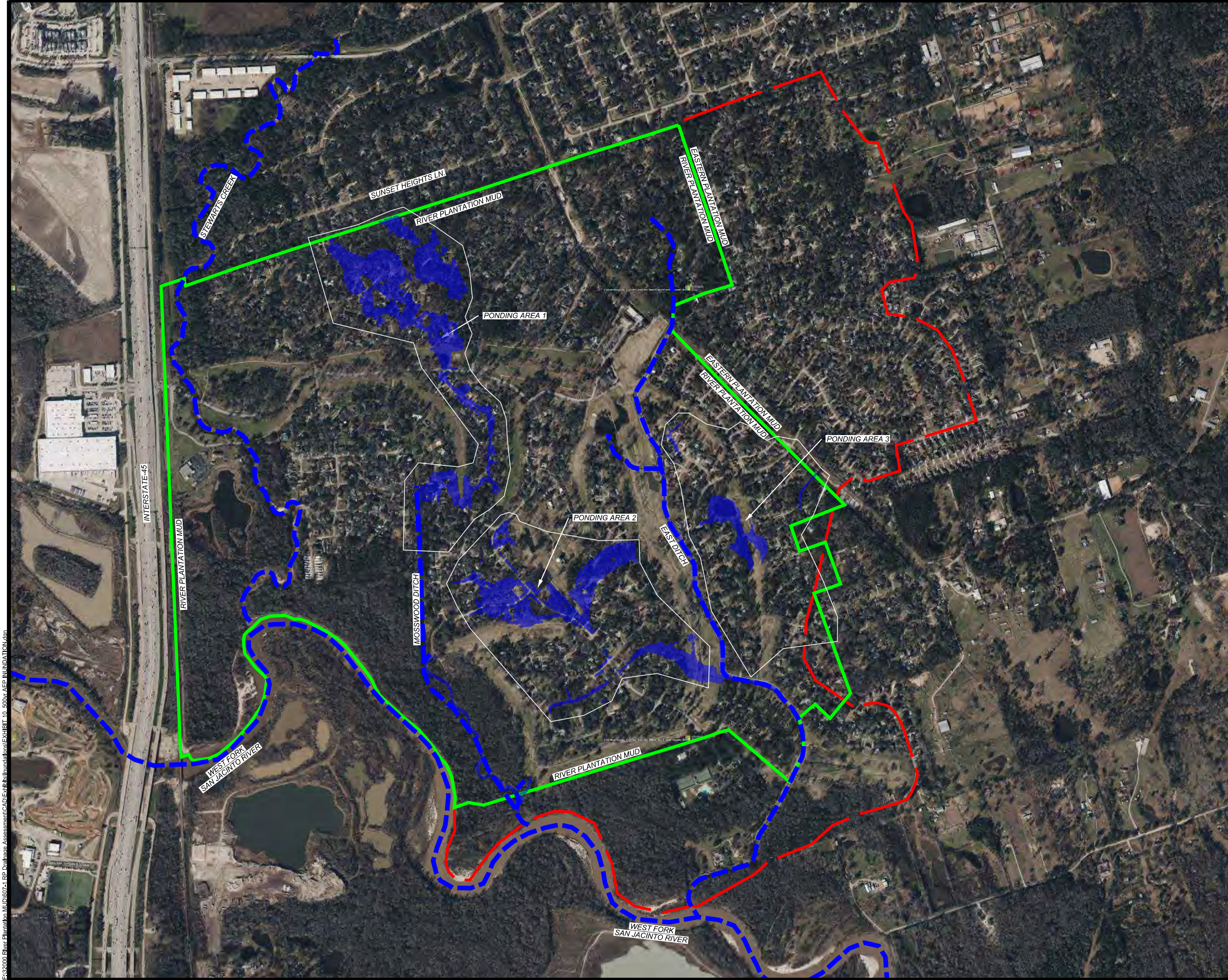
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 ER320000 River Plantation MUD 6/7/21 RE Drainage Assessment (CAD) with Inundation EXHIBIT 9 - 100yr AEP INUNDATION.dwg

EXHIBIT 10

Local Storm 0.2% AEP Inundation Layout



LEGEND

- MUD BOUNDARY
- - - CHANNEL FLOWLINE
- OVERALL DRAINAGE AREA
- 0.2% AEP LOCAL INUNDATION

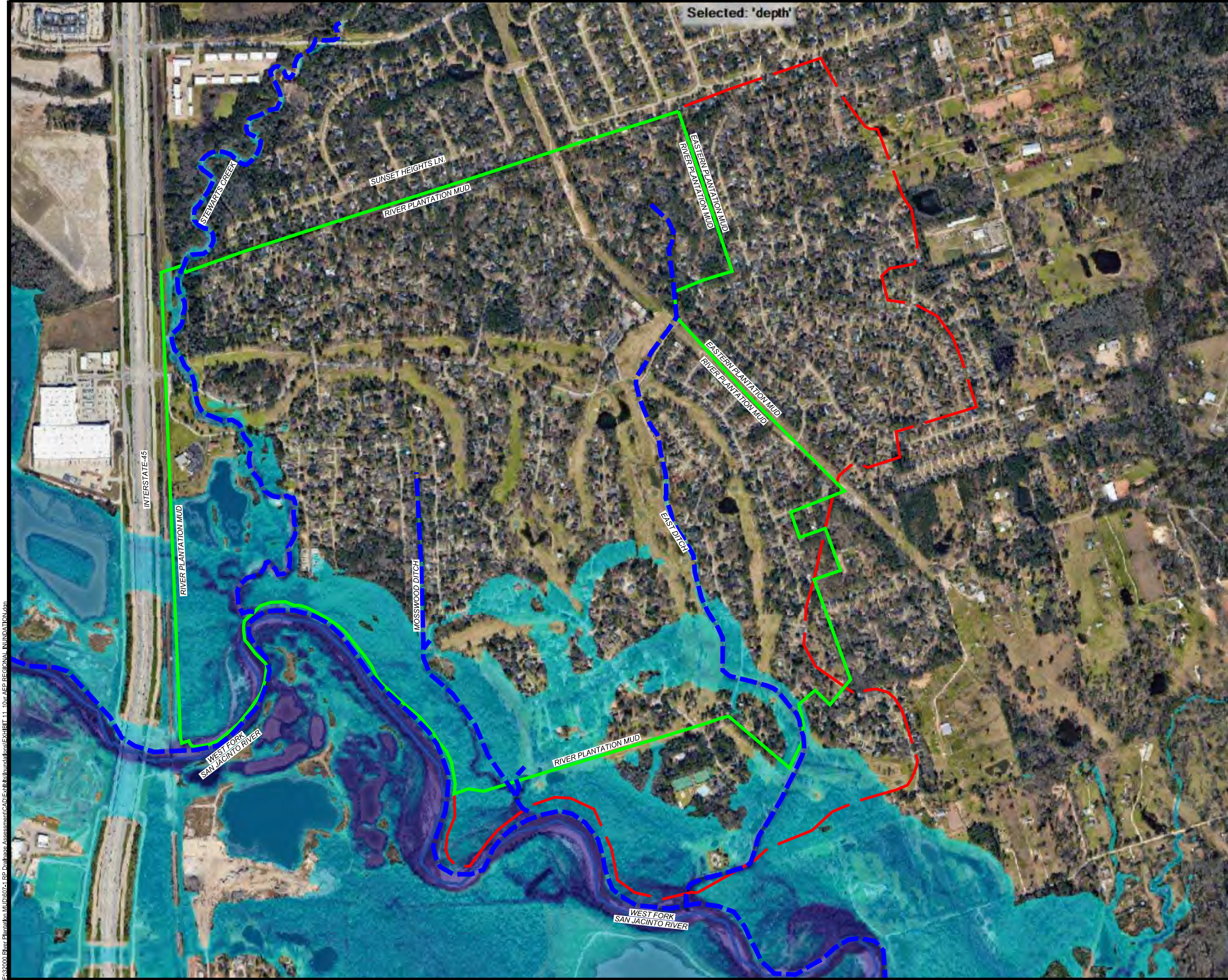
**EXHIBIT 10
EXIST. 0.2% AEP LOCAL
INUNDATION
RIVER PLANTATION
MUNICIPAL UTILITY DISTRICT
RIVER PLANTATION
DRAINAGE ASSESSMENT**

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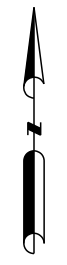
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EXHIBIT 11
Regional Storm 10% AEP Inundation Layout



Selected: 'depth'



LEGEND

- MUD BOUNDARY
- - - CHANNEL FLOWLINE
- OVERALL DRAINAGE AREA
- 10% AEP REGIONAL INUNDATION

NOTES

REGIONAL INUNDATION AS PER:
 "SAN JACINTO REGIONAL WATERSHED MASTER DRAINAGE PLAN"

PREPARED FOR:
 HARRIS COUNTY FLOOD CONTROL DISTRICT, SAN JACINTO RIVER AUTHORITY, MONTGOMERY COUNTY, & CITY OF HOUSTON.

PREPARED BY:
 HALFF ASSOCIATES, INC. TBPE FIRM REGISTRATION No. 312
 FREESE AND NICHOLS, INC. TBPE FIRM REGISTRATION No. 2144.

DATED:
 DECEMBER 2020

**EXHIBIT 11
 EXIST. 10% AEP REGIONAL INUNDATION
 RIVER PLANTATION MUNICIPAL UTILITY DISTRICT
 RIVER PLANTATION DRAINAGE ASSESSMENT**





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EXHIBIT 12
Regional Storm 1% AEP Inundation Layout



LEGEND

-  MUD BOUNDARY
-  CHANNEL FLOWLINE
-  OVERALL DRAINAGE AREA
-  1% AEP REGIONAL INUNDATION

NOTES

REGIONAL INUNDATION AS PER:
 "SAN JACINTO REGIONAL WATERSHED MASTER DRAINAGE PLAN"

PREPARED FOR:
 HARRIS COUNTY FLOOD CONTROL DISTRICT, SAN JACINTO RIVER AUTHORITY, MONTGOMERY COUNTY, & CITY OF HOUSTON.

PREPARED BY:
 HALFF ASSOCIATES, INC. TBPE FIRM REGISTRATION No. 312
 FREESE AND NICHOLS, INC. TBPE FIRM REGISTRATION No. 2144.

DATED:
 DECEMBER 2020

**EXHIBIT 12
 EXIST. 1% AEP REGIONAL
 INUNDATION**

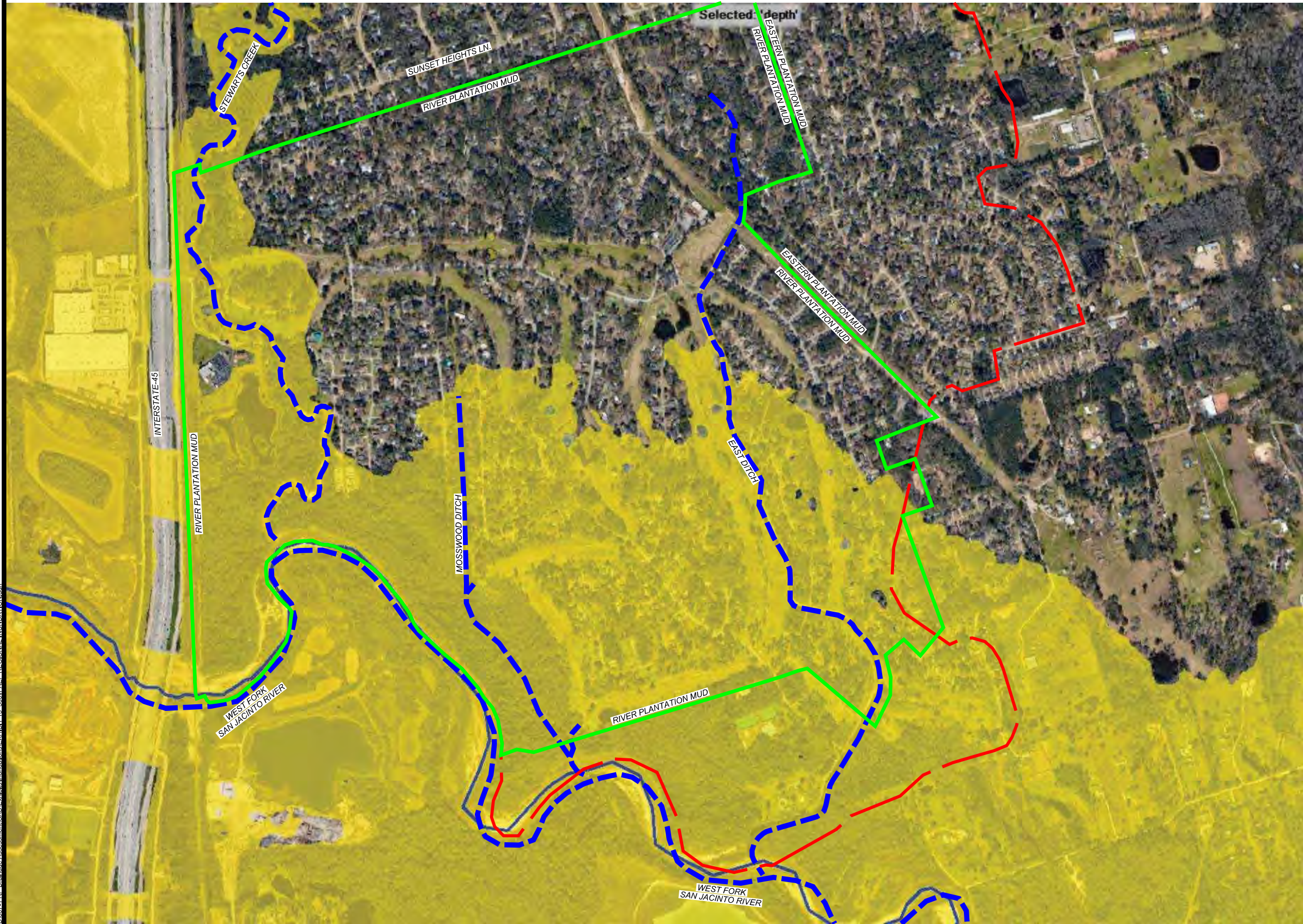
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EXHIBIT 13
Regional Storm 0.2% AEP Inundation Layout



LEGEND

-  MUD BOUNDARY
-  CHANNEL FLOWLINE
-  OVERALL DRAINAGE AREA
-  0.2% AEP REGIONAL INUNDATION

NOTES

REGIONAL INUNDATION AS PER:
"SAN JACINTO REGIONAL WATERSHED MASTER DRAINAGE PLAN"

PREPARED FOR:
HARRIS COUNTY FLOOD CONTROL DISTRICT, SAN JACINTO RIVER AUTHORITY, MONTGOMERY COUNTY, & CITY OF HOUSTON.

PREPARED BY:
HALFF ASSOCIATES, INC. TBPE FIRM REGISTRATION No. 312
FREESE AND NICHOLS, INC. TBPE FIRM REGISTRATION No. 2144.

DATED:
DECEMBER 2020

**EXHIBIT 13
EXIST. 0.2% AEP REGIONAL
INUNDATION**

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EXHIBIT 14
XPSWMM/XPSTORM Model Layout Area 1



EXHIBIT 14
XPSWMM/XPSTORM MODEL
LAYOUT AREA 1
RIVER PLANTATION
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RIVER PLANTATION
DRAINAGE ASSESSMENT



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EXHIBIT 15
XPSWMM/XPSTORM Model Layout Area 2



EXHIBIT 15
XPSWMM/XPSTORM MODEL
LAYOUT AREA 2
RIVER PLANTATION
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EXHIBIT 16
XPSWMM/XPSTORM Model Layout Area 3



LukeV 11/06/2024 2/1/2024
 E:\320000 River Plantation MUD\6721 RE Prelim Assessment\CAD\Exhibits\XPSWMM Model Layout\XPSWMM Layout Area 3.dwg

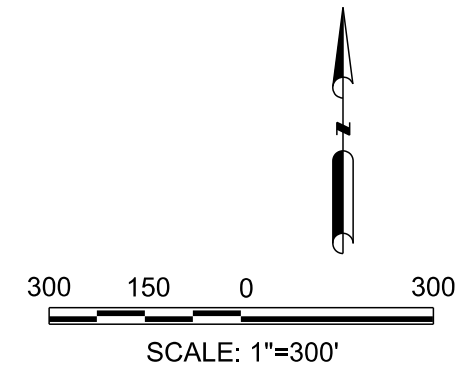
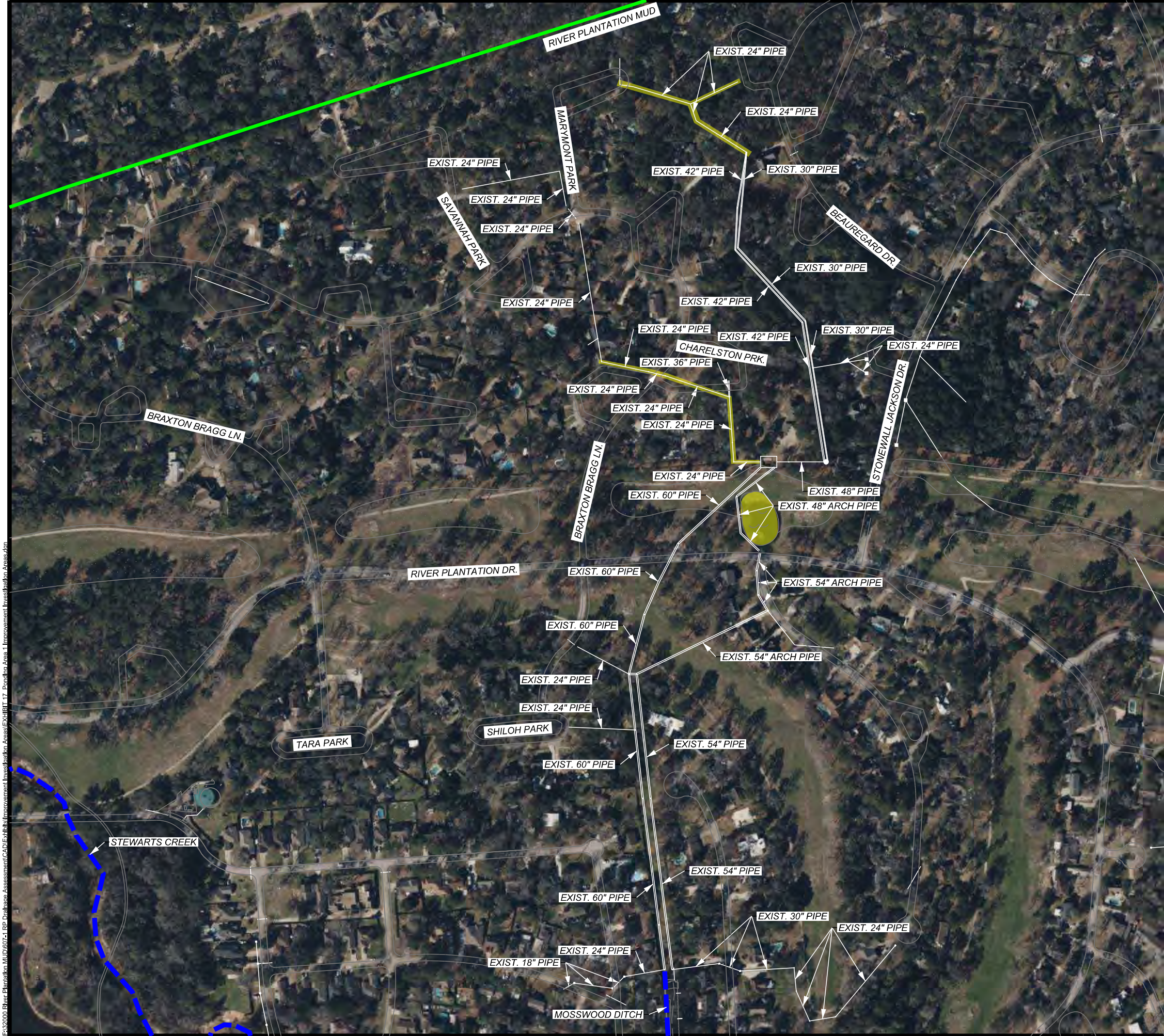
EXHIBIT 16
XPSWMM/XPSTORM MODEL
LAYOUT AREA 3
RIVER PLANTATION
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EXHIBIT 17
Ponding Area 1 Improvement Investigation Areas



LEGEND






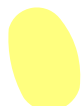
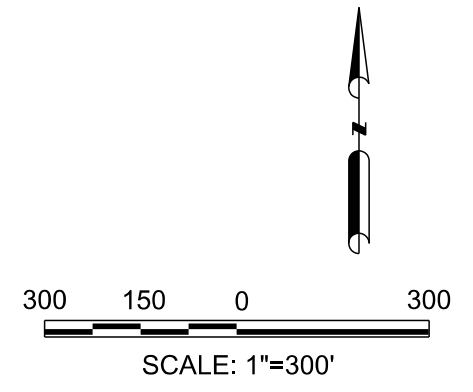
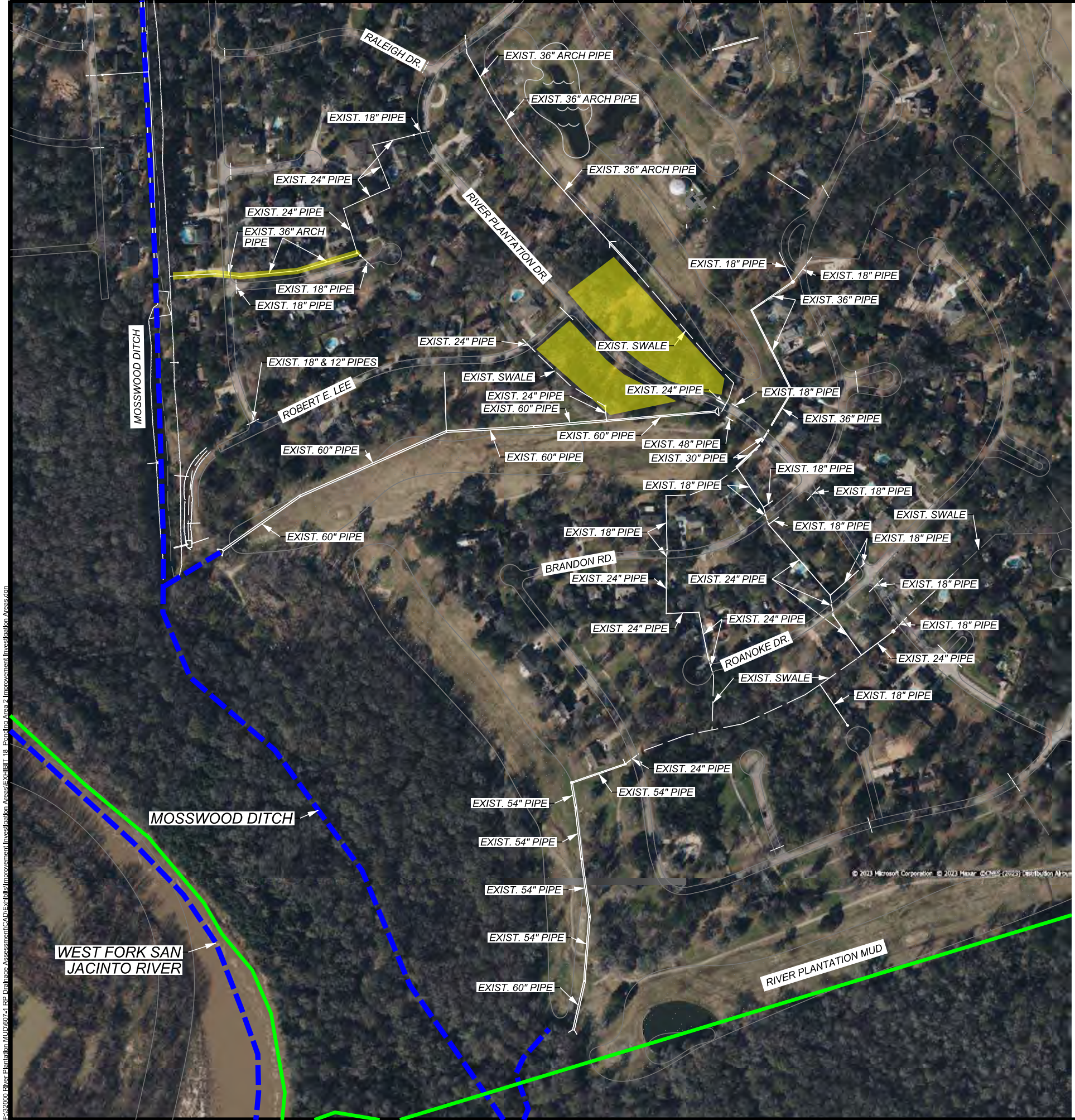
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-  MUD BOUNDARY
-  OVERALL DRAINAGE AREA
-  EXIST.STORM SEWER, MANHOLE & INLETS
-  CHANNEL FLOWLINE
-  PONDING AREA 1 IMPROVMENT INVESTIGATION AREAS

EXHIBIT 17
PONDING AREA 1 IMPROVMENT
INVESTIGATION AREAS
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EXHIBIT 18
Ponding Area 2 Improvement Investigation Areas



LEGEND

-  96 EXIST.CONTOUR LINE
-  MUD BOUNDARY
-  OVERALL DRAINAGE AREA
-  EXIST.STORM SEWER, MANHOLE & INLETS
-  CHANNEL FLOWLINE
-  PONDING AREA 2 IMPROVMENT INVESTIGATION AREAS

**EXHIBIT 18
PONDING AREA 2 IMPROVMENT
INVESTIGATION AREAS
RIVER PLANTATION
MUNICIPAL UTILITY DISTRICT
RIVER PLANTATION
DRAINAGE ASSESSMENT**

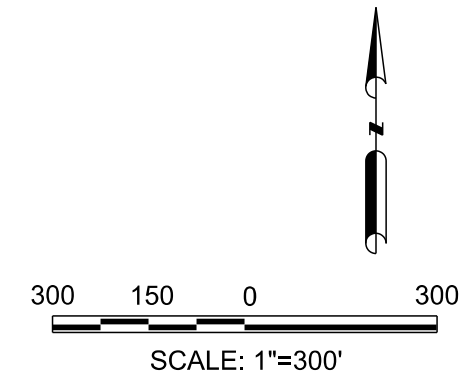
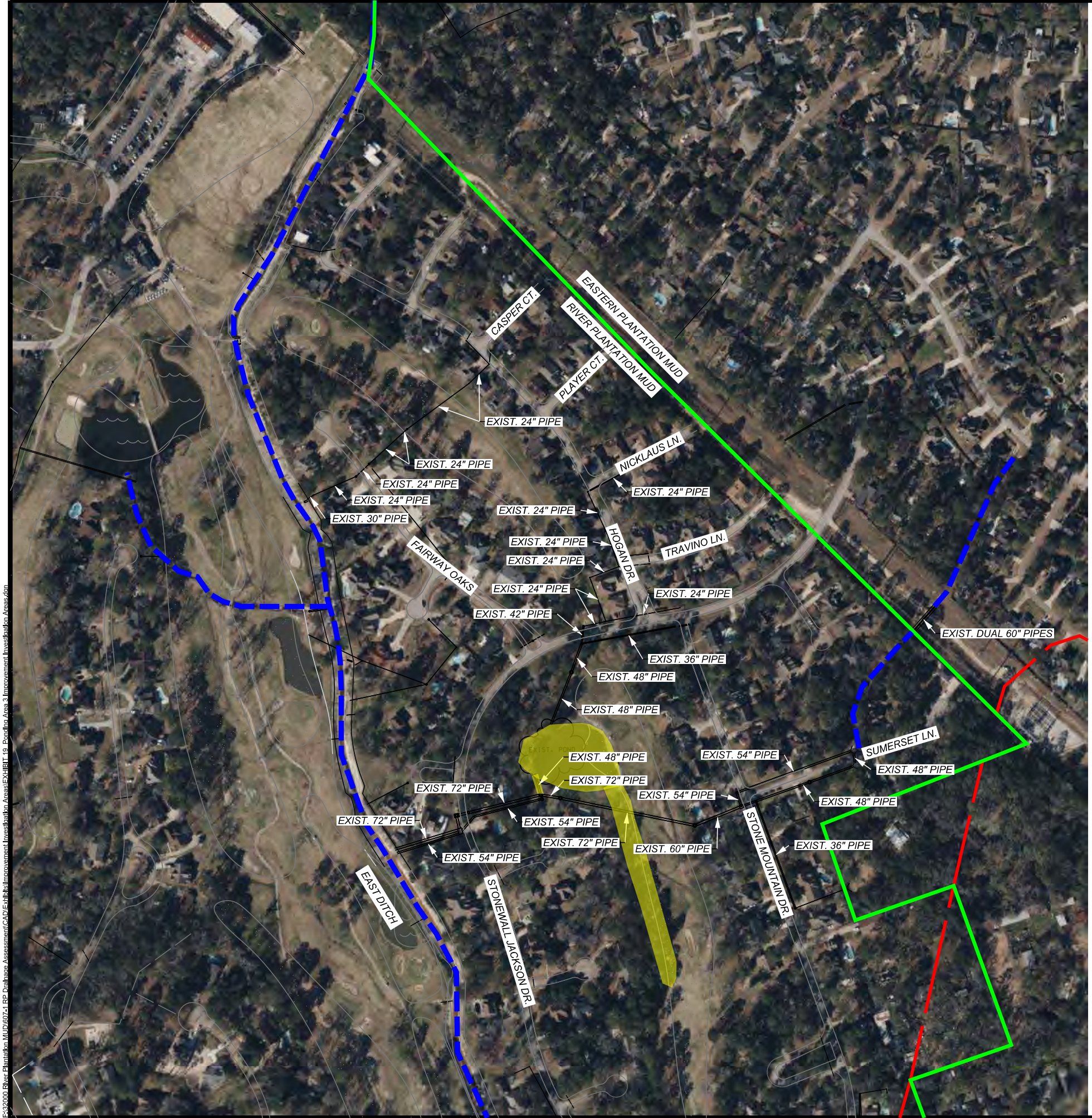


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 River Plantation MUD 06/07/21 RE Drainage Assessment (CAD) Exhibit 18 Drainage Assessment Investigation Areas.dwg

EXHIBIT 19
Ponding Area 3 Improvement Investigation Areas



LEGEND

-  96 EXIST.CONTOUR LINE
-  MUD BOUNDARY
-  OVERALL DRAINAGE AREA
-  EXIST.STORM SEWER, MANHOLE & INLETS
-  CHANNEL FLOWLINE
-  PONDING AREA 3 IMPROVEMENT INVESTIGATION AREAS

**EXHIBIT 19
PONDING AREA 3 IMPROVEMENT
INVESTIGATION AREAS
RIVER PLANTATION
MUNICIPAL UTILITY DISTRICT
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DRAINAGE ASSESSMENT**

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APPENDICES

APPENDIX A
Peak Runoff Rate Calculations

OA ROG EXISTING CALCULATIONS

Area = 1839.49 ac.
 Volume (100yr) = 1.38*area*43560 = 110576894.5 cft
 Volume (10yr) = 0.70*area*43560 = 56089729.08 cft
 Volume (2yr) = 0.41*area*43560 = 32852555.6 cft
 Volume (50yr) = 1.13*area*43560 = 90544848.37 cft
 The equation for the Site Runoff Curves

$Q = bA^m$

where Q peak discharge (cfs)
 A drainage area (acres)
 m 1 for 1 to 20 acres
 0.786 for 20 to 640 acres
 b variable dependent on impervious cover.

tp = time to Qp in seconds

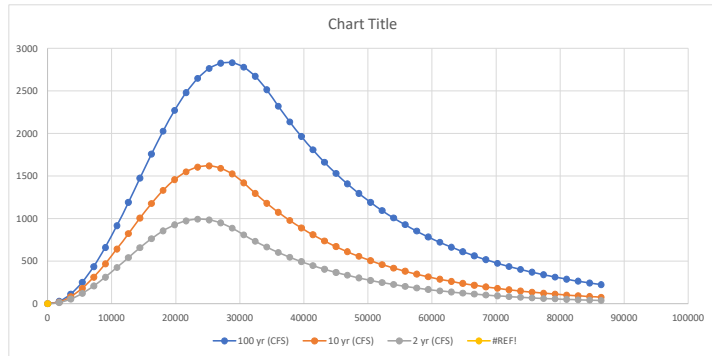
$T_p = \frac{V}{1.39 Q_p}$

$q_i = \left(\frac{Q_p}{2} \right) \left[1 - \cos \left(\frac{\pi t_i}{T_p} \right) \right]$ $t_i \leq 1.25 T_p$
 $q_i = 4.34 Q_p e^{-1.39 t_i / T_p}$ $t_i > 1.25 T_p$

| Existing Conditions | | | |
|---------------------|-------------|----------|----------|
| | 10 yrs | 100 yrs | 2 yrs |
| b= | 4.4 | 7.7 | 2.7 |
| Qp= | 1619.96 | 2834.93 | 994.07 |
| tp= | 24909.42397 | 28061.23 | 23775.98 |
| 1.25*tp= | 31136.77997 | 35076.54 | 29719.97 |

@ 30% Imp.

| ti (sec) | 100 yr (CFS) | 10 yr (CFS) | 2 yr (CFS) | ti (hr) |
|----------|--------------|-------------|-------------|---------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 28.68428894 | 20.7824274 | 13.99186691 | 0.5 |
| 3600.00 | 113.5762278 | 82.06324196 | 55.17970501 | 1 |
| 5400.00 | 251.2400186 | 180.6977675 | 121.2445786 | 1.5 |
| 7200.00 | 436.1040489 | 311.6244909 | 208.4669383 | 2 |
| 9000.00 | 660.6863895 | 468.1247978 | 311.9360374 | 2.5 |
| 10800.00 | 915.8976077 | 642.1677444 | 425.8264138 | 3 |
| 12600.00 | 1191.40864 | 824.8221713 | 543.7258722 | 3.5 |
| 14400.00 | 1476.068838 | 1006.715014 | 658.9965001 | 4 |
| 16200.00 | 1758.35726 | 1178.512289 | 765.148392 | 4.5 |
| 18000.00 | 2026.848959 | 1331.398076 | 856.2050408 | 5 |
| 19800.00 | 2270.677376 | 1457.526913 | 927.0398235 | 5.5 |
| 21600.00 | 2479.974139 | 1550.426393 | 973.6646378 | 6 |
| 23400.00 | 2646.268462 | 1605.329302 | 993.4544384 | 6.5 |
| 25200.00 | 2762.829981 | 1619.418251 | 985.2950305 | 7 |
| 27000.00 | 2824.941148 | 1591.970254 | 949.6458006 | 7.5 |
| 28800.00 | 2830.088161 | 1524.393828 | 888.5138528 | 8 |
| 30600.00 | 2778.062708 | 1420.156713 | 809.6179065 | 8.5 |
| 32400.00 | 2670.970394 | 1296.088411 | 733.7319395 | 9 |
| 34200.00 | 2513.145525 | 1179.877317 | 664.9588093 | 9.5 |
| 36000.00 | 2321.262749 | 1074.086051 | 602.6318254 | 10 |
| 37800.00 | 2135.545777 | 977.7803404 | 546.1467866 | 10.5 |
| 39600.00 | 1964.68744 | 890.1096828 | 494.9561241 | 11 |
| 41400.00 | 1807.498943 | 810.2998339 | 448.5635928 | 11.5 |
| 43200.00 | 1662.886606 | 737.6459705 | 406.519461 | 12 |
| 45000.00 | 1529.84425 | 671.5064659 | 368.4161506 | 12.5 |
| 46800.00 | 1407.446197 | 611.2972236 | 333.8842861 | 13 |
| 48600.00 | 1294.840829 | 556.4865188 | 302.5891137 | 13.5 |
| 50400.00 | 1191.244665 | 506.5903028 | 274.2272565 | 14 |
| 52200.00 | 1095.936905 | 461.1679282 | 248.5237729 | 14.5 |
| 54000.00 | 1008.254422 | 419.818257 | 225.2294922 | 15 |
| 55800.00 | 927.5871391 | 382.1761189 | 204.1185982 | 15.5 |
| 57600.00 | 853.3737936 | 347.9090854 | 184.9864408 | 16 |
| 59400.00 | 785.0980257 | 316.7145348 | 167.6475519 | 16.5 |
| 61200.00 | 722.2847884 | 288.3169792 | 151.9338473 | 17 |
| 63000.00 | 664.4970417 | 262.4656319 | 137.6929976 | 17.5 |
| 64800.00 | 611.332712 | 238.9321924 | 124.7869512 | 18 |
| 66600.00 | 562.4218939 | 217.5088301 | 113.0905962 | 18.5 |
| 68400.00 | 517.4242774 | 198.0063495 | 102.4905475 | 19 |
| 70200.00 | 476.0267794 | 180.2525185 | 92.88404764 | 19.5 |
| 72000.00 | 437.9413658 | 164.0905482 | 84.17797072 | 20 |
| 73800.00 | 402.903047 | 149.3777076 | 76.28791955 | 20.5 |
| 75600.00 | 370.6680345 | 135.9840636 | 69.13740757 | 21 |
| 77400.00 | 341.0120445 | 123.791333 | 62.65711732 | 21.5 |
| 79200.00 | 313.7287374 | 112.6918384 | 56.78422851 | 22 |
| 81000.00 | 288.6282825 | 102.5875571 | 51.46180907 | 22.5 |
| 82800.00 | 265.5360364 | 93.3892542 | 46.63826316 | 23 |
| 84600.00 | 244.2913287 | 85.01570044 | 42.26683106 | 23.5 |
| 86400.00 | 224.7463437 | 77.392943 | 38.3051359 | 24 |



OA DA DRAINAGE CALCULATIONS

Time of Concentration:

$T_c = T_{OL} + T_1 + \dots + T_n$

Example 2.1
 1. Area of catchment
 2. Length of main sewer
 3. Slope of main sewer
 4. Manning's roughness coefficient
 5. Time of travel in sewer
 6. Time of travel in gutter
 7. Time of travel in street
 8. Time of travel in gutter
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 18. Time of travel in gutter
 19. Time of travel in street
 20. Time of travel in gutter

Table 2.3 Manning's Roughness Coefficients for Open Channel Flow

| Surface | n |
|--------------------------------------------------------|-------|
| Smooth surfaces (concrete, asphalt, gravel, surf-walk) | 0.012 |
| Polished metal | 0.009 |
| Galvanized steel (Roughness Coef. = 0.15) | 0.014 |
| Cast-iron pipe (Roughness Coef. = 0.15) | 0.013 |
| Concrete (Roughness Coef. = 0.15) | 0.015 |
| Grass (Roughness Coef. = 0.15) | 0.040 |
| Wood (Roughness Coef. = 0.15) | 0.080 |

Channel Flow

Channel flow velocity is computed by dividing the channel discharge by the flow area computed from Manning's equation. This can be written as:

$V = \frac{Q}{A} = \frac{1.49}{n} R^{2/3} S^{1/2}$

Equation 4-17

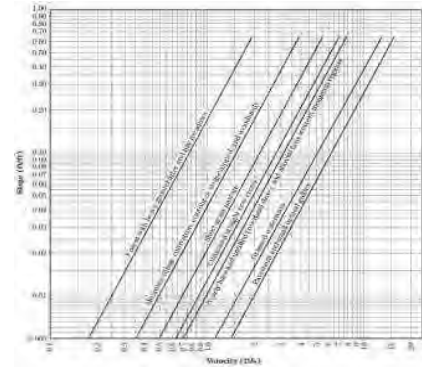
Where:

- V = channel flow velocity (ft/s)
- Q = channel flow length (ft)
- S = channel flow slope (ft/ft)
- n = Manning's roughness coefficient

| T_{OL} | $T = T_{OL}$; multiply by 60 to convert hrs. to min. (L= max 300') | $T =$ | $T =$ |
|------------|---------------------------------------------------------------------|---------------------|---------------------------|
| n= | 0.15 | D= 1247.23 (ft) | $L_{ch} = 8603.79$ (ft) |
| L= | 100 (ft) | S= 0.0056 (ft/ft) | $S_{ch} = 0.0023$ (ft/ft) |
| P_2 = | 4.89 (in) | V= 0.4125 (ft/s) | R= 5.2763819 (ft/s) |
| S= | 0.0056 (ft/ft) | | n= 0.015 |
| T_{OL} = | 13.19 (min) | T_1 = 50.39 (min) | T_{OL} = 9.93 (min) |

$T_c = 73.51$ (min)

avg. slope of East Ditch Channel



Intensity:

SEE FIG. 2.1-2.1a
 NOAA ATLAS 14

| | |
|-------------|--------------|
| I (500-YR)= | 7.17 (in/hr) |
| I (100-YR)= | 4.2 (in/hr) |
| I (10-YR)= | 2.7 (in/hr) |
| I (2-YR)= | 1.8 (in/hr) |

Peak Flow Rate:

Q=CIA
 C= 0.4 Single family residential districts; lots 1/4 - 1/2 acre; sub-basin slope <1%

| i (500-YR) | i (100-YR) | i (10-YR) | i (2-YR) |
|------------|------------|-----------|----------|
| 7.17 | 4.2 | 2.7 | 1.8 |

A= 1147.16 (Ac)

| | |
|-------------|---------------|
| Q (500-YR)= | 3291.29 (cfs) |
| Q (100-YR)= | 1927.24 (cfs) |
| Q (10-YR)= | 1238.94 (cfs) |
| Q (2-YR)= | 825.96 (cfs) |

OA DA EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 101939797.94 cft
 Volume (100-yr) = 1.38*area*43560 = 68959275.08 cft
 Volume (10-yr) = 0.70*area*43560 = 34979342.43 cft
 Volume (2-yr) = 0.41*area*43560 = 20487900.57 cft
 A= 1147.16 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Qp}$

$q_i = \left(\frac{Qp}{2}\right) \left[1 - \cos\left(\frac{\pi t_i}{TP}\right)\right]$ $t_i \leq 1.25 TP$

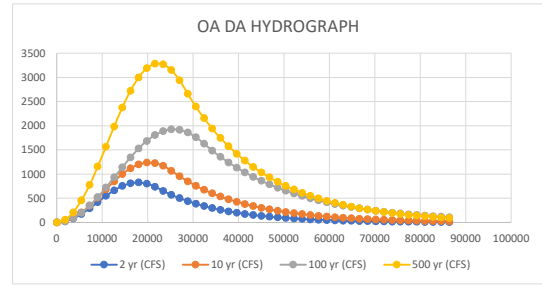
$q_i = 4.34 Qp e^{-1.39 t_i / TP}$ $t_i > 1.25 TP$

| OA DA Existing Conditions | | | | |
|---------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 825.96 | 1238.94 | 1927.24 | 3291.29 |
| TP= | 17845.324 | 20311.751 | 25742.035 | 22282.432 |
| 1.25*TP= | 22306.655 | 25389.688 | 32177.544 | 27853.041 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 20.56160279 | 23.85242803 | 23.15724275 | 52.71009394 |
| 3600.00 | 80.19894988 | 93.57285365 | 91.515962 | 207.4637634 |
| 5400.00 | 172.9735374 | 203.7921566 | 201.7906254 | 454.3474775 |
| 7200.00 | 289.6471567 | 346.0224271 | 348.6810902 | 777.545848 |
| 9000.00 | 418.6018071 | 509.3106133 | 525.1273445 | 1156.354765 |
| 10800.00 | 546.9965806 | 681.0820087 | 722.6488334 | 1566.507701 |
| 12600.00 | 662.0463197 | 848.1086205 | 931.7520607 | 1981.730232 |
| 14400.00 | 752.2947247 | 997.5278486 | 1142.386876 | 2375.423173 |
| 16200.00 | 808.7551366 | 1117.833025 | 1344.429516 | 2722.366526 |
| 18000.00 | 825.8054009 | 1199.759533 | 1528.169184 | 3000.335075 |
| 19800.00 | 801.7477047 | 1236.998272 | 1684.77478 | 3191.522136 |
| 21600.00 | 738.9776395 | 1226.681513 | 1806.719355 | 3283.680252 |
| 23400.00 | 651.8214147 | 1169.603741 | 1888.141871 | 3270.905767 |
| 25200.00 | 571.7168387 | 1070.160476 | 1925.128912 | 3154.017017 |
| 27000.00 | 501.4565897 | 955.1039958 | 1915.902764 | 2940.501902 |
| 28800.00 | 439.8308643 | 851.1734956 | 1860.906865 | 2661.545587 |
| 30600.00 | 385.7785363 | 758.5522862 | 1762.784489 | 2396.217702 |
| 32400.00 | 338.3688849 | 676.009737 | 1628.61047 | 2157.340196 |
| 34200.00 | 296.7855686 | 602.4491295 | 1487.096074 | 1942.276245 |
| 36000.00 | 260.3125691 | 536.8930857 | 1357.878248 | 1748.65189 |
| 37800.00 | 228.321862 | 478.4705818 | 1239.888512 | 1574.329831 |
| 39600.00 | 200.2626029 | 426.4053751 | 1132.151224 | 1417.385834 |
| 41400.00 | 175.6516427 | 380.0056908 | 1033.775523 | 1276.087489 |
| 43200.00 | 154.0652081 | 338.6550298 | 943.9479541 | 1148.875092 |
| 45000.00 | 135.1316047 | 301.8039782 | 861.9257473 | 1034.344423 |
| 46800.00 | 118.5248169 | 268.9629069 | 787.0306732 | 931.2312475 |
| 48600.00 | 103.9588944 | 239.6954663 | 718.6434359 | 838.3973626 |
| 50400.00 | 91.18302827 | 213.6127886 | 656.1985518 | 754.818032 |
| 52200.00 | 79.97723225 | 190.3683209 | 599.1796737 | 679.5706748 |
| 54000.00 | 70.14855505 | 169.6532208 | 547.115321 | 611.8246815 |
| 55800.00 | 61.52775781 | 151.192253 | 499.5749817 | 550.8322457 |
| 57600.00 | 53.96639999 | 134.7401321 | 456.1655519 | 495.9201093 |
| 59400.00 | 47.33428344 | 120.0782634 | 416.5280855 | 446.4821308 |
| 61200.00 | 41.51721052 | 107.0118392 | 380.3348265 | 401.9725948 |
| 63000.00 | 36.41501769 | 95.36724968 | 347.2864983 | 361.9001877 |
| 64800.00 | 31.9398509 | 84.98977664 | 317.1098292 | 325.8225749 |
| 66600.00 | 28.01465275 | 75.74153767 | 289.5552931 | 293.3415177 |
| 68400.00 | 24.5718357 | 67.49965413 | 264.3950456 | 264.0984776 |
| 70200.00 | 21.55211828 | 60.15461856 | 241.4210405 | 237.7706587 |
| 72000.00 | 18.90350432 | 53.60883965 | 220.4433092 | 214.0674442 |
| 73800.00 | 16.58038765 | 47.77534555 | 201.2883901 | 192.727189 |
| 75600.00 | 14.54276677 | 42.57662836 | 183.797894 | 173.514331 |
| 77400.00 | 12.75555613 | 37.94361426 | 167.8271947 | 156.2167914 |
| 79200.00 | 11.18798196 | 33.81474575 | 153.244233 | 140.6436331 |
| 81000.00 | 9.81305237 | 30.13516378 | 139.9284245 | 126.6229536 |
| 82800.00 | 8.607092607 | 26.85597883 | 127.7696629 | 113.9999872 |
| 84600.00 | 7.549337387 | 23.93362134 | 116.6674091 | 102.6353968 |
| 86400.00 | 6.621573346 | 21.32926281 | 106.5298604 | 92.40373563 |

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DA#1 DRAINAGE CALCULATIONS

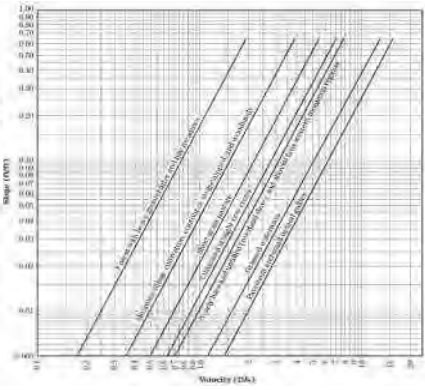
Time of Concentration:

$T_c = T_{OL} + T_1 + \dots + T_n$

Section 2.2
 1. Determine the time of concentration for each sub-basin.
 2. Determine the time of concentration for the entire drainage area.
 3. Determine the peak flow rate for each sub-basin.
 4. Determine the peak flow rate for the entire drainage area.
 5. Determine the peak flow rate for the entire drainage area.
 6. Determine the peak flow rate for the entire drainage area.
 7. Determine the peak flow rate for the entire drainage area.
 8. Determine the peak flow rate for the entire drainage area.
 9. Determine the peak flow rate for the entire drainage area.
 10. Determine the peak flow rate for the entire drainage area.

Table 2.11 Manning's Roughness Coefficient for Gravel (Shell Flow)

| Surface | n |
|---------------------|-------|
| Gravel (Shell Flow) | 0.012 |
| Gravel (Shell Flow) | 0.020 |
| Gravel (Shell Flow) | 0.040 |
| Gravel (Shell Flow) | 0.070 |
| Gravel (Shell Flow) | 0.100 |
| Gravel (Shell Flow) | 0.150 |
| Gravel (Shell Flow) | 0.200 |
| Gravel (Shell Flow) | 0.300 |
| Gravel (Shell Flow) | 0.400 |
| Gravel (Shell Flow) | 0.500 |
| Gravel (Shell Flow) | 0.600 |
| Gravel (Shell Flow) | 0.800 |



| $T_{OL} =$ | $T =$ |
|----------------------------------------------------------------------------|---------------------|
| $T_{OL} = T_t = T_0$; multiply by 60 to convert hrs. to min. (L=max 300') | |
| n= 0.15 | D= 1247.23 (ft) |
| L= 100 (ft) | S= 0.0056 (ft/ft) |
| $P_2 = 4.89$ (in) | V= 0.4125 (ft/s) |
| S= 0.0056 (ft/ft) | |
| $T_{OL} = 13.19$ (min) | $T_1 = 50.39$ (min) |

$T_c = 63.58$ (min)

Intensity:

SEE FIG. 2.1-2.1a

| | |
|-------------|-------------|
| I (100-YR)= | 4.5 (in/hr) |
| I (10-YR)= | 3 (in/hr) |
| I (2-YR)= | 2.1 (in/hr) |

Peak Flow Rate:

$Q = CIA$

C= 0.4 Single family residential districts; lots 1/4 - 1/2 acre; sub-basin slope <1%

| i (100-YR) | i (10-YR) | i (2-YR) |
|---------------|-----------|----------|
| 4.5 | 3 | 2.1 |
| A= 33.89 (Ac) | | |

| | |
|-------------|-------------|
| Q (100-YR)= | 61.00 (cfs) |
| Q (10-YR)= | 40.67 (cfs) |
| Q (2-YR)= | 28.47 (cfs) |

DA#1 EXISTING CALCULATIONS

Volume (100-yr) = 1.38*area*43560 = 2037222.79 cft
 Volume (10-yr) = 0.70*area*43560 = 1033373.88 cft
 Volume (2-yr) = 0.41*area*43560 = 605261.844 cft
 A = 33.89 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

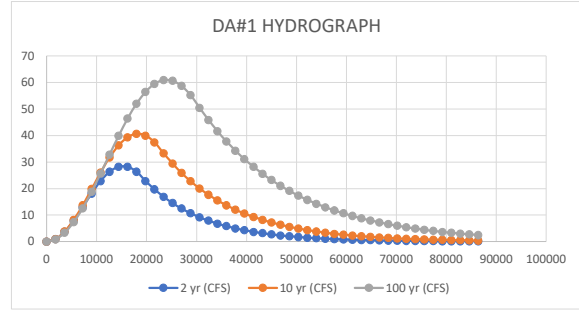
$q_i = \left(\frac{Q_p}{2}\right) \left[1 - \cos\left(\frac{\pi t_i}{T_p}\right)\right]$ $t_i \leq 1.25 T_p$
 $q_i = 4.34 Q_p e^{-1.3t_i/T_p}$ $t_i > 1.25 T_p$

| DA#1 Existing Conditions | | | |
|--------------------------|-----------|-----------|------------|
| | 2 - Year | 10 - Year | 100 - Year |
| Qp= | 28.47 | 40.67 | 61.00 |
| TP= | 15295.992 | 18280.576 | 24025.899 |
| 1.25*TP= | 19119.990 | 22850.719 | 30032.374 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) |
|----------|-------------|-------------|--------------|
| 0 | 0 | 0 | 0 |
| 1800.00 | 0.961674837 | 0.965143654 | 0.840937515 |
| 3600.00 | 3.716752532 | 3.768954445 | 3.317379388 |
| 5400.00 | 7.89295177 | 8.145269279 | 7.292770566 |
| 7200.00 | 12.92596144 | 13.67864874 | 12.54790147 |
| 9000.00 | 18.13569349 | 19.84381438 | 18.7929956 |
| 10800.00 | 22.81818013 | 26.05551288 | 25.68368824 |
| 12600.00 | 26.34069792 | 31.72407359 | 32.84001533 |
| 14400.00 | 28.22726479 | 36.31138543 | 39.86736529 |
| 16200.00 | 28.2229574 | 39.38197925 | 46.37823855 |
| 18000.00 | 26.3283578 | 40.64436649 | 52.0136149 |
| 19800.00 | 22.79947475 | 39.97870992 | 56.46275048 |
| 21600.00 | 19.70487173 | 37.44819971 | 59.48031267 |
| 23400.00 | 16.90965309 | 33.29305477 | 60.89990817 |
| 25200.00 | 14.51094792 | 29.40750091 | 60.64325814 |
| 27000.00 | 12.45250914 | 25.87416686 | 58.7245147 |
| 28800.00 | 10.68606853 | 22.76536563 | 55.24948049 |
| 30600.00 | 9.170204916 | 20.03008928 | 50.40977459 |
| 32400.00 | 7.869372913 | 17.62345851 | 45.86364897 |
| 34200.00 | 6.753069382 | 15.5059863 | 41.60739619 |
| 36000.00 | 5.795118186 | 13.64293001 | 37.74613351 |
| 37800.00 | 4.973056382 | 12.00372138 | 34.24320494 |
| 39600.00 | 4.26760749 | 10.56146494 | 31.06535626 |
| 41400.00 | 3.662229481 | 9.292496735 | 28.18241929 |
| 43200.00 | 3.142726879 | 8.175996042 | 25.56702554 |
| 45000.00 | 2.696917899 | 7.193643773 | 23.19434639 |
| 46800.00 | 2.314348791 | 6.329321891 | 21.04185735 |
| 48600.00 | 1.986048715 | 5.568848954 | 19.08912428 |
| 50400.00 | 1.704319381 | 4.899747431 | 17.31760936 |
| 52200.00 | 1.462554533 | 4.311038975 | 15.71049513 |
| 54000.00 | 1.255085042 | 3.793064297 | 14.25252481 |
| 55800.00 | 1.077045969 | 3.337324678 | 12.92985752 |
| 57600.00 | 0.924262484 | 2.936342528 | 11.72993681 |
| 59400.00 | 0.793151977 | 2.583538695 | 10.64137152 |
| 61200.00 | 0.680640044 | 2.273124516 | 9.653827612 |
| 63000.00 | 0.584088401 | 2.000006841 | 8.757930063 |
| 64800.00 | 0.501233013 | 1.759704467 | 7.945173881 |
| 66600.00 | 0.43013101 | 1.54827461 | 7.207843353 |
| 68400.00 | 0.369115123 | 1.362248214 | 6.538938805 |
| 70200.00 | 0.316754596 | 1.198573034 | 5.932110148 |
| 72000.00 | 0.271821629 | 1.054563554 | 5.381596595 |
| 73800.00 | 0.233262591 | 0.927856925 | 4.882171973 |
| 75600.00 | 0.200173315 | 0.816374195 | 4.429095113 |
| 77400.00 | 0.171777891 | 0.718286202 | 4.018064834 |
| 79200.00 | 0.147410477 | 0.631983558 | 3.645179116 |
| 81000.00 | 0.126499683 | 0.556050243 | 3.306898057 |
| 82800.00 | 0.108555173 | 0.489240375 | 3.000010262 |
| 84600.00 | 0.093156167 | 0.430457764 | 2.721602365 |
| 86400.00 | 0.079941574 | 0.37873793 | 2.469031366 |

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DA#1A DRAINAGE CALCULATIONS

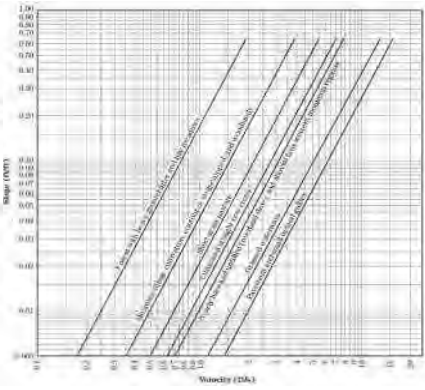
Time of Concentration:

$T_c = T_{OL} + T_1 + \dots + T_n$

Section 2.2
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Table 2.11 Manning's Roughness Coefficient for Concrete Sewer Flow

| Surface | n |
|-------------------------------------------------------|-------|
| Smooth Surface (asphalt, polished, glazed, buff, wet) | 0.012 |
| Polished concrete | 0.015 |
| Cast-in-place concrete | 0.016 |
| Cast-in-place concrete (interior) | 0.017 |
| Cast-in-place concrete (exterior) | 0.018 |
| Cast-in-place concrete (rough) | 0.019 |
| Cast-in-place concrete (very rough) | 0.020 |
| Cast-in-place concrete (extremely rough) | 0.021 |
| Cast-in-place concrete (unusually rough) | 0.022 |
| Cast-in-place concrete (extremely rough) | 0.023 |
| Cast-in-place concrete (extremely rough) | 0.024 |
| Cast-in-place concrete (extremely rough) | 0.025 |
| Cast-in-place concrete (extremely rough) | 0.026 |
| Cast-in-place concrete (extremely rough) | 0.027 |
| Cast-in-place concrete (extremely rough) | 0.028 |
| Cast-in-place concrete (extremely rough) | 0.029 |
| Cast-in-place concrete (extremely rough) | 0.030 |
| Cast-in-place concrete (extremely rough) | 0.031 |
| Cast-in-place concrete (extremely rough) | 0.032 |
| Cast-in-place concrete (extremely rough) | 0.033 |
| Cast-in-place concrete (extremely rough) | 0.034 |
| Cast-in-place concrete (extremely rough) | 0.035 |
| Cast-in-place concrete (extremely rough) | 0.036 |
| Cast-in-place concrete (extremely rough) | 0.037 |
| Cast-in-place concrete (extremely rough) | 0.038 |
| Cast-in-place concrete (extremely rough) | 0.039 |
| Cast-in-place concrete (extremely rough) | 0.040 |
| Cast-in-place concrete (extremely rough) | 0.041 |
| Cast-in-place concrete (extremely rough) | 0.042 |
| Cast-in-place concrete (extremely rough) | 0.043 |
| Cast-in-place concrete (extremely rough) | 0.044 |
| Cast-in-place concrete (extremely rough) | 0.045 |
| Cast-in-place concrete (extremely rough) | 0.046 |
| Cast-in-place concrete (extremely rough) | 0.047 |
| Cast-in-place concrete (extremely rough) | 0.048 |
| Cast-in-place concrete (extremely rough) | 0.049 |
| Cast-in-place concrete (extremely rough) | 0.050 |
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| Cast-in-place concrete (extremely rough) | 0.057 |
| Cast-in-place concrete (extremely rough) | 0.058 |
| Cast-in-place concrete (extremely rough) | 0.059 |
| Cast-in-place concrete (extremely rough) | 0.060 |
| Cast-in-place concrete (extremely rough) | 0.061 |
| Cast-in-place concrete (extremely rough) | 0.062 |
| Cast-in-place concrete (extremely rough) | 0.063 |
| Cast-in-place concrete (extremely rough) | 0.064 |
| Cast-in-place concrete (extremely rough) | 0.065 |
| Cast-in-place concrete (extremely rough) | 0.066 |
| Cast-in-place concrete (extremely rough) | 0.067 |
| Cast-in-place concrete (extremely rough) | 0.068 |
| Cast-in-place concrete (extremely rough) | 0.069 |
| Cast-in-place concrete (extremely rough) | 0.070 |
| Cast-in-place concrete (extremely rough) | 0.071 |
| Cast-in-place concrete (extremely rough) | 0.072 |
| Cast-in-place concrete (extremely rough) | 0.073 |
| Cast-in-place concrete (extremely rough) | 0.074 |
| Cast-in-place concrete (extremely rough) | 0.075 |
| Cast-in-place concrete (extremely rough) | 0.076 |
| Cast-in-place concrete (extremely rough) | 0.077 |
| Cast-in-place concrete (extremely rough) | 0.078 |
| Cast-in-place concrete (extremely rough) | 0.079 |
| Cast-in-place concrete (extremely rough) | 0.080 |



| | | |
|------------|----------------------------------------------------------------------|---------------------|
| $T_{OL} =$ | $T_t = T_{OL}$; multiply by 60 to convert hrs. to min. (L=max 300') | $T =$ |
| n = | 0.15 | D = 2177.48 (ft) |
| L = | 100 (ft) | S = 0.0093 (ft/ft) |
| $P_2 =$ | 4.89 (in) | V = 0.675 (ft/s) |
| S = | 0.0093 (ft/ft) | |
| $T_{OL} =$ | 10.77 (min) | $T_1 =$ 53.76 (min) |

$T_c = 64.53$ (min)

Intensity:

SEE FIG. 2.1-2.1a

| | |
|--------------|-------------|
| I (100-YR) = | 4.4 (in/hr) |
| I (10-YR) = | 2.9 (in/hr) |
| I (2-YR) = | 2 (in/hr) |

Peak Flow Rate:

$Q = CIA$

C = 0.4 Single family residential districts; lots 1/4 - 1/2 acre; sub-basin slope <1%

| | | |
|------------|------------|----------|
| i (100-YR) | i (10-YR) | i (2-YR) |
| 4.4 | 2.9 | 2 |
| A = | 65.25 (Ac) | |

| | |
|--------------|--------------|
| Q (100-YR) = | 114.84 (cfs) |
| Q (10-YR) = | 75.69 (cfs) |
| Q (2-YR) = | 52.20 (cfs) |

DA#1A EXISTING CALCULATIONS

Volume (100-yr) = 1.38*area*43560 = 3922360.20 cft
 Volume (10-yr) = 0.70*area*43560 = 1989603 cft
 Volume (2-yr) = 0.41*area*43560 = 1165338.9 cft
 A = 65.25 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

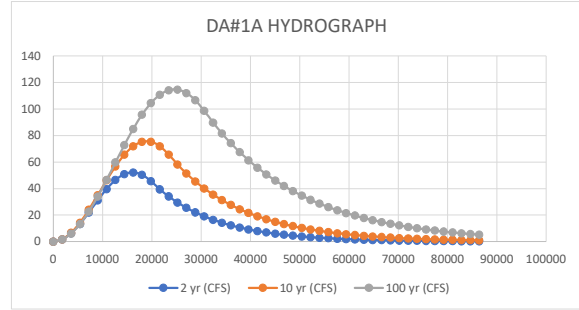
$q_i = \left(\frac{Q_p}{2}\right) \left[1 - \cos\left(\frac{\pi t_i}{T_p}\right)\right]$ $t_i \leq 1.25 T_p$
 $q_i = 4.34 Q_p e^{-1.3t_i/T_p}$ $t_i > 1.25 T_p$

| DA#1A Existing Conditions | | | |
|---------------------------|-----------|-----------|------------|
| | 2 - Year | 10 - Year | 100 - Year |
| Qp= | 52.20 | 75.69 | 114.84 |
| TP= | 16060.791 | 18910.940 | 24571.942 |
| 1.25*TP= | 20075.989 | 23638.675 | 30714.928 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) |
|----------|-------------|-------------|--------------|
| 0 | 0 | 0 | 0 |
| 1800.00 | 1.601143208 | 1.679416881 | 1.513844815 |
| 3600.00 | 6.208123821 | 6.56861528 | 5.975555989 |
| 5400.00 | 13.25569772 | 14.23366721 | 13.14987269 |
| 7200.00 | 21.87917717 | 23.99428108 | 22.65850158 |
| 9000.00 | 31.02052189 | 34.9841792 | 34.00006373 |
| 10800.00 | 39.55815318 | 46.22798197 | 46.57653181 |
| 12600.00 | 46.44456375 | 56.72777516 | 59.72476332 |
| 14400.00 | 50.83483944 | 65.55167713 | 72.75146735 |
| 16200.00 | 52.19032431 | 71.91654561 | 84.96976098 |
| 18000.00 | 50.34470991 | 75.25748339 | 95.73538785 |
| 19800.00 | 45.52444014 | 75.27797428 | 104.480689 |
| 21600.00 | 39.43286702 | 71.97619967 | 110.7445349 |
| 23400.00 | 34.08656181 | 65.64519991 | 114.1966403 |
| 25200.00 | 29.46510826 | 58.10140354 | 114.6549797 |
| 27000.00 | 25.47023105 | 51.3390629 | 112.0953853 |
| 28800.00 | 22.016979 | 45.36378157 | 106.6528216 |
| 30600.00 | 19.0319186 | 40.08395484 | 98.6142687 |
| 32400.00 | 16.45157248 | 35.41863971 | 89.77118156 |
| 34200.00 | 14.22106949 | 31.29631405 | 81.61666256 |
| 36000.00 | 12.29297793 | 27.65378007 | 74.20287326 |
| 37800.00 | 10.62629689 | 24.4351955 | 67.46252821 |
| 39600.00 | 9.185584337 | 21.59121747 | 61.33445394 |
| 41400.00 | 7.940203487 | 19.07824603 | 55.7630338 |
| 43200.00 | 6.863671282 | 16.85775581 | 50.69770314 |
| 45000.00 | 5.933095234 | 14.89570532 | 46.09249046 |
| 46800.00 | 5.128686618 | 13.16201513 | 41.90560016 |
| 48600.00 | 4.433339663 | 11.6301067 | 38.09903322 |
| 50400.00 | 3.832267798 | 10.27649494 | 34.6382423 |
| 52200.00 | 3.312689211 | 9.080428144 | 31.49181825 |
| 54000.00 | 2.863555051 | 8.023569884 | 28.63120501 |
| 55800.00 | 2.475314468 | 7.089717869 | 26.03044048 |
| 57600.00 | 2.139711514 | 6.264555578 | 23.66592084 |
| 59400.00 | 1.849609584 | 5.535432765 | 21.5161864 |
| 61200.00 | 1.598839653 | 4.891171531 | 19.56172677 |
| 63000.00 | 1.38206909 | 4.321894955 | 17.78480382 |
| 64800.00 | 1.194688265 | 3.81887568 | 16.16929071 |
| 66600.00 | 1.032712517 | 3.374402111 | 14.7005255 |
| 68400.00 | 0.89269743 | 2.981660195 | 13.3651781 |
| 70200.00 | 0.771665578 | 2.634628958 | 12.15112926 |
| 72000.00 | 0.667043216 | 2.327988199 | 11.04736063 |
| 73800.00 | 0.576605546 | 2.057036927 | 10.04385471 |
| 75600.00 | 0.498429408 | 1.817621292 | 9.131503965 |
| 77400.00 | 0.430852386 | 1.606070906 | 8.302028167 |
| 79200.00 | 0.372437451 | 1.419142572 | 7.547899222 |
| 81000.00 | 0.321942409 | 1.253970564 | 6.862272872 |
| 82800.00 | 0.278293481 | 1.108022694 | 6.238926565 |
| 84600.00 | 0.240562471 | 0.979061491 | 5.672202987 |
| 86400.00 | 0.207947029 | 0.865109901 | 5.156958716 |

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DA#1B EXISTING CALCULATIONS

Volume (100-yr) = 1.38*area*43560 = 2495282.33 cft
 Volume (10-yr) = 0.70*area*43560 = 1265722.92 cft
 Volume (2-yr) = 0.41*area*43560 = 741351.996 cft
 A = 41.51 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

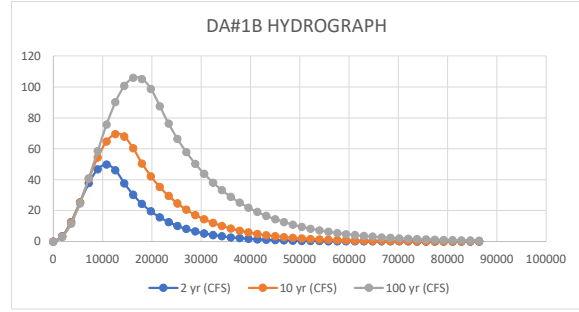
$q_i = \left(\frac{Q_p}{2}\right) \left[1 - \cos\left(\frac{\pi t_i}{T_p}\right)\right]$ $t_i \leq 1.25 T_p$
 $q_i = 4.34 Q_p e^{-1.3t_i/T_p}$ $t_i > 1.25 T_p$

| DA#1B Existing Conditions | | | |
|---------------------------|-----------|-----------|------------|
| | 2 - Year | 10 - Year | 100 - Year |
| Qp= | 49.81 | 69.74 | 106.27 |
| TP= | 10707.194 | 13057.554 | 16893.210 |
| 1.25*TP= | 13383.993 | 16321.942 | 21116.513 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) |
|----------|-------------|-------------|--------------|
| 0 | 0 | 0 | 0 |
| 1800.00 | 3.39350928 | 3.219028019 | 2.949130438 |
| 3600.00 | 12.64928764 | 12.28175493 | 11.46913941 |
| 5400.00 | 25.24508585 | 25.51485062 | 24.61422251 |
| 7200.00 | 37.74848135 | 40.4749735 | 40.92514686 |
| 9000.00 | 46.75223181 | 54.39990594 | 58.59124021 |
| 10800.00 | 49.80276695 | 64.71856652 | 75.65139326 |
| 12600.00 | 46.06879958 | 69.52573117 | 90.21176204 |
| 14400.00 | 37.62892667 | 67.93381125 | 100.6560031 |
| 16200.00 | 30.24190159 | 60.2367368 | 105.8247034 |
| 18000.00 | 24.30504117 | 50.42748622 | 105.1440868 |
| 19800.00 | 19.53366009 | 42.15400831 | 98.68970813 |
| 21600.00 | 15.69896031 | 35.23793372 | 87.4974558 |
| 23400.00 | 12.61705966 | 29.45655757 | 76.17950999 |
| 25200.00 | 10.14017434 | 24.62371349 | 66.32555985 |
| 27000.00 | 8.149532333 | 20.58377883 | 57.74623505 |
| 28800.00 | 6.549678044 | 17.20666345 | 50.27666061 |
| 30600.00 | 5.263894998 | 14.38362069 | 43.77328842 |
| 32400.00 | 4.230527113 | 12.02374561 | 38.11113857 |
| 34200.00 | 3.400022163 | 10.05104776 | 33.1813975 |
| 36000.00 | 2.732555636 | 8.402004196 | 28.88932688 |
| 37800.00 | 2.196121069 | 7.023513986 | 25.15244296 |
| 39600.00 | 1.764995261 | 5.871188298 | 21.89893137 |
| 41400.00 | 1.418504797 | 4.907921034 | 19.06626707 |
| 43200.00 | 1.140034709 | 4.102693979 | 16.60001276 |
| 45000.00 | 0.916231754 | 3.429577975 | 14.45277267 |
| 46800.00 | 0.736364095 | 2.866897982 | 12.58328176 |
| 48600.00 | 0.591806689 | 2.396535113 | 10.95561271 |
| 50400.00 | 0.475627695 | 2.003343189 | 9.538485435 |
| 52200.00 | 0.382256078 | 1.674661019 | 8.304666002 |
| 54000.00 | 0.307214469 | 1.399904691 | 7.230443226 |
| 55800.00 | 0.246904457 | 1.170226763 | 6.295173007 |
| 57600.00 | 0.19843405 | 0.978231366 | 5.480881593 |
| 59400.00 | 0.159478984 | 0.817736045 | 4.771920169 |
| 61200.00 | 0.128171281 | 0.683572682 | 4.154664119 |
| 63000.00 | 0.103009669 | 0.571421078 | 3.617251197 |
| 64800.00 | 0.082787593 | 0.477669832 | 3.149353557 |
| 66600.00 | 0.066535362 | 0.399300056 | 2.741979279 |
| 68400.00 | 0.053473645 | 0.333788161 | 2.387299562 |
| 70200.00 | 0.042976105 | 0.279024595 | 2.078498273 |
| 72000.00 | 0.034539363 | 0.233245914 | 1.80964096 |
| 73800.00 | 0.027758857 | 0.194977995 | 1.575560802 |
| 75600.00 | 0.022309449 | 0.162988573 | 1.371759313 |
| 77400.00 | 0.017929828 | 0.136247555 | 1.194319895 |
| 79200.00 | 0.01440998 | 0.11389385 | 1.039832571 |
| 81000.00 | 0.011581122 | 0.095207647 | 0.905328446 |
| 82800.00 | 0.009307604 | 0.07958723 | 0.78822661 |
| 84600.00 | 0.007480406 | 0.066529605 | 0.686264709 |
| 86400.00 | 0.00601191 | 0.055614304 | 0.597495193 |

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DA#2 DRAINAGE CALCULATIONS

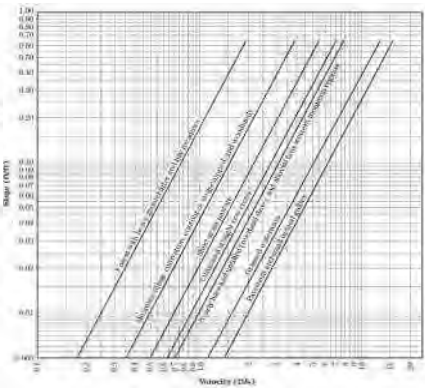
Time of Concentration:

$T_c = T_{OL} + T_1 + \dots + T_n$

Section 2.2
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Table 2.11 Manning's Roughness Coefficient for Gravel Shell Flow

| Surface | n |
|--------------------------------------------------------|-------|
| Smooth Surface (sandstone, asphalt, gravel, surf. w/c) | 0.012 |
| Polished Pipe (cast-iron) | 0.009 |
| Cast-iron Pipe (Rust-free) | 0.010 |
| Cast-iron Pipe (Rusted) | 0.015 |
| Concrete (Smooth) | 0.012 |
| Concrete (Rough) | 0.015 |
| Grass (Dry) | 0.40 |
| Grass (Wet) | 0.30 |
| Wood (Dry) | 0.12 |
| Wood (Wet) | 0.18 |



| $T_{OL} =$ | $T =$ |
|---------------------------------------------------------------------------|----------------------|
| $T = T_{OL}$; multiply by 60 to convert hrs. to min. ($L = \max 300'$) | |
| $n = 0.15$ | $D = 2057.4$ (ft) |
| $L = 100$ (ft) | $S = 0.0131$ (ft/ft) |
| $P_2 = 4.89$ (in) | $V = 0.775$ (ft/s) |
| $S = 0.0131$ (ft/ft) | |
| $T_{OL} = 9.39$ (min) | $T_1 = 44.25$ (min) |

$T_c = 53.63$ (min)

Intensity:

SEE FIG. 2.1-2.1a

| | |
|----------------|-------------|
| I (100-YR) = | 4.9 (in/hr) |
| I (10-YR) = | 3.3 (in/hr) |
| I (2-YR) = | 2.3 (in/hr) |

Peak Flow Rate:

$Q = CIA$

$C = 0.45$ Single family residential districts; lots 1/4 - 1/2 acre; sub-basin slope 1-3.5%

| i (100-YR) | i (10-YR) | i (2-YR) |
|------------------|-------------|------------|
| 4.9 | 3.3 | 2.3 |
| $A = 12.41$ (Ac) | | |

| | |
|----------------|-------------|
| Q (100-YR) = | 27.36 (cfs) |
| Q (10-YR) = | 18.43 (cfs) |
| Q (2-YR) = | 12.84 (cfs) |

DA#2 EXISTING CALCULATIONS

Volume (100-yr) = 1.38*area*43560 = 745999.85 cft
 Volume (10-yr)= 0.70*area*43560= 378405.72 cft
 Volume (2-yr)= 0.41*area*43560= 221637.636 cft
 A= 12.41 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

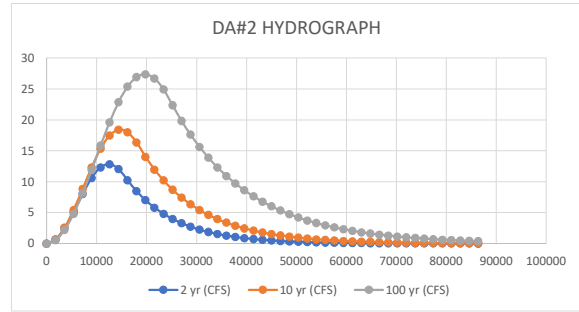
$q_i = \left(\frac{Q_p}{2}\right) \left[1 - \cos\left(\frac{\pi t_i}{T_p}\right)\right]$ $t_i \leq 1.25 T_p$
 $q_i = 4.34 Q_p e^{-1.3t_i/T_p}$ $t_i > 1.25 T_p$

| DA#2 Existing Conditions | | | |
|--------------------------|-----------|-----------|------------|
| | 2 - Year | 10 - Year | 100 - Year |
| Qp= | 12.84 | 18.43 | 27.36 |
| TP= | 12414.138 | 14772.182 | 19612.979 |
| 1.25*TP= | 15517.673 | 18465.228 | 24516.224 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) |
|----------|-------------|-------------|--------------|
| 0 | 0 | 0 | 0 |
| 1800.00 | 0.65484897 | 0.666935359 | 0.56476445 |
| 3600.00 | 2.485850105 | 2.571196558 | 2.212433287 |
| 5400.00 | 5.119600559 | 5.437124697 | 4.806982086 |
| 7200.00 | 8.018989844 | 8.849850956 | 8.134216103 |
| 9000.00 | 10.59273476 | 12.31535258 | 11.91945327 |
| 10800.00 | 12.31596198 | 15.33196711 | 15.85020074 |
| 12600.00 | 12.83724738 | 17.46301251 | 19.60195299 |
| 14400.00 | 12.0502833 | 18.40000083 | 22.86498154 |
| 16200.00 | 10.21978494 | 18.00729462 | 25.36990486 |
| 18000.00 | 8.464075395 | 16.34174161 | 26.90992729 |
| 19800.00 | 7.009988242 | 14.00378197 | 27.35791123 |
| 21600.00 | 5.805706218 | 11.95227444 | 26.67687306 |
| 23400.00 | 4.808314012 | 10.20130594 | 24.92303635 |
| 25200.00 | 3.982268956 | 8.706848513 | 22.34900861 |
| 27000.00 | 3.298134439 | 7.431324133 | 19.83549904 |
| 28800.00 | 2.731530919 | 6.342659837 | 17.6046745 |
| 30600.00 | 2.262267138 | 5.413481243 | 15.62474247 |
| 32400.00 | 1.873620602 | 4.620424226 | 13.86748601 |
| 34200.00 | 1.551741658 | 3.943547428 | 12.30786163 |
| 36000.00 | 1.285159958 | 3.365830831 | 10.92364237 |
| 37800.00 | 1.064375703 | 2.872747797 | 9.69510109 |
| 39600.00 | 0.881521113 | 2.451899789 | 8.60472926 |
| 41400.00 | 0.730080056 | 2.092704616 | 7.63698748 |
| 43200.00 | 0.604655838 | 1.786130342 | 6.778084006 |
| 45000.00 | 0.500778894 | 1.524468181 | 6.015778199 |
| 46800.00 | 0.414747506 | 1.301138658 | 5.339206081 |
| 48600.00 | 0.343495894 | 1.110526167 | 4.738725503 |
| 50400.00 | 0.284484963 | 0.947837773 | 4.205778735 |
| 52200.00 | 0.235611824 | 0.808982688 | 3.7327705 |
| 54000.00 | 0.195134854 | 0.690469412 | 3.312959735 |
| 55800.00 | 0.161611631 | 0.589317937 | 2.940363521 |
| 57600.00 | 0.133847536 | 0.502984817 | 2.609671811 |
| 59400.00 | 0.110853178 | 0.429299213 | 2.316171764 |
| 61200.00 | 0.091809139 | 0.366408304 | 2.055680572 |
| 63000.00 | 0.076036773 | 0.312730705 | 1.824485851 |
| 64800.00 | 0.062974024 | 0.266916696 | 1.619292738 |
| 66600.00 | 0.052155392 | 0.227814287 | 1.437176928 |
| 68400.00 | 0.043195348 | 0.194440251 | 1.275543004 |
| 70200.00 | 0.035774597 | 0.1659554 | 1.132087444 |
| 72000.00 | 0.029628694 | 0.141643485 | 1.004765795 |
| 73800.00 | 0.024538628 | 0.120893185 | 0.891763536 |
| 75600.00 | 0.020323011 | 0.103182735 | 0.79147022 |
| 77400.00 | 0.016831616 | 0.088066807 | 0.702456519 |
| 79200.00 | 0.013940026 | 0.075165313 | 0.623453856 |
| 81000.00 | 0.011545197 | 0.064153844 | 0.553336328 |
| 82800.00 | 0.009561788 | 0.054755519 | 0.491104657 |
| 84600.00 | 0.007919119 | 0.046734017 | 0.435871949 |
| 86400.00 | 0.006558653 | 0.039887639 | 0.386851058 |

ti (hrs)

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DA#3 DRAINAGE CALCULATIONS

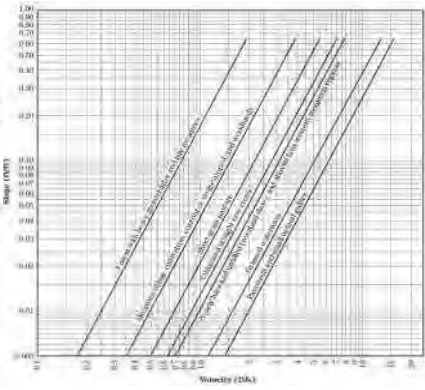
Time of Concentration:

$$T_c = T_{OL} + T_1 + \dots + T_n$$

Section 2.1
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Table 2.1.1. Manning's Roughness Coefficient for Common Channel Flow

| Surface | n |
|--------------------------------------------------------|-------|
| Smooth Surface (concrete, asphalt, gravel, burnt soil) | 0.012 |
| Polished pipe (concrete) | 0.009 |
| Cast-iron pipe (new) | 0.010 |
| Cast-iron pipe (old) | 0.013 |
| Concrete pipe (new) | 0.012 |
| Concrete pipe (old) | 0.015 |
| Grass (dry) | 0.030 |
| Grass (medium) | 0.040 |
| Grass (wet) | 0.050 |
| Wooden flume (new) | 0.012 |
| Wooden flume (old) | 0.015 |
| Smooth stone (new) | 0.015 |
| Smooth stone (old) | 0.018 |



| $T_{OL} = Tt = T_0t$; multiply by 60 to convert hrs. to min. (L=max 300') | T = |
|----------------------------------------------------------------------------|--------------------|
| n = 0.15 | D = 505.56 (ft) |
| L = 100 (ft) | S = 0.0199 (ft/ft) |
| $P_2 = 4.89$ (in) | V = 0.975 (ft/s) |
| $S = 0.0199$ (ft/ft) | |
| $T_{OL} = 7.94$ (min) | $T_1 = 8.64$ (min) |

$T_c = 16.58$ (min)

Intensity:

SEE FIG. 2.1-2.1a

| | |
|--------------|--------------|
| I (100-YR) = | 9.1 (in/hr) |
| I (10-YR) = | 6.15 (in/hr) |
| I (2-YR) = | 4 (in/hr) |

Peak Flow Rate:

$$Q = CIA$$

C = 0.28 Mixed use area. Residential lots b/w 1/4 and 1/2 acres; sub-basin slope 1-3.5%; and MOSTLY golf course

| i (100-YR) | i (10-YR) | i (2-YR) |
|----------------|-----------|----------|
| 9.1 | 6.15 | 4 |
| A = 20.46 (Ac) | | |

| | |
|--------------|-------------|
| Q (100-YR) = | 52.13 (cfs) |
| Q (10-YR) = | 35.23 (cfs) |
| Q (2-YR) = | 22.92 (cfs) |

DA#3 EXISTING CALCULATIONS

Volume (100-yr) = 1.38*area*43560 = 1229907.89 cft
 Volume (10-yr) = 0.70*area*43560 = 623866.32 cft
 Volume (2-yr) = 0.41*area*43560 = 365407.416 cft
 A = 20.46 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

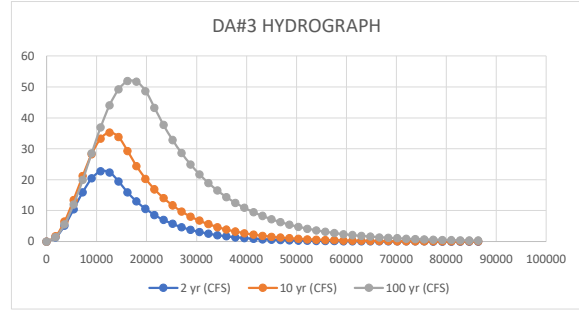
$q_i = \left(\frac{Q_p}{2}\right) \left[1 - \cos\left(\frac{\pi t_i}{T_p}\right)\right]$ $t_i \leq 1.25 T_p$
 $q_i = 4.34 Q_p e^{-1.3t_i/T_p}$ $t_i > 1.25 T_p$

| DA#3 Existing Conditions | | | |
|--------------------------|-----------|-----------|------------|
| | 2 - Year | 10 - Year | 100 - Year |
| Qp= | 22.92 | 35.23 | 52.13 |
| TP= | 11471.994 | 12739.077 | 16972.770 |
| 1.25*TP= | 14339.992 | 15923.846 | 21215.963 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) |
|----------|-------------|-------------|--------------|
| 0 | 0 | 0 | 0 |
| 1800.00 | 1.364014745 | 1.707279062 | 1.433386311 |
| 3600.00 | 5.131290054 | 6.49819074 | 5.575899793 |
| 5400.00 | 10.40484592 | 13.4441025 | 11.97194212 |
| 7200.00 | 15.92906023 | 21.1986736 | 19.9180693 |
| 9000.00 | 20.38862964 | 28.25881914 | 28.54035727 |
| 10800.00 | 22.72174044 | 33.25605619 | 36.89051702 |
| 12600.00 | 22.37288404 | 35.22175974 | 44.05018852 |
| 14400.00 | 19.45053845 | 33.77491331 | 49.23194299 |
| 16200.00 | 15.86157866 | 29.27258823 | 51.86588518 |
| 18000.00 | 12.93484385 | 24.36054331 | 51.66233117 |
| 19800.00 | 10.54814208 | 20.27275708 | 48.64366804 |
| 21600.00 | 8.601827954 | 16.87091599 | 43.26050897 |
| 23400.00 | 7.014642348 | 14.039916 | 37.68915162 |
| 25200.00 | 5.72031986 | 11.68396792 | 32.83530831 |
| 27000.00 | 4.664822193 | 9.723356344 | 28.60657312 |
| 28800.00 | 3.804082048 | 8.0917424 | 24.92244075 |
| 30600.00 | 3.102163304 | 6.733919107 | 21.71277385 |
| 32400.00 | 2.529760675 | 5.603943415 | 18.91646782 |
| 34200.00 | 2.062976202 | 4.663581683 | 16.48028746 |
| 36000.00 | 1.682321514 | 3.881016009 | 14.35785356 |
| 37800.00 | 1.371904181 | 3.229767653 | 12.5087599 |
| 39600.00 | 1.1187642 | 2.687801098 | 10.89780401 |
| 41400.00 | 0.912332911 | 2.236778468 | 9.494317045 |
| 43200.00 | 0.743991754 | 1.861439047 | 8.271579857 |
| 45000.00 | 0.606712445 | 1.549082923 | 7.206314367 |
| 46800.00 | 0.494763535 | 1.289141272 | 6.278240391 |
| 48600.00 | 0.40347113 | 1.07281876 | 5.469689553 |
| 50400.00 | 0.329023748 | 0.892795938 | 4.76526892 |
| 52200.00 | 0.268313192 | 0.742981589 | 4.151567956 |
| 54000.00 | 0.218804781 | 0.618306623 | 3.616903219 |
| 55800.00 | 0.178431525 | 0.514552562 | 3.151095931 |
| 57600.00 | 0.145507832 | 0.428208803 | 2.745278202 |
| 59400.00 | 0.118659127 | 0.356353836 | 2.391724204 |
| 61200.00 | 0.096764472 | 0.296556388 | 2.083703088 |
| 63000.00 | 0.078909758 | 0.246793167 | 1.815350847 |
| 64800.00 | 0.064349547 | 0.205380391 | 1.581558677 |
| 66600.00 | 0.052475946 | 0.170916828 | 1.377875716 |
| 68400.00 | 0.042793229 | 0.142236373 | 1.200424313 |
| 70200.00 | 0.03489714 | 0.118368601 | 1.045826205 |
| 72000.00 | 0.028458016 | 0.098505927 | 0.911138203 |
| 73800.00 | 0.023207021 | 0.08197628 | 0.793796159 |
| 75600.00 | 0.018924925 | 0.068220368 | 0.691566154 |
| 77400.00 | 0.01543295 | 0.056772746 | 0.602501964 |
| 79200.00 | 0.012585305 | 0.047246076 | 0.524908015 |
| 81000.00 | 0.010263099 | 0.039318016 | 0.457307096 |
| 82800.00 | 0.00836938 | 0.032720312 | 0.398412245 |
| 84600.00 | 0.006825085 | 0.027229727 | 0.347102238 |
| 86400.00 | 0.005565739 | 0.022660482 | 0.302400254 |

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DA#4 DRAINAGE CALCULATIONS

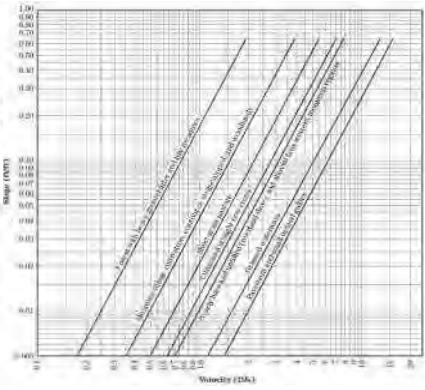
Time of Concentration:

$T_c = T_{OL} + T_1 + \dots + T_n$

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Table 2.1.1 (continued) - Response Coefficients for Ground Sheet Flow

| Surface | α |
|----------|----------|
| Asphalt | 0.012 |
| Concrete | 0.020 |
| Gravel | 0.040 |
| Grass | 0.060 |
| Gravel | 0.080 |
| Gravel | 0.100 |
| Gravel | 0.120 |
| Gravel | 0.140 |
| Gravel | 0.160 |
| Gravel | 0.180 |
| Gravel | 0.200 |
| Gravel | 0.220 |
| Gravel | 0.240 |
| Gravel | 0.260 |
| Gravel | 0.280 |
| Gravel | 0.300 |
| Gravel | 0.320 |
| Gravel | 0.340 |
| Gravel | 0.360 |
| Gravel | 0.380 |
| Gravel | 0.400 |
| Gravel | 0.420 |
| Gravel | 0.440 |
| Gravel | 0.460 |
| Gravel | 0.480 |
| Gravel | 0.500 |
| Gravel | 0.520 |
| Gravel | 0.540 |
| Gravel | 0.560 |
| Gravel | 0.580 |
| Gravel | 0.600 |
| Gravel | 0.620 |
| Gravel | 0.640 |
| Gravel | 0.660 |
| Gravel | 0.680 |
| Gravel | 0.700 |
| Gravel | 0.720 |
| Gravel | 0.740 |
| Gravel | 0.760 |
| Gravel | 0.780 |
| Gravel | 0.800 |
| Gravel | 0.820 |
| Gravel | 0.840 |
| Gravel | 0.860 |
| Gravel | 0.880 |
| Gravel | 0.900 |
| Gravel | 0.920 |
| Gravel | 0.940 |
| Gravel | 0.960 |
| Gravel | 0.980 |
| Gravel | 1.000 |



| $T_{OL} =$ | $T =$ |
|------------------------|-------------------|
| $T_{OL} =$ 12.92 (min) | $T =$ 63.62 (min) |

$T_c = 76.53$ (min)

Intensity:

SEE FIG. 2.1-2.1a

| | |
|---------------|-------------|
| I (100-YR)= | 4.2 (in/hr) |
| I (10-YR)= | 2.7 (in/hr) |
| I (2-YR)= | 1.8 (in/hr) |

Peak Flow Rate:

$Q = CIA$

$C =$ 0.28 Mixed use area. Residential lots b/w 1/4 and 1/2 acres; sub-basin slope <1%; and MOSTLY golf course

| i (100-YR) | i (10-YR) | i (2-YR) |
|------------------|-------------|------------|
| 4.2 | 2.7 | 1.8 |
| $A = 32.15$ (Ac) | | |

| | |
|---------------|-------------|
| Q (100-YR)= | 37.81 (cfs) |
| Q (10-YR)= | 24.31 (cfs) |
| Q (2-YR)= | 16.20 (cfs) |

DA#4 EXISTING CALCULATIONS

Volume (100-yr) = 1.38*area*43560 = 1932626.52 cft
 Volume (10-yr) = 0.70*area*43560 = 980317.8 cft
 Volume (2-yr) = 0.41*area*43560 = 574186.14 cft
 A = 32.15 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

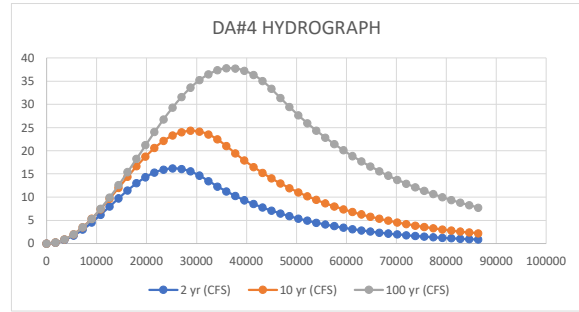
$q_i = \left(\frac{Q_p}{2}\right) \left[1 - \cos\left(\frac{\pi t_i}{T_p}\right)\right]$ $t_i \leq 1.25 T_p$
 $q_i = 1.34 Q_p e^{-1.3t_i/T_p}$ $t_i > 1.25 T_p$

| DA#4 Existing Conditions | | | |
|--------------------------|-----------|-----------|------------|
| | 2 - Year | 10 - Year | 100 - Year |
| Qp= | 16.20 | 24.31 | 37.81 |
| TP= | 25493.320 | 29016.787 | 36774.336 |
| 1.25*TP= | 31866.650 | 36270.983 | 45967.920 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) |
|----------|-------------|-------------|--------------|
| 0 | 0 | 0 | 0 |
| 1800.00 | 0.198500702 | 0.230045614 | 0.223062955 |
| 3600.00 | 0.784275951 | 0.911473117 | 0.886987691 |
| 5400.00 | 1.728621804 | 2.018484225 | 1.976106047 |
| 7200.00 | 2.985263777 | 3.509168408 | 3.464715591 |
| 9000.00 | 4.492624363 | 5.327089589 | 5.317686179 |
| 10800.00 | 6.176840437 | 7.403422766 | 7.491289 |
| 12600.00 | 7.955382668 | 9.659559673 | 9.934228544 |
| 14400.00 | 9.741099586 | 12.01008482 | 12.58885315 |
| 16200.00 | 11.44648815 | 14.36600927 | 15.39251552 |
| 18000.00 | 12.98798155 | 16.63813964 | 18.2790512 |
| 19800.00 | 14.29004409 | 18.74045496 | 21.18033995 |
| 21600.00 | 15.28887258 | 20.59336329 | 24.02791339 |
| 23400.00 | 15.9355228 | 22.12671506 | 26.75457077 |
| 25200.00 | 16.19830783 | 23.28245881 | 29.29596489 |
| 27000.00 | 16.06435079 | 24.01683905 | 31.59212062 |
| 28800.00 | 15.54021578 | 24.30205275 | 33.58885028 |
| 30600.00 | 14.65158627 | 24.12730194 | 35.23903247 |
| 32400.00 | 13.47599894 | 23.49920254 | 36.50372402 |
| 34200.00 | 12.29412486 | 22.4415339 | 37.3530791 |
| 36000.00 | 11.21590368 | 20.99433846 | 37.76705352 |
| 37800.00 | 10.23224481 | 19.396069 | 37.73587779 |
| 39600.00 | 9.334854945 | 17.89331969 | 37.26028762 |
| 41400.00 | 8.516168096 | 16.50699889 | 36.3515066 |
| 43200.00 | 7.769281845 | 15.22808608 | 35.03098134 |
| 45000.00 | 7.087899124 | 14.04825959 | 33.32987531 |
| 46800.00 | 6.466275132 | 12.95984253 | 31.37435965 |
| 48600.00 | 5.8991689 | 11.95575276 | 29.44015782 |
| 50400.00 | 5.381799105 | 11.02945686 | 27.62519785 |
| 52200.00 | 4.909803753 | 10.17492759 | 25.92212856 |
| 54000.00 | 4.479203408 | 9.386604688 | 24.32405201 |
| 55800.00 | 4.086367639 | 8.659358682 | 22.82449548 |
| 57600.00 | 3.727984411 | 7.988457516 | 21.4173853 |
| 59400.00 | 3.401032163 | 7.369535763 | 20.09702223 |
| 61200.00 | 3.102754331 | 6.798566213 | 18.85805839 |
| 63000.00 | 2.830636105 | 6.271833673 | 17.69547558 |
| 64800.00 | 2.582383233 | 5.785910792 | 16.60456499 |
| 66600.00 | 2.355902671 | 5.33763576 | 15.58090808 |
| 68400.00 | 2.149284942 | 4.924091734 | 14.62035873 |
| 70200.00 | 1.960788032 | 4.54258786 | 13.7190264 |
| 72000.00 | 1.788822706 | 4.190641764 | 12.87326042 |
| 73800.00 | 1.631939109 | 3.865963396 | 12.07963518 |
| 75600.00 | 1.48881454 | 3.566440135 | 11.33493623 |
| 77400.00 | 1.358242304 | 3.29012304 | 10.63614733 |
| 79200.00 | 1.239121534 | 3.035214164 | 9.98043815 |
| 81000.00 | 1.130447911 | 2.800054865 | 9.365152868 |
| 82800.00 | 1.031305199 | 2.583115004 | 8.787799385 |
| 84600.00 | 0.940857516 | 2.382982993 | 8.246039239 |
| 86400.00 | 0.858342289 | 2.198356611 | 7.737678133 |

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DA#4A DRAINAGE CALCULATIONS

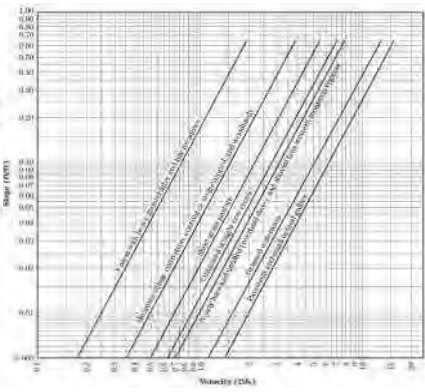
Time of Concentration:

$T_c = T_{OL} + T_1 + \dots + T_n$

Section 2.1
 n = 0.15
 L = 100 ft
 P₂ = 4.89 in
 S = 0.0035 ft/ft
 T_{OL} = 15.92 (min)

Table 2.1.1 (continued) Hydraulic Conditions for Overland Sheet Flow

| Surface | n |
|-----------------|-------|
| Asphalt | 0.012 |
| Concrete | 0.015 |
| Grass (mowed) | 0.04 |
| Grass (pasture) | 0.05 |
| Grass (rough) | 0.07 |
| Grass (rough) | 0.10 |
| Grass (rough) | 0.15 |
| Grass (rough) | 0.20 |
| Grass (rough) | 0.25 |
| Grass (rough) | 0.30 |
| Grass (rough) | 0.35 |
| Grass (rough) | 0.40 |
| Grass (rough) | 0.45 |
| Grass (rough) | 0.50 |
| Grass (rough) | 0.55 |
| Grass (rough) | 0.60 |
| Grass (rough) | 0.65 |
| Grass (rough) | 0.70 |
| Grass (rough) | 0.75 |
| Grass (rough) | 0.80 |
| Grass (rough) | 0.85 |
| Grass (rough) | 0.90 |
| Grass (rough) | 0.95 |
| Grass (rough) | 1.00 |



| | | |
|-------------------|--------------------------------------------------------------------------|------------------|
| T _{OL} = | Tt=T _{OL} ; multiply by 60 to convert hrs. to min. (L=max 300') | T = |
| n = | 0.15 | D = |
| L = | 100 (ft) | S = |
| P ₂ = | 4.89 (in) | V = |
| S = | 0.0035 (ft/ft) | |
| T _{OL} = | 15.92 (min) | T ₁ = |
| | | 130.58 (min) |

T_c = 146.50 (min)

Intensity:

SEE FIG. 2.1-2.1a

| | |
|--------------|-------------|
| I (100-YR) = | 3.1 (in/hr) |
| I (10-YR) = | 1.8 (in/hr) |
| I (2-YR) = | 1.2 (in/hr) |

Peak Flow Rate:

Q=CIA

C = 0.35 Mixed use area. Residential lots b/w 1/4 and 1/2 acres; sub-basin slope <1%; and golf course

| | | |
|------------|------------|----------|
| i (100-YR) | i (10-YR) | i (2-YR) |
| 3.1 | 1.8 | 1.2 |
| A = | 60.49 (Ac) | |

| | |
|--------------|-------------|
| Q (100-YR) = | 65.63 (cfs) |
| Q (10-YR) = | 38.11 (cfs) |
| Q (2-YR) = | 25.41 (cfs) |

DA#4A EXISTING CALCULATIONS

Volume (100-yr) = 1.38*area*43560 = 3636223.27 cft
 Volume (10-yr) = 0.70*area*43560 = 1844461.08 cft
 Volume (2-yr) = 0.41*area*43560 = 1080327.204 cft
 A = 60.49 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

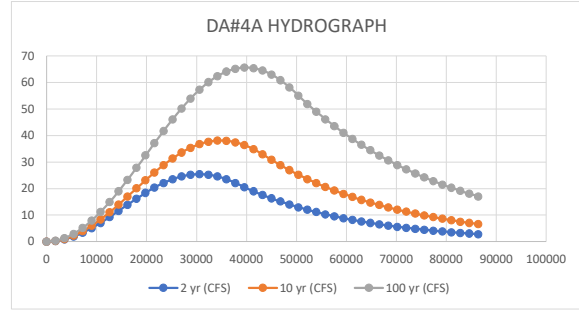
$q_i = \left(\frac{Q_p}{2}\right) \left[1 - \cos\left(\frac{\pi t_i}{T_p}\right)\right]$ $t_i \leq 1.25 T_p$
 $q_i = 1.34 Q_p e^{-1.3 t_i / T_p}$ $t_i > 1.25 T_p$

| DA#4A Existing Conditions | | | |
|---------------------------|-----------|-----------|------------|
| | 2 - Year | 10 - Year | 100 - Year |
| Qp= | 25.41 | 38.11 | 65.63 |
| TP= | 30591.984 | 34820.144 | 39858.635 |
| 1.25*TP= | 38239.979 | 43525.180 | 49823.293 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) |
|----------|-------------|-------------|--------------|
| 0 | 0 | 0 | 0 |
| 1800.00 | 0.216404059 | 0.250722345 | 0.329704346 |
| 3600.00 | 0.858243005 | 0.996291236 | 1.312192228 |
| 5400.00 | 1.903648358 | 2.217085872 | 2.92772131 |
| 7200.00 | 3.317001485 | 3.880979155 | 5.143828782 |
| 9000.00 | 5.050147186 | 5.944183161 | 7.915983674 |
| 10800.00 | 7.044034414 | 8.352401483 | 11.18848167 |
| 12600.00 | 9.230728243 | 11.04225813 | 14.89556445 |
| 14400.00 | 11.53572452 | 13.94296537 | 18.96274104 |
| 16200.00 | 13.88048833 | 16.97818661 | 23.30828467 |
| 18000.00 | 16.18512982 | 20.06804529 | 27.84487499 |
| 19800.00 | 18.37112617 | 23.13122701 | 32.48135271 |
| 21600.00 | 20.36399699 | 26.08711941 | 37.1245514 |
| 23400.00 | 22.09584199 | 28.85793361 | 41.68116955 |
| 25200.00 | 23.50765443 | 31.37075133 | 46.05964544 |
| 27000.00 | 24.5513316 | 33.55944391 | 50.17199698 |
| 28800.00 | 25.19131376 | 35.36641251 | 53.93558963 |
| 30600.00 | 25.4057957 | 36.74410396 | 57.2747969 |
| 32400.00 | 25.18746966 | 37.65626216 | 60.12251999 |
| 34200.00 | 24.54377436 | 38.07888228 | 62.42153611 |
| 36000.00 | 23.49664154 | 38.00084241 | 64.1256483 |
| 37800.00 | 22.08174868 | 37.42419629 | 65.20061375 |
| 39600.00 | 20.49248126 | 36.36411924 | 65.62483184 |
| 41400.00 | 18.98344767 | 34.84850885 | 65.38977825 |
| 43200.00 | 17.5855369 | 32.91725074 | 64.5001762 |
| 45000.00 | 16.29056605 | 30.82280898 | 62.97390154 |
| 46800.00 | 15.09095478 | 28.8195071 | 60.8416236 |
| 48600.00 | 13.97968098 | 26.9464081 | 58.14618886 |
| 50400.00 | 12.9502396 | 25.19504956 | 55.04345471 |
| 52200.00 | 11.99660464 | 23.55751905 | 51.90501839 |
| 54000.00 | 11.11319383 | 22.02641843 | 48.94552765 |
| 55800.00 | 10.29483599 | 20.59483036 | 46.15477946 |
| 57600.00 | 9.536740706 | 19.25628713 | 43.52315256 |
| 59400.00 | 8.834470352 | 18.00474137 | 41.04157426 |
| 61200.00 | 8.183914065 | 16.83453874 | 38.70148918 |
| 63000.00 | 7.581263704 | 15.74039242 | 36.49482973 |
| 64800.00 | 7.022991554 | 14.71735919 | 34.41398834 |
| 66600.00 | 6.505829672 | 13.76081713 | 32.45179117 |
| 68400.00 | 6.026750766 | 12.86644469 | 30.60147344 |
| 70200.00 | 5.582950465 | 12.03020122 | 28.85665608 |
| 72000.00 | 5.17183091 | 11.24830867 | 27.21132371 |
| 73800.00 | 4.790985541 | 10.51723455 | 25.65980397 |
| 75600.00 | 4.438185018 | 9.833675969 | 24.1967479 |
| 77400.00 | 4.111364162 | 9.194544684 | 22.81711152 |
| 79200.00 | 3.808609871 | 8.596953185 | 21.51613847 |
| 81000.00 | 3.528149923 | 8.038201631 | 20.28934355 |
| 82800.00 | 3.268342598 | 7.515765651 | 19.13249733 |
| 84600.00 | 3.027667069 | 7.027284947 | 18.0416115 |
| 86400.00 | 2.804714502 | 6.570552625 | 17.01292519 |

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DA#4B DRAINAGE CALCULATIONS

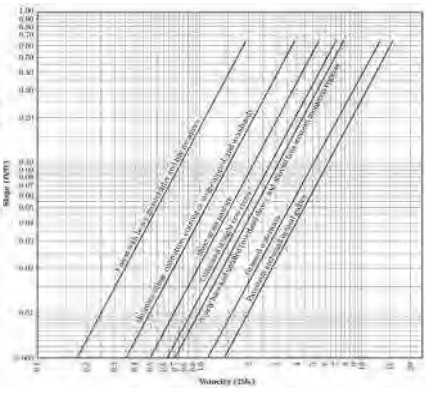
Time of Concentration:

$T_c = T_{OL} + T_1 + \dots + T_n$

Section 2.2
 1. Determine the length of the longest overland flow path.
 2. Determine the length of the longest pipe flow path.
 3. Determine the time of travel for overland flow.
 4. Determine the time of travel for pipe flow.
 5. Determine the time of travel for the longest pipe flow path.
 6. Determine the time of travel for the longest overland flow path.
 7. Determine the time of travel for the longest pipe flow path.
 8. Determine the time of travel for the longest overland flow path.
 9. Determine the time of travel for the longest pipe flow path.
 10. Determine the time of travel for the longest overland flow path.

Table 2.11 (continued) Longitudinal Conditions for Overland Sheet Flow

| Surface | n |
|---------------------------------------------------------------------------------------------------------------------------|-------|
| Asphalt | 0.012 |
| Concrete | 0.015 |
| Gravel | 0.020 |
| Grass | 0.030 |
| Grass (dry) | 0.040 |
| Grass (flooded) | 0.050 |
| Grass (matted) | 0.060 |
| Grass (matted, dry) | 0.070 |
| Grass (matted, flooded) | 0.080 |
| Grass (matted, dry, matted) | 0.090 |
| Grass (matted, dry, matted, flooded) | 0.100 |
| Grass (matted, dry, matted, flooded, matted) | 0.110 |
| Grass (matted, dry, matted, flooded, matted, flooded) | 0.120 |
| Grass (matted, dry, matted, flooded, matted, flooded, matted) | 0.130 |
| Grass (matted, dry, matted, flooded, matted, flooded, matted, flooded) | 0.140 |
| Grass (matted, dry, matted, flooded, matted, flooded, matted, flooded, matted) | 0.150 |
| Grass (matted, dry, matted, flooded, matted, flooded, matted, flooded, matted, flooded) | 0.160 |
| Grass (matted, dry, matted, flooded, matted, flooded, matted, flooded, matted, flooded, matted) | 0.170 |
| Grass (matted, dry, matted, flooded, matted, flooded, matted, flooded, matted, flooded, matted, flooded) | 0.180 |
| Grass (matted, dry, matted, flooded, matted, flooded, matted, flooded, matted, flooded, matted, flooded, matted) | 0.190 |
| Grass (matted, dry, matted, flooded, matted, flooded, matted, flooded, matted, flooded, matted, flooded, matted, flooded) | 0.200 |



| | | |
|------------|----------------------------------------------------------------------|-------------|
| $T_{OL} =$ | $T_t = T_{OL}$; multiply by 60 to convert hrs. to min. (L=max 300') | $T =$ |
| n= | 0.15 | D= |
| L= | 100 (ft) | S= |
| $P_2 =$ | 4.89 (in) | V= |
| S= | 0.0061 (ft/ft) | |
| $T_{OL} =$ | 12.74 (min) | $T_1 =$ |
| | | 90.13 (min) |

$T_c = 102.87$ (min)

Intensity:

SEE FIG. 2.1-2.1a

| | |
|-------------|-------------|
| I (100-YR)= | 3.6 (in/hr) |
| I (10-YR)= | 2.2 (in/hr) |
| I (2-YR)= | 1.5 (in/hr) |

Peak Flow Rate:

$Q = CIA$

C= 0.35 Mixed use area. Residential lots b/w 1/4 and 1/2 acres; sub-basin slope <1%; and golf course

| | | |
|------------|------------|----------|
| i (100-YR) | i (10-YR) | i (2-YR) |
| 3.6 | 2.2 | 1.5 |
| A= | 49.53 (Ac) | |

| | |
|--------------------|--------------------|
| Q (100-YR)= | 62.41 (cfs) |
| Q (10-YR)= | 38.14 (cfs) |
| Q (2-YR)= | 26.00 (cfs) |

DA#4B EXISTING CALCULATIONS

Volume (100-yr) = 1.38*area*43560 = 2977386.98 cft
 Volume (10-yr) = 0.70*area*43560 = 1510268.76 cft
 Volume (2-yr) = 0.41*area*43560 = 884585.988 cft
 A = 49.53 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

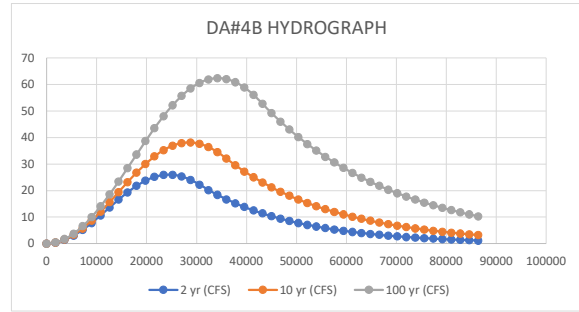
$q_i = \left(\frac{Q_p}{2}\right) \left[1 - \cos\left(\frac{\pi t_i}{T_p}\right)\right]$ $t_i \leq 1.25 T_p$
 $q_i = 4.34 Q_p e^{-1.3t_i/T_p}$ $t_i > 1.25 T_p$

| DA#4B Existing Conditions | | | |
|---------------------------|-----------|-----------|------------|
| | 2 - Year | 10 - Year | 100 - Year |
| Qp= | 26.00 | 38.14 | 62.41 |
| TP= | 24473.587 | 28489.209 | 34322.713 |
| 1.25*TP= | 30591.984 | 35611.511 | 42903.392 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) |
|----------|-------------|-------------|--------------|
| 0 | 0 | 0 | 0 |
| 1800.00 | 0.345528667 | 0.37441797 | 0.422549702 |
| 3600.00 | 1.363749262 | 1.482968597 | 1.678754836 |
| 5400.00 | 3.00054172 | 3.282119427 | 3.734593432 |
| 7200.00 | 5.16890788 | 5.70121834 | 6.534386936 |
| 9000.00 | 7.75359586 | 8.645268039 | 10.00230817 |
| 10800.00 | 10.61722452 | 11.99865657 | 14.04443495 |
| 12600.00 | 13.60758818 | 15.62969735 | 18.55129382 |
| 14400.00 | 16.56574392 | 19.39580048 | 23.40082492 |
| 16200.00 | 19.334461 | 23.14907223 | 28.46168775 |
| 18000.00 | 21.76657762 | 26.74212271 | 33.59681828 |
| 19800.00 | 23.73282289 | 30.0338539 | 38.66714108 |
| 21600.00 | 25.12868768 | 32.89500049 | 43.5353593 |
| 23400.00 | 25.87997953 | 35.21320611 | 48.06955684 |
| 25200.00 | 25.94676608 | 36.8974355 | 52.14700292 |
| 27000.00 | 25.3254975 | 37.88154948 | 55.65724413 |
| 28800.00 | 24.04919523 | 38.12690218 | 58.50521214 |
| 30600.00 | 22.21283016 | 37.62385868 | 60.61377506 |
| 32400.00 | 20.18736217 | 36.39217334 | 61.9258264 |
| 34200.00 | 18.34658566 | 34.48021408 | 62.40583169 |
| 36000.00 | 16.67365962 | 32.02000481 | 62.04079088 |
| 37800.00 | 15.15327867 | 29.49511022 | 60.84059043 |
| 39600.00 | 13.77153305 | 27.1693128 | 58.83773552 |
| 41400.00 | 12.51578134 | 25.02691303 | 56.08646974 |
| 43200.00 | 11.37453485 | 23.05344932 | 52.73768768 |
| 45000.00 | 10.33735246 | 21.23560045 | 49.26204508 |
| 46800.00 | 9.394745132 | 19.56109561 | 46.01546242 |
| 48600.00 | 8.538089073 | 18.01863162 | 42.98284365 |
| 50400.00 | 7.759546852 | 16.59779655 | 40.15008763 |
| 52200.00 | 7.051995691 | 15.28899953 | 37.50402252 |
| 54000.00 | 6.408962299 | 14.08340595 | 35.0323446 |
| 55800.00 | 5.824563647 | 12.97287784 | 32.72356099 |
| 57600.00 | 5.293453152 | 11.94991893 | 30.56693624 |
| 59400.00 | 4.810771754 | 11.00762408 | 28.55244242 |
| 61200.00 | 4.372103465 | 10.13963262 | 26.67071249 |
| 63000.00 | 3.973434968 | 9.340085471 | 24.91299674 |
| 64800.00 | 3.611118898 | 8.60358554 | 23.27112208 |
| 66600.00 | 3.281840472 | 7.925161325 | 21.7374541 |
| 68400.00 | 2.982587168 | 7.300233343 | 20.30486149 |
| 70200.00 | 2.710621156 | 6.724583219 | 18.96668296 |
| 72000.00 | 2.463454255 | 6.194325216 | 17.7166962 |
| 73800.00 | 2.238825169 | 5.705879997 | 16.549089 |
| 75600.00 | 2.034678796 | 5.255950471 | 15.45843218 |
| 77400.00 | 1.849147428 | 4.841499536 | 14.43965438 |
| 79200.00 | 1.680533663 | 4.459729574 | 13.48801846 |
| 81000.00 | 1.527294876 | 4.108063571 | 12.59909948 |
| 82800.00 | 1.388029107 | 3.78412772 | 11.76876412 |
| 84600.00 | 1.261462231 | 3.485735397 | 10.99315147 |
| 86400.00 | 1.146436304 | 3.2108724 | 10.26865505 |

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DA#5 DRAINAGE CALCULATIONS

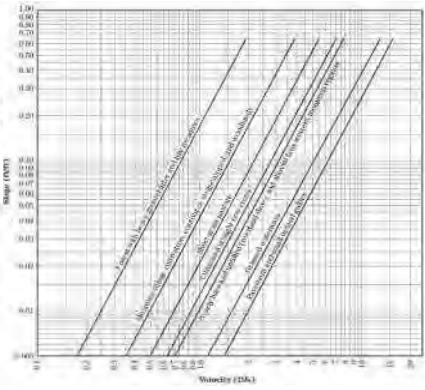
Time of Concentration:

$T_c = T_{OL} + T_1 + \dots + T_n$

Section 2.1
 1. Determine the length of the longest flow path (L) in feet.
 2. Determine the slope of the longest flow path (S) in ft/ft.
 3. Determine the runoff coefficient (C) for the area of the basin.
 4. Determine the time of travel (T) in minutes for the longest flow path.
 5. Determine the time of concentration (T_c) in minutes for the basin.
 6. Determine the peak flow rate (Q) in cfs for the basin.
 7. Determine the peak flow rate (Q) in cfs for the basin.
 8. Determine the peak flow rate (Q) in cfs for the basin.
 9. Determine the peak flow rate (Q) in cfs for the basin.
 10. Determine the peak flow rate (Q) in cfs for the basin.

Table 2.1.1 (continued) - Runoff Coefficients for Various Land Uses

| Surface | C |
|--------------------------------------------------------------------|------|
| Asphalt (Surface Impervious, adjacent to street, curb and gutter) | 0.90 |
| Asphalt (Surface Impervious, not adjacent to street) | 0.85 |
| Concrete (Surface Impervious, adjacent to street, curb and gutter) | 0.90 |
| Concrete (Surface Impervious, not adjacent to street) | 0.85 |
| Grass (Grass Cover 50% or more) | 0.25 |
| Grass (Grass Cover 25% to 50%) | 0.30 |
| Grass (Grass Cover 10% to 25%) | 0.35 |
| Grass (Grass Cover 5% to 10%) | 0.40 |
| Grass (Grass Cover 0% to 5%) | 0.45 |
| Grass (Grass Cover 0% to 5%) | 0.50 |
| Grass (Grass Cover 0% to 5%) | 0.55 |
| Grass (Grass Cover 0% to 5%) | 0.60 |
| Grass (Grass Cover 0% to 5%) | 0.65 |
| Grass (Grass Cover 0% to 5%) | 0.70 |
| Grass (Grass Cover 0% to 5%) | 0.75 |
| Grass (Grass Cover 0% to 5%) | 0.80 |
| Grass (Grass Cover 0% to 5%) | 0.85 |
| Grass (Grass Cover 0% to 5%) | 0.90 |
| Grass (Grass Cover 0% to 5%) | 0.95 |
| Grass (Grass Cover 0% to 5%) | 1.00 |



| $T_{OL} = Tt = T_0$; multiply by 60 to convert hrs. to min. (L = max 300') | T = |
|-----------------------------------------------------------------------------|------------------------------|
| n = 0.15 | D = 1638.56 (ft) |
| L = 100 (ft) | S = 0.0113 (ft/ft) |
| P ₂ = 4.89 (in) | V = 0.7 (ft/s) |
| S = 0.0113 (ft/ft) | |
| T _{OL} = 9.96 (min) | T ₁ = 39.01 (min) |

T_c = 48.97 (min)

Intensity:

SEE FIG. 2.1-2.1a

| | |
|--------------|-------------|
| I (100-YR) = | 5.1 (in/hr) |
| I (10-YR) = | 3.5 (in/hr) |
| I (2-YR) = | 2.4 (in/hr) |

Peak Flow Rate:

$Q = CIA$

C = 0.4 Mixed use area. Residential lots b/w 1/4 and 1/2 acres; sub-basin slope 1-3.5%; and golf course

| i (100-YR) | i (10-YR) | i (2-YR) |
|----------------|-----------|----------|
| 5.1 | 3.5 | 2.4 |
| A = 28.49 (Ac) | | |

| | |
|---------------------|--------------------|
| Q (100-YR) = | 58.12 (cfs) |
| Q (10-YR) = | 39.89 (cfs) |
| Q (2-YR) = | 27.35 (cfs) |

DA#5 EXISTING CALCULATIONS

Volume (100-yr) = 1.38*area*43560 = 1712613.67 cft
 Volume (10-yr) = 0.70*area*43560 = 868717.08 cft
 Volume (2-yr) = 0.41*area*43560 = 508820.004 cft
 A = 28.49 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

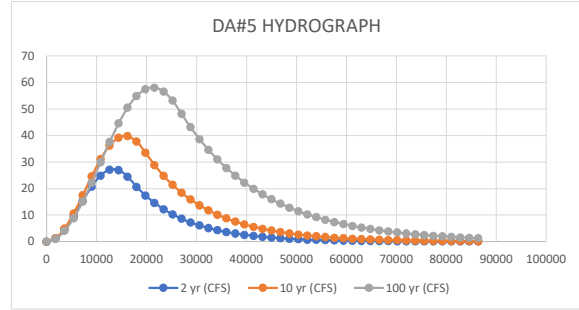
$q_i = \left(\frac{Q_p}{2}\right) \left[1 - \cos\left(\frac{\pi t_i}{T_p}\right)\right]$ $t_i \leq 1.25 T_p$
 $q_i = 1.34 Q_p e^{-1.3t_i/T_p}$ $t_i > 1.25 T_p$

| DA#5 Existing Conditions | | | |
|--------------------------|-----------|-----------|------------|
| | 2 - Year | 10 - Year | 100 - Year |
| Qp= | 27.35 | 39.89 | 58.12 |
| TP= | 13383.993 | 15669.065 | 21199.323 |
| 1.25*TP= | 16729.991 | 19586.331 | 26499.154 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) |
|----------|-------------|-------------|--------------|
| 0 | 0 | 0 | 0 |
| 1800.00 | 1.202560033 | 1.284695713 | 1.027748176 |
| 3600.00 | 4.59874039 | 4.973266826 | 4.038296657 |
| 5400.00 | 9.591239275 | 10.5904898 | 8.818699331 |
| 7200.00 | 15.30200304 | 17.41265985 | 15.03082241 |
| 9000.00 | 20.7266535 | 24.56083072 | 22.23526175 |
| 10800.00 | 24.91113254 | 31.11405525 | 29.9224234 |
| 12600.00 | 27.11949665 | 36.22803727 | 37.54856882 |
| 14400.00 | 26.96335072 | 39.24390791 | 44.57427538 |
| 16200.00 | 24.47015686 | 39.77311219 | 50.50259146 |
| 18000.00 | 20.66100931 | 37.74746913 | 54.91418756 |
| 19800.00 | 17.34687886 | 33.48750756 | 57.49701679 |
| 21600.00 | 14.5643517 | 28.84202767 | 58.06838704 |
| 23400.00 | 12.22815598 | 24.84098163 | 56.58788341 |
| 25200.00 | 10.26669788 | 21.3949718 | 53.16022684 |
| 27000.00 | 8.619867584 | 18.42700199 | 48.16651381 |
| 28800.00 | 7.2371972 | 15.87075719 | 43.13277554 |
| 30600.00 | 6.076314144 | 13.66912176 | 38.6250982 |
| 32400.00 | 5.101642605 | 11.77290329 | 34.58850473 |
| 34200.00 | 4.283313313 | 10.13973351 | 30.97376357 |
| 36000.00 | 3.596248181 | 8.733121567 | 27.73678819 |
| 37800.00 | 3.019391773 | 7.521638732 | 24.83809943 |
| 39600.00 | 2.535066052 | 6.478216155 | 22.24234396 |
| 41400.00 | 2.128428628 | 5.579540051 | 19.91786313 |
| 43200.00 | 1.787017905 | 4.805530787 | 17.83630684 |
| 45000.00 | 1.500371189 | 4.138894234 | 15.97228777 |
| 46800.00 | 1.259704057 | 3.564735351 | 14.30307175 |
| 48600.00 | 1.057641152 | 3.070225381 | 12.80830051 |
| 50400.00 | 0.887990158 | 2.644315205 | 11.46974334 |
| 52200.00 | 0.745552043 | 2.277488469 | 10.27107477 |
| 54000.00 | 0.625961722 | 1.961548954 | 9.197675475 |
| 55800.00 | 0.525554294 | 1.689437445 | 8.236453925 |
| 57600.00 | 0.441252726 | 1.455073999 | 7.375686764 |
| 59400.00 | 0.370473556 | 1.2532221 | 6.604875804 |
| 61200.00 | 0.311047722 | 1.079371656 | 5.914619992 |
| 63000.00 | 0.261154094 | 0.929638228 | 5.29650075 |
| 64800.00 | 0.219263655 | 0.800676236 | 4.742979301 |
| 66600.00 | 0.184092655 | 0.689604208 | 4.247304722 |
| 68400.00 | 0.154563262 | 0.593940401 | 3.803431611 |
| 70200.00 | 0.129770532 | 0.511547342 | 3.405946351 |
| 72000.00 | 0.108954682 | 0.440584076 | 3.050001087 |
| 73800.00 | 0.0914778 | 0.379465032 | 2.731254597 |
| 75600.00 | 0.076804298 | 0.326824591 | 2.44581935 |
| 77400.00 | 0.0644845 | 0.281486577 | 2.190214086 |
| 79200.00 | 0.05414086 | 0.242437979 | 1.961321364 |
| 81000.00 | 0.045456392 | 0.208806311 | 1.756349535 |
| 82800.00 | 0.038164956 | 0.17984012 | 1.572798699 |
| 84600.00 | 0.032043104 | 0.1548922 | 1.408430212 |
| 86400.00 | 0.026903228 | 0.133405125 | 1.261239384 |

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DA#5A DRAINAGE CALCULATIONS

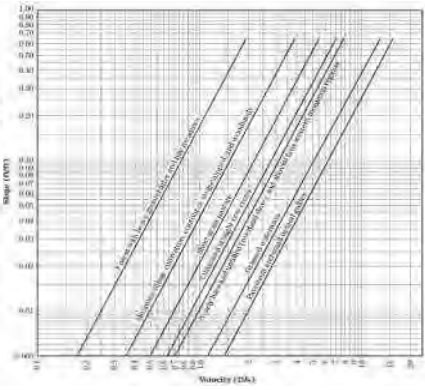
Time of Concentration:

$T_c = T_{OL} + T_1 + \dots + T_n$

Section 2.1
 1. Determine the length of the longest flow path (L) in feet.
 2. Determine the slope of the longest flow path (S) in feet per foot.
 3. Determine the runoff coefficient (C) for the area of the basin.
 4. Determine the time of travel (T_{OL}) in minutes.
 5. Determine the time of travel (T₁) in minutes.
 6. Determine the time of travel (T_n) in minutes.
 7. Determine the total time of concentration (T_c) in minutes.

Table 2.1.1. Manning's Roughness Coefficient (n) for Common Channel Flow

| Surface | n |
|--------------------------------------------------------|-------|
| Smooth Surface (concrete, asphalt, gravel, surf, etc.) | 0.012 |
| Polished concrete | 0.010 |
| Cast-in-place concrete | 0.012 |
| Cast-in-place concrete (finished) | 0.013 |
| Cast-in-place concrete (rough) | 0.015 |
| Grass (dry) | 0.030 |
| Grass (wet) | 0.040 |
| Grass (flooded) | 0.050 |
| Grass (flooded, rough) | 0.060 |
| Grass (flooded, very rough) | 0.070 |
| Grass (flooded, very rough, rough) | 0.080 |



| $T_{OL} =$ | $T =$ |
|------------------------------------------------------------------------------|---------------------|
| $T_{OL} = T_t = T_0$; multiply by 60 to convert hrs. to min. (L = max 300') | |
| n = 0.15 | D = 1740.15 (ft) |
| L = 100 (ft) | S = 0.0124 (ft/ft) |
| $P_2 = 4.89$ (in) | V = 0.775 (ft/s) |
| S = 0.0124 (ft/ft) | |
| $T_{OL} = 9.60$ (min) | $T_1 = 37.42$ (min) |

$T_c = 47.02$ (min)

Intensity:

SEE FIG. 2.1-2.1a

| | |
|--------------|-------------|
| I (100-YR) = | 5.3 (in/hr) |
| I (10-YR) = | 3.5 (in/hr) |
| I (2-YR) = | 2.5 (in/hr) |

Peak Flow Rate:

$Q = CIA$

C = 0.45 Single family residential districts; lots 1/4-1/2 acre; basin slope 1-3.5%

| i (100-YR) | i (10-YR) | i (2-YR) |
|----------------|-----------|----------|
| 5.3 | 3.5 | 2.5 |
| A = 34.81 (Ac) | | |

| | |
|--------------|-------------|
| Q (100-YR) = | 83.02 (cfs) |
| Q (10-YR) = | 54.83 (cfs) |
| Q (2-YR) = | 39.16 (cfs) |

DA#5A EXISTING CALCULATIONS

Volume (100-yr) = 1.38*area*43560 = 2092526.57 cft
 Volume (10-yr) = 0.70*area*43560 = 1061426.52 cft
 Volume (2-yr) = 0.41*area*43560 = 621692.676 cft
 A = 34.81 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

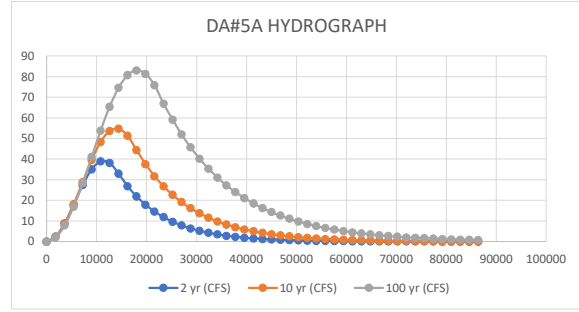
$q_i = \left(\frac{Q_p}{2}\right) \left[1 - \cos\left(\frac{\pi t_i}{T_p}\right)\right]$ $t_i \leq 1.25 T_p$
 $q_i = 4.34 Q_p e^{-1.3t_i/T_p}$ $t_i > 1.25 T_p$

| DA#5A Existing Conditions | | | |
|---------------------------|-----------|-----------|------------|
| | 2 - Year | 10 - Year | 100 - Year |
| Qp= | 39.16 | 54.83 | 83.02 |
| TP= | 11421.007 | 13928.058 | 18132.754 |
| 1.25*TP= | 14276.259 | 17410.072 | 22665.943 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) |
|----------|-------------|-------------|--------------|
| 0 | 0 | 0 | 0 |
| 1800.00 | 2.351483557 | 2.228508274 | 2.002289858 |
| 3600.00 | 8.841143786 | 8.551703415 | 7.815997527 |
| 5400.00 | 17.9102634 | 17.941507 | 16.88027172 |
| 7200.00 | 27.38057837 | 28.87124551 | 28.32067736 |
| 9000.00 | 34.97746364 | 39.56386985 | 41.0335528 |
| 10800.00 | 38.8762634 | 48.2808829 | 53.79248057 |
| 12600.00 | 38.14054547 | 53.60499913 | 65.36660053 |
| 14400.00 | 32.94701807 | 54.67057879 | 74.63935152 |
| 16200.00 | 26.8856212 | 51.30437094 | 80.71618663 |
| 18000.00 | 21.90480476 | 44.34377503 | 83.01087052 |
| 19800.00 | 17.84673183 | 37.48594791 | 81.30203389 |
| 21600.00 | 14.54045541 | 31.6886934 | 75.75452906 |
| 23400.00 | 11.84669807 | 26.78799244 | 66.90352661 |
| 25200.00 | 9.651984841 | 22.64519177 | 59.16338323 |
| 27000.00 | 7.863863063 | 19.14308104 | 52.00056504 |
| 28800.00 | 6.407007811 | 16.18257666 | 45.70493803 |
| 30600.00 | 5.220048818 | 13.67991844 | 40.17151274 |
| 32400.00 | 4.252985242 | 11.56429983 | 35.30801058 |
| 34200.00 | 3.46507937 | 9.775864615 | 31.03332501 |
| 36000.00 | 2.823140537 | 8.264013416 | 27.27616893 |
| 37800.00 | 2.300126964 | 6.98597213 | 23.97388586 |
| 39600.00 | 1.874006618 | 5.905581724 | 21.07140503 |
| 41400.00 | 1.52682911 | 4.992275212 | 18.52032301 |
| 43200.00 | 1.243969529 | 4.220212836 | 16.2780965 |
| 45000.00 | 1.01351237 | 3.567550991 | 14.30733284 |
| 46800.00 | 0.825749586 | 3.015824218 | 12.57516645 |
| 48600.00 | 0.67277164 | 2.549422765 | 11.05271073 |
| 50400.00 | 0.54813431 | 2.155150952 | 9.714576346 |
| 52200.00 | 0.446587228 | 1.821853829 | 8.538447795 |
| 54000.00 | 0.363852706 | 1.540101575 | 7.504711287 |
| 55800.00 | 0.29644554 | 1.301922702 | 6.59612764 |
| 57600.00 | 0.241526191 | 1.100578527 | 5.797544793 |
| 59400.00 | 0.196781172 | 0.930372511 | 5.095645121 |
| 61200.00 | 0.160325593 | 0.786489095 | 4.478723343 |
| 63000.00 | 0.130623755 | 0.664857452 | 3.936491319 |
| 64800.00 | 0.106424465 | 0.562036312 | 3.459906478 |
| 66600.00 | 0.086708323 | 0.475116607 | 3.041021017 |
| 68400.00 | 0.070644783 | 0.401639156 | 2.672849363 |
| 70200.00 | 0.057557167 | 0.339525096 | 2.349251675 |
| 72000.00 | 0.046894156 | 0.287017063 | 2.064831452 |
| 73800.00 | 0.038206568 | 0.242629471 | 1.814845541 |
| 75600.00 | 0.031128439 | 0.205106482 | 1.595125032 |
| 77400.00 | 0.0253616 | 0.173386477 | 1.402005742 |
| 79200.00 | 0.020663123 | 0.146572014 | 1.232267101 |
| 81000.00 | 0.016835084 | 0.123904446 | 1.083078452 |
| 82800.00 | 0.013716225 | 0.10474245 | 0.95195184 |
| 84600.00 | 0.011175164 | 0.088543883 | 0.836700521 |
| 86400.00 | 0.009104859 | 0.074850447 | 0.735402499 |

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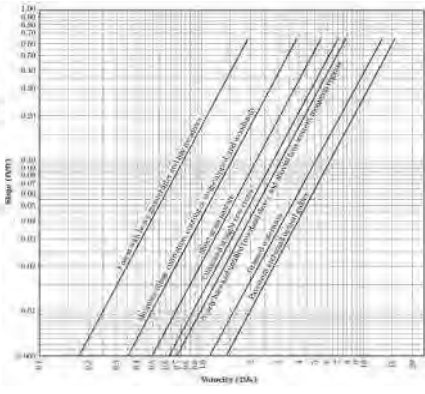
DA#6 DRAINAGE CALCULATIONS

Time of Concentration:

$T_c = T_{OL} + T_1 + \dots + T_n$

Section 2.2
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| Surface | a |
|----------|--------|
| Asphalt | 0.012 |
| Concrete | 0.009 |
| Gravel | 0.008 |
| Grass | 0.007 |
| Gravel | 0.006 |
| Grass | 0.005 |
| Grass | 0.004 |
| Grass | 0.003 |
| Grass | 0.002 |
| Grass | 0.001 |
| Grass | 0.0005 |
| Grass | 0.0002 |
| Grass | 0.0001 |



| T_{OL} | $T = T_{OL}$; multiply by 60 to convert hrs. to min. ($L = \max 300'$) | $T =$ |
|------------|---------------------------------------------------------------------------|----------------------|
| $n =$ | 0.15 | $D = 2888.24$ (ft) |
| $L =$ | 100 (ft) | $S = 0.0051$ (ft/ft) |
| $P_2 =$ | 4.89 (in) | $V = 0.525$ (ft/s) |
| $S =$ | 0.0051 (ft/ft) | |
| $T_{OL} =$ | 13.69 (min) | $T_1 = 91.69$ (min) |

$T_c = 105.38$ (min)

Intensity:

SEE FIG. 2.1-2.1a

| | |
|---------------|-------------|
| I (100-YR)= | 4.7 (in/hr) |
| I (10-YR)= | 2.2 (in/hr) |
| I (2-YR)= | 1.5 (in/hr) |

Peak Flow Rate:

$Q = CIA$

$C =$ 0.35 Mixed use area. Residential lots b/w 1/4 and 1/2 acres; sub-basin slope <1%; and golf course

| i (100-YR) | i (10-YR) | i (2-YR) |
|------------------|-------------|------------|
| 4.7 | 2.2 | 1.5 |
| $A = 30.47$ (Ac) | | |

| | |
|---------------|-------------|
| Q (100-YR)= | 50.12 (cfs) |
| Q (10-YR)= | 23.46 (cfs) |
| Q (2-YR)= | 16.00 (cfs) |

DA#6 EXISTING CALCULATIONS

Volume (100-yr) = 1.38*area*43560 = 1831637.02 cft
 Volume (10-yr) = 0.70*area*43560 = 929091.24 cft
 Volume (2-yr) = 0.41*area*43560 = 544182.012 cft
 A = 30.47 Ac

TP = time to Qp in seconds

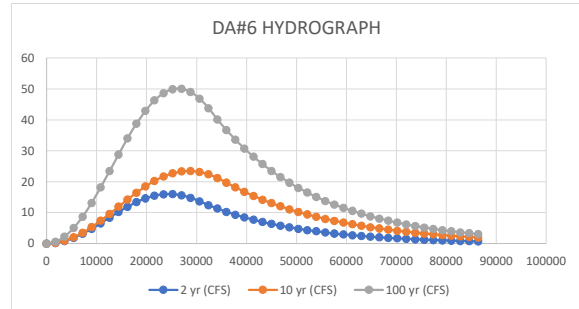
TP = $\frac{V}{1.39 Q_p}$

$q_i = \left(\frac{Q_p}{2}\right) \left[1 - \cos\left(\frac{\pi t_i}{T_p}\right)\right]$ $t_i \leq 1.25 T_p$
 $q_i = 4.34 Q_p e^{-1.3t_i/T_p}$ $t_i > 1.25 T_p$

| DA#6 Existing Conditions | | | |
|--------------------------|-----------|-----------|------------|
| | 2 - Year | 10 - Year | 100 - Year |
| Qp= | 16.00 | 23.46 | 50.12 |
| TP= | 24473.587 | 28489.209 | 26289.738 |
| 1.25*TP= | 30591.984 | 35611.511 | 32862.172 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) |
|----------|-------------|-------------|--------------|
| 0 | 0 | 0 | 0 |
| 1800.00 | 0.212563264 | 0.230335464 | 0.577531269 |
| 3600.00 | 0.838954977 | 0.912296652 | 2.283507245 |
| 5400.00 | 1.845881409 | 2.019103148 | 5.039301229 |
| 7200.00 | 3.179822796 | 3.507290992 | 8.717901475 |
| 9000.00 | 4.769878003 | 5.318419486 | 13.14976503 |
| 10800.00 | 6.531533031 | 7.381366153 | 18.13063182 |
| 12600.00 | 8.371153075 | 9.615119688 | 23.43093873 |
| 14400.00 | 10.19095936 | 11.93196125 | 28.80640001 |
| 16200.00 | 11.89422626 | 14.24090916 | 34.00926611 |
| 18000.00 | 13.39042237 | 16.45129172 | 38.79974222 |
| 19800.00 | 14.60002248 | 18.47630786 | 42.95704015 |
| 21600.00 | 15.45873438 | 20.2364358 | 46.28955427 |
| 23400.00 | 15.92091614 | 21.66255583 | 48.64369239 |
| 25200.00 | 15.96200207 | 22.69866464 | 49.91095467 |
| 27000.00 | 15.57980838 | 23.30407455 | 50.03293427 |
| 28800.00 | 14.79464928 | 23.4550113 | 49.00400929 |
| 30600.00 | 13.66494922 | 23.14554763 | 46.87160184 |
| 32400.00 | 12.41891632 | 22.38783609 | 43.73399239 |
| 34200.00 | 11.28650242 | 21.2116318 | 40.09305572 |
| 36000.00 | 10.25734724 | 19.69815358 | 36.67865691 |
| 37800.00 | 9.322035153 | 18.14488206 | 33.55503463 |
| 39600.00 | 8.472009124 | 16.71409168 | 30.6974258 |
| 41400.00 | 7.699492377 | 15.39612437 | 28.08317623 |
| 43200.00 | 6.997417259 | 14.1820836 | 25.69156098 |
| 45000.00 | 6.359360579 | 13.06377439 | 23.50362011 |
| 46800.00 | 5.779484841 | 12.03364796 | 21.50200834 |
| 48600.00 | 5.252484838 | 11.08475076 | 19.67085753 |
| 50400.00 | 4.77353912 | 10.21067759 | 17.99565091 |
| 52200.00 | 4.338265874 | 9.405528282 | 16.46310798 |
| 54000.00 | 3.942682844 | 8.663867946 | 15.06107925 |
| 55800.00 | 3.583170893 | 7.980690242 | 13.77844987 |
| 57600.00 | 3.256440895 | 7.351383602 | 12.60505159 |
| 59400.00 | 2.959503641 | 6.771700093 | 11.53158208 |
| 61200.00 | 2.689642491 | 6.237726751 | 10.54953121 |
| 63000.00 | 2.444388522 | 5.745859162 | 9.651113616 |
| 64800.00 | 2.221497937 | 5.292777133 | 8.829206924 |
| 66600.00 | 2.01893154 | 4.875422281 | 8.077295327 |
| 68400.00 | 1.834836079 | 4.490977386 | 7.389417913 |
| 70200.00 | 1.667527289 | 4.136847379 | 6.760121412 |
| 72000.00 | 1.515474483 | 3.81064182 | 6.184416966 |
| 73800.00 | 1.377286552 | 3.510158762 | 5.657740575 |
| 75600.00 | 1.251699231 | 3.233369894 | 5.17591692 |
| 77400.00 | 1.13756354 | 2.978406841 | 4.735126259 |
| 79200.00 | 1.033835266 | 2.743548559 | 4.331874146 |
| 81000.00 | 0.939565412 | 2.527209712 | 3.962963729 |
| 82800.00 | 0.853891518 | 2.327929974 | 3.625470406 |
| 84600.00 | 0.776029763 | 2.144364174 | 3.316718639 |
| 86400.00 | 0.705267801 | 1.975273209 | 3.034260743 |

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DA#6A DRAINAGE CALCULATIONS

Time of Concentration:

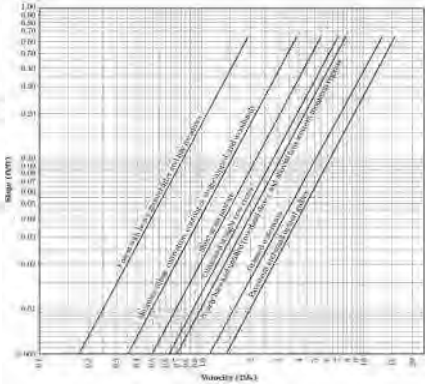
$T_c = T_{OL} + T_1 + \dots + T_n$

Section 2.1
 2.1.1.1.1.1
 2.1.1.1.1.2
 2.1.1.1.1.3
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Table 2.1.1.1.1.1

| Surface | n |
|--------------------------------------------------------|-------|
| Asphalt Surface (asphalt, asphalt, gravel, surf, etc.) | 0.012 |
| Gravel Surface | 0.020 |
| Concrete Slab, Residue Cover = 20% | 0.008 |
| Concrete Slab, Residue Cover = 50% | 0.010 |
| Grass, Short (Short Grass) | 0.244 |
| Grass, Medium (Medium Grass) | 0.316 |
| Grass, Long (Long Grass) | 0.375 |
| Wooded Slope (Wooded Slope) | 0.400 |
| Wooded Slope (Wooded Slope) | 0.480 |

Source: SCS TR-55 (1975, 1980)



| $T_{OL} = Tt = T_0$; multiply by 60 to convert hrs. to min. (L=max 300') | T = |
|---------------------------------------------------------------------------|--------------------|
| n = 0.15 | D = 416.48 (ft) |
| L = 100 (ft) | S = 0.0264 (ft/ft) |
| $P_2 = 4.89$ (in) | V = 1.15 (ft/s) |
| $S = 0.0264$ (ft/ft) | |
| $T_{OL} = 7.09$ (min) | $T_1 = 6.04$ (min) |

$T_c = 13.13$ (min)

Intensity:

SEE FIG. 2.1-2.1a

| | |
|--------------|--------------|
| I (100-YR) = | 10.4 (in/hr) |
| I (10-YR) = | 7 (in/hr) |
| I (2-YR) = | 4.8 (in/hr) |

Peak Flow Rate:

$Q = CIA$

C = 0.45 Single family residential districts; lots 1/4-1/2 acre; basin slope 1-3.5%

| i (100-YR) | i (10-YR) | i (2-YR) |
|------------|-----------|----------|
| 10.4 | 7 | 4.8 |
| A = | 2.6 (Ac) | |

| | |
|---------------------|--------------------|
| Q (100-YR) = | 12.17 (cfs) |
| Q (10-YR) = | 8.19 (cfs) |
| Q (2-YR) = | 5.62 (cfs) |

DA#6A EXISTING CALCULATIONS

Volume (100-yr) = 1.38*area*43560 = 156293.28 cft
 Volume (10-yr) = 0.70*area*43560 = 79279.2 cft
 Volume (2-yr) = 0.41*area*43560 = 46434.96 cft
 A = 2.60 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

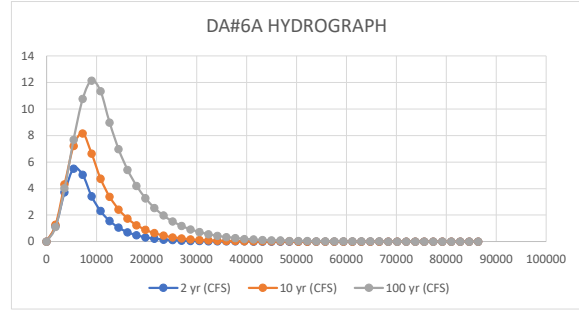
$q_i = \left(\frac{Q_p}{2}\right) \left[1 - \cos\left(\frac{\pi t_i}{T_p}\right)\right]$ $t_i \leq 1.25 T_p$
 $q_i = 1.34 Q_p e^{-1.3t_i/T_p}$ $t_i > 1.25 T_p$

| DA#6A Existing Conditions | | | |
|---------------------------|----------|-----------|------------|
| | 2 - Year | 10 - Year | 100 - Year |
| Qp= | 5.62 | 8.19 | 12.17 |
| TP= | 5948.441 | 6964.029 | 9240.730 |
| 1.25*TP= | 7435.552 | 8705.036 | 11550.913 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) |
|----------|-------------|-------------|--------------|
| 0 | 0 | 0 | 0 |
| 1800.00 | 1.176111617 | 1.27747365 | 1.104067984 |
| 3600.00 | 3.719233836 | 4.312854831 | 4.015559866 |
| 5400.00 | 5.499027921 | 7.212312297 | 7.677774473 |
| 7200.00 | 5.024584684 | 8.166820158 | 10.76154221 |
| 9000.00 | 3.409590447 | 6.624177826 | 12.14763586 |
| 10800.00 | 2.300696294 | 4.733731849 | 11.33298453 |
| 12600.00 | 1.552445527 | 3.38279222 | 8.971893684 |
| 14400.00 | 1.047546832 | 2.417391515 | 6.964807949 |
| 16200.00 | 0.70685531 | 1.727502417 | 5.40672365 |
| 18000.00 | 0.476966198 | 1.234497839 | 4.197195506 |
| 19800.00 | 0.321843454 | 0.882189743 | 3.258248666 |
| 21600.00 | 0.217170963 | 0.630425359 | 2.529351885 |
| 23400.00 | 0.146540893 | 0.450510943 | 1.963515255 |
| 25200.00 | 0.098881697 | 0.321941538 | 1.524260891 |
| 27000.00 | 0.066722604 | 0.23006401 | 1.183271307 |
| 28800.00 | 0.045022548 | 0.164407019 | 0.918563872 |
| 30600.00 | 0.030379956 | 0.117487598 | 0.713073648 |
| 32400.00 | 0.020499545 | 0.083958312 | 0.553553262 |
| 34200.00 | 0.01383252 | 0.059997806 | 0.429718886 |
| 36000.00 | 0.009333798 | 0.042875287 | 0.333587269 |
| 37800.00 | 0.006298186 | 0.030639291 | 0.258961078 |
| 39600.00 | 0.00424984 | 0.021895274 | 0.201029375 |
| 41400.00 | 0.002867673 | 0.015646674 | 0.156057465 |
| 43200.00 | 0.001935025 | 0.011181336 | 0.121146138 |
| 45000.00 | 0.001305701 | 0.007990342 | 0.09404476 |
| 46800.00 | 0.000881051 | 0.005710012 | 0.073006181 |
| 48600.00 | 0.000594508 | 0.004080456 | 0.056674103 |
| 50400.00 | 0.000401158 | 0.002915952 | 0.043995644 |
| 52200.00 | 0.00027069 | 0.002083781 | 0.03415346 |
| 54000.00 | 0.000182654 | 0.0014891 | 0.026513053 |
| 55800.00 | 0.00012325 | 0.001064132 | 0.020581867 |
| 57600.00 | 8.31655E-05 | 0.000760444 | 0.015977535 |
| 59400.00 | 5.61178E-05 | 0.000543424 | 0.012403231 |
| 61200.00 | 3.78667E-05 | 0.000388338 | 0.009628527 |
| 63000.00 | 2.55514E-05 | 0.000277512 | 0.007474547 |
| 64800.00 | 1.72414E-05 | 0.000198314 | 0.00580243 |
| 66600.00 | 1.1634E-05 | 0.000141718 | 0.004504379 |
| 68400.00 | 7.85029E-06 | 0.000101274 | 0.003496713 |
| 70200.00 | 5.29716E-06 | 7.23717E-05 | 0.00271447 |
| 72000.00 | 3.57437E-06 | 5.17178E-05 | 0.002107221 |
| 73800.00 | 2.41189E-06 | 3.69583E-05 | 0.001635818 |
| 75600.00 | 1.62747E-06 | 2.64109E-05 | 0.001269872 |
| 77400.00 | 1.09817E-06 | 1.88736E-05 | 0.000985792 |
| 79200.00 | 7.41017E-07 | 1.34874E-05 | 0.000765262 |
| 81000.00 | 5.00018E-07 | 9.63826E-06 | 0.000594067 |
| 82800.00 | 3.37398E-07 | 6.88764E-06 | 0.000461169 |
| 84600.00 | 2.27667E-07 | 4.92201E-06 | 0.000358002 |
| 86400.00 | 1.53623E-07 | 3.51734E-06 | 0.000277914 |

ti (hrs)

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DA#6B DRAINAGE CALCULATIONS

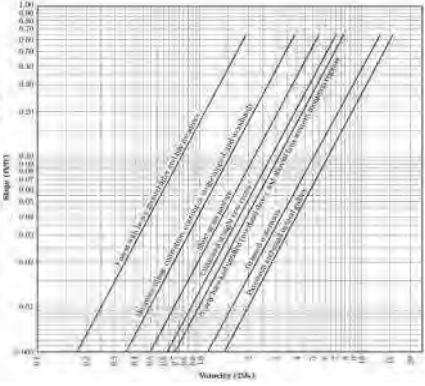
Time of Concentration:

$T_c = T_{OL} + T_1 + \dots + T_n$

Section 2.2
 1. Determine the time of concentration for each sub-area.
 2. Determine the time of concentration for the entire drainage area.
 3. Determine the time of concentration for the entire drainage area.
 4. Determine the time of concentration for the entire drainage area.
 5. Determine the time of concentration for the entire drainage area.
 6. Determine the time of concentration for the entire drainage area.
 7. Determine the time of concentration for the entire drainage area.
 8. Determine the time of concentration for the entire drainage area.
 9. Determine the time of concentration for the entire drainage area.
 10. Determine the time of concentration for the entire drainage area.

Table 2.11 Manning's Roughness Coefficient for Common Channel Flow

| Surface | n |
|--------------------------------------------------------|-------|
| Smooth Surface (concrete, asphalt, gravel, surf. seal) | 0.012 |
| Polished metal pipe | 0.009 |
| Cast-iron pipe, new | 0.010 |
| Cast-iron pipe, old | 0.011 |
| Concrete pipe, new | 0.012 |
| Concrete pipe, old | 0.013 |
| Grass, dense (winter) | 0.244 |
| Grass, moderate (winter) | 0.300 |
| Grass, light (winter) | 0.350 |
| Wooden flume (unplaned) | 0.400 |
| Wooden flume (planed) | 0.450 |



| $T_{OL} =$ | $T =$ |
|--------------------------------------------------------------------|---------------------|
| $T = T_{OL}$; multiply by 60 to convert hrs. to min. (L=max 300') | |
| n= 0.011 | D= 2803.91 (ft) |
| L= 100 (ft) | S= 0.0073 (ft/ft) |
| $P_2 = 4.89$ (in) | V= 1.75 (ft/s) |
| S= 0.0073 (ft/ft) | |
| $T_{OL} = 1.47$ (min) | $T_1 = 26.70$ (min) |

$T_c = 28.17$ (min)

Intensity:

SEE FIG. 2.1-2.1a

| | |
|-------------|-------------|
| I (100-YR)= | 7 (in/hr) |
| I (10-YR)= | 4.7 (in/hr) |
| I (2-YR)= | 3.3 (in/hr) |

Peak Flow Rate:

$Q = CIA$

C= 0.4 Single family residential districts; lots 1/4-1/2 acre; basin slope <1%

| i (100-YR) | i (10-YR) | i (2-YR) |
|---------------|-----------|----------|
| 7 | 4.7 | 3.3 |
| A= 41.39 (Ac) | | |

| | |
|--------------------|---------------------|
| Q (100-YR)= | 115.89 (cfs) |
| Q (10-YR)= | 77.81 (cfs) |
| Q (2-YR)= | 54.63 (cfs) |

DA#6B EXISTING CALCULATIONS

Volume (100-yr) = 1.38*area*43560 = 2488068.79 cft
 Volume (10-yr)= 0.70*area*43560= 1262063.88 cft
 Volume (2-yr)= 0.41*area*43560= 739208.844 cft
 A= 41.39 Ac

TP = time to Qp in seconds

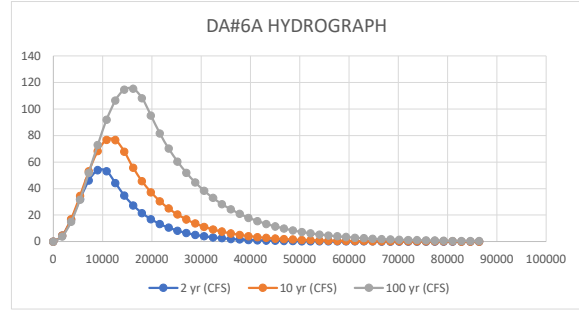
TP = $\frac{V}{1.39 Q_p}$

$q_i = \left(\frac{Q_p}{2}\right) \left[1 - \cos\left(\frac{\pi t_i}{T_p}\right)\right]$ $t_i \leq 1.25 T_p$
 $q_i = 4.34 Q_p e^{-1.3t_i/T_p}$ $t_i > 1.25 T_p$

| DA#6B Existing Conditions | | | |
|---------------------------|-----------|-----------|------------|
| | 2 - Year | 10 - Year | 100 - Year |
| Qp= | 54.63 | 77.81 | 115.89 |
| TP= | 9733.813 | 11668.452 | 15445.221 |
| 1.25*TP= | 12167.266 | 14585.566 | 19306.526 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) |
|----------|-------------|-------------|--------------|
| 0 | 0 | 0 | 0 |
| 1800.00 | 4.481660118 | 4.480172869 | 3.84054823 |
| 3600.00 | 16.45612883 | 16.8888973 | 14.85310478 |
| 5400.00 | 31.99437197 | 34.36837341 | 31.57788797 |
| 7200.00 | 45.99801821 | 52.89302884 | 51.79792557 |
| 9000.00 | 53.87222448 | 68.19655372 | 72.83292801 |
| 10800.00 | 53.03332498 | 76.75448499 | 91.89457716 |
| 12600.00 | 44.06878016 | 76.59589684 | 106.4561349 |
| 14400.00 | 34.65189749 | 67.75731274 | 114.5873778 |
| 16200.00 | 27.24727109 | 55.55196243 | 115.2104599 |
| 18000.00 | 21.42490991 | 45.45751306 | 108.2427878 |
| 19800.00 | 16.84670597 | 37.19734467 | 95.01152088 |
| 21600.00 | 13.24680026 | 30.43814668 | 81.65434089 |
| 23400.00 | 10.41614411 | 24.90717501 | 70.17497799 |
| 25200.00 | 8.190359626 | 20.38124638 | 60.30943955 |
| 27000.00 | 6.440194195 | 16.67773257 | 51.83084631 |
| 28800.00 | 5.064014667 | 13.64719108 | 44.54421478 |
| 30600.00 | 3.981905478 | 11.16733486 | 38.28197323 |
| 32400.00 | 3.131027906 | 9.138097884 | 32.90010793 |
| 34200.00 | 2.461970983 | 7.477597292 | 28.27485134 |
| 36000.00 | 1.935882179 | 6.118829321 | 24.29983573 |
| 37800.00 | 1.522211202 | 5.006965579 | 20.88364708 |
| 39600.00 | 1.196935934 | 4.097140645 | 17.94772278 |
| 41400.00 | 0.941167446 | 3.352641675 | 15.42454495 |
| 43200.00 | 0.740053111 | 2.743426984 | 13.25608768 |
| 45000.00 | 0.5819141 | 2.244913815 | 11.39248264 |
| 46800.00 | 0.457567186 | 1.836986393 | 9.790872227 |
| 48600.00 | 0.359791471 | 1.503184213 | 8.414423967 |
| 50400.00 | 0.28290906 | 1.230037842 | 7.231483473 |
| 52200.00 | 0.222455346 | 1.006525401 | 6.214846486 |
| 54000.00 | 0.174919746 | 0.823627817 | 5.341133253 |
| 55800.00 | 0.13754184 | 0.67396489 | 4.590250859 |
| 57600.00 | 0.108151071 | 0.551497489 | 3.944931151 |
| 59400.00 | 0.085040698 | 0.451283865 | 3.390333615 |
| 61200.00 | 0.066868689 | 0.369280243 | 2.913704087 |
| 63000.00 | 0.052579784 | 0.30217765 | 2.504081448 |
| 64800.00 | 0.041344219 | 0.247268393 | 2.152045544 |
| 66600.00 | 0.032509537 | 0.202336798 | 1.849500554 |
| 68400.00 | 0.025562703 | 0.165569806 | 1.589488804 |
| 70200.00 | 0.02010031 | 0.135483812 | 1.366030766 |
| 72000.00 | 0.015805155 | 0.110864799 | 1.173987542 |
| 73800.00 | 0.012427814 | 0.090719352 | 1.008942685 |
| 75600.00 | 0.009772164 | 0.074234572 | 0.867100633 |
| 77400.00 | 0.007683989 | 0.060745271 | 0.745199425 |
| 79200.00 | 0.006042028 | 0.049707136 | 0.640435679 |
| 81000.00 | 0.004750931 | 0.040674761 | 0.550400128 |
| 82800.00 | 0.003735723 | 0.033283675 | 0.473022211 |
| 84600.00 | 0.002937451 | 0.027235637 | 0.406522456 |
| 86400.00 | 0.002309759 | 0.022286599 | 0.34937156 |

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DA#7 DRAINAGE CALCULATIONS

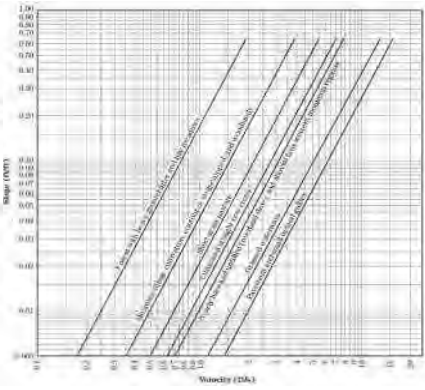
Time of Concentration:

$$T_c = T_{OL} + T_1 + \dots + T_n$$

Section 2.3
 1. ...
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 9. ...
 10. ...

Table 2.3 (Continued) - Impervious Conditions for Ground Sheet Flow

| Surface | n |
|------------------------|-------|
| Asphalt | 0.012 |
| Concrete | 0.010 |
| Gravel | 0.008 |
| Grass (Short) | 0.015 |
| Grass (Medium) | 0.020 |
| Grass (Long) | 0.025 |
| Grass (Turf) | 0.030 |
| Grass (Matted) | 0.035 |
| Grass (Matted, Wet) | 0.040 |
| Grass (Matted, Dry) | 0.045 |
| Grass (Matted, Snow) | 0.050 |
| Grass (Matted, Ice) | 0.055 |
| Grass (Matted, Frost) | 0.060 |
| Grass (Matted, Spring) | 0.065 |
| Grass (Matted, Summer) | 0.070 |
| Grass (Matted, Autumn) | 0.075 |
| Grass (Matted, Winter) | 0.080 |



| | | | |
|------------|--------------------------------------------------------------------|---------|----------------|
| $T_{OL} =$ | $T = T_{OL}$; multiply by 60 to convert hrs. to min. (L=max 300') | $T =$ | |
| n= | 0.15 | D= | 2354.93 (ft) |
| L= | 100 (ft) | S= | 0.0053 (ft/ft) |
| $P_2 =$ | 4.89 (in) | V= | 0.525 (ft/s) |
| S= | 0.0053 (ft/ft) | | |
| $T_{OL} =$ | 13.48 (min) | $T_1 =$ | 74.76 (min) |

$T_c = 88.24$ (min)

Intensity:

SEE FIG. 2.1-2.1a

| | |
|-------------|-------------|
| I (100-YR)= | 3.9 (in/hr) |
| I (10-YR)= | 2.5 (in/hr) |
| I (2-YR)= | 1.6 (in/hr) |

Peak Flow Rate:

$$Q = CIA$$

C= 0.28 Mixed use area. Residential lots b/w 1/4 and 1/2 acres; sub-basin slope <1%; and MOSTLY golf course

| | | |
|------------|------------|----------|
| i (100-YR) | i (10-YR) | i (2-YR) |
| 3.9 | 2.5 | 1.6 |
| A= | 45.05 (Ac) | |

| | |
|-------------|-------------|
| Q (100-YR)= | 49.19 (cfs) |
| Q (10-YR)= | 31.54 (cfs) |
| Q (2-YR)= | 20.18 (cfs) |

DA#7 EXISTING CALCULATIONS

Volume (100-yr) = 1.38*area*43560 = 2708081.64 cft
 Volume (10-yr) = 0.70*area*43560 = 1373664.6 cft
 Volume (2-yr) = 0.41*area*43560 = 804574.98 cft
 A = 45.05 Ac

TP = time to Qp in seconds

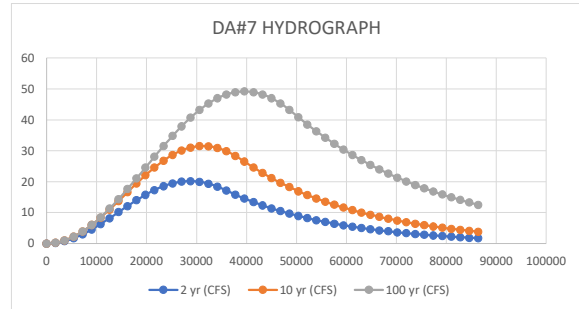
TP = $\frac{V}{1.39 Q_p}$

$q_i = \left(\frac{Q_p}{2}\right) \left[1 - \cos\left(\frac{\pi t_i}{T_p}\right)\right]$ $t_i \leq 1.25 T_p$
 $q_i = 1.34 Q_p e^{-1.3t_i/T_p}$ $t_i > 1.25 T_p$

| DA#7 Existing Conditions | | | |
|--------------------------|-----------|-----------|------------|
| | 2 - Year | 10 - Year | 100 - Year |
| Qp= | 20.18 | 31.54 | 49.19 |
| TP= | 28679.985 | 31338.129 | 39603.131 |
| 1.25*TP= | 35849.981 | 39172.662 | 49503.913 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) |
|----------|-------------|-------------|--------------|
| 0 | 0 | 0 | 0 |
| 1800.00 | 0.195520502 | 0.256007515 | 0.250325533 |
| 3600.00 | 0.774505453 | 1.015716776 | 0.996207031 |
| 5400.00 | 1.714518784 | 2.254457889 | 2.222462893 |
| 7200.00 | 2.979134326 | 3.932005449 | 3.904134026 |
| 9000.00 | 4.51934735 | 5.993884774 | 6.006991859 |
| 10800.00 | 6.275473531 | 8.373140847 | 8.488235026 |
| 12600.00 | 8.179461761 | 10.99251254 | 11.29736054 |
| 14400.00 | 10.15753117 | 13.76694149 | 14.37719174 |
| 16200.00 | 12.13303021 | 16.6063342 | 17.66504204 |
| 18000.00 | 14.02940691 | 19.41848761 | 21.09399084 |
| 19800.00 | 15.77317535 | 22.11208318 | 24.59424566 |
| 21600.00 | 17.29676331 | 24.59965232 | 28.09456265 |
| 23400.00 | 18.54113069 | 26.80041665 | 31.52369669 |
| 25200.00 | 19.45805739 | 28.64291118 | 34.81185153 |
| 27000.00 | 20.01201186 | 30.06730493 | 37.89210036 |
| 28800.00 | 20.18152799 | 31.02734383 | 40.70174812 |
| 30600.00 | 19.9600369 | 31.49185272 | 43.1836075 |
| 32400.00 | 19.35612154 | 31.4457477 | 45.28716297 |
| 34200.00 | 18.39318403 | 30.89052592 | 46.96959897 |
| 36000.00 | 17.1309239 | 29.844217 | 48.19667136 |
| 37800.00 | 15.78871183 | 28.34079752 | 48.94340443 |
| 39600.00 | 14.5516624 | 26.47617086 | 49.19459924 |
| 41400.00 | 13.4115361 | 24.57121643 | 48.945143 |
| 43200.00 | 12.36073897 | 22.80332304 | 48.20011312 |
| 45000.00 | 11.39227205 | 21.16262917 | 46.97467386 |
| 46800.00 | 10.49968475 | 19.63998285 | 45.2937677 |
| 48600.00 | 9.677031888 | 18.22689058 | 43.19160764 |
| 50400.00 | 8.918834077 | 16.91546998 | 40.82291431 |
| 52200.00 | 8.220041249 | 15.69840579 | 38.48071902 |
| 54000.00 | 7.575999009 | 14.56890909 | 36.27290607 |
| 55800.00 | 6.982417637 | 13.52067942 | 34.19176534 |
| 57600.00 | 6.43534351 | 12.54786963 | 32.23002906 |
| 59400.00 | 5.931132774 | 11.64505329 | 30.38084648 |
| 61200.00 | 5.466427073 | 10.80719437 | 28.63775986 |
| 63000.00 | 5.038131177 | 10.02961921 | 26.99468201 |
| 64800.00 | 4.643392369 | 9.307990406 | 25.44587497 |
| 66600.00 | 4.279581443 | 8.638282628 | 23.98592999 |
| 68400.00 | 3.944275191 | 8.016760172 | 22.60974867 |
| 70200.00 | 3.635240267 | 7.439956114 | 21.31252509 |
| 72000.00 | 3.350418304 | 6.904652976 | 20.0897291 |
| 73800.00 | 3.087912212 | 6.407864776 | 18.93709045 |
| 75600.00 | 2.845973536 | 5.946820374 | 17.85058389 |
| 77400.00 | 2.622990814 | 5.51894801 | 16.82641513 |
| 79200.00 | 2.417478843 | 5.121860965 | 15.86100757 |
| 81000.00 | 2.228068786 | 4.753344242 | 14.9509898 |
| 82800.00 | 2.053499052 | 4.411342213 | 14.09318387 |
| 84600.00 | 1.8926069 | 4.093947151 | 13.28459415 |
| 86400.00 | 1.744320687 | 3.799388592 | 12.52239688 |

ti (hrs)
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DA#7A DRAINAGE CALCULATIONS

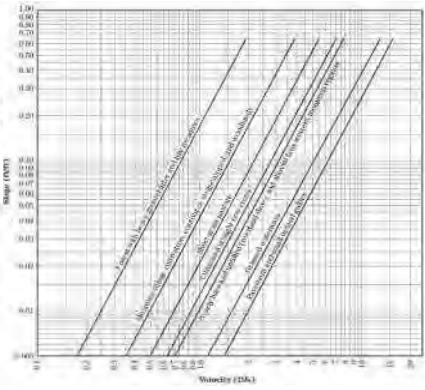
Time of Concentration:

$T_c = T_{OL} + T_1 + \dots + T_n$

Section 2.1
 1. Determine the length of the pipe (L) in feet.
 2. Determine the slope of the pipe (S) in ft/ft.
 3. Determine the roughness coefficient (n) for the pipe material.
 4. Calculate the velocity (V) in ft/s using the Manning equation.
 5. Calculate the travel time (T) in minutes for the pipe section.
 6. Repeat steps 1-5 for all pipe sections in the drainage area.
 7. Sum the travel times for all pipe sections to determine the total travel time (T_{OL}).
 8. Determine the time of concentration (T_c) by adding T_{OL} to the time of travel for the overland flow (T₁).

Table 2.1 Manning's Roughness Coefficient (n) for Common Pipe Flow

| Surface | n |
|--------------------------------------------------------|-------|
| Smooth Surface (concrete, asphalt, gravel, surf. seal) | 0.012 |
| Polished metal pipe | 0.009 |
| Commercially available cast-iron pipe | 0.009 |
| Commercially available steel pipe | 0.009 |
| Commercially available aluminum pipe | 0.009 |
| Commercially available plastic pipe | 0.009 |
| Commercially available fiberglass pipe | 0.009 |
| Commercially available concrete pipe | 0.012 |
| Commercially available masonry pipe | 0.012 |
| Commercially available brick pipe | 0.012 |
| Commercially available stone pipe | 0.012 |
| Commercially available rubble pipe | 0.012 |
| Commercially available earth pipe | 0.012 |
| Commercially available earth pipe (with 1% slope) | 0.012 |
| Commercially available earth pipe (with 2% slope) | 0.012 |
| Commercially available earth pipe (with 3% slope) | 0.012 |
| Commercially available earth pipe (with 4% slope) | 0.012 |
| Commercially available earth pipe (with 5% slope) | 0.012 |
| Commercially available earth pipe (with 6% slope) | 0.012 |
| Commercially available earth pipe (with 7% slope) | 0.012 |
| Commercially available earth pipe (with 8% slope) | 0.012 |
| Commercially available earth pipe (with 9% slope) | 0.012 |
| Commercially available earth pipe (with 10% slope) | 0.012 |
| Commercially available earth pipe (with 11% slope) | 0.012 |
| Commercially available earth pipe (with 12% slope) | 0.012 |
| Commercially available earth pipe (with 13% slope) | 0.012 |
| Commercially available earth pipe (with 14% slope) | 0.012 |
| Commercially available earth pipe (with 15% slope) | 0.012 |
| Commercially available earth pipe (with 16% slope) | 0.012 |
| Commercially available earth pipe (with 17% slope) | 0.012 |
| Commercially available earth pipe (with 18% slope) | 0.012 |
| Commercially available earth pipe (with 19% slope) | 0.012 |
| Commercially available earth pipe (with 20% slope) | 0.012 |
| Commercially available earth pipe (with 21% slope) | 0.012 |
| Commercially available earth pipe (with 22% slope) | 0.012 |
| Commercially available earth pipe (with 23% slope) | 0.012 |
| Commercially available earth pipe (with 24% slope) | 0.012 |
| Commercially available earth pipe (with 25% slope) | 0.012 |
| Commercially available earth pipe (with 26% slope) | 0.012 |
| Commercially available earth pipe (with 27% slope) | 0.012 |
| Commercially available earth pipe (with 28% slope) | 0.012 |
| Commercially available earth pipe (with 29% slope) | 0.012 |
| Commercially available earth pipe (with 30% slope) | 0.012 |
| Commercially available earth pipe (with 31% slope) | 0.012 |
| Commercially available earth pipe (with 32% slope) | 0.012 |
| Commercially available earth pipe (with 33% slope) | 0.012 |
| Commercially available earth pipe (with 34% slope) | 0.012 |
| Commercially available earth pipe (with 35% slope) | 0.012 |
| Commercially available earth pipe (with 36% slope) | 0.012 |
| Commercially available earth pipe (with 37% slope) | 0.012 |
| Commercially available earth pipe (with 38% slope) | 0.012 |
| Commercially available earth pipe (with 39% slope) | 0.012 |
| Commercially available earth pipe (with 40% slope) | 0.012 |
| Commercially available earth pipe (with 41% slope) | 0.012 |
| Commercially available earth pipe (with 42% slope) | 0.012 |
| Commercially available earth pipe (with 43% slope) | 0.012 |
| Commercially available earth pipe (with 44% slope) | 0.012 |
| Commercially available earth pipe (with 45% slope) | 0.012 |
| Commercially available earth pipe (with 46% slope) | 0.012 |
| Commercially available earth pipe (with 47% slope) | 0.012 |
| Commercially available earth pipe (with 48% slope) | 0.012 |
| Commercially available earth pipe (with 49% slope) | 0.012 |
| Commercially available earth pipe (with 50% slope) | 0.012 |
| Commercially available earth pipe (with 51% slope) | 0.012 |
| Commercially available earth pipe (with 52% slope) | 0.012 |
| Commercially available earth pipe (with 53% slope) | 0.012 |
| Commercially available earth pipe (with 54% slope) | 0.012 |
| Commercially available earth pipe (with 55% slope) | 0.012 |
| Commercially available earth pipe (with 56% slope) | 0.012 |
| Commercially available earth pipe (with 57% slope) | 0.012 |
| Commercially available earth pipe (with 58% slope) | 0.012 |
| Commercially available earth pipe (with 59% slope) | 0.012 |
| Commercially available earth pipe (with 60% slope) | 0.012 |
| Commercially available earth pipe (with 61% slope) | 0.012 |
| Commercially available earth pipe (with 62% slope) | 0.012 |
| Commercially available earth pipe (with 63% slope) | 0.012 |
| Commercially available earth pipe (with 64% slope) | 0.012 |
| Commercially available earth pipe (with 65% slope) | 0.012 |
| Commercially available earth pipe (with 66% slope) | 0.012 |
| Commercially available earth pipe (with 67% slope) | 0.012 |
| Commercially available earth pipe (with 68% slope) | 0.012 |
| Commercially available earth pipe (with 69% slope) | 0.012 |
| Commercially available earth pipe (with 70% slope) | 0.012 |
| Commercially available earth pipe (with 71% slope) | 0.012 |
| Commercially available earth pipe (with 72% slope) | 0.012 |
| Commercially available earth pipe (with 73% slope) | 0.012 |
| Commercially available earth pipe (with 74% slope) | 0.012 |
| Commercially available earth pipe (with 75% slope) | 0.012 |
| Commercially available earth pipe (with 76% slope) | 0.012 |
| Commercially available earth pipe (with 77% slope) | 0.012 |
| Commercially available earth pipe (with 78% slope) | 0.012 |
| Commercially available earth pipe (with 79% slope) | 0.012 |
| Commercially available earth pipe (with 80% slope) | 0.012 |
| Commercially available earth pipe (with 81% slope) | 0.012 |
| Commercially available earth pipe (with 82% slope) | 0.012 |
| Commercially available earth pipe (with 83% slope) | 0.012 |
| Commercially available earth pipe (with 84% slope) | 0.012 |
| Commercially available earth pipe (with 85% slope) | 0.012 |
| Commercially available earth pipe (with 86% slope) | 0.012 |
| Commercially available earth pipe (with 87% slope) | 0.012 |
| Commercially available earth pipe (with 88% slope) | 0.012 |
| Commercially available earth pipe (with 89% slope) | 0.012 |
| Commercially available earth pipe (with 90% slope) | 0.012 |
| Commercially available earth pipe (with 91% slope) | 0.012 |
| Commercially available earth pipe (with 92% slope) | 0.012 |
| Commercially available earth pipe (with 93% slope) | 0.012 |
| Commercially available earth pipe (with 94% slope) | 0.012 |
| Commercially available earth pipe (with 95% slope) | 0.012 |
| Commercially available earth pipe (with 96% slope) | 0.012 |
| Commercially available earth pipe (with 97% slope) | 0.012 |
| Commercially available earth pipe (with 98% slope) | 0.012 |
| Commercially available earth pipe (with 99% slope) | 0.012 |
| Commercially available earth pipe (with 100% slope) | 0.012 |



| | | |
|------------|----------------------------------------------------------------------|--------------------|
| $T_{OL} =$ | $T_t = T_{OL}$; multiply by 60 to convert hrs. to min. (L=max 300') | $T =$ |
| n = | 0.15 | D = 2388.94 (ft) |
| L = | 100 (ft) | S = 0.0051 (ft/ft) |
| $P_2 =$ | 4.89 (in) | V = 0.5 (ft/s) |
| S = | 0.0051 (ft/ft) | |
| $T_{OL} =$ | 13.69 (min) | $T_1 =$ |
| | | 79.63 (min) |

$T_c = 93.32$ (min)

Intensity:

SEE FIG. 2.1-2.1a

| | |
|--------------|-------------|
| I (100-YR) = | 3.8 (in/hr) |
| I (10-YR) = | 2.4 (in/hr) |
| I (2-YR) = | 1.6 (in/hr) |

Peak Flow Rate:

$Q = CIA$

C = 0.4 Single family residential districts; lots 1/4-1/2 acre; basin slope <1%

| | | |
|------------|------------|----------|
| i (100-YR) | i (10-YR) | i (2-YR) |
| 3.8 | 2.4 | 1.6 |
| A = | 40.44 (Ac) | |

| | |
|--------------|-------------|
| Q (100-YR) = | 61.47 (cfs) |
| Q (10-YR) = | 38.82 (cfs) |
| Q (2-YR) = | 25.88 (cfs) |

DA#7A EXISTING CALCULATIONS

Volume (100-yr) = 1.38*area*43560 = 2430961.63 cft
 Volume (10-yr) = 0.70*area*43560 = 1233096.48 cft
 Volume (2-yr) = 0.41*area*43560 = 722242.224 cft
 A = 40.44 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

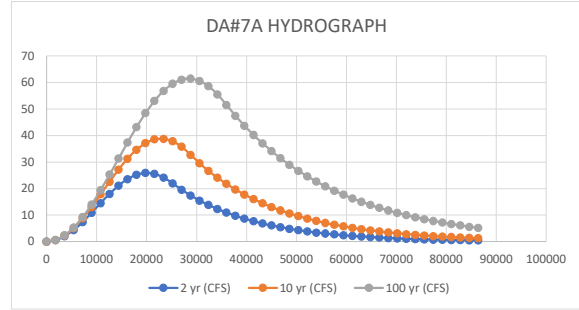
$q_i = \left(\frac{Q_p}{2}\right) \left[1 - \cos\left(\frac{\pi t_i}{T_p}\right)\right]$ $t_i \leq 1.25 T_p$
 $q_i = 1.34 Q_p e^{-1.3t_i/T_p}$ $t_i > 1.25 T_p$

| DA#7A Existing Conditions | | | |
|---------------------------|-----------|-----------|------------|
| | 2 - Year | 10 - Year | 100 - Year |
| Qp= | 25.88 | 38.82 | 61.47 |
| TP= | 20075.989 | 22850.719 | 28451.723 |
| 1.25*TP= | 25094.987 | 28563.399 | 35564.654 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) |
|----------|-------------|-------------|--------------|
| 0 | 0 | 0 | 0 |
| 1800.00 | 0.509974752 | 0.591357156 | 0.605051353 |
| 3600.00 | 1.999704547 | 2.329397541 | 2.396382781 |
| 5400.00 | 4.351773988 | 5.108223259 | 5.303464356 |
| 7200.00 | 7.380801022 | 8.758521905 | 9.211835823 |
| 9000.00 | 10.84804812 | 13.05788268 | 13.96761323 |
| 10800.00 | 14.48023875 | 17.74434778 | 19.38354779 |
| 12600.00 | 17.99109609 | 22.53237331 | 25.24639842 |
| 14400.00 | 21.10390641 | 27.13022738 | 31.32532762 |
| 16200.00 | 23.57332865 | 31.25776513 | 37.38099029 |
| 18000.00 | 25.20473142 | 34.66349783 | 43.17495736 |
| 19800.00 | 25.86953316 | 37.13991596 | 48.47910352 |
| 21600.00 | 25.51533645 | 38.53613266 | 53.08458909 |
| 23400.00 | 24.17005788 | 38.76707716 | 56.81008273 |
| 25200.00 | 21.96843388 | 37.81867814 | 59.5089009 |
| 27000.00 | 19.55145002 | 35.74872107 | 61.0747833 |
| 28800.00 | 17.40038457 | 32.733902 | 61.44607657 |
| 30600.00 | 15.48598099 | 29.5477477 | 60.60816183 |
| 32400.00 | 13.78220154 | 26.67171773 | 58.5940302 |
| 34200.00 | 12.26587321 | 24.07562613 | 55.48298392 |
| 36000.00 | 10.91637248 | 21.73222511 | 51.49642941 |
| 37800.00 | 9.715344853 | 19.61691901 | 47.43061438 |
| 39600.00 | 8.6464552 | 17.70750624 | 43.68580902 |
| 41400.00 | 7.695165601 | 15.98394615 | 40.23666855 |
| 43200.00 | 6.84853761 | 14.42814878 | 37.05984923 |
| 45000.00 | 6.095056277 | 13.02378494 | 34.1338504 |
| 46800.00 | 5.424473535 | 11.75611486 | 31.43886896 |
| 48600.00 | 4.827668818 | 10.61183344 | 28.95666529 |
| 50400.00 | 4.296525011 | 9.57893065 | 26.67043989 |
| 52200.00 | 3.823818051 | 8.646565452 | 24.56471962 |
| 54000.00 | 3.403118672 | 7.804952019 | 22.62525299 |
| 55800.00 | 3.028704959 | 7.045257028 | 20.83891373 |
| 57600.00 | 2.695484528 | 6.359506948 | 19.19361192 |
| 59400.00 | 2.398925264 | 5.740504351 | 17.67821218 |
| 61200.00 | 2.134993676 | 5.18175237 | 16.2824583 |
| 63000.00 | 1.900100043 | 4.677386512 | 14.99690386 |
| 64800.00 | 1.691049586 | 4.222113104 | 13.81284823 |
| 66600.00 | 1.504999021 | 3.811153733 | 12.72227775 |
| 68400.00 | 1.33941788 | 3.440195091 | 11.71781144 |
| 70200.00 | 1.192054103 | 3.105343708 | 10.79265111 |
| 72000.00 | 1.060903401 | 2.803085083 | 9.940535272 |
| 73800.00 | 0.944181999 | 2.530246802 | 9.155696825 |
| 75600.00 | 0.840302375 | 2.283965234 | 8.432823993 |
| 77400.00 | 0.747851667 | 2.061655482 | 7.767024385 |
| 79200.00 | 0.665572456 | 1.860984249 | 7.153791879 |
| 81000.00 | 0.592345666 | 1.679845351 | 6.588976126 |
| 82800.00 | 0.527175344 | 1.516337606 | 6.068754463 |
| 84600.00 | 0.469175111 | 1.368744888 | 5.589606037 |
| 86400.00 | 0.417556107 | 1.235518107 | 5.148287978 |

ti (hrs)

- 0
- 0.5
- 1
- 1.5
- 2
- 2.5
- 3
- 3.5
- 4
- 4.5
- 5
- 5.5
- 6
- 6.5
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- 7.5
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- 8.5
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- 9.5
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- 10.5
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- 13.5
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- 14.5
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- 15.5
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- 16.5
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- 18.5
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- 19.5
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- 20.5
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- 21.5
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- 22.5
- 23
- 23.5
- 24



DA#7B DRAINAGE CALCULATIONS

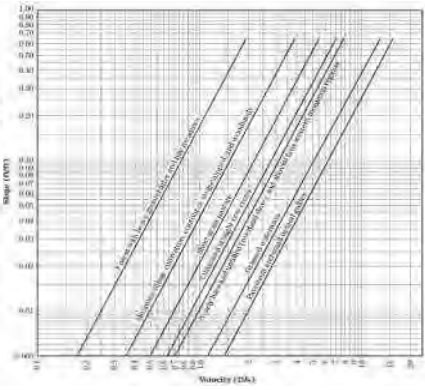
Time of Concentration:

$T_c = T_{OL} + T_1 + \dots + T_n$

Section 2.1
 1. Determine the time of concentration for each sub-area.
 2. Determine the time of concentration for the entire watershed.
 3. Determine the peak flow rate for each sub-area.
 4. Determine the peak flow rate for the entire watershed.
 5. Determine the peak flow rate for the entire watershed.
 6. Determine the peak flow rate for the entire watershed.
 7. Determine the peak flow rate for the entire watershed.
 8. Determine the peak flow rate for the entire watershed.
 9. Determine the peak flow rate for the entire watershed.
 10. Determine the peak flow rate for the entire watershed.

Table 2.1.1 (continued) - Hydrologic Conditions for Groundwater Flow

| Parameter | Value |
|--------------------------------|-------|
| Soil Moisture Deficit (inches) | 0.012 |
| Water Table Depth (feet) | 6.00 |
| Unsat. Water Content (%) | 1.00 |
| Unsat. Water Content (%) | 1.00 |
| Unsat. Water Content (%) | 1.00 |
| Unsat. Water Content (%) | 1.00 |
| Unsat. Water Content (%) | 1.00 |
| Unsat. Water Content (%) | 1.00 |
| Unsat. Water Content (%) | 1.00 |
| Unsat. Water Content (%) | 1.00 |
| Unsat. Water Content (%) | 1.00 |



| | | |
|------------|----------------------------------------------------------------------|-------------|
| $T_{OL} =$ | $T_t = T_{OL}$; multiply by 60 to convert hrs. to min. (L=max 300') | $T =$ |
| $n =$ | 0.15 | $D =$ |
| $L =$ | 100 (ft) | $S =$ |
| $P_2 =$ | 4.89 (in) | $V =$ |
| $S =$ | 0.0040 (ft/ft) | |
| $T_{OL} =$ | 15.09 (min) | $T_1 =$ |
| | | 55.18 (min) |

$T_c = 70.27$ (min)

Intensity:

SEE FIG. 2.1-2.1a

| | |
|---------------|-------------|
| I (100-YR)= | 4.3 (in/hr) |
| I (10-YR)= | 2.8 (in/hr) |
| I (2-YR)= | 1.9 (in/hr) |

Peak Flow Rate:

$Q = CIA$

$C =$ 0.4 Single family residential districts; lots 1/4-1/2 acre; basin slope <1%

| | | |
|--------------|-------------|------------|
| i (100-YR) | i (10-YR) | i (2-YR) |
| 4.3 | 2.8 | 1.9 |
| $A =$ | 12.83 (Ac) | |

| | |
|---------------------------------|--------------------|
| Q (100-YR)= | 22.07 (cfs) |
| Q (10-YR)= | 14.37 (cfs) |
| Q (2-YR)= | 9.75 (cfs) |

DA#7B EXISTING CALCULATIONS

Volume (100-yr) = 1.38*area*43560 = 771247.22 cft
 Volume (10-yr) = 0.70*area*43560 = 391212.36 cft
 Volume (2-yr) = 0.41*area*43560 = 229138.668 cft
 A = 12.83 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

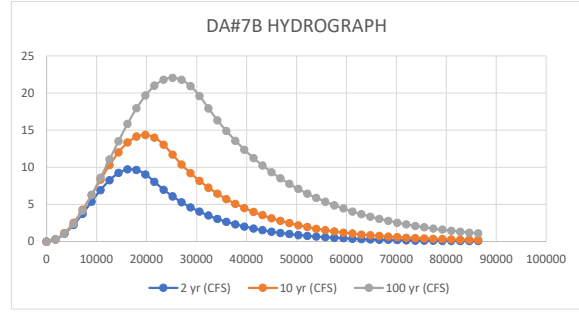
$q_i = \left(\frac{Q_p}{2}\right) \left[1 - \cos\left(\frac{\pi t_i}{T_p}\right)\right]$ $t_i \leq 1.25 T_p$
 $q_i = 4.34 Q_p e^{-1.3t_i/T_p}$ $t_i > 1.25 T_p$

| DA#7B Existing Conditions | | | |
|---------------------------|-----------|-----------|------------|
| | 2 - Year | 10 - Year | 100 - Year |
| Qp= | 9.75 | 14.37 | 22.07 |
| TP= | 16906.096 | 19586.331 | 25143.383 |
| 1.25*TP= | 21132.620 | 24482.914 | 31429.229 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) |
|----------|-------------|-------------|--------------|
| 0 | 0 | 0 | 0 |
| 1800.00 | 0.270200057 | 0.297374964 | 0.277882403 |
| 3600.00 | 1.050850655 | 1.16488348 | 1.097532868 |
| 5400.00 | 2.255422757 | 2.530714137 | 2.417666175 |
| 7200.00 | 3.750398929 | 4.281804958 | 4.171788129 |
| 9000.00 | 5.370072706 | 6.273202552 | 6.271544831 |
| 10800.00 | 6.934915867 | 8.34006119 | 8.611173003 |
| 12600.00 | 8.271477736 | 10.31128856 | 11.07282721 |
| 14400.00 | 9.231610842 | 12.02370862 | 13.53251564 |
| 16200.00 | 9.708891909 | 13.33556908 | 15.8663455 |
| 18000.00 | 9.650418047 | 14.13827556 | 17.95676343 |
| 19800.00 | 9.06267063 | 14.36538091 | 19.69847651 |
| 21600.00 | 8.038836464 | 13.99808558 | 21.00375589 |
| 23400.00 | 6.99738168 | 13.06679388 | 21.80685555 |
| 25200.00 | 6.094953497 | 11.70942614 | 22.06732392 |
| 27000.00 | 5.307121101 | 10.39082387 | 21.77204139 |
| 28800.00 | 4.621123753 | 9.220709823 | 20.93588113 |
| 30600.00 | 4.023798277 | 8.1823627 | 19.60095996 |
| 32400.00 | 3.503682965 | 7.260944183 | 17.93568994 |
| 34200.00 | 3.050797648 | 6.443286905 | 16.34180165 |
| 36000.00 | 2.656452191 | 5.717706277 | 14.8895572 |
| 37800.00 | 2.313079744 | 5.073833519 | 13.56636914 |
| 39600.00 | 2.014091547 | 4.502467481 | 12.36076863 |
| 41400.00 | 1.753750501 | 3.995443158 | 11.26230605 |
| 43200.00 | 1.527061083 | 3.545515009 | 10.26146037 |
| 45000.00 | 1.329673491 | 3.146253414 | 9.349556702 |
| 46800.00 | 1.157800178 | 2.791952797 | 8.518691039 |
| 48600.00 | 1.008143173 | 2.477550087 | 7.761661792 |
| 50400.00 | 0.8778308 | 2.198552368 | 7.071907349 |
| 52200.00 | 0.764362577 | 1.950972673 | 6.443449212 |
| 54000.00 | 0.665561232 | 1.731273008 | 5.870840171 |
| 55800.00 | 0.579530929 | 1.536313793 | 5.349117092 |
| 57600.00 | 0.504620884 | 1.363308999 | 4.8737579 |
| 59400.00 | 0.439393695 | 1.20978633 | 4.440642383 |
| 61200.00 | 0.382597759 | 1.073551899 | 4.046016478 |
| 63000.00 | 0.333143254 | 0.952658872 | 3.686459734 |
| 64800.00 | 0.290081228 | 0.845379647 | 3.358855666 |
| 66600.00 | 0.25258539 | 0.750181171 | 3.06036474 |
| 68400.00 | 0.219936256 | 0.665703026 | 2.788399762 |
| 70200.00 | 0.191507342 | 0.590737993 | 2.540603456 |
| 72000.00 | 0.166753144 | 0.524214796 | 2.314828027 |
| 73800.00 | 0.145198668 | 0.465182798 | 2.10911655 |
| 75600.00 | 0.126430319 | 0.412798412 | 1.921686003 |
| 77400.00 | 0.110087963 | 0.366313049 | 1.75091182 |
| 79200.00 | 0.095858016 | 0.325062418 | 1.5953138 |
| 81000.00 | 0.083467429 | 0.288457033 | 1.453543286 |
| 82800.00 | 0.072678447 | 0.255973793 | 1.324371471 |
| 84600.00 | 0.063284046 | 0.227148501 | 1.206678749 |
| 86400.00 | 0.055103964 | 0.201569235 | 1.099445008 |

ti (hrs)

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23.5
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DA#8 EXISTING CALCULATIONS

Volume (100-yr) = 1.38*area*43560 = 1181817.65 cft
 Volume (10-yr) = 0.70*area*43560 = 599472.72 cft
 Volume (2-yr) = 0.41*area*43560 = 351119.736 cft
 A = 19.66 Ac

TP = time to Qp in seconds

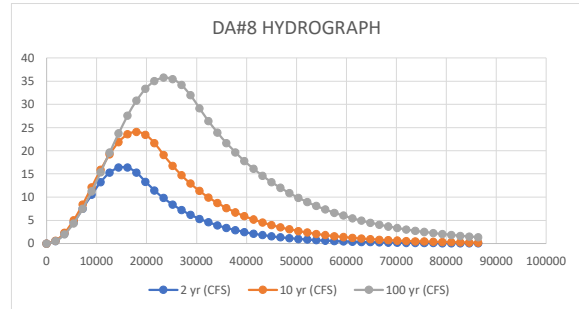
TP = $\frac{V}{1.39 Q_p}$

$q_i = \left(\frac{Q_p}{2}\right) \left[1 - \cos\left(\frac{\pi t_i}{T_p}\right)\right]$ $t_i \leq 1.25 T_p$
 $q_i = 4.34 Q_p e^{-1.3t_i/T_p}$ $t_i > 1.25 T_p$

| DA#8 Existing Conditions | | | |
|--------------------------|-----------|-----------|------------|
| | 2 - Year | 10 - Year | 100 - Year |
| Qp= | 16.51 | 24.08 | 35.78 |
| TP= | 15295.992 | 17907.503 | 23761.878 |
| 1.25*TP= | 19119.990 | 22384.378 | 29702.348 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) |
|----------|-------------|-------------|--------------|
| 0 | 0 | 0 | 0 |
| 1800.00 | 0.557879236 | 0.595418596 | 0.504228603 |
| 3600.00 | 2.156133219 | 2.322792027 | 1.988492058 |
| 5400.00 | 4.578797044 | 5.011296242 | 4.369125414 |
| 7200.00 | 7.498506993 | 8.395058689 | 7.511937148 |
| 9000.00 | 10.52073573 | 12.13945108 | 11.23977327 |
| 10800.00 | 13.23710302 | 15.87418158 | 15.34250314 |
| 12600.00 | 15.28055831 | 19.22991384 | 19.58886412 |
| 14400.00 | 16.37497863 | 21.87479154 | 23.73949736 |
| 16200.00 | 16.37247986 | 23.54725647 | 27.56044 |
| 18000.00 | 15.27339966 | 24.0819146 | 30.83631317 |
| 19800.00 | 13.32062098 | 23.42589232 | 33.38246247 |
| 21600.00 | 11.43103506 | 21.64406523 | 35.05536659 |
| 23400.00 | 9.809494827 | 19.11879663 | 35.76072728 |
| 25200.00 | 8.417976871 | 16.77685873 | 35.45878476 |
| 27000.00 | 7.223851569 | 14.72179418 | 34.16655894 |
| 28800.00 | 6.199117946 | 12.9184627 | 31.95688999 |
| 30600.00 | 5.319747083 | 11.33602851 | 29.11306059 |
| 32400.00 | 4.565118662 | 9.94743302 | 26.38273523 |
| 34200.00 | 3.917537446 | 8.728932146 | 23.90846941 |
| 36000.00 | 3.36181834 | 7.65969032 | 21.66624894 |
| 37800.00 | 2.884930318 | 6.721424204 | 19.63431181 |
| 39600.00 | 2.47569086 | 5.898090058 | 17.7929369 |
| 41400.00 | 2.124503735 | 5.175609407 | 16.12425261 |
| 43200.00 | 1.823133976 | 4.541628301 | 14.61206342 |
| 45000.00 | 1.56451478 | 3.985306078 | 13.24169265 |
| 46800.00 | 1.342581801 | 3.49712999 | 11.99984008 |
| 48600.00 | 1.152130945 | 3.068752544 | 10.87445281 |
| 50400.00 | 0.988696342 | 2.692848766 | 9.85460833 |
| 52200.00 | 0.848445622 | 2.362990945 | 8.930408454 |
| 54000.00 | 0.728090054 | 2.073538729 | 8.092883298 |
| 55800.00 | 0.624807428 | 1.819542673 | 7.3339042 |
| 57600.00 | 0.536175876 | 1.596659611 | 6.646104836 |
| 59400.00 | 0.460117081 | 1.401078386 | 6.022809717 |
| 61200.00 | 0.394847544 | 1.229454688 | 5.457969411 |
| 63000.00 | 0.338836765 | 1.078853864 | 4.946101817 |
| 64800.00 | 0.29077135 | 0.946700737 | 4.482238969 |
| 66600.00 | 0.249524215 | 0.830735576 | 4.061878813 |
| 68400.00 | 0.214128159 | 0.728975451 | 3.680941513 |
| 70200.00 | 0.183753182 | 0.639680331 | 3.335729854 |
| 72000.00 | 0.157687023 | 0.561323328 | 3.02289336 |
| 73800.00 | 0.135318458 | 0.492564587 | 2.739395775 |
| 75600.00 | 0.116122968 | 0.43222838 | 2.482485591 |
| 77400.00 | 0.099650438 | 0.379282996 | 2.24966935 |
| 79200.00 | 0.085514606 | 0.332823105 | 2.038687435 |
| 81000.00 | 0.073384 | 0.292054271 | 1.847492147 |
| 82800.00 | 0.062974172 | 0.256279374 | 1.674227827 |
| 84600.00 | 0.054041022 | 0.224886688 | 1.517212845 |
| 86400.00 | 0.046375077 | 0.197339418 | 1.374923281 |

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DA#9 DRAINAGE CALCULATIONS

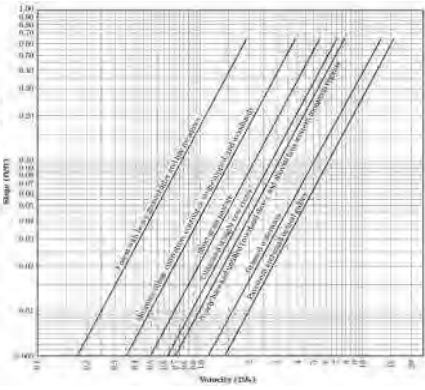
Time of Concentration:

$$T_c = T_{OL} + T_1 + \dots + T_n$$

Section 2.2
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Table 2.11 Manning's Roughness Coefficient for Concrete Sewer Flow

| Surface | n |
|--------------------------------------------------------|-------|
| Smooth Surface (asphalt, concrete, gravel, surf. seal) | 0.012 |
| Polished Ductile Iron | 0.009 |
| Cast-iron Pipe, Rigid Joint | 0.010 |
| Cast-iron Pipe, Flexible Joint | 0.011 |
| Concrete Pipe, Rigid Joint | 0.012 |
| Concrete Pipe, Flexible Joint | 0.013 |
| Corrugated Metal Pipe | 0.014 |
| Clay Pipe, Rigid Joint | 0.015 |
| Clay Pipe, Flexible Joint | 0.016 |
| Stoneware Pipe, Rigid Joint | 0.017 |
| Stoneware Pipe, Flexible Joint | 0.018 |
| Brick Pipe, Rigid Joint | 0.019 |
| Brick Pipe, Flexible Joint | 0.020 |
| Unfinished Concrete | 0.021 |
| Unfinished Masonry | 0.022 |
| Unfinished Metal | 0.023 |
| Unfinished Wood | 0.024 |
| Unfinished Plastic | 0.025 |
| Unfinished Rubber | 0.026 |
| Unfinished Glass | 0.027 |
| Unfinished Paper | 0.028 |
| Unfinished Fabric | 0.029 |
| Unfinished Leather | 0.030 |
| Unfinished Stone | 0.031 |
| Unfinished Brick | 0.032 |
| Unfinished Tile | 0.033 |
| Unfinished Slate | 0.034 |
| Unfinished Marble | 0.035 |
| Unfinished Granite | 0.036 |
| Unfinished Quartz | 0.037 |
| Unfinished Gneiss | 0.038 |
| Unfinished Schist | 0.039 |
| Unfinished Slate | 0.040 |
| Unfinished Marble | 0.041 |
| Unfinished Granite | 0.042 |
| Unfinished Quartz | 0.043 |
| Unfinished Gneiss | 0.044 |
| Unfinished Schist | 0.045 |
| Unfinished Slate | 0.046 |
| Unfinished Marble | 0.047 |
| Unfinished Granite | 0.048 |
| Unfinished Quartz | 0.049 |
| Unfinished Gneiss | 0.050 |
| Unfinished Schist | 0.051 |
| Unfinished Slate | 0.052 |
| Unfinished Marble | 0.053 |
| Unfinished Granite | 0.054 |
| Unfinished Quartz | 0.055 |
| Unfinished Gneiss | 0.056 |
| Unfinished Schist | 0.057 |
| Unfinished Slate | 0.058 |
| Unfinished Marble | 0.059 |
| Unfinished Granite | 0.060 |
| Unfinished Quartz | 0.061 |
| Unfinished Gneiss | 0.062 |
| Unfinished Schist | 0.063 |
| Unfinished Slate | 0.064 |
| Unfinished Marble | 0.065 |
| Unfinished Granite | 0.066 |
| Unfinished Quartz | 0.067 |
| Unfinished Gneiss | 0.068 |
| Unfinished Schist | 0.069 |
| Unfinished Slate | 0.070 |
| Unfinished Marble | 0.071 |
| Unfinished Granite | 0.072 |
| Unfinished Quartz | 0.073 |
| Unfinished Gneiss | 0.074 |
| Unfinished Schist | 0.075 |
| Unfinished Slate | 0.076 |
| Unfinished Marble | 0.077 |
| Unfinished Granite | 0.078 |
| Unfinished Quartz | 0.079 |
| Unfinished Gneiss | 0.080 |
| Unfinished Schist | 0.081 |
| Unfinished Slate | 0.082 |
| Unfinished Marble | 0.083 |
| Unfinished Granite | 0.084 |
| Unfinished Quartz | 0.085 |
| Unfinished Gneiss | 0.086 |
| Unfinished Schist | 0.087 |
| Unfinished Slate | 0.088 |
| Unfinished Marble | 0.089 |
| Unfinished Granite | 0.090 |
| Unfinished Quartz | 0.091 |
| Unfinished Gneiss | 0.092 |
| Unfinished Schist | 0.093 |
| Unfinished Slate | 0.094 |
| Unfinished Marble | 0.095 |
| Unfinished Granite | 0.096 |
| Unfinished Quartz | 0.097 |
| Unfinished Gneiss | 0.098 |
| Unfinished Schist | 0.099 |
| Unfinished Slate | 0.100 |



| | | |
|------------|-----------------------------------------------------------------------------|----------------------|
| $T_{OL} =$ | $T_t = T_{OL}$; multiply by 60 to convert hrs. to min. ($L = \max 300'$) | $T =$ |
| $n =$ | 0.15 | $D =$ 419.46 (ft) |
| $L =$ | 100 (ft) | $S =$ 0.0236 (ft/ft) |
| $P_2 =$ | 4.89 (in) | $V =$ 1.125 (ft/s) |
| $S =$ | 0.0236 (ft/ft) | |
| $T_{OL} =$ | 7.42 (min) | $T_1 =$ 6.21 (min) |

$T_c = 13.63$ (min)

Intensity:

SEE FIG. 2.1-2.1a

| | |
|---------------|-------------|
| I (100-YR)= | 10 (in/hr) |
| I (10-YR)= | 6.7 (in/hr) |
| I (2-YR)= | 4.7 (in/hr) |

Peak Flow Rate:

$$Q = CIA$$

$C =$ 0.45 Single family residential district; lots 1/4-1/2 acre; basin slope 1-3.5%

| | | |
|--------------|-------------|------------|
| i (100-YR) | i (10-YR) | i (2-YR) |
| 10 | 6.7 | 4.7 |
| $A =$ | 6.64 (Ac) | |

| | |
|---------------|-------------|
| Q (100-YR)= | 29.88 (cfs) |
| Q (10-YR)= | 20.02 (cfs) |
| Q (2-YR)= | 14.04 (cfs) |

DA#9 EXISTING CALCULATIONS

Volume (100-yr) = 1.38*area*43560 = 399148.99 cft
 Volume (10-yr) = 0.70*area*43560 = 202466.88 cft
 Volume (2-yr) = 0.41*area*43560 = 118587.744 cft
 A = 6.64 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

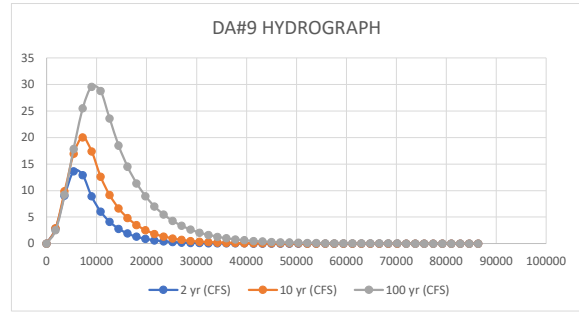
$q_i = \left(\frac{Q_p}{2}\right) \left[1 - \cos\left(\frac{\pi t_i}{T_p}\right)\right]$ $t_i \leq 1.25 T_p$
 $q_i = 1.34 Q_p e^{-1.3t_i/T_p}$ $t_i > 1.25 T_p$

| DA#9 Existing Conditions | | | |
|--------------------------|----------|-----------|------------|
| | 2 - Year | 10 - Year | 100 - Year |
| Qp= | 14.04 | 20.02 | 29.88 |
| TP= | 6075.004 | 7275.851 | 9610.360 |
| 1.25*TP= | 7593.755 | 9094.814 | 12012.950 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) |
|----------|-------------|-------------|--------------|
| 0 | 0 | 0 | 0 |
| 1800.00 | 2.828668498 | 2.874087222 | 2.512576034 |
| 3600.00 | 9.035667051 | 9.845890864 | 9.205185217 |
| 5400.00 | 13.62012942 | 16.91182009 | 17.82673124 |
| 7200.00 | 12.88843736 | 20.01423202 | 25.47730916 |
| 9000.00 | 8.882796347 | 17.37155209 | 29.58360455 |
| 10800.00 | 6.04318668 | 12.61535786 | 28.76444214 |
| 12600.00 | 4.111329791 | 9.145876152 | 23.58599257 |
| 14400.00 | 2.797039632 | 6.630572952 | 18.48881134 |
| 16200.00 | 1.902895438 | 4.807029631 | 14.49318462 |
| 18000.00 | 1.294586965 | 3.484998061 | 11.36105488 |
| 19800.00 | 0.880739623 | 2.52655224 | 8.905811352 |
| 21600.00 | 0.599189011 | 1.831698644 | 6.981171788 |
| 23400.00 | 0.407643146 | 1.327944013 | 5.47246709 |
| 25200.00 | 0.277329743 | 0.96273222 | 4.289809355 |
| 27000.00 | 0.188674303 | 0.697961148 | 3.362736405 |
| 28800.00 | 0.128359808 | 0.506007542 | 2.636013676 |
| 30600.00 | 0.087326361 | 0.366845108 | 2.066343377 |
| 32400.00 | 0.05941029 | 0.265955192 | 1.619784826 |
| 34200.00 | 0.040418294 | 0.192812069 | 1.269732277 |
| 36000.00 | 0.027497568 | 0.139784802 | 0.995329768 |
| 37800.00 | 0.018707277 | 0.10134112 | 0.78022853 |
| 39600.00 | 0.012727025 | 0.073470237 | 0.611612933 |
| 41400.00 | 0.008658511 | 0.053264417 | 0.479436941 |
| 43200.00 | 0.0058906 | 0.038615612 | 0.375825572 |
| 45000.00 | 0.004007521 | 0.027995528 | 0.294605711 |
| 46800.00 | 0.002726416 | 0.020296185 | 0.230938316 |
| 48600.00 | 0.001854848 | 0.014714318 | 0.181030115 |
| 50400.00 | 0.001261899 | 0.01066758 | 0.141907602 |
| 52200.00 | 0.000858501 | 0.007733777 | 0.111239876 |
| 54000.00 | 0.00058406 | 0.00560683 | 0.087199768 |
| 55800.00 | 0.00039735 | 0.004064837 | 0.06835498 |
| 57600.00 | 0.000270327 | 0.002946923 | 0.05358275 |
| 59400.00 | 0.00018391 | 0.002136459 | 0.042002953 |
| 61200.00 | 0.000125119 | 0.001548889 | 0.032925673 |
| 63000.00 | 8.51214E-05 | 0.001122913 | 0.025810089 |
| 64800.00 | 5.79102E-05 | 0.000814089 | 0.020232257 |
| 66600.00 | 3.93978E-05 | 0.000590198 | 0.015859853 |
| 68400.00 | 2.68033E-05 | 0.000427881 | 0.012432372 |
| 70200.00 | 1.82349E-05 | 0.000310205 | 0.009745606 |
| 72000.00 | 1.24057E-05 | 0.000224892 | 0.007639478 |
| 73800.00 | 8.43989E-06 | 0.000163042 | 0.005988506 |
| 75600.00 | 5.74187E-06 | 0.000118202 | 0.004694327 |
| 77400.00 | 3.90633E-06 | 8.56943E-05 | 0.003679833 |
| 79200.00 | 2.65758E-06 | 6.21266E-05 | 0.002884583 |
| 81000.00 | 1.80801E-06 | 4.50405E-05 | 0.002261194 |
| 82800.00 | 1.23004E-06 | 3.26535E-05 | 0.001772526 |
| 84600.00 | 8.36825E-07 | 2.36731E-05 | 0.001389465 |
| 86400.00 | 5.69313E-07 | 1.71625E-05 | 0.001089187 |

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DA#10 EXISTING CALCULATIONS

Volume (100-yr) = 1.38*area*43560 = 992462.33 cft
 Volume (10-yr) = 0.70*area*43560 = 503422.92 cft
 Volume (2-yr) = 0.41*area*43560 = 294861.996 cft
 A = 16.51 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

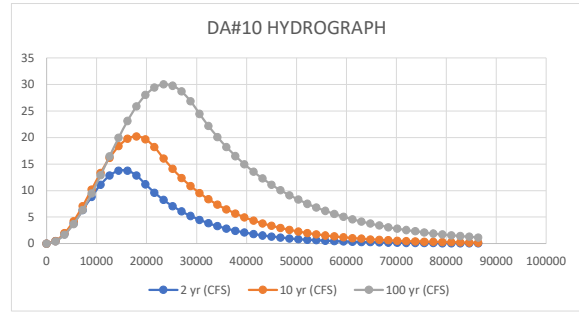
$q_i = \left(\frac{Q_p}{2}\right) \left[1 - \cos\left(\frac{\pi t_i}{T_p}\right)\right]$ $t_i \leq 1.25 T_p$
 $q_i = 4.34 Q_p e^{-1.3t_i/T_p}$ $t_i > 1.25 T_p$

| DA#10 Existing Conditions | | | |
|---------------------------|-----------|-----------|------------|
| | 2 - Year | 10 - Year | 100 - Year |
| Qp= | 13.87 | 20.22 | 30.05 |
| TP= | 15295.992 | 17907.503 | 23761.878 |
| 1.25*TP= | 19119.990 | 22384.378 | 29702.348 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) |
|----------|-------------|-------------|--------------|
| 0 | 0 | 0 | 0 |
| 1800.00 | 0.468493702 | 0.500018363 | 0.423439178 |
| 3600.00 | 1.810669351 | 1.950625451 | 1.669888295 |
| 5400.00 | 3.84516476 | 4.208367292 | 3.669087517 |
| 7200.00 | 6.297067673 | 7.049970445 | 6.308345997 |
| 9000.00 | 8.835063425 | 10.19442204 | 9.438894033 |
| 10800.00 | 11.11620401 | 13.33075981 | 12.88426892 |
| 12600.00 | 12.83224912 | 16.14882388 | 16.45026178 |
| 14400.00 | 13.75131725 | 18.36992922 | 19.93586477 |
| 16200.00 | 13.74921885 | 19.77442545 | 23.14460144 |
| 18000.00 | 12.82623745 | 20.22341862 | 25.89560175 |
| 19800.00 | 11.18634041 | 19.67250672 | 28.03379733 |
| 21600.00 | 9.599511133 | 18.17617075 | 29.43866238 |
| 23400.00 | 8.237780244 | 16.05551029 | 30.03100749 |
| 25200.00 | 7.069216589 | 14.08880659 | 29.77744336 |
| 27000.00 | 6.066418586 | 12.3630123 | 28.69226287 |
| 28800.00 | 5.205871683 | 10.84861746 | 26.83663549 |
| 30600.00 | 4.467396965 | 9.519726894 | 24.44845525 |
| 32400.00 | 3.833677981 | 8.353617455 | 22.15559302 |
| 34200.00 | 3.289854692 | 7.330349427 | 20.07776347 |
| 36000.00 | 2.823175015 | 6.432425594 | 18.1948001 |
| 37800.00 | 2.422695806 | 5.644492045 | 16.48842767 |
| 39600.00 | 2.079026251 | 4.953075629 | 14.94208485 |
| 41400.00 | 1.784107664 | 4.346353576 | 13.54076351 |
| 43200.00 | 1.531024514 | 3.813951335 | 12.27086302 |
| 45000.00 | 1.313842269 | 3.346765175 | 11.12005827 |
| 46800.00 | 1.127468237 | 2.936806517 | 10.07718004 |
| 48600.00 | 0.967532142 | 2.577065336 | 9.132106609 |
| 50400.00 | 0.830283652 | 2.261390291 | 8.27566549 |
| 52200.00 | 0.712504436 | 1.984383546 | 7.499544434 |
| 54000.00 | 0.611432696 | 1.741308465 | 6.796210745 |
| 55800.00 | 0.524698405 | 1.528008623 | 6.158838166 |
| 57600.00 | 0.450267737 | 1.340836733 | 5.581240632 |
| 59400.00 | 0.386395371 | 1.176592276 | 5.057812223 |
| 61200.00 | 0.331583568 | 1.032466781 | 4.583472786 |
| 63000.00 | 0.284547049 | 0.905995793 | 4.153618566 |
| 64800.00 | 0.244182858 | 0.795016743 | 3.764077588 |
| 66600.00 | 0.209544496 | 0.697631961 | 3.411069136 |
| 68400.00 | 0.179819731 | 0.612176231 | 3.091167059 |
| 70200.00 | 0.154311548 | 0.537188315 | 2.801266525 |
| 72000.00 | 0.132421808 | 0.471385969 | 2.538553885 |
| 73800.00 | 0.11363722 | 0.413644015 | 2.300479361 |
| 75600.00 | 0.097517304 | 0.362975105 | 2.084732305 |
| 77400.00 | 0.083684066 | 0.318512832 | 1.889218767 |
| 79200.00 | 0.07181313 | 0.27949692 | 1.712041178 |
| 81000.00 | 0.061626137 | 0.245260224 | 1.551479926 |
| 82800.00 | 0.052884211 | 0.215217318 | 1.405976675 |
| 84600.00 | 0.045382364 | 0.188854488 | 1.274119231 |
| 86400.00 | 0.038944685 | 0.165720946 | 1.154627842 |

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DA#11 EXISTING CALCULATIONS

Volume (100-yr) = 1.38*area*43560 = 1507027.90 cft
 Volume (10-yr) = 0.70*area*43560 = 764434.44 cft
 Volume (2-yr) = 0.41*area*43560 = 447740.172 cft
 A = 25.07 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

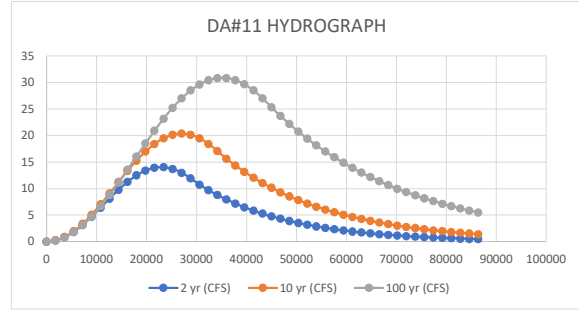
$q_i = \left(\frac{Q_p}{2}\right) \left[1 - \cos\left(\frac{\pi t_i}{T_p}\right)\right]$ $t_i \leq 1.25 T_p$
 $q_i = 1.34 Q_p e^{-1.3 t_i / T_p}$ $t_i > 1.25 T_p$

| DA#11 Existing Conditions | | | |
|---------------------------|-----------|-----------|------------|
| | 2 - Year | 10 - Year | 100 - Year |
| Qp= | 14.04 | 20.36 | 30.89 |
| TP= | 22943.988 | 27015.629 | 35102.775 |
| 1.25*TP= | 28679.985 | 33769.536 | 43878.469 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) |
|----------|-------------|-------------|--------------|
| 0 | 0 | 0 | 0 |
| 1800.00 | 0.212123993 | 0.222166563 | 0.1999528 |
| 3600.00 | 0.8356757 | 0.878967699 | 0.794633343 |
| 5400.00 | 1.832969135 | 1.941731127 | 1.768642146 |
| 7200.00 | 3.143730246 | 3.364062516 | 3.096756872 |
| 9000.00 | 4.688739738 | 5.083870799 | 4.744585474 |
| 10800.00 | 6.374620899 | 7.026078725 | 6.669456788 |
| 12600.00 | 8.099483069 | 9.105900313 | 8.821525524 |
| 14400.00 | 9.759079665 | 11.23254214 | 11.14506302 |
| 16200.00 | 11.2531086 | 13.31316686 | 13.57990038 |
| 18000.00 | 12.49127432 | 15.256946 | 16.06298654 |
| 19800.00 | 13.398745 | 16.97902497 | 18.53002101 |
| 21600.00 | 13.92067529 | 18.40422741 | 20.91711897 |
| 23400.00 | 14.02552094 | 19.47033691 | 23.16246561 |
| 25200.00 | 13.70694533 | 20.13081308 | 25.20791679 |
| 27000.00 | 12.98420242 | 20.35682319 | 27.00050475 |
| 28800.00 | 11.91654445 | 20.13850091 | 28.49380974 |
| 30600.00 | 10.76112628 | 19.48537697 | 29.64916205 |
| 32400.00 | 9.717736487 | 18.42596313 | 30.43664337 |
| 34200.00 | 8.775512894 | 17.04023431 | 30.83586157 |
| 36000.00 | 7.924646512 | 15.62638361 | 30.83647874 |
| 37800.00 | 7.156279422 | 14.32984197 | 30.4384789 |
| 39600.00 | 6.462412561 | 13.1408761 | 29.65216841 |
| 41400.00 | 5.835822451 | 12.05056029 | 28.49790908 |
| 43200.00 | 5.269985992 | 11.05070942 | 27.00559091 |
| 45000.00 | 4.759012563 | 10.1338175 | 25.32140818 |
| 46800.00 | 4.29758269 | 9.293001309 | 23.68847906 |
| 48600.00 | 3.880892671 | 8.521948744 | 22.16085442 |
| 50400.00 | 3.504604567 | 7.814871426 | 20.73174336 |
| 52200.00 | 3.164801043 | 7.166461245 | 19.39479294 |
| 54000.00 | 2.857944584 | 6.571850512 | 18.14405989 |
| 55800.00 | 2.58084067 | 6.026575414 | 16.97398421 |
| 57600.00 | 2.33060452 | 5.52654251 | 15.87936448 |
| 59400.00 | 2.104631057 | 5.067997995 | 14.85533468 |
| 61200.00 | 1.900567792 | 4.647499523 | 13.8973426 |
| 63000.00 | 1.71629033 | 4.261890363 | 13.00112959 |
| 64800.00 | 1.549880257 | 3.908275703 | 12.16271164 |
| 66600.00 | 1.399605165 | 3.584000918 | 11.37836166 |
| 68400.00 | 1.26390062 | 3.286631639 | 10.64459291 |
| 70200.00 | 1.141353874 | 3.01393548 | 9.958143503 |
| 72000.00 | 1.030689158 | 2.763865282 | 9.315961901 |
| 73800.00 | 0.930754401 | 2.534543737 | 8.715193361 |
| 75600.00 | 0.840509233 | 2.324249303 | 8.153167233 |
| 77400.00 | 0.759014162 | 2.131403276 | 7.627385093 |
| 79200.00 | 0.685420784 | 1.954557937 | 7.135509637 |
| 81000.00 | 0.618962959 | 1.792385689 | 6.675354287 |
| 82800.00 | 0.558948829 | 1.643669087 | 6.244873474 |
| 84600.00 | 0.504753618 | 1.507291696 | 5.842153544 |
| 86400.00 | 0.45581313 | 1.382229718 | 5.465404251 |

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DA#12 EXISTING CALCULATIONS

Volume (100-yr) = 1.38*area*43560 = 940164.19 cft
 Volume (10-yr) = 0.70*area*43560 = 476894.88 cft
 Volume (2-yr) = 0.41*area*43560 = 279324.144 cft
 A = 15.64 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

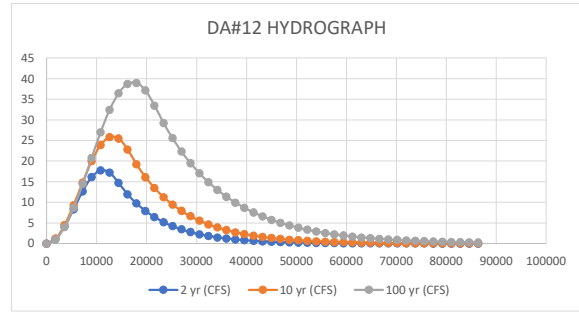
$q_i = \left(\frac{Q_p}{2}\right) \left[1 - \cos\left(\frac{\pi t_i}{T_p}\right)\right]$ $t_i \leq 1.25 T_p$
 $q_i = 1.34 Q_p e^{-1.3t_i/T_p}$ $t_i > 1.25 T_p$

| DA#12 Existing Conditions | | | |
|---------------------------|-----------|-----------|------------|
| | 2 - Year | 10 - Year | 100 - Year |
| Qp= | 17.83 | 25.96 | 39.10 |
| TP= | 11270.731 | 13214.874 | 17298.647 |
| 1.25*TP= | 14088.413 | 16518.592 | 21623.309 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) |
|----------|-------------|-------------|--------------|
| 0 | 0 | 0 | 0 |
| 1800.00 | 1.09873382 | 1.170486314 | 1.035300289 |
| 3600.00 | 4.124101161 | 4.470864892 | 4.031549321 |
| 5400.00 | 8.330359342 | 9.305959949 | 8.671405153 |
| 7200.00 | 12.68068014 | 14.80383166 | 14.4634464 |
| 9000.00 | 16.1027244 | 19.97301798 | 20.79422016 |
| 10800.00 | 17.75296993 | 23.88133054 | 26.99321475 |
| 12600.00 | 17.22463687 | 25.8239614 | 32.40387559 |
| 14400.00 | 14.69922864 | 25.45058504 | 36.45314296 |
| 16200.00 | 11.94338541 | 22.82853451 | 38.71214652 |
| 18000.00 | 9.704213641 | 19.1785351 | 38.94162825 |
| 19800.00 | 7.884846646 | 16.06621292 | 37.11728305 |
| 21600.00 | 6.406578516 | 13.45896318 | 33.43233291 |
| 23400.00 | 5.20549297 | 11.27482193 | 29.23825138 |
| 25200.00 | 4.229528511 | 9.445126481 | 25.53901134 |
| 27000.00 | 3.436567344 | 7.912356826 | 22.30780124 |
| 28800.00 | 2.792272253 | 6.628327389 | 19.48540566 |
| 30600.00 | 2.268771003 | 5.552672224 | 17.02010115 |
| 32400.00 | 1.8434169 | 4.651576033 | 14.86670837 |
| 34200.00 | 1.497809106 | 3.896711119 | 12.98576405 |
| 36000.00 | 1.21699661 | 3.264346844 | 11.34279786 |
| 37800.00 | 0.988831449 | 2.734603617 | 9.907700687 |
| 39600.00 | 0.803443187 | 2.290827935 | 8.654172814 |
| 41400.00 | 0.652811918 | 1.919068854 | 7.559241994 |
| 43200.00 | 0.530421325 | 1.607639408 | 6.602842438 |
| 45000.00 | 0.430976786 | 1.346749212 | 5.767447092 |
| 46800.00 | 0.350176325 | 1.128196678 | 5.037746437 |
| 48600.00 | 0.284524509 | 0.945111186 | 4.400367919 |
| 50400.00 | 0.231181238 | 0.791737089 | 3.843630891 |
| 52200.00 | 0.187838878 | 0.663252776 | 3.357332545 |
| 54000.00 | 0.152622438 | 0.555619095 | 2.93256094 |
| 55800.00 | 0.124008453 | 0.465452374 | 2.561531677 |
| 57600.00 | 0.10075908 | 0.389918046 | 2.237445246 |
| 59400.00 | 0.081868549 | 0.326641546 | 1.954362413 |
| 61200.00 | 0.066519656 | 0.273633653 | 1.707095379 |
| 63000.00 | 0.054048407 | 0.229227963 | 1.49111271 |
| 64800.00 | 0.043915295 | 0.192028497 | 1.30245629 |
| 66600.00 | 0.03568196 | 0.160865817 | 1.137668786 |
| 68400.00 | 0.028992229 | 0.134760265 | 0.99373029 |
| 70200.00 | 0.023556703 | 0.112891162 | 0.868002974 |
| 72000.00 | 0.019140241 | 0.09457101 | 0.758182749 |
| 73800.00 | 0.015551787 | 0.079223881 | 0.66225704 |
| 75600.00 | 0.012636105 | 0.066367308 | 0.578467906 |
| 77400.00 | 0.01026706 | 0.055597119 | 0.505279821 |
| 79200.00 | 0.00834217 | 0.046574733 | 0.441351533 |
| 81000.00 | 0.006778162 | 0.039016514 | 0.385511489 |
| 82800.00 | 0.005507377 | 0.032684854 | 0.336736358 |
| 84600.00 | 0.004474842 | 0.027380706 | 0.294132284 |
| 86400.00 | 0.003635889 | 0.022937322 | 0.256918502 |

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DA#13 DRAINAGE CALCULATIONS

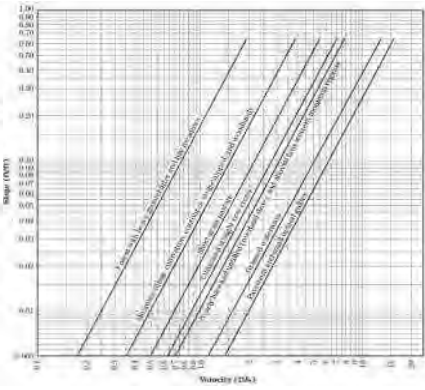
Time of Concentration:

$T_c = T_{OL} + T_1 + \dots + T_n$

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Table 2.1.1 (continued) Longstone Conditions for Gravel Shell Flow

| Surface | n |
|--------------------------------------------------------|-------|
| Smooth Surface (asphalt, concrete, gravel, surf, etc.) | 0.012 |
| Polished Stone Course | 0.009 |
| Unfinished Stone, Resilient Course in 20% Gravel | 0.008 |
| Unfinished Stone, Resilient Course in 10% Gravel | 0.009 |
| Gravel, Dense Gravel | 0.008 |
| Gravel, Stone Gravel | 0.009 |
| Gravel, Light Gravel | 0.010 |
| Gravel, Heavy Gravel | 0.011 |
| Gravel, Very Heavy Gravel | 0.012 |
| Gravel, Very Heavy Gravel | 0.013 |
| Gravel, Very Heavy Gravel | 0.014 |
| Gravel, Very Heavy Gravel | 0.015 |
| Gravel, Very Heavy Gravel | 0.016 |
| Gravel, Very Heavy Gravel | 0.017 |
| Gravel, Very Heavy Gravel | 0.018 |
| Gravel, Very Heavy Gravel | 0.019 |
| Gravel, Very Heavy Gravel | 0.020 |
| Gravel, Very Heavy Gravel | 0.021 |
| Gravel, Very Heavy Gravel | 0.022 |
| Gravel, Very Heavy Gravel | 0.023 |
| Gravel, Very Heavy Gravel | 0.024 |
| Gravel, Very Heavy Gravel | 0.025 |
| Gravel, Very Heavy Gravel | 0.026 |
| Gravel, Very Heavy Gravel | 0.027 |
| Gravel, Very Heavy Gravel | 0.028 |
| Gravel, Very Heavy Gravel | 0.029 |
| Gravel, Very Heavy Gravel | 0.030 |
| Gravel, Very Heavy Gravel | 0.031 |
| Gravel, Very Heavy Gravel | 0.032 |
| Gravel, Very Heavy Gravel | 0.033 |
| Gravel, Very Heavy Gravel | 0.034 |
| Gravel, Very Heavy Gravel | 0.035 |
| Gravel, Very Heavy Gravel | 0.036 |
| Gravel, Very Heavy Gravel | 0.037 |
| Gravel, Very Heavy Gravel | 0.038 |
| Gravel, Very Heavy Gravel | 0.039 |
| Gravel, Very Heavy Gravel | 0.040 |
| Gravel, Very Heavy Gravel | 0.041 |
| Gravel, Very Heavy Gravel | 0.042 |
| Gravel, Very Heavy Gravel | 0.043 |
| Gravel, Very Heavy Gravel | 0.044 |
| Gravel, Very Heavy Gravel | 0.045 |
| Gravel, Very Heavy Gravel | 0.046 |
| Gravel, Very Heavy Gravel | 0.047 |
| Gravel, Very Heavy Gravel | 0.048 |
| Gravel, Very Heavy Gravel | 0.049 |
| Gravel, Very Heavy Gravel | 0.050 |
| Gravel, Very Heavy Gravel | 0.051 |
| Gravel, Very Heavy Gravel | 0.052 |
| Gravel, Very Heavy Gravel | 0.053 |
| Gravel, Very Heavy Gravel | 0.054 |
| Gravel, Very Heavy Gravel | 0.055 |
| Gravel, Very Heavy Gravel | 0.056 |
| Gravel, Very Heavy Gravel | 0.057 |
| Gravel, Very Heavy Gravel | 0.058 |
| Gravel, Very Heavy Gravel | 0.059 |
| Gravel, Very Heavy Gravel | 0.060 |
| Gravel, Very Heavy Gravel | 0.061 |
| Gravel, Very Heavy Gravel | 0.062 |
| Gravel, Very Heavy Gravel | 0.063 |
| Gravel, Very Heavy Gravel | 0.064 |
| Gravel, Very Heavy Gravel | 0.065 |
| Gravel, Very Heavy Gravel | 0.066 |
| Gravel, Very Heavy Gravel | 0.067 |
| Gravel, Very Heavy Gravel | 0.068 |
| Gravel, Very Heavy Gravel | 0.069 |
| Gravel, Very Heavy Gravel | 0.070 |
| Gravel, Very Heavy Gravel | 0.071 |
| Gravel, Very Heavy Gravel | 0.072 |
| Gravel, Very Heavy Gravel | 0.073 |
| Gravel, Very Heavy Gravel | 0.074 |
| Gravel, Very Heavy Gravel | 0.075 |
| Gravel, Very Heavy Gravel | 0.076 |
| Gravel, Very Heavy Gravel | 0.077 |
| Gravel, Very Heavy Gravel | 0.078 |
| Gravel, Very Heavy Gravel | 0.079 |
| Gravel, Very Heavy Gravel | 0.080 |



| $T_{OL} =$ | $T =$ |
|-----------------------------------------------------------------------------------|---------------------|
| $T_{OL} = Tt = T_0l$; multiply by 60 to convert hrs. to min. ($L = \max 300'$) | |
| n = 0.8 | D = 408.8 (ft) |
| L = 100 (ft) | S = 0.0110 (ft/ft) |
| $P_2 = 4.89$ (in) | V = 0.2625 (ft/s) |
| S = 0.0110 (ft/ft) | |
| $T_{OL} = 38.42$ (min) | $T_1 = 25.96$ (min) |

$T_c = 64.37$ (min)

Intensity:

SEE FIG. 2.1-2.1a

| | |
|--------------|-------------|
| I (100-YR) = | 4.5 (in/hr) |
| I (10-YR) = | 3 (in/hr) |
| I (2-YR) = | 2 (in/hr) |

Peak Flow Rate:

$Q = CIA$

C = 0.2 Woodlands; basin slope 1-3.5%

| i (100-YR) | i (10-YR) | i (2-YR) |
|----------------|-----------|----------|
| 4.5 | 3 | 2 |
| A = 16.24 (Ac) | | |

| | |
|--------------|-------------|
| Q (100-YR) = | 14.62 (cfs) |
| Q (10-YR) = | 9.74 (cfs) |
| Q (2-YR) = | 6.50 (cfs) |

DA#13 EXISTING CALCULATIONS

Volume (100-yr) = 1.38*area*43560 = 976231.87 cft
 Volume (10-yr) = 0.70*area*43560 = 495190.08 cft
 Volume (2-yr) = 0.41*area*43560 = 290039.904 cft
 A = 16.24 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

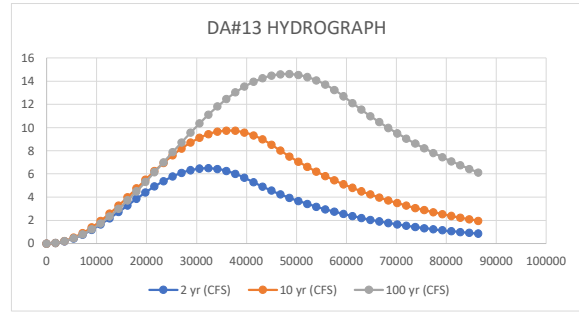
$q_i = \left(\frac{Q_p}{2}\right) \left[1 - \cos\left(\frac{\pi t_i}{T_p}\right)\right]$ $t_i \leq 1.25 T_p$
 $q_i = 1.34 Q_p e^{-1.3 t_i / T_p}$ $t_i > 1.25 T_p$

| DA#13 Existing Conditions | | | |
|---------------------------|-----------|-----------|------------|
| | 2 - Year | 10 - Year | 100 - Year |
| Qp= | 6.50 | 9.74 | 14.62 |
| TP= | 32121.583 | 36561.151 | 48051.799 |
| 1.25*TP= | 40151.978 | 45701.439 | 60064.748 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) |
|----------|-------------|-------------|--------------|
| 0 | 0 | 0 | 0 |
| 1800.00 | 0.050201302 | 0.058158924 | 0.05054669 |
| 3600.00 | 0.199253377 | 0.231247166 | 0.201487537 |
| 5400.00 | 0.442548709 | 0.515132286 | 0.450734537 |
| 7200.00 | 0.77256652 | 0.903036592 | 0.794839794 |
| 9000.00 | 1.179105256 | 1.385698961 | 1.229043217 |
| 10800.00 | 1.649597939 | 1.951595944 | 1.747338359 |
| 12600.00 | 2.169500636 | 2.587216883 | 2.342555517 |
| 14400.00 | 2.722742048 | 3.27738648 | 3.006460902 |
| 16200.00 | 3.292220302 | 4.005627097 | 3.729870547 |
| 18000.00 | 3.860331613 | 4.754552162 | 4.50277347 |
| 19800.00 | 4.409514448 | 5.506281267 | 5.314489489 |
| 21600.00 | 4.922792396 | 6.242867057 | 6.153778357 |
| 23400.00 | 5.384298941 | 6.946723719 | 7.00903386 |
| 25200.00 | 5.779767933 | 7.601046843 | 7.868425037 |
| 27000.00 | 6.096974581 | 8.190214619 | 8.720063714 |
| 28800.00 | 6.326113352 | 8.700160805 | 9.552168963 |
| 30600.00 | 6.460101079 | 9.118710556 | 10.35323006 |
| 32400.00 | 6.494795914 | 9.435871097 | 11.11216574 |
| 34200.00 | 6.429125368 | 9.644070294 | 11.81847745 |
| 36000.00 | 6.265119455 | 9.738337441 | 12.4623946 |
| 37800.00 | 6.00784795 | 9.716421931 | 13.03500973 |
| 39600.00 | 5.665263661 | 9.578846993 | 13.52840171 |
| 41400.00 | 5.278025033 | 9.328897195 | 13.93574532 |
| 43200.00 | 4.907201229 | 8.97254003 | 14.25140569 |
| 45000.00 | 4.562430787 | 8.518283441 | 14.4710162 |
| 46800.00 | 4.241883247 | 8.008189183 | 14.59153893 |
| 48600.00 | 3.943856756 | 7.511703753 | 14.61130665 |
| 50400.00 | 3.666769028 | 7.045999038 | 14.53004592 |
| 52200.00 | 3.409148947 | 6.609166718 | 14.34888083 |
| 54000.00 | 3.169628753 | 6.199416786 | 14.07031748 |
| 55800.00 | 2.946936783 | 5.815070208 | 13.69820931 |
| 57600.00 | 2.73989072 | 5.454552048 | 13.23770379 |
| 59400.00 | 2.547391311 | 5.11638501 | 12.69517121 |
| 61200.00 | 2.368416537 | 4.799183387 | 12.11298367 |
| 63000.00 | 2.202016184 | 4.501647381 | 11.53724456 |
| 64800.00 | 2.047306797 | 4.222557779 | 10.98887075 |
| 66600.00 | 1.903466992 | 3.960770955 | 10.46656156 |
| 68400.00 | 1.769733092 | 3.715214185 | 9.969078106 |
| 70200.00 | 1.645395077 | 3.484881251 | 9.495240415 |
| 72000.00 | 1.529792809 | 3.268828318 | 9.043924582 |
| 73800.00 | 1.422312533 | 3.066170065 | 8.614060125 |
| 75600.00 | 1.322383613 | 2.876076059 | 8.204627446 |
| 77400.00 | 1.229475504 | 2.697767352 | 7.814655406 |
| 79200.00 | 1.14309494 | 2.530513288 | 7.443219027 |
| 81000.00 | 1.062783306 | 2.373628511 | 7.089437295 |
| 82800.00 | 0.988114212 | 2.226470153 | 6.752471072 |
| 84600.00 | 0.918691223 | 2.088435204 | 6.431521103 |
| 86400.00 | 0.85414576 | 1.958958037 | 6.125826125 |

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DA#14 DRAINAGE CALCULATIONS

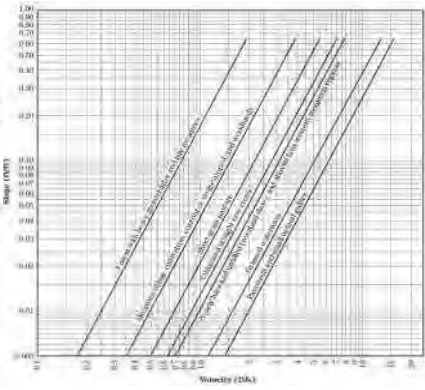
Time of Concentration:

$T_c = T_{OL} + T_1 + \dots + T_n$

Section 2.1
 1. Determine the length of the longest overland flow path (L) in feet.
 2. Determine the slope of the overland flow path (S) in feet per foot.
 3. Determine the roughness coefficient (n) for the overland flow path.
 4. Calculate the time of overland flow (T_{OL}) in minutes.
 5. Determine the time of travel through the pipe network (T₁, T₂, etc.) in minutes.
 6. Calculate the total time of concentration (T_c) in minutes.

Table 2.1.1. Manning's Roughness Coefficient for Overland Flow

| Surface | n |
|---------------------------------------------------|-------|
| Asphalt (Surfaced) (asphalt, gravel, surf. seal) | 0.012 |
| Gravel (Surfaced) | 0.020 |
| Concrete (Surfaced) (asphalt, gravel, surf. seal) | 0.010 |
| Grass (Grass) | 0.030 |
| Grass (Grass) (Grass) | 0.040 |
| Grass (Grass) (Grass) | 0.050 |
| Grass (Grass) (Grass) | 0.060 |
| Grass (Grass) (Grass) | 0.070 |
| Grass (Grass) (Grass) | 0.080 |
| Grass (Grass) (Grass) | 0.090 |
| Grass (Grass) (Grass) | 0.100 |
| Grass (Grass) (Grass) | 0.110 |
| Grass (Grass) (Grass) | 0.120 |
| Grass (Grass) (Grass) | 0.130 |
| Grass (Grass) (Grass) | 0.140 |
| Grass (Grass) (Grass) | 0.150 |
| Grass (Grass) (Grass) | 0.160 |
| Grass (Grass) (Grass) | 0.170 |
| Grass (Grass) (Grass) | 0.180 |
| Grass (Grass) (Grass) | 0.190 |
| Grass (Grass) (Grass) | 0.200 |
| Grass (Grass) (Grass) | 0.210 |
| Grass (Grass) (Grass) | 0.220 |
| Grass (Grass) (Grass) | 0.230 |
| Grass (Grass) (Grass) | 0.240 |
| Grass (Grass) (Grass) | 0.250 |
| Grass (Grass) (Grass) | 0.260 |
| Grass (Grass) (Grass) | 0.270 |
| Grass (Grass) (Grass) | 0.280 |
| Grass (Grass) (Grass) | 0.290 |
| Grass (Grass) (Grass) | 0.300 |
| Grass (Grass) (Grass) | 0.310 |
| Grass (Grass) (Grass) | 0.320 |
| Grass (Grass) (Grass) | 0.330 |
| Grass (Grass) (Grass) | 0.340 |
| Grass (Grass) (Grass) | 0.350 |
| Grass (Grass) (Grass) | 0.360 |
| Grass (Grass) (Grass) | 0.370 |
| Grass (Grass) (Grass) | 0.380 |
| Grass (Grass) (Grass) | 0.390 |
| Grass (Grass) (Grass) | 0.400 |
| Grass (Grass) (Grass) | 0.410 |
| Grass (Grass) (Grass) | 0.420 |
| Grass (Grass) (Grass) | 0.430 |
| Grass (Grass) (Grass) | 0.440 |
| Grass (Grass) (Grass) | 0.450 |
| Grass (Grass) (Grass) | 0.460 |
| Grass (Grass) (Grass) | 0.470 |
| Grass (Grass) (Grass) | 0.480 |
| Grass (Grass) (Grass) | 0.490 |
| Grass (Grass) (Grass) | 0.500 |
| Grass (Grass) (Grass) | 0.510 |
| Grass (Grass) (Grass) | 0.520 |
| Grass (Grass) (Grass) | 0.530 |
| Grass (Grass) (Grass) | 0.540 |
| Grass (Grass) (Grass) | 0.550 |
| Grass (Grass) (Grass) | 0.560 |
| Grass (Grass) (Grass) | 0.570 |
| Grass (Grass) (Grass) | 0.580 |
| Grass (Grass) (Grass) | 0.590 |
| Grass (Grass) (Grass) | 0.600 |
| Grass (Grass) (Grass) | 0.610 |
| Grass (Grass) (Grass) | 0.620 |
| Grass (Grass) (Grass) | 0.630 |
| Grass (Grass) (Grass) | 0.640 |
| Grass (Grass) (Grass) | 0.650 |
| Grass (Grass) (Grass) | 0.660 |
| Grass (Grass) (Grass) | 0.670 |
| Grass (Grass) (Grass) | 0.680 |
| Grass (Grass) (Grass) | 0.690 |
| Grass (Grass) (Grass) | 0.700 |
| Grass (Grass) (Grass) | 0.710 |
| Grass (Grass) (Grass) | 0.720 |
| Grass (Grass) (Grass) | 0.730 |
| Grass (Grass) (Grass) | 0.740 |
| Grass (Grass) (Grass) | 0.750 |
| Grass (Grass) (Grass) | 0.760 |
| Grass (Grass) (Grass) | 0.770 |
| Grass (Grass) (Grass) | 0.780 |
| Grass (Grass) (Grass) | 0.790 |
| Grass (Grass) (Grass) | 0.800 |
| Grass (Grass) (Grass) | 0.810 |
| Grass (Grass) (Grass) | 0.820 |
| Grass (Grass) (Grass) | 0.830 |
| Grass (Grass) (Grass) | 0.840 |
| Grass (Grass) (Grass) | 0.850 |
| Grass (Grass) (Grass) | 0.860 |
| Grass (Grass) (Grass) | 0.870 |
| Grass (Grass) (Grass) | 0.880 |
| Grass (Grass) (Grass) | 0.890 |
| Grass (Grass) (Grass) | 0.900 |
| Grass (Grass) (Grass) | 0.910 |
| Grass (Grass) (Grass) | 0.920 |
| Grass (Grass) (Grass) | 0.930 |
| Grass (Grass) (Grass) | 0.940 |
| Grass (Grass) (Grass) | 0.950 |
| Grass (Grass) (Grass) | 0.960 |
| Grass (Grass) (Grass) | 0.970 |
| Grass (Grass) (Grass) | 0.980 |
| Grass (Grass) (Grass) | 0.990 |
| Grass (Grass) (Grass) | 1.000 |



| $T_{OL} = Tt = T_0l$; multiply by 60 to convert hrs. to min. (L = max 300') | T = |
|------------------------------------------------------------------------------|------------------------------|
| n = 0.8 | D = 2180.62 (ft) |
| L = 100 (ft) | S = 0.0065 (ft/ft) |
| P ₂ = 4.89 (in) | V = 1.625 (ft/s) |
| S = 0.0065 (ft/ft) | |
| T _{OL} = 47.41 (min) | T ₁ = 22.37 (min) |

T_c = 69.78 (min)

Intensity:

SEE FIG. 2.1-2.1a

| | |
|--------------|-------------|
| I (100-YR) = | 4.3 (in/hr) |
| I (10-YR) = | 3.8 (in/hr) |
| I (2-YR) = | 1.9 (in/hr) |

Peak Flow Rate:

Q = CIA

C = 0.18 Mixed use area. MUD facilities; and MOSTLY woodlands; basin slope <1%

| i (100-YR) | i (10-YR) | i (2-YR) |
|----------------|-----------|----------|
| 4.3 | 3.8 | 1.9 |
| A = 46.99 (Ac) | | |

| | |
|---------------------|--------------------|
| Q (100-YR) = | 36.37 (cfs) |
| Q (10-YR) = | 32.14 (cfs) |
| Q (2-YR) = | 16.07 (cfs) |

DA#14 EXISTING CALCULATIONS

Volume (100-yr) = 1.38*area*43560 = 2824700.47 cft
 Volume (10-yr) = 0.70*area*43560 = 1432819.08 cft
 Volume (2-yr) = 0.41*area*43560 = 839222.604 cft
 A = 46.99 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

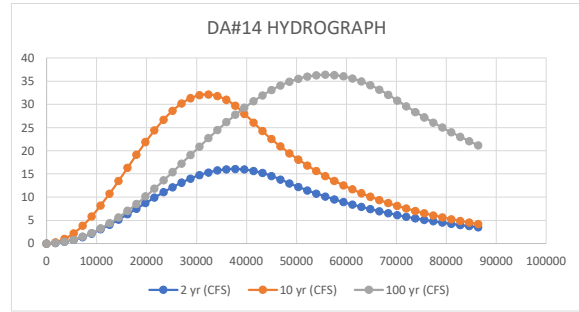
$q_i = \left(\frac{Q_p}{2}\right) \left[1 - \cos\left(\frac{\pi t_i}{T_p}\right)\right]$ $t_i \leq 1.25 T_p$
 $q_i = 4.34 Q_p e^{-1.3t_i/T_p}$ $t_i > 1.25 T_p$

| DA#14 Existing Conditions | | | |
|---------------------------|-----------|-----------|------------|
| | 2 - Year | 10 - Year | 100 - Year |
| Qp= | 16.07 | 32.14 | 36.37 |
| TP= | 37569.103 | 32071.185 | 55874.184 |
| 1.25*TP= | 46961.378 | 40088.981 | 69842.730 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) |
|----------|-------------|-------------|--------------|
| 0 | 0 | 0 | 0 |
| 1800.00 | 0.090852016 | 0.249167177 | 0.093054642 |
| 3600.00 | 0.361353605 | 0.988942257 | 0.371266233 |
| 5400.00 | 0.805387847 | 2.196385473 | 0.831787516 |
| 7200.00 | 1.412913683 | 3.834055088 | 1.469905447 |
| 9000.00 | 2.17019298 | 5.851168429 | 2.279089434 |
| 10800.00 | 3.060101189 | 8.185176609 | 3.251058171 |
| 12600.00 | 4.062514594 | 10.76370412 | 4.375864386 |
| 14400.00 | 5.154765368 | 13.50679311 | 5.641996648 |
| 16200.00 | 6.312154169 | 16.32938285 | 7.036497174 |
| 18000.00 | 7.508508673 | 19.14394735 | 8.545094441 |
| 19800.00 | 8.716775417 | 21.86320946 | 10.15234924 |
| 21600.00 | 9.909631559 | 24.4028473 | 11.8418127 |
| 23400.00 | 11.06010274 | 26.68410896 | 13.5961946 |
| 25200.00 | 12.14217308 | 28.63625456 | 15.39754033 |
| 27000.00 | 13.13137343 | 30.19874979 | 17.22741467 |
| 28800.00 | 14.00533477 | 31.32314308 | 19.0670904 |
| 30600.00 | 14.74429399 | 31.97456798 | 20.89774002 |
| 32400.00 | 15.33154081 | 32.13282441 | 22.7006284 |
| 34200.00 | 15.75379568 | 31.79300495 | 24.4573045 |
| 36000.00 | 16.00151004 | 30.96564712 | 26.14979025 |
| 37800.00 | 16.06908227 | 29.67640655 | 27.76076449 |
| 39600.00 | 15.95498433 | 27.96526142 | 29.2737403 |
| 41400.00 | 15.66179635 | 26.04614799 | 30.67323364 |
| 43200.00 | 15.19614827 | 24.21342413 | 31.9449219 |
| 45000.00 | 14.5685699 | 22.50965894 | 33.07579043 |
| 46800.00 | 13.79325283 | 20.92577833 | 34.05426577 |
| 48600.00 | 12.97680523 | 19.45334666 | 34.87033404 |
| 50400.00 | 12.19319887 | 18.08452189 | 35.51564349 |
| 52200.00 | 11.45691069 | 16.81201377 | 35.98358993 |
| 54000.00 | 10.76508338 | 15.62904503 | 36.26938432 |
| 55800.00 | 10.11503218 | 14.52931529 | 36.37010181 |
| 57600.00 | 9.504234415 | 13.50696746 | 36.28471163 |
| 59400.00 | 8.930319767 | 12.55655662 | 36.01408768 |
| 61200.00 | 8.391061043 | 11.67302094 | 35.56099956 |
| 63000.00 | 7.88436554 | 10.85165481 | 34.93008425 |
| 64800.00 | 7.408266921 | 10.08808368 | 34.12779863 |
| 66600.00 | 6.960917591 | 9.378240836 | 33.1623534 |
| 68400.00 | 6.540581518 | 8.718345725 | 32.04362907 |
| 70200.00 | 6.145627504 | 8.104883794 | 30.82460773 |
| 72000.00 | 5.774522847 | 7.534587799 | 29.56033761 |
| 73800.00 | 5.425827403 | 7.004420389 | 28.34792149 |
| 75600.00 | 5.098187986 | 6.511557937 | 27.18523256 |
| 77400.00 | 4.790333125 | 6.053375499 | 26.07023128 |
| 79200.00 | 4.501068127 | 5.627432833 | 25.00096173 |
| 81000.00 | 4.22927044 | 5.231461405 | 23.97554823 |
| 82800.00 | 3.973885298 | 4.863352304 | 22.99219203 |
| 84600.00 | 3.733921627 | 4.521145011 | 22.04916815 |
| 86400.00 | 3.508448199 | 4.203016959 | 21.14482235 |

ti (hrs)

- 0
- 0.5
- 1
- 1.5
- 2
- 2.5
- 3
- 3.5
- 4
- 4.5
- 5
- 5.5
- 6
- 6.5
- 7
- 7.5
- 8
- 8.5
- 9
- 9.5
- 10
- 10.5
- 11
- 11.5
- 12
- 12.5
- 13
- 13.5
- 14
- 14.5
- 15
- 15.5
- 16
- 16.5
- 17
- 17.5
- 18
- 18.5
- 19
- 19.5
- 20
- 20.5
- 21
- 21.5
- 22
- 22.5
- 23
- 23.5
- 24



DA#14A DRAINAGE CALCULATIONS

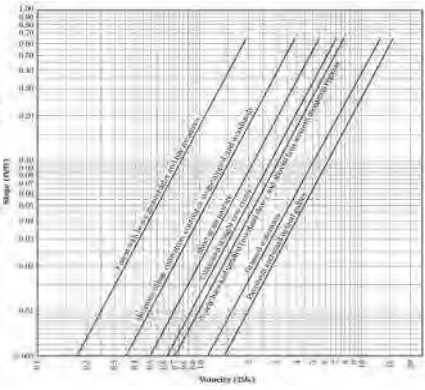
Time of Concentration:

$T_c = T_{OL} + T_1 + \dots + T_n$

Section 2.1
 1. Determine the length of the longest flow path (L) in feet.
 2. Determine the slope of the longest flow path (S) in feet per foot.
 3. Determine the runoff coefficient (C) for the area of the basin.
 4. Determine the time of travel (T) in minutes for the longest flow path.
 5. Determine the time of concentration (T_c) in minutes for the basin.

Table 2.1.1 (continued) Longitudinal Conditions for Ground Sheet Flow

| Surface | n |
|-------------------------|-------|
| Asphalt | 0.012 |
| Concrete | 0.015 |
| Gravel | 0.020 |
| Grass | 0.030 |
| Grass (dry) | 0.040 |
| Grass (flooded) | 0.050 |
| Grass (mowed) | 0.060 |
| Grass (rough) | 0.070 |
| Grass (very rough) | 0.080 |
| Grass (extremely rough) | 0.090 |
| Grass (very rough) | 0.100 |
| Grass (rough) | 0.110 |
| Grass (extremely rough) | 0.120 |
| Grass (very rough) | 0.130 |
| Grass (rough) | 0.140 |
| Grass (extremely rough) | 0.150 |
| Grass (very rough) | 0.160 |
| Grass (rough) | 0.170 |
| Grass (extremely rough) | 0.180 |
| Grass (very rough) | 0.190 |
| Grass (rough) | 0.200 |
| Grass (extremely rough) | 0.210 |
| Grass (very rough) | 0.220 |
| Grass (rough) | 0.230 |
| Grass (extremely rough) | 0.240 |
| Grass (very rough) | 0.250 |
| Grass (rough) | 0.260 |
| Grass (extremely rough) | 0.270 |
| Grass (very rough) | 0.280 |
| Grass (rough) | 0.290 |
| Grass (extremely rough) | 0.300 |
| Grass (very rough) | 0.310 |
| Grass (rough) | 0.320 |
| Grass (extremely rough) | 0.330 |
| Grass (very rough) | 0.340 |
| Grass (rough) | 0.350 |
| Grass (extremely rough) | 0.360 |
| Grass (very rough) | 0.370 |
| Grass (rough) | 0.380 |
| Grass (extremely rough) | 0.390 |
| Grass (very rough) | 0.400 |
| Grass (rough) | 0.410 |
| Grass (extremely rough) | 0.420 |
| Grass (very rough) | 0.430 |
| Grass (rough) | 0.440 |
| Grass (extremely rough) | 0.450 |
| Grass (very rough) | 0.460 |
| Grass (rough) | 0.470 |
| Grass (extremely rough) | 0.480 |
| Grass (very rough) | 0.490 |
| Grass (rough) | 0.500 |
| Grass (extremely rough) | 0.510 |
| Grass (very rough) | 0.520 |
| Grass (rough) | 0.530 |
| Grass (extremely rough) | 0.540 |
| Grass (very rough) | 0.550 |
| Grass (rough) | 0.560 |
| Grass (extremely rough) | 0.570 |
| Grass (very rough) | 0.580 |
| Grass (rough) | 0.590 |
| Grass (extremely rough) | 0.600 |
| Grass (very rough) | 0.610 |
| Grass (rough) | 0.620 |
| Grass (extremely rough) | 0.630 |
| Grass (very rough) | 0.640 |
| Grass (rough) | 0.650 |
| Grass (extremely rough) | 0.660 |
| Grass (very rough) | 0.670 |
| Grass (rough) | 0.680 |
| Grass (extremely rough) | 0.690 |
| Grass (very rough) | 0.700 |
| Grass (rough) | 0.710 |
| Grass (extremely rough) | 0.720 |
| Grass (very rough) | 0.730 |
| Grass (rough) | 0.740 |
| Grass (extremely rough) | 0.750 |
| Grass (very rough) | 0.760 |
| Grass (rough) | 0.770 |
| Grass (extremely rough) | 0.780 |
| Grass (very rough) | 0.790 |
| Grass (rough) | 0.800 |
| Grass (extremely rough) | 0.810 |
| Grass (very rough) | 0.820 |
| Grass (rough) | 0.830 |
| Grass (extremely rough) | 0.840 |
| Grass (very rough) | 0.850 |
| Grass (rough) | 0.860 |
| Grass (extremely rough) | 0.870 |
| Grass (very rough) | 0.880 |
| Grass (rough) | 0.890 |
| Grass (extremely rough) | 0.900 |
| Grass (very rough) | 0.910 |
| Grass (rough) | 0.920 |
| Grass (extremely rough) | 0.930 |
| Grass (very rough) | 0.940 |
| Grass (rough) | 0.950 |
| Grass (extremely rough) | 0.960 |
| Grass (very rough) | 0.970 |
| Grass (rough) | 0.980 |
| Grass (extremely rough) | 0.990 |
| Grass (very rough) | 1.000 |



| | | |
|------------|----------------------------------------------------------------------|----------------------|
| $T_{OL} =$ | $T_t = T_{OL}$; multiply by 60 to convert hrs. to min. (L=max 300') | $T =$ |
| $n =$ | 0.15 | $D =$ 289.47 (ft) |
| $L =$ | 100 (ft) | $S =$ 0.0058 (ft/ft) |
| $P_2 =$ | 4.89 (in) | $V =$ 0.55 (ft/s) |
| $S =$ | 0.0058 (ft/ft) | |
| $T_{OL} =$ | 13.00 (min) | $T_1 =$ 8.77 (min) |

$T_c = 21.78$ (min)

Intensity:

SEE FIG. 2.1-2.1a

| | |
|---------------|-------------|
| I (100-YR)= | 7.9 (in/hr) |
| I (10-YR)= | 5.4 (in/hr) |
| I (2-YR)= | 3.7 (in/hr) |

Peak Flow Rate:

$Q = CIA$

$C =$ 0.15 Mixed use area; lots 1/4-1/2 acre; MOSTLY golf course; basin slope <1%

| | | |
|--------------|-------------|------------|
| i (100-YR) | i (10-YR) | i (2-YR) |
| 7.9 | 5.4 | 3.7 |
| $A =$ | 7.47 (Ac) | |

| | |
|---------------|------------|
| Q (100-YR)= | 8.85 (cfs) |
| Q (10-YR)= | 6.05 (cfs) |
| Q (2-YR)= | 4.15 (cfs) |

DA#14A EXISTING CALCULATIONS

Volume (100-yr) = 1.38*area*43560 = 449042.62 cft
 Volume (10-yr) = 0.70*area*43560 = 227775.24 cft
 Volume (2-yr) = 0.41*area*43560 = 133411.212 cft
 A = 7.47 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

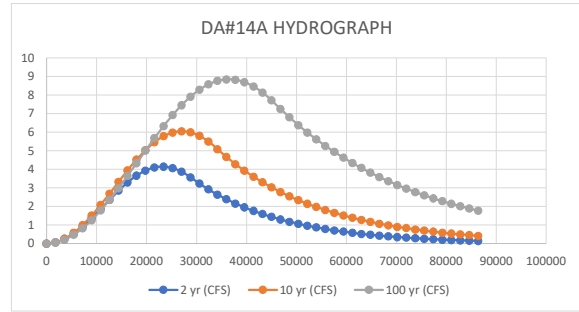
$q_i = \left(\frac{Q_p}{2}\right) \left[1 - \cos\left(\frac{\pi t_i}{T_p}\right)\right]$ $t_i \leq 1.25 T_p$
 $q_i = 1.34 Q_p e^{-1.3t_i/T_p}$ $t_i > 1.25 T_p$

| DA#14A Existing Conditions | | | |
|----------------------------|-----------|-----------|------------|
| | 2 - Year | 10 - Year | 100 - Year |
| Qp= | 4.15 | 6.05 | 8.85 |
| TP= | 23150.690 | 27082.334 | 36495.037 |
| 1.25*TP= | 28938.363 | 33852.918 | 45618.796 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) |
|----------|-------------|-------------|--------------|
| 0 | 0 | 0 | 0 |
| 1800.00 | 0.061533278 | 0.065711252 | 0.053025773 |
| 3600.00 | 0.24247997 | 0.259990483 | 0.210832532 |
| 5400.00 | 0.532097534 | 0.574398119 | 0.469639043 |
| 7200.00 | 0.913191793 | 0.995276158 | 0.823243998 |
| 9000.00 | 1.363137733 | 1.504341477 | 1.263174608 |
| 10800.00 | 1.855222716 | 2.079480059 | 1.778889621 |
| 12600.00 | 2.360232369 | 2.695707639 | 2.3580319 |
| 14400.00 | 2.848184998 | 3.326255024 | 2.986724519 |
| 16200.00 | 3.290111565 | 3.943730965 | 3.649903265 |
| 18000.00 | 3.659775527 | 4.521312043 | 4.331677599 |
| 19800.00 | 3.935230471 | 5.033907887 | 5.01571141 |
| 21600.00 | 4.100123035 | 5.459251113 | 5.685614445 |
| 23400.00 | 4.144663787 | 5.77886463 | 6.325335043 |
| 25200.00 | 4.066208408 | 5.978864288 | 6.91954475 |
| 27000.00 | 3.869414678 | 6.050562016 | 7.454005604 |
| 28800.00 | 3.565965957 | 5.990843234 | 7.915911298 |
| 30600.00 | 3.227393628 | 5.802302152 | 8.29419403 |
| 32400.00 | 2.917123375 | 5.493129076 | 8.579789702 |
| 34200.00 | 2.636681412 | 5.085471502 | 8.765855108 |
| 36000.00 | 2.383200151 | 4.664518257 | 8.847931902 |
| 37800.00 | 2.154087685 | 4.278409694 | 8.824053429 |
| 39600.00 | 1.947001284 | 3.924261521 | 8.694791845 |
| 41400.00 | 1.759823441 | 3.599428196 | 8.463244408 |
| 43200.00 | 1.590640215 | 3.301483162 | 8.134959267 |
| 45000.00 | 1.437721669 | 3.028200725 | 7.717802517 |
| 46800.00 | 1.299504174 | 2.77753942 | 7.25315194 |
| 48600.00 | 1.174574421 | 2.54762677 | 6.802687925 |
| 50400.00 | 1.061654974 | 2.336745291 | 6.380200413 |
| 52200.00 | 0.959591206 | 2.143319664 | 5.983951897 |
| 54000.00 | 0.867339488 | 1.965904971 | 5.612312778 |
| 55800.00 | 0.783956525 | 1.803175895 | 5.263754665 |
| 57600.00 | 0.708589707 | 1.653916826 | 4.936844092 |
| 59400.00 | 0.640468389 | 1.517012774 | 4.630236615 |
| 61200.00 | 0.578896015 | 1.391441045 | 4.342671293 |
| 63000.00 | 0.523242992 | 1.276263599 | 4.072965493 |
| 64800.00 | 0.472940254 | 1.170620041 | 3.820010032 |
| 66600.00 | 0.427473444 | 1.073721198 | 3.582764615 |
| 68400.00 | 0.386377653 | 0.984843221 | 3.360253554 |
| 70200.00 | 0.349232667 | 0.903322176 | 3.151561758 |
| 72000.00 | 0.315658669 | 0.828549089 | 2.955830967 |
| 73800.00 | 0.285312357 | 0.759965394 | 2.772256227 |
| 75600.00 | 0.257883432 | 0.697058759 | 2.600082573 |
| 77400.00 | 0.233091427 | 0.639359263 | 2.438601931 |
| 79200.00 | 0.210682839 | 0.58643588 | 2.2871502 |
| 81000.00 | 0.190428533 | 0.537893265 | 2.145104525 |
| 82800.00 | 0.172121405 | 0.493368796 | 2.011880734 |
| 84600.00 | 0.155574259 | 0.45252987 | 1.886930935 |
| 86400.00 | 0.140617898 | 0.415071413 | 1.769741265 |

ti (hrs)

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DA#15 DRAINAGE CALCULATIONS

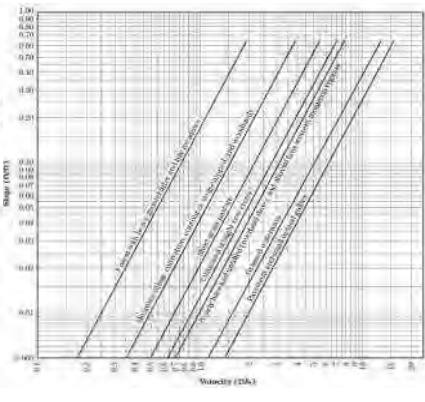
Time of Concentration:

$T_c = T_{OL} + T_1 + \dots + T_n$

Section 2.1
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Table 2.11 Manning's Roughness Coefficient for Gravel (Shell Flow)

| Surface | n |
|--------------------------|-------|
| Gravel (Shell Flow) | 0.012 |
| Gravel (Smooth) | 0.009 |
| Gravel (Rough) | 0.006 |
| Gravel (Very Rough) | 0.015 |
| Gravel (Extremely Rough) | 0.020 |
| Gravel (Smooth) | 0.010 |
| Gravel (Rough) | 0.012 |
| Gravel (Very Rough) | 0.015 |
| Gravel (Extremely Rough) | 0.020 |
| Gravel (Smooth) | 0.010 |
| Gravel (Rough) | 0.012 |
| Gravel (Very Rough) | 0.015 |
| Gravel (Extremely Rough) | 0.020 |



| | | |
|------------|----------------------------------------------------------------------|-------------------|
| $T_{OL} =$ | $T_t = T_{OL}$; multiply by 60 to convert hrs. to min. (L=max 300') | $T =$ |
| n= | 0.15 | D= 4872.04 (ft) |
| L= | 100 (ft) | S= 0.0076 (ft/ft) |
| $P_2 =$ | 4.89 (in) | V= 1.75 (ft/s) |
| $S =$ | 0.0076 (ft/ft) | |
| $T_{OL} =$ | 11.67 (min) | $T_1 =$ |
| | | 46.40 (min) |

$T_c = 58.07$ (min)

Intensity:

SEE FIG. 2.1-2.1a

| | |
|-------------|-------------|
| I (100-YR)= | 4.7 (in/hr) |
| I (10-YR)= | 3.2 (in/hr) |
| I (2-YR)= | 2.2 (in/hr) |

Peak Flow Rate:

$Q = CIA$

C= 0.18 Mixed use area. Lots 1/4-1/2 acre; golf course; and MOSTLY woodlands; basin slope <1%

| | | |
|------------|------------|----------|
| i (100-YR) | i (10-YR) | i (2-YR) |
| 4.7 | 3.2 | 2.2 |
| A= | 75.07 (Ac) | |

| | |
|-------------|-------------|
| Q (100-YR)= | 63.51 (cfs) |
| Q (10-YR)= | 43.24 (cfs) |
| Q (2-YR)= | 29.73 (cfs) |

DA#15 EXISTING CALCULATIONS

Volume (100-yr) = 1.38*area*43560 = 4512667.90 cft
 Volume (10-yr) = 0.70*area*43560 = 2289034.44 cft
 Volume (2-yr) = 0.41*area*43560 = 1340720.172 cft
 A = 75.07 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

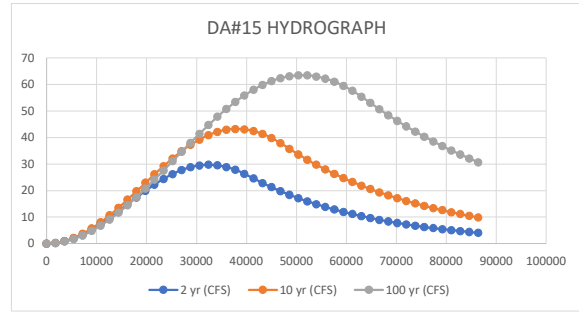
$q_i = \left(\frac{Q_p}{2}\right) \left[1 - \cos\left(\frac{\pi t_i}{T_p}\right)\right]$ $t_i \leq 1.25 T_p$
 $q_i = 1.34 Q_p e^{-1.3t_i/T_p}$ $t_i > 1.25 T_p$

| DA#15 Existing Conditions | | | |
|---------------------------|-----------|-----------|------------|
| | 2 - Year | 10 - Year | 100 - Year |
| Qp= | 29.73 | 43.24 | 63.51 |
| TP= | 32446.043 | 38084.532 | 51118.935 |
| 1.25*TP= | 40557.554 | 47605.665 | 63898.668 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) |
|----------|-------------|-------------|--------------|
| 0 | 0 | 0 | 0 |
| 1800.00 | 0.225176614 | 0.23789119 | 0.194095306 |
| 3600.00 | 0.893883933 | 0.946329625 | 0.774008465 |
| 5400.00 | 1.985861103 | 2.109725109 | 1.732650214 |
| 7200.00 | 3.468022813 | 3.702475471 | 3.058301443 |
| 9000.00 | 5.295461729 | 5.689529972 | 4.734756462 |
| 10800.00 | 7.412809124 | 8.02716065 | 6.741521111 |
| 12600.00 | 9.755912468 | 10.66392462 | 9.054063291 |
| 14400.00 | 12.25377915 | 13.54179613 | 11.64411287 |
| 16200.00 | 14.83072747 | 16.59744354 | 14.48000725 |
| 18000.00 | 17.40867966 | 19.76362296 | 17.5270785 |
| 19800.00 | 19.90952753 | 22.97065813 | 20.74807705 |
| 21600.00 | 22.25749905 | 26.14797366 | 24.10362719 |
| 23400.00 | 24.38145412 | 29.22564821 | 27.5527083 |
| 25200.00 | 26.21704 | 32.13595317 | 31.0531564 |
| 27000.00 | 27.70864113 | 34.81484315 | 34.56217956 |
| 28800.00 | 28.81106416 | 37.20336535 | 38.03688102 |
| 30600.00 | 29.4909073 | 39.24895694 | 41.4347836 |
| 32400.00 | 29.72757229 | 40.90660178 | 44.71434896 |
| 34200.00 | 29.51388853 | 42.13982103 | 47.83548537 |
| 36000.00 | 28.85633032 | 42.92147594 | 50.7600379 |
| 37800.00 | 27.77482072 | 43.2343651 | 53.45225475 |
| 39600.00 | 26.30212788 | 43.07160291 | 55.87922439 |
| 41400.00 | 24.56199702 | 42.43677121 | 58.01127783 |
| 43200.00 | 22.85296065 | 41.34384037 | 59.82235135 |
| 45000.00 | 21.26283991 | 39.81686188 | 61.29030514 |
| 46800.00 | 19.78336059 | 37.88943907 | 62.39719388 |
| 48600.00 | 18.40682419 | 35.7198493 | 63.12948619 |
| 50400.00 | 17.12606791 | 33.59120478 | 63.47823003 |
| 52200.00 | 15.93442731 | 31.58941207 | 63.4391621 |
| 54000.00 | 14.82570167 | 29.70691172 | 63.01276 |
| 55800.00 | 13.79412174 | 27.93659477 | 62.20423636 |
| 57600.00 | 12.83431966 | 26.27177589 | 61.02347514 |
| 59400.00 | 11.94130111 | 24.70616818 | 59.4849108 |
| 61200.00 | 11.11041924 | 23.23385935 | 57.60735183 |
| 63000.00 | 10.33735056 | 21.84928947 | 55.41375082 |
| 64800.00 | 9.618072403 | 20.54722994 | 53.04484952 |
| 66600.00 | 8.948841985 | 19.32276373 | 50.67142647 |
| 68400.00 | 8.326176963 | 18.17126685 | 48.40419915 |
| 70200.00 | 7.746837293 | 17.08839085 | 46.23841599 |
| 72000.00 | 7.207808376 | 16.07004642 | 44.16953798 |
| 73800.00 | 6.706285367 | 15.11238795 | 42.19322924 |
| 75600.00 | 6.239658586 | 14.211799 | 40.30534788 |
| 77400.00 | 5.805499937 | 13.36487862 | 38.50193732 |
| 79200.00 | 5.401550269 | 12.56842858 | 36.77921803 |
| 81000.00 | 5.025707627 | 11.81944119 | 35.13357958 |
| 82800.00 | 4.676016309 | 11.11508803 | 33.56157309 |
| 84600.00 | 4.350656693 | 10.45270922 | 32.05990399 |
| 86400.00 | 4.047935765 | 9.829803399 | 30.62542513 |

ti (hrs)

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DA#15A DRAINAGE CALCULATIONS

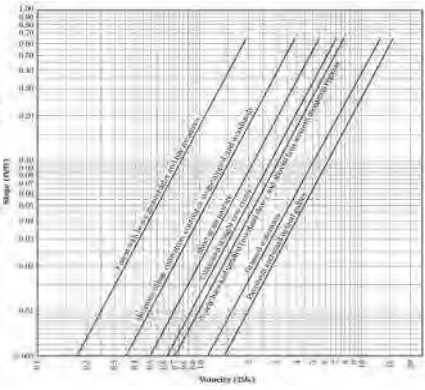
Time of Concentration:

$$T_c = T_{OL} + T_1 + \dots + T_n$$

Section 2.2
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Table 2.1. Manning's Roughness Coefficient for Concrete Sewer Flow

| Surface | n |
|--------------------------------------------------------|-------|
| Smooth Surface (asphalt, concrete, gravel, surf. etc.) | 0.012 |
| Polished pipe material | 0.009 |
| Cast-in-place concrete | 0.010 |
| Cast-in-place concrete (interior) | 0.011 |
| Cast-in-place concrete (exterior) | 0.012 |
| Cast-in-place concrete (interior) with 10% sand | 0.013 |
| Cast-in-place concrete (exterior) with 10% sand | 0.014 |
| Cast-in-place concrete (interior) with 20% sand | 0.015 |
| Cast-in-place concrete (exterior) with 20% sand | 0.016 |
| Cast-in-place concrete (interior) with 30% sand | 0.017 |
| Cast-in-place concrete (exterior) with 30% sand | 0.018 |
| Cast-in-place concrete (interior) with 40% sand | 0.019 |
| Cast-in-place concrete (exterior) with 40% sand | 0.020 |
| Cast-in-place concrete (interior) with 50% sand | 0.021 |
| Cast-in-place concrete (exterior) with 50% sand | 0.022 |
| Cast-in-place concrete (interior) with 60% sand | 0.023 |
| Cast-in-place concrete (exterior) with 60% sand | 0.024 |
| Cast-in-place concrete (interior) with 70% sand | 0.025 |
| Cast-in-place concrete (exterior) with 70% sand | 0.026 |
| Cast-in-place concrete (interior) with 80% sand | 0.027 |
| Cast-in-place concrete (exterior) with 80% sand | 0.028 |
| Cast-in-place concrete (interior) with 90% sand | 0.029 |
| Cast-in-place concrete (exterior) with 90% sand | 0.030 |



| $T_{OL} = Tt = T_0t$; multiply by 60 to convert hrs. to min. (L= max 300') | T = |
|-----------------------------------------------------------------------------|----------------------|
| n = 0.15 | D = 4161.67 (ft) |
| L = 100 (ft) | S = 0.0039 (ft/ft) |
| $P_2 = 4.89$ (in) | V = 0.5 (ft/s) |
| S = 0.0039 (ft/ft) | |
| $T_{OL} = 15.24$ (min) | $T_1 = 138.72$ (min) |

$T_c = 153.96$ (min)

Intensity:

SEE FIG. 2.1-2.1a

| | |
|--------------|--------------|
| I (100-YR) = | 3 (in/hr) |
| I (10-YR) = | 1.8 (in/hr) |
| I (2-YR) = | 1.15 (in/hr) |

Peak Flow Rate:

$$Q = CIA$$

C = 0.35 Mixed use area; lots 1/4-1/2 acre; MOSTLY golf course; basin slope <1%

| i (100-YR) | i (10-YR) | i (2-YR) |
|------------|------------|----------|
| 3 | 1.8 | 1.15 |
| A = | 57.45 (Ac) | |

| | |
|---------------------|--------------------|
| Q (100-YR) = | 60.32 (cfs) |
| Q (10-YR) = | 36.19 (cfs) |
| Q (2-YR) = | 23.12 (cfs) |

DA#15A EXISTING CALCULATIONS

Volume (100-yr) = 1.38*area*43560 = 3453480.36 cft
 Volume (10-yr) = 0.70*area*43560 = 1751765.4 cft
 Volume (2-yr) = 0.41*area*43560 = 1026034.02 cft
 A = 57.45 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

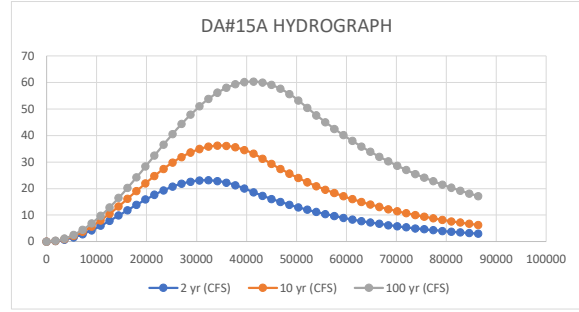
$q_i = \left(\frac{Q_p}{2}\right) \left[1 - \cos\left(\frac{\pi t_i}{T_p}\right)\right]$ $t_i \leq 1.25 T_p$
 $q_i = 1.34 Q_p e^{-1.3t_i/T_p}$ $t_i > 1.25 T_p$

| DA#15A Existing Conditions | | | |
|----------------------------|-----------|-----------|------------|
| | 2 - Year | 10 - Year | 100 - Year |
| Qp= | 23.12 | 36.19 | 60.32 |
| TP= | 31922.070 | 34820.144 | 41187.256 |
| 1.25*TP= | 39902.587 | 43525.180 | 51484.070 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) |
|----------|-------------|-------------|--------------|
| 0 | 0 | 0 | 0 |
| 1800.00 | 0.180935004 | 0.238121983 | 0.283828536 |
| 3600.00 | 0.71807698 | 0.946221383 | 1.129972279 |
| 5400.00 | 1.594614068 | 2.105663471 | 2.522506178 |
| 7200.00 | 2.783111774 | 3.685935733 | 4.435221714 |
| 9000.00 | 4.246371633 | 5.645450861 | 6.832120162 |
| 10800.00 | 5.938595476 | 7.932641184 | 9.668090118 |
| 12600.00 | 7.80681885 | 10.48731575 | 12.88975653 |
| 14400.00 | 9.792568743 | 13.24224435 | 16.43648524 |
| 16200.00 | 11.83369371 | 16.12492677 | 20.24152419 |
| 18000.00 | 13.86630915 | 19.05950077 | 24.23325973 |
| 19800.00 | 15.82679677 | 21.9687385 | 28.33656444 |
| 21600.00 | 17.65379582 | 24.77607886 | 32.47421109 |
| 23400.00 | 19.29012355 | 27.40764235 | 36.56832609 |
| 25200.00 | 20.68456498 | 29.7941753 | 40.54185518 |
| 27000.00 | 21.79347588 | 31.87287242 | 44.32001358 |
| 28800.00 | 22.58214874 | 33.58902957 | 47.83169357 |
| 30600.00 | 23.02589912 | 34.89748342 | 51.01080271 |
| 32400.00 | 23.11083818 | 35.76379999 | 53.79750782 |
| 34200.00 | 22.83430745 | 36.16518081 | 56.13936105 |
| 36000.00 | 22.20496198 | 36.09106293 | 57.99228699 |
| 37800.00 | 21.24249949 | 35.54339687 | 59.32141218 |
| 39600.00 | 19.97704382 | 34.53659531 | 60.10172153 |
| 41400.00 | 18.592314 | 33.0971538 | 60.31852901 |
| 43200.00 | 17.2781855 | 31.26295347 | 59.96775416 |
| 45000.00 | 16.05694128 | 29.27377047 | 59.05599882 |
| 46800.00 | 14.92201616 | 27.37114702 | 57.60042289 |
| 48600.00 | 13.867309 | 25.59218293 | 55.62842141 |
| 50400.00 | 12.88714989 | 23.92884108 | 53.17710889 |
| 52200.00 | 11.97626967 | 22.3736067 | 50.39956273 |
| 54000.00 | 11.12977164 | 20.91945344 | 47.31599855 |
| 55800.00 | 10.34310516 | 19.55981161 | 44.08617042 |
| 57600.00 | 9.612041278 | 18.28853853 | 40.75015875 |
| 59400.00 | 8.932649924 | 17.09989075 | 37.3651284 |
| 61200.00 | 8.301278819 | 15.9884981 | 33.93651284 |
| 63000.00 | 7.714533829 | 14.94933947 | 30.54128199 |
| 64800.00 | 7.169260725 | 13.97772005 | 27.2617706 |
| 66600.00 | 6.66252822 | 13.06925019 | 24.199158748 |
| 68400.00 | 6.191612216 | 12.21982555 | 21.42469443 |
| 70200.00 | 5.753981157 | 11.42560853 | 18.99538676 |
| 72000.00 | 5.347282419 | 10.68301096 | 16.87827483 |
| 73800.00 | 4.969329668 | 9.988677884 | 15.04826667 |
| 75600.00 | 4.6180911 | 9.339472383 | 13.570855156 |
| 77400.00 | 4.291678523 | 8.732461433 | 12.4058445 |
| 79200.00 | 3.988337204 | 8.164902637 | 11.50407133 |
| 81000.00 | 3.706436436 | 7.634231835 | 10.83695534 |
| 82800.00 | 3.444460775 | 7.138051523 | 10.3640367 |
| 84600.00 | 3.201001888 | 6.674120023 | 10.0479522 |
| 86400.00 | 2.974750986 | 6.240341351 | 9.8470887 |

ti (hrs)

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DA#15B DRAINAGE CALCULATIONS

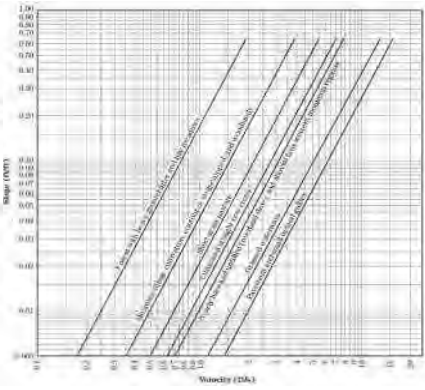
Time of Concentration:

$T_c = T_{OL} + T_1 + \dots + T_n$

Section 2.2
 1. Determine the time of concentration for each sub-area.
 2. Determine the time of concentration for the entire watershed.
 3. Determine the peak flow rate for each sub-area.
 4. Determine the peak flow rate for the entire watershed.
 5. Determine the peak flow rate for the entire watershed.
 6. Determine the peak flow rate for the entire watershed.
 7. Determine the peak flow rate for the entire watershed.
 8. Determine the peak flow rate for the entire watershed.
 9. Determine the peak flow rate for the entire watershed.
 10. Determine the peak flow rate for the entire watershed.

Table 2.11 (continued) - Longhorns Conditions for Groundwater Flow

| Surface | n |
|----------------------------------------------------------------------------------------------------------|-------|
| Asphalt Surface (asphalt, asphalt, gravel, surf. seal) | 0.012 |
| Grass (mowed) | 0.20 |
| Grass (pasture) | 0.06 |
| Grass (rough) | 0.15 |
| Grass (rough, mowed) | 0.10 |
| Grass (rough, mowed, 1/2 in. deep) | 0.07 |
| Grass (rough, mowed, 1/4 in. deep) | 0.05 |
| Grass (rough, mowed, 1/8 in. deep) | 0.03 |
| Grass (rough, mowed, 1/4 in. deep, 1/2 in. deep) | 0.04 |
| Grass (rough, mowed, 1/4 in. deep, 1/2 in. deep, 1/8 in. deep) | 0.03 |
| Grass (rough, mowed, 1/4 in. deep, 1/2 in. deep, 1/8 in. deep, 1/4 in. deep) | 0.02 |
| Grass (rough, mowed, 1/4 in. deep, 1/2 in. deep, 1/8 in. deep, 1/4 in. deep, 1/8 in. deep) | 0.01 |
| Grass (rough, mowed, 1/4 in. deep, 1/2 in. deep, 1/8 in. deep, 1/4 in. deep, 1/8 in. deep, 1/4 in. deep) | 0.005 |



| | | |
|------------|----------------------------------------------------------------------|--------------------|
| $T_{OL} =$ | $T_t = T_{OL}$; multiply by 60 to convert hrs. to min. (L=max 300') | $T =$ |
| n = | 0.15 | D = 2378.48 (ft) |
| L = | 100 (ft) | S = 0.0049 (ft/ft) |
| $P_2 =$ | 4.89 (in) | V = 0.5 (ft/s) |
| S = | 0.0049 (ft/ft) | |
| $T_{OL} =$ | 13.91 (min) | $T_1 =$ |
| | | 79.28 (min) |

$T_c = 93.19$ (min)

Intensity:

SEE FIG. 2.1-2.1a

| | |
|--------------|-------------|
| I (100-YR) = | 3.7 (in/hr) |
| I (10-YR) = | 2.3 (in/hr) |
| I (2-YR) = | 1.5 (in/hr) |

Peak Flow Rate:

$Q = CIA$

C = 0.35 Mixed use area; lots 1/4-1/2 acre; golf course; basin slope <1%

| | | |
|------------|------------|----------|
| i (100-YR) | i (10-YR) | i (2-YR) |
| 3.7 | 2.3 | 1.5 |
| A = | 23.58 (Ac) | |

| | |
|--------------|-------------|
| Q (100-YR) = | 30.54 (cfs) |
| Q (10-YR) = | 18.98 (cfs) |
| Q (2-YR) = | 12.38 (cfs) |

DA#15B EXISTING CALCULATIONS

Volume (100-yr) = 1.38*area*43560 = 1417459.82 cft
 Volume (10-yr) = 0.70*area*43560 = 719001.36 cft
 Volume (2-yr) = 0.41*area*43560 = 421129.368 cft
 A = 23.58 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

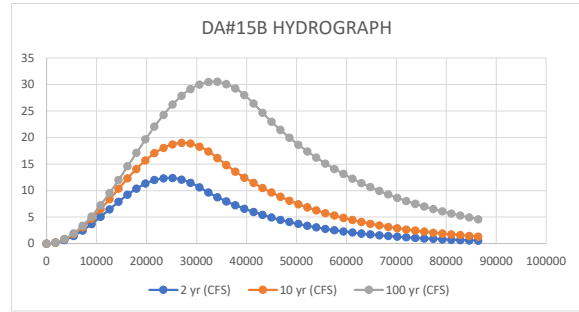
$q_i = \left(\frac{Q_p}{2}\right) \left[1 - \cos\left(\frac{\pi t_i}{T_p}\right)\right]$ $t_i \leq 1.25 T_p$
 $q_i = 4.34 Q_p e^{-1.3t_i/T_p}$ $t_i > 1.25 T_p$

| DA#15B Existing Conditions | | | |
|----------------------------|-----------|-----------|------------|
| | 2 - Year | 10 - Year | 100 - Year |
| Qp= | 12.38 | 18.98 | 30.54 |
| TP= | 24473.587 | 27250.547 | 33395.072 |
| 1.25*TP= | 30591.984 | 34063.184 | 41743.840 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) |
|----------|-------------|-------------|--------------|
| 0 | 0 | 0 | 0 |
| 1800.00 | 0.164497597 | 0.203617433 | 0.218371311 |
| 3600.00 | 0.649247075 | 0.805732977 | 0.867238731 |
| 5400.00 | 1.428483217 | 1.780511236 | 1.928041406 |
| 7200.00 | 2.460788367 | 3.086126713 | 3.370435071 |
| 9000.00 | 3.69129384 | 4.666558448 | 5.153160052 |
| 10800.00 | 5.054596287 | 6.453993744 | 7.225221493 |
| 12600.00 | 6.478233985 | 8.371737858 | 9.527348071 |
| 14400.00 | 7.886538293 | 10.33750479 | 11.99368745 |
| 16200.00 | 9.204655568 | 12.26694801 | 14.55368997 |
| 18000.00 | 10.36252575 | 14.07727953 | 17.13412677 |
| 19800.00 | 11.29860617 | 15.69082217 | 19.66118444 |
| 21600.00 | 11.96314265 | 17.03834255 | 22.06257648 |
| 23400.00 | 12.320814 | 18.06202164 | 24.26961107 |
| 25200.00 | 12.35260941 | 18.71793574 | 26.21915597 |
| 27000.00 | 12.05683891 | 18.97794106 | 27.85544445 |
| 28800.00 | 11.44922317 | 18.83088139 | 29.13167047 |
| 30600.00 | 10.57497547 | 18.28306672 | 30.01132758 |
| 32400.00 | 9.610700583 | 17.35800251 | 30.46925319 |
| 34200.00 | 8.734352713 | 16.11633546 | 30.49234832 |
| 36000.00 | 7.937914272 | 14.79018149 | 30.07995236 |
| 37800.00 | 7.214098749 | 13.57315185 | 29.24386187 |
| 39600.00 | 6.556284055 | 12.4562671 | 28.00799324 |
| 41400.00 | 5.958451928 | 11.4312867 | 26.40769849 |
| 43200.00 | 5.415132884 | 10.49064816 | 24.6579338 |
| 45000.00 | 4.921356169 | 9.627411304 | 22.98929077 |
| 46800.00 | 4.472604284 | 8.835207037 | 21.43356756 |
| 48600.00 | 4.06477166 | 8.108190345 | 19.98312271 |
| 50400.00 | 3.69412709 | 7.440997182 | 18.63083185 |
| 52200.00 | 3.357279596 | 6.828704892 | 17.37005274 |
| 54000.00 | 3.051147406 | 6.266795881 | 16.19459264 |
| 55800.00 | 2.772929756 | 5.751124297 | 15.09867785 |
| 57600.00 | 2.520081271 | 5.277885431 | 14.07692543 |
| 59400.00 | 2.290288673 | 4.84358765 | 13.12431668 |
| 61200.00 | 2.081449621 | 4.445026637 | 12.23617253 |
| 63000.00 | 1.891653474 | 4.079261743 | 11.40813057 |
| 64800.00 | 1.719163812 | 3.743594298 | 10.63612356 |
| 66600.00 | 1.562402551 | 3.43547692 | 9.916359546 |
| 68400.00 | 1.419935502 | 3.152849108 | 9.245303148 |
| 70200.00 | 1.290459254 | 2.89341275 | 8.619658242 |
| 72000.00 | 1.172789246 | 2.655324457 | 8.036351758 |
| 73800.00 | 1.06584893 | 2.436827573 | 7.492518586 |
| 75600.00 | 0.968659923 | 2.236309995 | 6.985487501 |
| 77400.00 | 0.880333058 | 2.05229227 | 6.512768045 |
| 79200.00 | 0.800060242 | 1.883416688 | 6.072038294 |
| 81000.00 | 0.72710707 | 1.728437255 | 5.661133453 |
| 82800.00 | 0.660806104 | 1.586210511 | 5.278035219 |
| 84600.00 | 0.600550765 | 1.455687082 | 4.920861874 |
| 86400.00 | 0.545789785 | 1.335903946 | 4.587859039 |

ti (hrs)

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DA#15A DRAINAGE CALCULATIONS

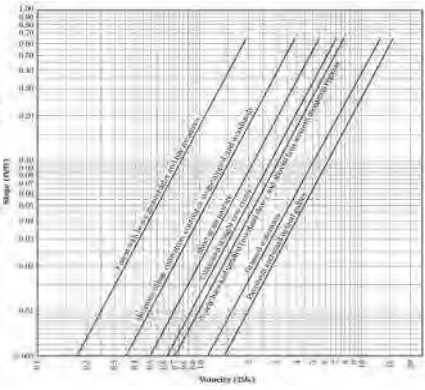
Time of Concentration:

$T_c = T_{OL} + T_1 + \dots + T_n$

Section 2.2
 1. Determine the length of the longest flow path (L) in feet.
 2. Determine the slope of the longest flow path (S) in feet per foot.
 3. Determine the runoff coefficient (C) for the area of the basin.
 4. Determine the time of travel (T_{OL}) in minutes.
 5. Determine the time of travel (T₁) in minutes.
 6. Determine the time of travel (T_n) in minutes.
 7. Determine the time of concentration (T_c) in minutes.

Table 2.11 Manning's Roughness Coefficient for Concrete Sewer Flow

| Surface | n |
|--------------------------------------------------------|-------|
| Smooth Surface (asphalt, concrete, gravel, surf, etc.) | 0.012 |
| Polished tile (asphalt) | 0.010 |
| Unfinished tile (asphalt) | 0.015 |
| Cast-in-place concrete (interior) | 0.013 |
| Cast-in-place concrete (exterior) | 0.015 |
| Concrete (open channel) | 0.015 |
| Grass (open channel) | 0.030 |
| Grass (storm drain) | 0.040 |
| Grass (storm drain) | 0.045 |
| Grass (storm drain) | 0.050 |
| Grass (storm drain) | 0.055 |
| Grass (storm drain) | 0.060 |
| Grass (storm drain) | 0.065 |
| Grass (storm drain) | 0.070 |
| Grass (storm drain) | 0.075 |
| Grass (storm drain) | 0.080 |



| $T_{OL} =$ | $T =$ |
|----------------------------------------------------------------------------|---------------------|
| $T_{OL} = Tt = T_0l$; multiply by 60 to convert hrs. to min. (L=max 300') | |
| n= 0.15 | D= 1630.41 (ft) |
| L= 100 (ft) | S= 0.0128 (ft/ft) |
| $P_2 = 4.89$ (in) | V= 0.8 (ft/s) |
| S= 0.0128 (ft/ft) | |
| $T_{OL} = 9.48$ (min) | $T_1 = 33.97$ (min) |

$T_c = 43.44$ (min)

Intensity:

SEE FIG. 2.1-2.1a

| | |
|-------------|-------------|
| I (100-YR)= | 5.5 (in/hr) |
| I (10-YR)= | 3.7 (in/hr) |
| I (2-YR)= | 2.6 (in/hr) |

Peak Flow Rate:

$Q = CIA$

C= 0.45 Single family residential district; lots 1/4-1/2 acre; basin slope 1-3.5%

| i (100-YR) | i (10-YR) | i (2-YR) |
|--------------|-----------|----------|
| 5.5 | 3.7 | 2.6 |
| A= 28.7 (Ac) | | |

| | |
|-------------|-------------|
| Q (100-YR)= | 71.03 (cfs) |
| Q (10-YR)= | 47.79 (cfs) |
| Q (2-YR)= | 33.58 (cfs) |

DA#15A EXISTING CALCULATIONS

Volume (100-yr) = 1.38*area*43560 = 1725237.36 cft
 Volume (10-yr) = 0.70*area*43560 = 875120.4 cft
 Volume (2-yr) = 0.41*area*43560 = 512570.52 cft
 A = 28.70 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

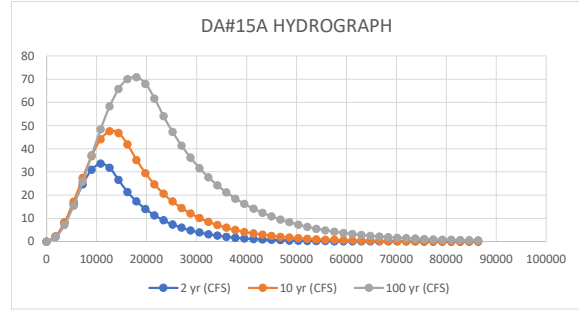
$q_i = \left(\frac{Q_p}{2}\right) \left[1 - \cos\left(\frac{\pi t_i}{T_p}\right)\right]$ $t_i \leq 1.25 T_p$
 $q_i = 4.34 Q_p e^{-1.3t_i/T_p}$ $t_i > 1.25 T_p$

| DA#15A Existing Conditions | | | |
|----------------------------|-----------|-----------|------------|
| | 2 - Year | 10 - Year | 100 - Year |
| Qp= | 33.58 | 47.79 | 71.03 |
| TP= | 10981.738 | 13175.190 | 17473.381 |
| 1.25*TP= | 13727.172 | 16468.987 | 21841.727 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) |
|----------|-------------|-------------|--------------|
| 0 | 0 | 0 | 0 |
| 1800.00 | 2.177172077 | 2.167154292 | 1.843716597 |
| 3600.00 | 8.144040371 | 8.275480529 | 7.183444664 |
| 5400.00 | 16.3531021 | 17.21688647 | 15.46479317 |
| 7200.00 | 24.67534329 | 27.36933981 | 25.82796077 |
| 9000.00 | 30.95239697 | 36.89111593 | 37.19700369 |
| 10800.00 | 33.55631402 | 44.05489939 | 48.39154432 |
| 12600.00 | 31.8117705 | 47.56113079 | 58.24932255 |
| 14400.00 | 26.49952911 | 46.77375571 | 65.74686606 |
| 16200.00 | 21.41402179 | 41.8356094 | 70.10575115 |
| 18000.00 | 17.30447086 | 35.11158275 | 70.87342166 |
| 19800.00 | 13.98358116 | 29.39793743 | 67.97017511 |
| 21600.00 | 11.30000124 | 24.61406343 | 61.69743766 |
| 23400.00 | 9.131425381 | 20.60866073 | 54.05910972 |
| 25200.00 | 7.379019502 | 17.25505008 | 47.2834381 |
| 27000.00 | 5.96291669 | 14.44716651 | 41.35701697 |
| 28800.00 | 4.818577244 | 12.09620484 | 36.17340281 |
| 30600.00 | 3.893847233 | 10.12781097 | 31.63949354 |
| 32400.00 | 3.146581555 | 8.47973033 | 27.6738563 |
| 34200.00 | 2.542723144 | 7.099838917 | 24.2052649 |
| 36000.00 | 2.054750807 | 5.944494776 | 21.17142051 |
| 37800.00 | 1.660424922 | 4.977157729 | 18.51783273 |
| 39600.00 | 1.34177386 | 4.167233717 | 16.19684086 |
| 41400.00 | 1.084274915 | 3.489107197 | 14.16675795 |
| 43200.00 | 0.876192424 | 2.921330997 | 12.39112197 |
| 45000.00 | 0.708042909 | 2.445948007 | 10.83804102 |
| 46800.00 | 0.572162857 | 2.047923245 | 9.479620445 |
| 48600.00 | 0.462359457 | 1.714668343 | 8.29146186 |
| 50400.00 | 0.373628355 | 1.435643417 | 7.252224937 |
| 52200.00 | 0.301925582 | 1.202023721 | 6.343244101 |
| 54000.00 | 0.243983241 | 1.006420542 | 5.548193289 |
| 55800.00 | 0.197160576 | 0.84264752 | 4.852792716 |
| 57600.00 | 0.159323619 | 0.70552499 | 4.244552401 |
| 59400.00 | 0.128747927 | 0.590716165 | 3.712547834 |
| 61200.00 | 0.104039997 | 0.494589975 | 3.247223763 |
| 63000.00 | 0.084073749 | 0.41410623 | 2.840222574 |
| 64800.00 | 0.067939211 | 0.346719461 | 2.484234183 |
| 66600.00 | 0.054901041 | 0.29029842 | 2.172864736 |
| 68400.00 | 0.044365018 | 0.243058675 | 1.900521777 |
| 70200.00 | 0.035850957 | 0.20350617 | 1.662313794 |
| 72000.00 | 0.028970823 | 0.170389974 | 1.453962371 |
| 73800.00 | 0.023411051 | 0.142662717 | 1.271725342 |
| 75600.00 | 0.018918252 | 0.119447467 | 1.112329573 |
| 77400.00 | 0.015287662 | 0.100009993 | 0.972912184 |
| 79200.00 | 0.012353817 | 0.083735545 | 0.85096912 |
| 81000.00 | 0.009983004 | 0.070109409 | 0.744310181 |
| 82800.00 | 0.008067172 | 0.05870063 | 0.651019681 |
| 84600.00 | 0.006519007 | 0.049148381 | 0.569422044 |
| 86400.00 | 0.005267948 | 0.041150552 | 0.498051709 |

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DA#15A DRAINAGE CALCULATIONS

Time of Concentration:

$T_c = T_{OL} + T_1 + \dots + T_n$

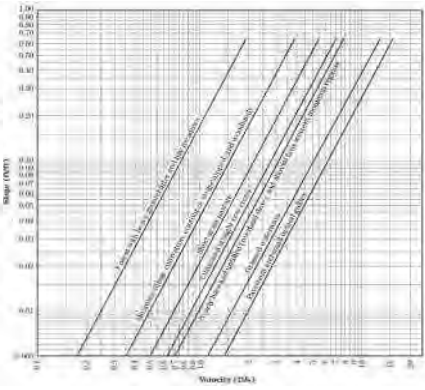
Section 2.1
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Table 2.1 (continued) Slope Length Correction Factor for Overland Flow

| Slope Length (ft) | Factor |
|-------------------|--------|
| 0-100 | 1.00 |
| 100-200 | 1.05 |
| 200-300 | 1.10 |
| 300-400 | 1.15 |
| 400-500 | 1.20 |
| 500-600 | 1.25 |
| 600-700 | 1.30 |
| 700-800 | 1.35 |
| 800-900 | 1.40 |
| 900-1000 | 1.45 |
| 1000-1200 | 1.50 |
| 1200-1400 | 1.55 |
| 1400-1600 | 1.60 |
| 1600-1800 | 1.65 |
| 1800-2000 | 1.70 |
| 2000-2500 | 1.75 |
| 2500-3000 | 1.80 |
| 3000-3500 | 1.85 |
| 3500-4000 | 1.90 |
| 4000-4500 | 1.95 |
| 4500-5000 | 2.00 |
| 5000-6000 | 2.10 |
| 6000-7000 | 2.20 |
| 7000-8000 | 2.30 |
| 8000-9000 | 2.40 |
| 9000-10000 | 2.50 |

| | | |
|------------|----------------------------------------------------------------------|----------------------|
| $T_{OL} =$ | $T_t = T_{OL}$; multiply by 60 to convert hrs. to min. (L=max 300') | $T =$ |
| $n =$ | 0.15 | $D =$ 2064.26 (ft) |
| $L =$ | 100 (ft) | $S =$ 0.0026 (ft/ft) |
| $P_2 =$ | 4.89 (in) | $V =$ 0.5 (ft/s) |
| $S =$ | 0.0026 (ft/ft) | |
| $T_{OL} =$ | 17.93 (min) | $T_1 =$ 68.81 (min) |

$T_c = 86.73$ (min)



Intensity:

SEE FIG. 2.1-2.1a

| | |
|---------------|-------------|
| I (100-YR)= | 4 (in/hr) |
| I (10-YR)= | 2.5 (in/hr) |
| I (2-YR)= | 1.7 (in/hr) |

Peak Flow Rate:

$Q = CIA$

$C =$ 0.35 Mixed use area; lots 1/4-1/2 acre; MOSTLY golf course; basin slope <1%

| | | |
|--------------|-------------|------------|
| i (100-YR) | i (10-YR) | i (2-YR) |
| 4 | 2.5 | 1.7 |
| $A =$ | 46.71 (Ac) | |

| | |
|---------------|-------------|
| Q (100-YR)= | 65.39 (cfs) |
| Q (10-YR)= | 40.87 (cfs) |
| Q (2-YR)= | 27.79 (cfs) |

DA#15A EXISTING CALCULATIONS

Volume (100-yr) = 1.38*area*43560 = 2807868.89 cft
 Volume (10-yr) = 0.70*area*43560 = 1424281.32 cft
 Volume (2-yr) = 0.41*area*43560 = 834221.916 cft
 A = 46.71 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

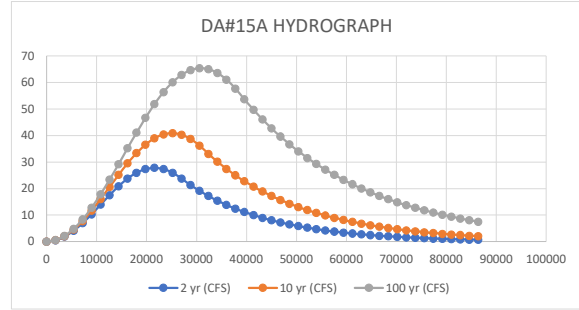
$q_i = \left(\frac{Q_p}{2}\right) \left[1 - \cos\left(\frac{\pi t_i}{T_p}\right)\right]$ $t_i \leq 1.25 T_p$
 $q_i = 1.34 Q_p e^{-1.3 t_i / T_p}$ $t_i > 1.25 T_p$

| DA#15A Existing Conditions | | | |
|----------------------------|-----------|-----------|------------|
| | 2 - Year | 10 - Year | 100 - Year |
| Qp= | 27.79 | 40.87 | 65.39 |
| TP= | 21594.341 | 25070.504 | 30890.442 |
| 1.25*TP= | 26992.927 | 31338.129 | 38613.052 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) |
|----------|-------------|-------------|--------------|
| 0 | 0 | 0 | 0 |
| 1800.00 | 0.473749154 | 0.517647952 | 0.546337808 |
| 3600.00 | 1.862694569 | 2.044367073 | 2.167093595 |
| 5400.00 | 4.072132579 | 4.502811747 | 4.808104584 |
| 7200.00 | 6.951415166 | 7.768433901 | 8.381112881 |
| 9000.00 | 10.30422172 | 11.67579278 | 12.7667149 |
| 10800.00 | 13.90194493 | 16.02693639 | 17.81835162 |
| 12600.00 | 17.49927814 | 20.60143002 | 23.36720632 |
| 14400.00 | 20.85094126 | 25.16752375 | 29.22784614 |
| 16200.00 | 23.72840496 | 29.49389321 | 35.20441891 |
| 18000.00 | 25.93547264 | 33.36135876 | 41.09719821 |
| 19800.00 | 27.32165791 | 36.57398948 | 46.70925781 |
| 21600.00 | 27.79244529 | 38.96902922 | 51.85305266 |
| 23400.00 | 27.31573469 | 40.42514209 | 56.35668628 |
| 25200.00 | 25.92403006 | 40.86855947 | 60.06965525 |
| 27000.00 | 23.74122356 | 40.27681726 | 62.86787874 |
| 28800.00 | 21.30307027 | 38.67989389 | 64.65784509 |
| 30600.00 | 19.11530809 | 36.15869164 | 65.37973682 |
| 32400.00 | 17.15222261 | 33.05719511 | 65.00942957 |
| 34200.00 | 15.39074019 | 30.11135881 | 63.55929837 |
| 36000.00 | 13.81015679 | 27.42803575 | 61.07780403 |
| 37800.00 | 12.39189462 | 24.98383251 | 57.64787366 |
| 39600.00 | 11.11928377 | 22.75744032 | 53.6118403 |
| 41400.00 | 9.977366287 | 20.72944933 | 49.70066722 |
| 43200.00 | 8.952720342 | 18.88217934 | 46.07482802 |
| 45000.00 | 8.033302499 | 17.19952571 | 42.71350659 |
| 46800.00 | 7.208306143 | 15.66681893 | 39.59740544 |
| 48600.00 | 6.468034468 | 14.27069673 | 36.70863486 |
| 50400.00 | 5.803786499 | 12.99898761 | 34.03061031 |
| 52200.00 | 5.207754828 | 11.8406047 | 31.5479571 |
| 54000.00 | 4.672933843 | 10.78544914 | 29.24642221 |
| 55800.00 | 4.193037388 | 9.824321996 | 27.11279243 |
| 57600.00 | 3.762424877 | 8.948844077 | 25.13481847 |
| 59400.00 | 3.376034994 | 8.151382898 | 23.30114469 |
| 61200.00 | 3.029326206 | 7.424986131 | 21.60124389 |
| 63000.00 | 2.718223384 | 6.763320989 | 20.02535686 |
| 64800.00 | 2.439069899 | 6.160619022 | 18.56443636 |
| 66600.00 | 2.18858465 | 5.611625827 | 17.21009516 |
| 68400.00 | 1.963823493 | 5.111555236 | 15.95455794 |
| 70200.00 | 1.762144641 | 4.656047594 | 14.79061659 |
| 72000.00 | 1.58117761 | 4.241131749 | 13.71158888 |
| 73800.00 | 1.418795356 | 3.863190432 | 12.71128004 |
| 75600.00 | 1.273089278 | 3.518928718 | 11.78394727 |
| 77400.00 | 1.142346783 | 3.205345308 | 10.9242667 |
| 79200.00 | 1.025031154 | 2.919706356 | 10.12730286 |
| 81000.00 | 0.919763493 | 2.659521638 | 9.388480354 |
| 82800.00 | 0.825306508 | 2.422522844 | 8.703557555 |
| 84600.00 | 0.740549976 | 2.206643798 | 8.068602294 |
| 86400.00 | 0.664497689 | 2.01000245 | 7.479969261 |

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DA#16 DRAINAGE CALCULATIONS

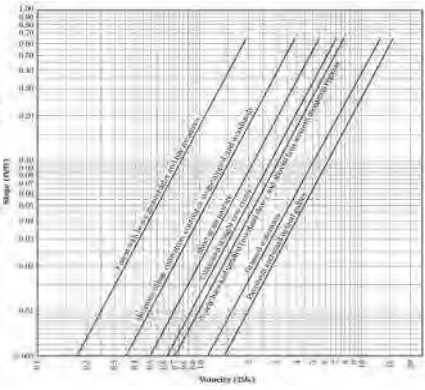
Time of Concentration:

$T_c = T_{OL} + T_1 + \dots + T_n$

Section 2.1
 1. Determine the time of concentration for each sub-area.
 2. Determine the time of concentration for the entire drainage area.
 3. Determine the time of concentration for the entire drainage area.
 4. Determine the time of concentration for the entire drainage area.
 5. Determine the time of concentration for the entire drainage area.
 6. Determine the time of concentration for the entire drainage area.
 7. Determine the time of concentration for the entire drainage area.
 8. Determine the time of concentration for the entire drainage area.
 9. Determine the time of concentration for the entire drainage area.
 10. Determine the time of concentration for the entire drainage area.

Table 2.1.1 (continued) - Longitudinal Conditions for Groundwater Flow

| Surface | n |
|-------------------------------------------------------|-------|
| Asphalt Surface (asphalt, asphalt, gravel, surf. w/c) | 0.012 |
| Gravel (asphalt) | 0.015 |
| Concrete Slab (asphalt cover in 20%) | 0.008 |
| Concrete Slab (asphalt cover 10%) | 0.010 |
| Grass (short grass) | 0.030 |
| Grass (medium grass) | 0.040 |
| Grass (tall grass) | 0.050 |
| Grass (bare) | 0.060 |
| Grass (matted) | 0.070 |
| Grass (matted) | 0.080 |
| Grass (matted) | 0.090 |
| Grass (matted) | 0.100 |
| Grass (matted) | 0.110 |
| Grass (matted) | 0.120 |
| Grass (matted) | 0.130 |
| Grass (matted) | 0.140 |
| Grass (matted) | 0.150 |
| Grass (matted) | 0.160 |
| Grass (matted) | 0.170 |
| Grass (matted) | 0.180 |
| Grass (matted) | 0.190 |
| Grass (matted) | 0.200 |
| Grass (matted) | 0.210 |
| Grass (matted) | 0.220 |
| Grass (matted) | 0.230 |
| Grass (matted) | 0.240 |
| Grass (matted) | 0.250 |
| Grass (matted) | 0.260 |
| Grass (matted) | 0.270 |
| Grass (matted) | 0.280 |
| Grass (matted) | 0.290 |
| Grass (matted) | 0.300 |
| Grass (matted) | 0.310 |
| Grass (matted) | 0.320 |
| Grass (matted) | 0.330 |
| Grass (matted) | 0.340 |
| Grass (matted) | 0.350 |
| Grass (matted) | 0.360 |
| Grass (matted) | 0.370 |
| Grass (matted) | 0.380 |
| Grass (matted) | 0.390 |
| Grass (matted) | 0.400 |
| Grass (matted) | 0.410 |
| Grass (matted) | 0.420 |
| Grass (matted) | 0.430 |
| Grass (matted) | 0.440 |
| Grass (matted) | 0.450 |
| Grass (matted) | 0.460 |
| Grass (matted) | 0.470 |
| Grass (matted) | 0.480 |
| Grass (matted) | 0.490 |
| Grass (matted) | 0.500 |
| Grass (matted) | 0.510 |
| Grass (matted) | 0.520 |
| Grass (matted) | 0.530 |
| Grass (matted) | 0.540 |
| Grass (matted) | 0.550 |
| Grass (matted) | 0.560 |
| Grass (matted) | 0.570 |
| Grass (matted) | 0.580 |
| Grass (matted) | 0.590 |
| Grass (matted) | 0.600 |
| Grass (matted) | 0.610 |
| Grass (matted) | 0.620 |
| Grass (matted) | 0.630 |
| Grass (matted) | 0.640 |
| Grass (matted) | 0.650 |
| Grass (matted) | 0.660 |
| Grass (matted) | 0.670 |
| Grass (matted) | 0.680 |
| Grass (matted) | 0.690 |
| Grass (matted) | 0.700 |
| Grass (matted) | 0.710 |
| Grass (matted) | 0.720 |
| Grass (matted) | 0.730 |
| Grass (matted) | 0.740 |
| Grass (matted) | 0.750 |
| Grass (matted) | 0.760 |
| Grass (matted) | 0.770 |
| Grass (matted) | 0.780 |
| Grass (matted) | 0.790 |
| Grass (matted) | 0.800 |
| Grass (matted) | 0.810 |
| Grass (matted) | 0.820 |
| Grass (matted) | 0.830 |
| Grass (matted) | 0.840 |
| Grass (matted) | 0.850 |
| Grass (matted) | 0.860 |
| Grass (matted) | 0.870 |
| Grass (matted) | 0.880 |
| Grass (matted) | 0.890 |
| Grass (matted) | 0.900 |
| Grass (matted) | 0.910 |
| Grass (matted) | 0.920 |
| Grass (matted) | 0.930 |
| Grass (matted) | 0.940 |
| Grass (matted) | 0.950 |
| Grass (matted) | 0.960 |
| Grass (matted) | 0.970 |
| Grass (matted) | 0.980 |
| Grass (matted) | 0.990 |
| Grass (matted) | 1.000 |



| | | |
|------------|-----------------------------------------------------------------------------|----------------------|
| $T_{OL} =$ | $T_t = T_{OL}$; multiply by 60 to convert hrs. to min. ($L = \max 300'$) | $T =$ |
| $n =$ | 0.8 | $D =$ 297.95 (ft) |
| $L =$ | 100 (ft) | $S =$ 0.0098 (ft/ft) |
| $P_2 =$ | 4.89 (in) | $V =$ 1.2 (ft/s) |
| $S =$ | 0.0098 (ft/ft) | |
| $T_{OL} =$ | 40.23 (min) | $T_1 =$ 4.14 (min) |

$T_c = 44.37$ (min)

Intensity:

SEE FIG. 2.1-2.1a

| | |
|---------------|-------------|
| I (100-YR)= | 5.2 (in/hr) |
| I (10-YR)= | 3.6 (in/hr) |
| I (2-YR)= | 2.4 (in/hr) |

Peak Flow Rate:

$Q = CIA$

$C =$ 0.18 Woodlands; basin slope <1%

| | | |
|----------------|-------------|------------|
| i (100-YR) | i (10-YR) | i (2-YR) |
| 5.2 | 3.6 | 2.4 |
| $A =$ 3.1 (Ac) | | |

| | |
|---------------|------------|
| Q (100-YR)= | 2.90 (cfs) |
| Q (10-YR)= | 2.01 (cfs) |
| Q (2-YR)= | 1.34 (cfs) |

DA#16 EXISTING CALCULATIONS

Volume (100-yr) = 1.38*area*43560 = 186349.68 cft
 Volume (10-yr) = 0.70*area*43560 = 94525.2 cft
 Volume (2-yr) = 0.41*area*43560 = 55364.76 cft
 A = 3.10 Ac

TP = time to Qp in seconds

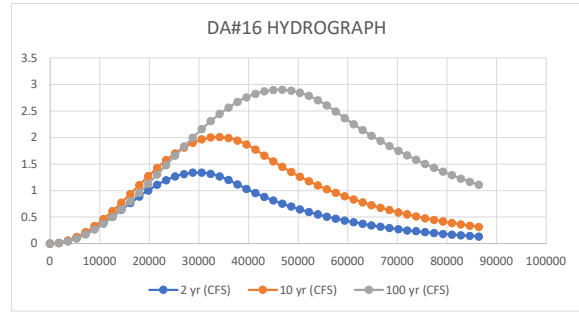
TP = $\frac{V}{1.39 Q_p}$

$q_i = \left(\frac{Q_p}{2}\right) \left[1 - \cos\left(\frac{\pi t_i}{T_p}\right)\right]$ $t_i \leq 1.25 T_p$
 $q_i = 1.34 Q_p e^{-1.3t_i/T_p}$ $t_i > 1.25 T_p$

| DA#16 Existing Conditions | | | |
|---------------------------|-----------|-----------|------------|
| | 2 - Year | 10 - Year | 100 - Year |
| Qp= | 1.34 | 2.01 | 2.90 |
| TP= | 29742.206 | 33852.918 | 46203.652 |
| 1.25*TP= | 37177.758 | 42316.147 | 57754.566 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) |
|----------|-------------|-------------|--------------|
| 0 | 0 | 0 | 0 |
| 1800.00 | 0.012066329 | 0.013980386 | 0.010852443 |
| 3600.00 | 0.047830441 | 0.055532355 | 0.043247411 |
| 5400.00 | 0.106003382 | 0.123499171 | 0.096700257 |
| 7200.00 | 0.184488577 | 0.215988755 | 0.170411291 |
| 9000.00 | 0.280457386 | 0.330426355 | 0.26327775 |
| 10800.00 | 0.390451054 | 0.463626225 | 0.373910293 |
| 12600.00 | 0.510505364 | 0.611880309 | 0.500653786 |
| 14400.00 | 0.63629351 | 0.771061467 | 0.641612068 |
| 16200.00 | 0.763282036 | 0.93673837 | 0.794676313 |
| 18000.00 | 0.886894222 | 1.104298857 | 0.957556583 |
| 19800.00 | 1.002675036 | 1.26907833 | 1.127816087 |
| 21600.00 | 1.10645169 | 1.426489614 | 1.302907634 |
| 23400.00 | 1.194484029 | 1.572150646 | 1.480211745 |
| 25200.00 | 1.263599333 | 1.702006475 | 1.657075837 |
| 27000.00 | 1.311306658 | 1.812442137 | 1.830853913 |
| 28800.00 | 1.335886612 | 1.900383292 | 1.998946141 |
| 30600.00 | 1.336453324 | 1.963381809 | 2.158837757 |
| 32400.00 | 1.312986369 | 1.999683918 | 2.30813668 |
| 34200.00 | 1.266331505 | 2.008279031 | 2.444609304 |
| 36000.00 | 1.198170194 | 1.988927874 | 2.566213912 |
| 37800.00 | 1.113768408 | 1.942169151 | 2.671131223 |
| 39600.00 | 1.029499904 | 1.869304543 | 2.757791607 |
| 41400.00 | 0.951607215 | 1.772362477 | 2.824898571 |
| 43200.00 | 0.879607941 | 1.659424197 | 2.87144815 |
| 45000.00 | 0.813056183 | 1.548595084 | 2.896743935 |
| 46800.00 | 0.751539779 | 1.445167992 | 2.900407484 |
| 48600.00 | 0.694677748 | 1.348648557 | 2.882383989 |
| 50400.00 | 0.64211794 | 1.258575432 | 2.842943092 |
| 52200.00 | 0.593534843 | 1.174518084 | 2.782674854 |
| 54000.00 | 0.548627578 | 1.096074731 | 2.702480926 |
| 55800.00 | 0.507118028 | 1.022870429 | 2.603561059 |
| 57600.00 | 0.46874912 | 0.954555274 | 2.487395158 |
| 59400.00 | 0.433283231 | 0.89080273 | 2.36751342 |
| 61200.00 | 0.400500716 | 0.831308071 | 2.250595545 |
| 63000.00 | 0.370198549 | 0.775786924 | 2.139451571 |
| 64800.00 | 0.342189065 | 0.723973905 | 2.033796359 |
| 66600.00 | 0.316298799 | 0.675621359 | 1.93358851 |
| 68400.00 | 0.292367409 | 0.630498168 | 1.837881373 |
| 70200.00 | 0.270246684 | 0.58838865 | 1.74711898 |
| 72000.00 | 0.249799629 | 0.54909153 | 1.660838819 |
| 73800.00 | 0.230899613 | 0.512418974 | 1.578819539 |
| 75600.00 | 0.213429585 | 0.478195693 | 1.50085072 |
| 77400.00 | 0.197281352 | 0.446258106 | 1.426732332 |
| 79200.00 | 0.182354906 | 0.416453557 | 1.356274225 |
| 81000.00 | 0.168557805 | 0.388639585 | 1.28929564 |
| 82800.00 | 0.155804602 | 0.362683244 | 1.225624741 |
| 84600.00 | 0.144016316 | 0.338460467 | 1.165098182 |
| 86400.00 | 0.13311994 | 0.315855474 | 1.107560682 |

ti (hrs)
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DA#16A DRAINAGE CALCULATIONS

Time of Concentration:

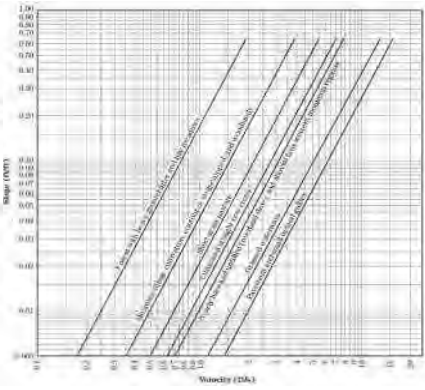
$T_c = T_{OL} + T_1 + \dots + T_n$

Section 2.1
 1. Determine the time of concentration for each sub-area.
 2. Determine the time of concentration for the entire drainage area.
 3. Determine the peak flow rate for each sub-area.
 4. Determine the peak flow rate for the entire drainage area.
 5. Determine the peak flow rate for the entire drainage area.
 6. Determine the peak flow rate for the entire drainage area.
 7. Determine the peak flow rate for the entire drainage area.
 8. Determine the peak flow rate for the entire drainage area.
 9. Determine the peak flow rate for the entire drainage area.
 10. Determine the peak flow rate for the entire drainage area.

Table 2.1.1 (continued) - Longitudinal Conditions for Groundwater Flow

| Barriers | a |
|-----------------------------------------------------------|-------|
| Surface (Surface Impervious, asphalt, gravel, surf, etc.) | 0.012 |
| Surface (Soil) | 0.05 |
| Subsurface (Soil, Residual Cover, etc.) | 0.06 |
| Subsurface (Soil, Residual Cover, etc.) | 0.17 |
| Gravel (Soil, Residual Cover, etc.) | 0.19 |
| Gravel (Soil, Residual Cover, etc.) | 0.24 |
| Gravel (Soil, Residual Cover, etc.) | 0.36 |
| Gravel (Soil, Residual Cover, etc.) | 0.42 |
| Gravel (Soil, Residual Cover, etc.) | 0.46 |
| Gravel (Soil, Residual Cover, etc.) | 0.80 |

Source: SCS TR-55 (1975, 1980)



| | | |
|------------|----------------------------------------------------------------------|---------------------|
| $T_{OL} =$ | $T_t = T_{OL}$; multiply by 60 to convert hrs. to min. (L=max 300') | $T =$ |
| n= | 0.15 | D= 1034.24 (ft) |
| L= | 100 (ft) | S= 0.0058 (ft/ft) |
| $P_2 =$ | 4.89 (in) | V= 0.55 (ft/s) |
| S= | 0.0058 (ft/ft) | |
| $T_{OL} =$ | 13.00 (min) | $T_1 =$ 31.34 (min) |

$T_c = 44.35$ (min)

Intensity:

SEE FIG. 2.1-2.1a

| | |
|-------------|-------------|
| I (100-YR)= | 5.5 (in/hr) |
| I (10-YR)= | 3.7 (in/hr) |
| I (2-YR)= | 2.5 (in/hr) |

Peak Flow Rate:

$Q = CIA$

C= 0.15 Mixed use area; lots 1/4-1/2 acre; MOSTLY golf course; basin slope <1%

| | | |
|--------------|-----------|----------|
| i (100-YR) | i (10-YR) | i (2-YR) |
| 5.5 | 3.7 | 2.5 |
| A= 8.18 (Ac) | | |

| | |
|-------------|------------|
| Q (100-YR)= | 6.75 (cfs) |
| Q (10-YR)= | 4.54 (cfs) |
| Q (2-YR)= | 3.07 (cfs) |

DA#16A EXISTING CALCULATIONS

Volume (100-yr) = 1.38*area*43560 = 491722.70 cft
 Volume (10-yr) = 0.70*area*43560 = 249424.56 cft
 Volume (2-yr) = 0.41*area*43560 = 146091.528 cft
 A = 8.18 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

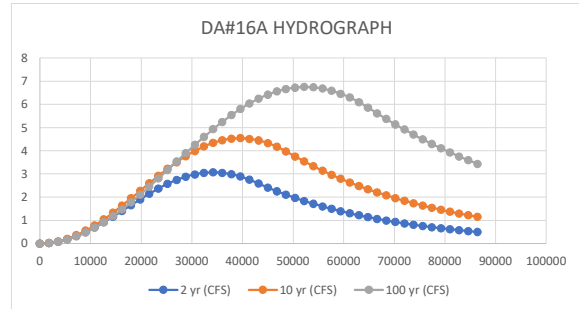
$q_i = \left(\frac{Q_p}{2}\right) \left[1 - \cos\left(\frac{\pi t_i}{T_p}\right)\right]$ $t_i \leq 1.25 T_p$
 $q_i = 1.34 Q_p e^{-1.3 t_i / T_p}$ $t_i > 1.25 T_p$

| DA#16A Existing Conditions | | | |
|----------------------------|-----------|-----------|------------|
| | 2 - Year | 10 - Year | 100 - Year |
| Qp= | 3.07 | 4.54 | 6.75 |
| TP= | 34263.022 | 39525.569 | 52420.144 |
| 1.25*TP= | 42828.777 | 49406.961 | 65525.180 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) |
|----------|-------------|-------------|--------------|
| 0 | 0 | 0 | 0 |
| 1800.00 | 0.020841644 | 0.023191769 | 0.019614371 |
| 3600.00 | 0.082800155 | 0.092293184 | 0.078229451 |
| 5400.00 | 0.184191664 | 0.205892243 | 0.175163784 |
| 7200.00 | 0.322260617 | 0.361667695 | 0.30929042 |
| 9000.00 | 0.493254662 | 0.556436467 | 0.479050015 |
| 10800.00 | 0.692526632 | 0.786218708 | 0.682468959 |
| 12600.00 | 0.914660839 | 1.046319108 | 0.917182319 |
| 14400.00 | 1.15362026 | 1.331422849 | 1.180461339 |
| 16200.00 | 1.402910607 | 1.635704197 | 1.469245158 |
| 18000.00 | 1.657556824 | 1.95294555 | 1.780176402 |
| 19800.00 | 1.905287216 | 2.276664487 | 2.109640209 |
| 21600.00 | 2.144720205 | 2.600246221 | 2.453806261 |
| 23400.00 | 2.367548632 | 2.917078772 | 2.808673314 |
| 25200.00 | 2.567716607 | 3.220688071 | 3.170115714 |
| 27000.00 | 2.739784091 | 3.504870247 | 3.533931361 |
| 28800.00 | 2.879074742 | 3.7638184 | 3.895890566 |
| 30600.00 | 2.981803008 | 3.992241254 | 4.251785223 |
| 32400.00 | 3.045177005 | 4.185471278 | 4.59747773 |
| 34200.00 | 3.067474393 | 4.339560063 | 4.928949096 |
| 36000.00 | 3.04808919 | 4.451359 | 5.242345662 |
| 37800.00 | 2.987548233 | 4.518583622 | 5.534023908 |
| 39600.00 | 2.887496866 | 4.539860277 | 5.800592806 |
| 41400.00 | 2.750654223 | 4.514754206 | 6.03895325 |
| 43200.00 | 2.584810981 | 4.443778417 | 6.246334081 |
| 45000.00 | 2.414173956 | 4.328383212 | 6.420324307 |
| 46800.00 | 2.254801582 | 4.170926544 | 6.558901134 |
| 48600.00 | 2.10595022 | 3.974625841 | 6.660453477 |
| 50400.00 | 1.966925322 | 3.755112243 | 6.7238007 |
| 52200.00 | 1.837078193 | 3.539254077 | 6.748206331 |
| 54000.00 | 1.715802958 | 3.335804261 | 6.733386634 |
| 55800.00 | 1.602533742 | 3.144049516 | 6.679513901 |
| 57600.00 | 1.496742026 | 2.963317565 | 6.587214452 |
| 59400.00 | 1.397934179 | 2.792974775 | 6.457561352 |
| 61200.00 | 1.30564916 | 2.632423939 | 6.292061937 |
| 63000.00 | 1.219456363 | 2.481102176 | 6.092640289 |
| 64800.00 | 1.138953608 | 2.338478965 | 5.861614867 |
| 66600.00 | 1.063765264 | 2.20405428 | 5.615549621 |
| 68400.00 | 0.993540501 | 2.077356838 | 5.370387895 |
| 70200.00 | 0.927951644 | 1.957942448 | 5.135929356 |
| 72000.00 | 0.866692655 | 1.845392453 | 4.911706727 |
| 73800.00 | 0.809477695 | 1.73931226 | 4.697273131 |
| 75600.00 | 0.756039797 | 1.639329961 | 4.492201204 |
| 77400.00 | 0.706129617 | 1.545095026 | 4.296082235 |
| 79200.00 | 0.659514271 | 1.456277074 | 4.108525361 |
| 81000.00 | 0.615976251 | 1.372564716 | 3.929156781 |
| 82800.00 | 0.575312405 | 1.293664464 | 3.757619011 |
| 84600.00 | 0.537332994 | 1.219299699 | 3.593570179 |
| 86400.00 | 0.501860805 | 1.149209705 | 3.436683333 |

ti (hrs)

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DA#17 EXISTING CALCULATIONS

Volume (100-yr) = 1.38*area*43560 = 735179.54 cft
 Volume (10-yr) = 0.70*area*43560 = 372917.16 cft
 Volume (2-yr) = 0.41*area*43560 = 218422.908 cft
 A = 12.23 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

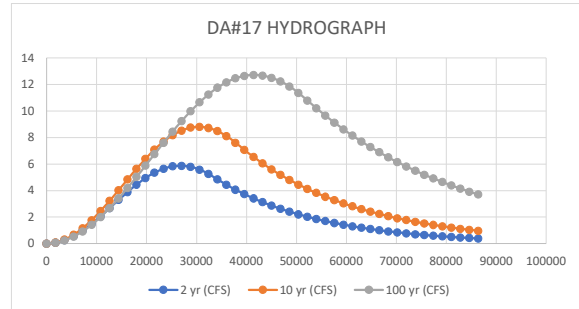
$q_i = \left(\frac{Q_p}{2}\right) \left[1 - \cos\left(\frac{\pi t_i}{T_p}\right)\right]$ $t_i \leq 1.25 T_p$
 $q_i = 1.34 Q_p e^{-1.3t_i/T_p}$ $t_i > 1.25 T_p$

| DA#17 Existing Conditions | | | |
|---------------------------|-----------|-----------|------------|
| | 2 - Year | 10 - Year | 100 - Year |
| Qp= | 5.87 | 8.81 | 12.72 |
| TP= | 26767.986 | 30467.626 | 41583.287 |
| 1.25*TP= | 33459.982 | 38084.532 | 51979.109 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) |
|----------|-------------|-------------|--------------|
| 0 | 0 | 0 | 0 |
| 1800.00 | 0.065253726 | 0.075616994 | 0.058713442 |
| 3600.00 | 0.258113535 | 0.299870568 | 0.233769652 |
| 5400.00 | 0.570004323 | 0.665057725 | 0.521936303 |
| 7200.00 | 0.987058529 | 1.158634467 | 0.917892541 |
| 9000.00 | 1.490732719 | 1.763646679 | 1.414327228 |
| 10800.00 | 2.058632087 | 2.459312494 | 2.002073942 |
| 12600.00 | 2.665506192 | 3.221736136 | 2.67028023 |
| 14400.00 | 3.28437166 | 4.024728734 | 3.406607991 |
| 16200.00 | 3.88771195 | 4.840707891 | 4.197461296 |
| 18000.00 | 4.448700813 | 5.641645131 | 5.028237427 |
| 19800.00 | 4.942395068 | 6.400028657 | 5.883596513 |
| 21600.00 | 5.346843646 | 7.089808374 | 6.747744769 |
| 23400.00 | 5.644063596 | 7.687290691 | 7.604726123 |
| 25200.00 | 5.820839663 | 8.171952389 | 8.438716836 |
| 27000.00 | 5.869311874 | 8.52714558 | 9.23431768 |
| 28800.00 | 5.787325015 | 8.740669555 | 9.976838278 |
| 30600.00 | 5.578524457 | 8.805189871 | 10.65256835 |
| 32400.00 | 5.252194076 | 8.718490287 | 11.24903088 |
| 34200.00 | 4.839724492 | 8.483548892 | 11.75521247 |
| 36000.00 | 4.43461116 | 8.108435806 | 12.16176673 |
| 37800.00 | 4.063408191 | 7.606035974 | 12.46118685 |
| 39600.00 | 3.723277088 | 7.054035703 | 12.64794416 |
| 41400.00 | 3.411616953 | 6.532547957 | 12.7185903 |
| 43200.00 | 3.1260446 | 6.049612535 | 12.67182081 |
| 45000.00 | 2.864376329 | 5.602379356 | 12.50849927 |
| 46800.00 | 2.624611226 | 5.188209042 | 12.23164133 |
| 48600.00 | 2.40491587 | 4.804657335 | 11.84635904 |
| 50400.00 | 2.203610303 | 4.449460674 | 11.35976645 |
| 52200.00 | 2.019155194 | 4.120522841 | 10.79498197 |
| 54000.00 | 1.850140059 | 3.815902584 | 10.20429577 |
| 55800.00 | 1.695272482 | 3.533802163 | 9.645931098 |
| 57600.00 | 1.55336823 | 3.272556743 | 9.118119348 |
| 59400.00 | 1.423342197 | 3.030624562 | 8.619188714 |
| 61200.00 | 1.304200105 | 2.806577841 | 8.14755886 |
| 63000.00 | 1.195030905 | 2.59909435 | 7.701735927 |
| 64800.00 | 1.094999808 | 2.40694961 | 7.280307796 |
| 66600.00 | 1.0033419 | 2.229009665 | 6.881939619 |
| 68400.00 | 0.919356297 | 2.064224388 | 6.505369586 |
| 70200.00 | 0.842400782 | 1.911621287 | 6.149404935 |
| 72000.00 | 0.771886895 | 1.770299763 | 5.812918167 |
| 73800.00 | 0.707275433 | 1.639425796 | 5.494843481 |
| 75600.00 | 0.64807233 | 1.518227024 | 5.194173393 |
| 77400.00 | 0.593824874 | 1.405988184 | 4.909955549 |
| 79200.00 | 0.544118249 | 1.302046888 | 4.641289704 |
| 81000.00 | 0.498572359 | 1.20578972 | 4.387324875 |
| 82800.00 | 0.456838928 | 1.116648612 | 4.147256644 |
| 84600.00 | 0.41859883 | 1.034097489 | 3.920324608 |
| 86400.00 | 0.38359652 | 0.95764917 | 3.705809973 |

ti (hrs)

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DA#18 DRAINAGE CALCULATIONS

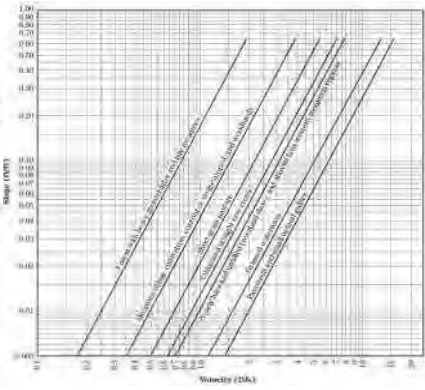
Time of Concentration:

$T_c = T_{OL} + T_1 + \dots + T_n$

Section 2.2
 1. Determine the length of the pipe (L) in feet.
 2. Determine the slope of the pipe (S) in feet per foot.
 3. Determine the roughness coefficient (n) for the pipe material.
 4. Calculate the velocity (V) in feet per second using the Manning equation.
 5. Calculate the time of travel (T) in minutes for the pipe section.
 6. Repeat steps 1-5 for all pipe sections in the drainage area.
 7. Sum the times for all pipe sections to determine the total time of travel (T_{OL}).
 8. Determine the time of travel for the overland flow (T₁) using the Kirpich equation.
 9. Sum T_{OL} and T₁ to determine the total time of concentration (T_c).

Table 2.1 Manning's Roughness Coefficient for Concrete Sewer Pipe

| Surface | n |
|----------------------------------------------------------|-------|
| Smooth Surface (asbestos, cast-iron, glazed, burnt wood) | 0.012 |
| Polished concrete | 0.015 |
| Unfinished concrete | 0.016 |
| Cast-iron pipe, finished | 0.017 |
| Cast-iron pipe, rough | 0.018 |
| Concrete pipe, finished | 0.018 |
| Concrete pipe, rough | 0.019 |
| Clay pipe, finished | 0.020 |
| Clay pipe, rough | 0.022 |
| Stoneware pipe, finished | 0.020 |
| Stoneware pipe, rough | 0.022 |
| Brick pipe, finished | 0.020 |
| Brick pipe, rough | 0.022 |
| Galvanized iron pipe, finished | 0.020 |
| Galvanized iron pipe, rough | 0.022 |
| Steel pipe, finished | 0.020 |
| Steel pipe, rough | 0.022 |
| Aluminum pipe, finished | 0.020 |
| Aluminum pipe, rough | 0.022 |
| Plastic pipe, finished | 0.020 |
| Plastic pipe, rough | 0.022 |
| Asbestos pipe, finished | 0.020 |
| Asbestos pipe, rough | 0.022 |
| Wood pipe, finished | 0.020 |
| Wood pipe, rough | 0.022 |
| Other pipe, finished | 0.020 |
| Other pipe, rough | 0.022 |



| | | |
|------------|--------------------------------------------------------------------|-------------|
| $T_{OL} =$ | $T = T_{OL}$; multiply by 60 to convert hrs. to min. (L=max 300') | $T =$ |
| n = | 0.15 | D = |
| L = | 100 (ft) | S = |
| $P_2 =$ | 4.89 (in) | V = |
| $S =$ | 0.0081 (ft/ft) | |
| $T_{OL} =$ | 11.38 (min) | $T_1 =$ |
| | | 44.07 (min) |

$T_c = 55.45$ (min)

Intensity:

SEE FIG. 2.1-2.1a

| | |
|--------------|-------------|
| I (100-YR) = | 5.8 (in/hr) |
| I (10-YR) = | 3.2 (in/hr) |
| I (2-YR) = | 2.2 (in/hr) |

Peak Flow Rate:

$Q = CIA$

C = 0.4 Single family residential districts; lots 1/4-1/2 acre; basin slope <1%

| | | |
|----------------|-----------|----------|
| i (100-YR) | i (10-YR) | i (2-YR) |
| 5.8 | 3.2 | 2.2 |
| A = 19.17 (Ac) | | |

| | |
|--------------|-------------|
| Q (100-YR) = | 44.47 (cfs) |
| Q (10-YR) = | 24.54 (cfs) |
| Q (2-YR) = | 16.87 (cfs) |

DA#18 EXISTING CALCULATIONS

Volume (100-yr) = 1.38*area*43560 = 1152362.38 cft
 Volume (10-yr) = 0.70*area*43560 = 584531.64 cft
 Volume (2-yr) = 0.41*area*43560 = 342368.532 cft
 A = 19.17 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

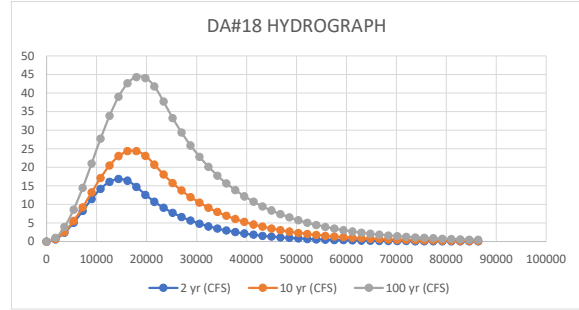
$q_i = \left(\frac{Q_p}{2}\right) \left[1 - \cos\left(\frac{\pi t_i}{T_p}\right)\right]$ $t_i \leq 1.25 T_p$
 $q_i = 4.34 Q_p e^{-1.3t_i/T_p}$ $t_i > 1.25 T_p$

| DA#18 Existing Conditions | | | |
|---------------------------|-----------|-----------|------------|
| | 2 - Year | 10 - Year | 100 - Year |
| Qp= | 16.87 | 24.54 | 44.47 |
| TP= | 14600.719 | 17138.040 | 18640.784 |
| 1.25*TP= | 18250.899 | 21422.549 | 23300.980 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) |
|----------|-------------|-------------|--------------|
| 0 | 0 | 0 | 0 |
| 1800.00 | 0.62474889 | 0.661836504 | 1.01539117 |
| 3600.00 | 2.406447739 | 2.575940898 | 3.968835449 |
| 5400.00 | 5.081162755 | 5.535801679 | 8.590613517 |
| 7200.00 | 8.252672276 | 9.222081356 | 14.45864772 |
| 9000.00 | 11.45116147 | 13.23706956 | 21.03704772 |
| 10800.00 | 14.20281886 | 17.14759179 | 27.72505002 |
| 12600.00 | 16.10002484 | 20.53174427 | 33.91188181 |
| 14400.00 | 16.86173484 | 23.02441297 | 39.03253901 |
| 16200.00 | 16.37511218 | 24.35666545 | 42.61938449 |
| 18000.00 | 14.71224321 | 24.38476583 | 44.34485442 |
| 19800.00 | 12.55929092 | 23.10568238 | 44.05137259 |
| 21600.00 | 10.69947451 | 20.68938019 | 41.76574083 |
| 23400.00 | 9.115065131 | 18.04885348 | 37.74611186 |
| 25200.00 | 7.765279713 | 15.74532968 | 33.29313675 |
| 27000.00 | 6.615374454 | 13.73579806 | 29.36548693 |
| 28800.00 | 5.635750519 | 11.98273725 | 25.90118885 |
| 30600.00 | 4.801192152 | 10.4534146 | 22.84558011 |
| 32400.00 | 4.090217621 | 9.119275044 | 20.1504469 |
| 34200.00 | 3.484526271 | 7.955407924 | 17.77326328 |
| 36000.00 | 2.968527462 | 6.940081852 | 15.6765202 |
| 37800.00 | 2.528939261 | 6.054338957 | 13.82713357 |
| 39600.00 | 2.154446563 | 5.281640907 | 12.19592234 |
| 41400.00 | 1.835409835 | 4.60756011 | 10.75714796 |
| 43200.00 | 1.563616996 | 4.019510326 | 9.488108319 |
| 45000.00 | 1.332072032 | 3.506511663 | 8.368779515 |
| 46800.00 | 1.134814922 | 3.058985559 | 7.381499896 |
| 48600.00 | 0.96676822 | 2.668575938 | 6.510691388 |
| 50400.00 | 0.823606364 | 2.327993186 | 5.742613689 |
| 52200.00 | 0.701644332 | 2.030878041 | 5.065147466 |
| 54000.00 | 0.597742794 | 1.771682857 | 4.467603122 |
| 55800.00 | 0.50927298 | 1.545568016 | 3.940552135 |
| 57600.00 | 0.433819435 | 1.348311569 | 3.475678278 |
| 59400.00 | 0.369578189 | 1.176230401 | 3.065646407 |
| 61200.00 | 0.314849973 | 1.026111462 | 2.703986715 |
| 63000.00 | 0.268226071 | 0.895151777 | 2.384992653 |
| 64800.00 | 0.228506373 | 0.780906103 | 2.103630881 |
| 66600.00 | 0.194668483 | 0.68124128 | 1.855461851 |
| 68400.00 | 0.165841406 | 0.594296394 | 1.636569757 |
| 70200.00 | 0.141283127 | 0.518448037 | 1.443500748 |
| 72000.00 | 0.12036151 | 0.452279989 | 1.27320843 |
| 73800.00 | 0.102538027 | 0.394556781 | 1.123005795 |
| 75600.00 | 0.087353897 | 0.344200622 | 0.990522829 |
| 77400.00 | 0.074418277 | 0.300271277 | 0.873669111 |
| 79200.00 | 0.063398202 | 0.261948508 | 0.770600831 |
| 81000.00 | 0.054010011 | 0.228516766 | 0.679691698 |
| 82800.00 | 0.046012051 | 0.199351821 | 0.599507274 |
| 84600.00 | 0.039198453 | 0.173909116 | 0.528782348 |
| 86400.00 | 0.033393831 | 0.15171359 | 0.466400966 |

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DA#19 DRAINAGE CALCULATIONS

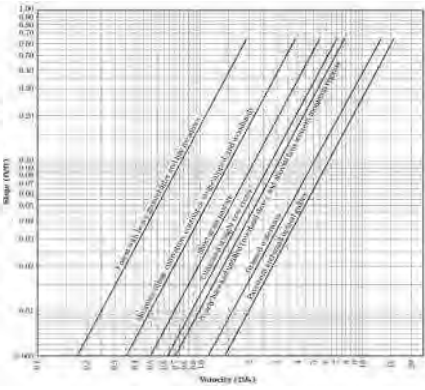
Time of Concentration:

$T_c = T_{OL} + T_1 + \dots + T_n$

Section 2.1
 1. Determine the length of the pipe (L) in feet.
 2. Determine the slope of the pipe (S) in ft/ft.
 3. Determine the roughness coefficient (n) for the pipe material.
 4. Calculate the velocity (V) in ft/s using the Manning equation.
 5. Calculate the travel time (T) in minutes for the pipe section.
 6. Repeat steps 1-5 for all pipe sections in the catchment.
 7. Sum the travel times for all pipe sections to determine the total travel time (T_{OL}).
 8. Determine the time of concentration (T_c) by adding T_{OL} and the time of travel from the catchment to the pipe inlet (T₁).

Table 2.1 Manning's Roughness Coefficients for Common Pipe Flow

| Surface | n |
|---------------------------------------------------------|-------|
| Smooth Surfaces (concrete, asphalt, galvnl, corrugated) | 0.012 |
| Galvanized Steel | 0.014 |
| Cast Iron | 0.015 |
| Concrete | 0.016 |
| Asphalt | 0.017 |
| Clay | 0.018 |
| Stoneware | 0.019 |
| Brick | 0.020 |
| Unfinished Concrete | 0.022 |
| Weathered Masonry | 0.025 |
| Weathered Concrete | 0.030 |
| Weathered Brick | 0.035 |
| Weathered Masonry | 0.040 |
| Weathered Stone | 0.045 |
| Weathered Mortar | 0.050 |
| Weathered Plaster | 0.055 |
| Weathered Limestone | 0.060 |
| Weathered Sandstone | 0.065 |
| Weathered Granite | 0.070 |
| Weathered Slate | 0.075 |
| Weathered Shale | 0.080 |
| Weathered Sandstone | 0.085 |
| Weathered Limestone | 0.090 |
| Weathered Granite | 0.095 |
| Weathered Slate | 0.100 |
| Weathered Shale | 0.105 |
| Weathered Sandstone | 0.110 |
| Weathered Limestone | 0.115 |
| Weathered Granite | 0.120 |
| Weathered Slate | 0.125 |
| Weathered Shale | 0.130 |
| Weathered Sandstone | 0.135 |
| Weathered Limestone | 0.140 |
| Weathered Granite | 0.145 |
| Weathered Slate | 0.150 |
| Weathered Shale | 0.155 |
| Weathered Sandstone | 0.160 |
| Weathered Limestone | 0.165 |
| Weathered Granite | 0.170 |
| Weathered Slate | 0.175 |
| Weathered Shale | 0.180 |
| Weathered Sandstone | 0.185 |
| Weathered Limestone | 0.190 |
| Weathered Granite | 0.195 |
| Weathered Slate | 0.200 |
| Weathered Shale | 0.205 |
| Weathered Sandstone | 0.210 |
| Weathered Limestone | 0.215 |
| Weathered Granite | 0.220 |
| Weathered Slate | 0.225 |
| Weathered Shale | 0.230 |
| Weathered Sandstone | 0.235 |
| Weathered Limestone | 0.240 |
| Weathered Granite | 0.245 |
| Weathered Slate | 0.250 |
| Weathered Shale | 0.255 |
| Weathered Sandstone | 0.260 |
| Weathered Limestone | 0.265 |
| Weathered Granite | 0.270 |
| Weathered Slate | 0.275 |
| Weathered Shale | 0.280 |
| Weathered Sandstone | 0.285 |
| Weathered Limestone | 0.290 |
| Weathered Granite | 0.295 |
| Weathered Slate | 0.300 |
| Weathered Shale | 0.305 |
| Weathered Sandstone | 0.310 |
| Weathered Limestone | 0.315 |
| Weathered Granite | 0.320 |
| Weathered Slate | 0.325 |
| Weathered Shale | 0.330 |
| Weathered Sandstone | 0.335 |
| Weathered Limestone | 0.340 |
| Weathered Granite | 0.345 |
| Weathered Slate | 0.350 |
| Weathered Shale | 0.355 |
| Weathered Sandstone | 0.360 |
| Weathered Limestone | 0.365 |
| Weathered Granite | 0.370 |
| Weathered Slate | 0.375 |
| Weathered Shale | 0.380 |
| Weathered Sandstone | 0.385 |
| Weathered Limestone | 0.390 |
| Weathered Granite | 0.395 |
| Weathered Slate | 0.400 |
| Weathered Shale | 0.405 |
| Weathered Sandstone | 0.410 |
| Weathered Limestone | 0.415 |
| Weathered Granite | 0.420 |
| Weathered Slate | 0.425 |
| Weathered Shale | 0.430 |
| Weathered Sandstone | 0.435 |
| Weathered Limestone | 0.440 |
| Weathered Granite | 0.445 |
| Weathered Slate | 0.450 |
| Weathered Shale | 0.455 |
| Weathered Sandstone | 0.460 |
| Weathered Limestone | 0.465 |
| Weathered Granite | 0.470 |
| Weathered Slate | 0.475 |
| Weathered Shale | 0.480 |
| Weathered Sandstone | 0.485 |
| Weathered Limestone | 0.490 |
| Weathered Granite | 0.495 |
| Weathered Slate | 0.500 |
| Weathered Shale | 0.505 |
| Weathered Sandstone | 0.510 |
| Weathered Limestone | 0.515 |
| Weathered Granite | 0.520 |
| Weathered Slate | 0.525 |
| Weathered Shale | 0.530 |
| Weathered Sandstone | 0.535 |
| Weathered Limestone | 0.540 |
| Weathered Granite | 0.545 |
| Weathered Slate | 0.550 |
| Weathered Shale | 0.555 |
| Weathered Sandstone | 0.560 |
| Weathered Limestone | 0.565 |
| Weathered Granite | 0.570 |
| Weathered Slate | 0.575 |
| Weathered Shale | 0.580 |
| Weathered Sandstone | 0.585 |
| Weathered Limestone | 0.590 |
| Weathered Granite | 0.595 |
| Weathered Slate | 0.600 |
| Weathered Shale | 0.605 |
| Weathered Sandstone | 0.610 |
| Weathered Limestone | 0.615 |
| Weathered Granite | 0.620 |
| Weathered Slate | 0.625 |
| Weathered Shale | 0.630 |
| Weathered Sandstone | 0.635 |
| Weathered Limestone | 0.640 |
| Weathered Granite | 0.645 |
| Weathered Slate | 0.650 |
| Weathered Shale | 0.655 |
| Weathered Sandstone | 0.660 |
| Weathered Limestone | 0.665 |
| Weathered Granite | 0.670 |
| Weathered Slate | 0.675 |
| Weathered Shale | 0.680 |
| Weathered Sandstone | 0.685 |
| Weathered Limestone | 0.690 |
| Weathered Granite | 0.695 |
| Weathered Slate | 0.700 |
| Weathered Shale | 0.705 |
| Weathered Sandstone | 0.710 |
| Weathered Limestone | 0.715 |
| Weathered Granite | 0.720 |
| Weathered Slate | 0.725 |
| Weathered Shale | 0.730 |
| Weathered Sandstone | 0.735 |
| Weathered Limestone | 0.740 |
| Weathered Granite | 0.745 |
| Weathered Slate | 0.750 |
| Weathered Shale | 0.755 |
| Weathered Sandstone | 0.760 |
| Weathered Limestone | 0.765 |
| Weathered Granite | 0.770 |
| Weathered Slate | 0.775 |
| Weathered Shale | 0.780 |
| Weathered Sandstone | 0.785 |
| Weathered Limestone | 0.790 |
| Weathered Granite | 0.795 |
| Weathered Slate | 0.800 |
| Weathered Shale | 0.805 |
| Weathered Sandstone | 0.810 |
| Weathered Limestone | 0.815 |
| Weathered Granite | 0.820 |
| Weathered Slate | 0.825 |
| Weathered Shale | 0.830 |
| Weathered Sandstone | 0.835 |
| Weathered Limestone | 0.840 |
| Weathered Granite | 0.845 |
| Weathered Slate | 0.850 |
| Weathered Shale | 0.855 |
| Weathered Sandstone | 0.860 |
| Weathered Limestone | 0.865 |
| Weathered Granite | 0.870 |
| Weathered Slate | 0.875 |
| Weathered Shale | 0.880 |
| Weathered Sandstone | 0.885 |
| Weathered Limestone | 0.890 |
| Weathered Granite | 0.895 |
| Weathered Slate | 0.900 |
| Weathered Shale | 0.905 |
| Weathered Sandstone | 0.910 |
| Weathered Limestone | 0.915 |
| Weathered Granite | 0.920 |
| Weathered Slate | 0.925 |
| Weathered Shale | 0.930 |
| Weathered Sandstone | 0.935 |
| Weathered Limestone | 0.940 |
| Weathered Granite | 0.945 |
| Weathered Slate | 0.950 |
| Weathered Shale | 0.955 |
| Weathered Sandstone | 0.960 |
| Weathered Limestone | 0.965 |
| Weathered Granite | 0.970 |
| Weathered Slate | 0.975 |
| Weathered Shale | 0.980 |
| Weathered Sandstone | 0.985 |
| Weathered Limestone | 0.990 |
| Weathered Granite | 0.995 |
| Weathered Slate | 1.000 |



| | | |
|------------|----------------------------------------------------------------------|---------------------|
| $T_{OL} =$ | $T_t = T_{OL}$; multiply by 60 to convert hrs. to min. (L=max 300') | $T =$ |
| n= | 0.24 | D= 2594.29 (ft) |
| L= | 100 (ft) | S= 0.0104 (ft/ft) |
| $P_2 =$ | 4.89 (in) | V= 0.7 (ft/s) |
| S= | 0.0104 (ft/ft) | |
| $T_{OL} =$ | 15.00 (min) | $T_1 =$ 61.77 (min) |

$T_c = 76.76$ (min)

Intensity:

SEE FIG. 2.1-2.1a

| | |
|-------------|-------------|
| I (100-YR)= | 4.2 (in/hr) |
| I (10-YR)= | 2.6 (in/hr) |
| I (2-YR)= | 1.8 (in/hr) |

Peak Flow Rate:

$Q = CIA$

C= 0.28 Single family residential districts; lots 1/4-1/2 acre; MOSTLY golf course; and woodlands; basin slope <1%

| | | |
|------------|------------|----------|
| i (100-YR) | i (10-YR) | i (2-YR) |
| 4.2 | 2.6 | 1.8 |
| A= | 32.18 (Ac) | |

| | |
|--------------------|--------------------|
| Q (100-YR)= | 37.84 (cfs) |
| Q (10-YR)= | 23.43 (cfs) |
| Q (2-YR)= | 16.22 (cfs) |

DA#19 EXISTING CALCULATIONS

Volume (100-yr) = 1.38*area*43560 = 1934429.90 cft
 Volume (10-yr) = 0.70*area*43560 = 981232.56 cft
 Volume (2-yr) = 0.41*area*43560 = 574721.928 cft
 A = 32.18 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

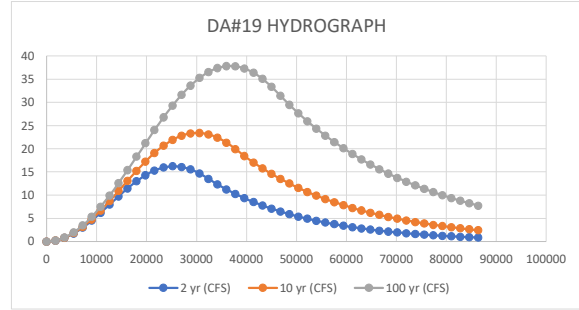
$q_i = \left(\frac{Q_p}{2}\right) \left[1 - \cos\left(\frac{\pi t_i}{T_p}\right)\right]$ $t_i \leq 1.25 T_p$
 $q_i = 1.34 Q_p e^{-1.3t_i/T_p}$ $t_i > 1.25 T_p$

| DA#19 Existing Conditions | | | |
|---------------------------|-----------|-----------|------------|
| | 2 - Year | 10 - Year | 100 - Year |
| Qp= | 16.22 | 23.43 | 37.84 |
| TP= | 25493.320 | 30132.817 | 36774.336 |
| 1.25*TP= | 31866.650 | 37666.021 | 45967.920 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) |
|----------|-------------|-------------|--------------|
| 0 | 0 | 0 | 0 |
| 1800.00 | 0.198685928 | 0.20565902 | 0.223271101 |
| 3600.00 | 0.785007779 | 0.815414403 | 0.887815362 |
| 5400.00 | 1.730234826 | 1.807854704 | 1.977950003 |
| 7200.00 | 2.988049404 | 3.148130568 | 3.467948607 |
| 9000.00 | 4.496816547 | 4.789178464 | 5.32264825 |
| 10800.00 | 6.182604208 | 6.673373303 | 7.498279316 |
| 12600.00 | 7.962806042 | 8.734551941 | 9.943498431 |
| 14400.00 | 9.750189259 | 10.90033648 | 12.60660013 |
| 16200.00 | 11.45716917 | 13.0946758 | 15.40687868 |
| 18000.00 | 13.00010097 | 15.2405161 | 18.29610786 |
| 19800.00 | 14.3033785 | 17.2625066 | 21.20010388 |
| 21600.00 | 15.30313902 | 19.08964548 | 24.05033446 |
| 23400.00 | 15.95039265 | 20.65777311 | 26.77953616 |
| 25200.00 | 16.2134229 | 21.91182498 | 29.32330171 |
| 27000.00 | 16.07934085 | 22.80776531 | 31.62160005 |
| 28800.00 | 15.55471676 | 23.3141333 | 33.62019291 |
| 30600.00 | 14.66525805 | 23.41314795 | 35.27191492 |
| 32400.00 | 13.48857375 | 23.10133238 | 36.53778659 |
| 34200.00 | 12.30559683 | 22.38963593 | 37.38793423 |
| 36000.00 | 11.22636953 | 21.30304969 | 37.80229494 |
| 37800.00 | 10.24179279 | 19.9052814 | 37.77109012 |
| 39600.00 | 9.34356554 | 18.41800825 | 37.29505616 |
| 41400.00 | 8.524114754 | 17.04186045 | 36.38542714 |
| 43200.00 | 7.776531564 | 15.768535 | 35.06366966 |
| 45000.00 | 7.094513026 | 14.59034925 | 33.36097629 |
| 46800.00 | 6.472308981 | 13.50019462 | 31.40363588 |
| 48600.00 | 5.904673568 | 12.49149364 | 29.4676292 |
| 50400.00 | 5.386821001 | 11.55816028 | 27.65097564 |
| 52200.00 | 4.914385218 | 10.69456327 | 25.94631717 |
| 54000.00 | 4.483383069 | 9.895492085 | 24.34674941 |
| 55800.00 | 4.090180735 | 9.156125512 | 22.84579361 |
| 57600.00 | 3.73146309 | 8.472002571 | 21.43737042 |
| 59400.00 | 3.404205755 | 7.838995596 | 20.11577528 |
| 61200.00 | 3.105649591 | 7.253285329 | 18.87565533 |
| 63000.00 | 2.833277445 | 6.711337878 | 17.71198769 |
| 64800.00 | 2.584792922 | 6.209883393 | 16.62005914 |
| 66600.00 | 2.358101025 | 5.74589634 | 15.59544703 |
| 68400.00 | 2.151290496 | 5.316577247 | 14.63400136 |
| 70200.00 | 1.962617694 | 4.91933581 | 13.73182798 |
| 72000.00 | 1.790491903 | 4.551775265 | 12.8852728 |
| 73800.00 | 1.633461913 | 4.211677931 | 12.090907 |
| 75600.00 | 1.490203792 | 3.896991824 | 11.34551316 |
| 77400.00 | 1.359509715 | 3.605818281 | 10.64607219 |
| 79200.00 | 1.24027779 | 3.336400501 | 9.989751156 |
| 81000.00 | 1.131502762 | 3.087112948 | 9.373891735 |
| 82800.00 | 1.032267537 | 2.856451542 | 8.795999509 |
| 84600.00 | 0.941735454 | 2.643024583 | 8.253733833 |
| 86400.00 | 0.85914323 | 2.445544355 | 7.744898361 |

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DA#20 DRAINAGE CALCULATIONS

Time of Concentration:

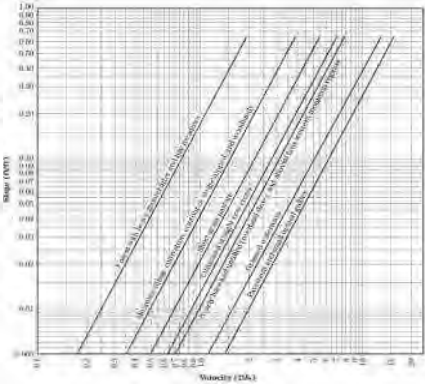
$T_c = T_{OL} + T_1 + \dots + T_n$

Section 2.1
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Table 2.11 (continued) Long-term Conditions for Gravel Shell Flow

| Surface | n |
|--------------------------------------------------------|-------|
| Smooth Surface (asphalt, concrete, gravel, surf. seal) | 0.012 |
| Polished Stone Course | 0.009 |
| Unfinished Gravel, Residual Cover in 20% | 0.008 |
| Unfinished Gravel, Residual Cover in 10% | 0.010 |
| Grass, Dense (lawn) | 0.244 |
| Grass, Sparse | 0.300 |
| Grass, Pasture | 0.325 |
| Wooded Slope (unimproved) | 0.400 |
| Wooded Slope (improved) | 0.300 |

Source: SCS TR-55 (1975), para.



| $T_{OL} =$ | $T = T_{OL}$; multiply by 60 to convert hrs. to min. (L=max 300') | $T =$ |
|------------|--------------------------------------------------------------------|---------------------|
| n= | 0.41 | D= 1316.52 (ft) |
| L= | 100 (ft) | S= 0.0202 (ft/ft) |
| $P_2 =$ | 4.89 (in) | V= 0.975 (ft/s) |
| $S =$ | 0.0202 (ft/ft) | |
| $T_{OL} =$ | 17.65 (min) | $T_1 =$ 22.50 (min) |

$T_c = 40.15$ (min)

Intensity:

SEE FIG. 2.1-2.1a

| | |
|-------------|-------------|
| I (100-YR)= | 5.8 (in/hr) |
| I (10-YR)= | 3.9 (in/hr) |
| I (2-YR)= | 2.7 (in/hr) |

Peak Flow Rate:

$Q = CIA$

C= 0.18 Lawn areas clay soil; woodlands; basin slope 1-3.5%

| i (100-YR) | i (10-YR) | i (2-YR) |
|---------------|-----------|----------|
| 5.8 | 3.9 | 2.7 |
| A= 17.12 (Ac) | | |

| | |
|--------------------|--------------------|
| Q (100-YR)= | 17.87 (cfs) |
| Q (10-YR)= | 12.02 (cfs) |
| Q (2-YR)= | 8.32 (cfs) |

DA#20 EXISTING CALCULATIONS

Volume (100-yr) = 1.38*area*43560 = 1029131.14 cft
 Volume (10-yr) = 0.70*area*43560 = 522023.04 cft
 Volume (2-yr) = 0.41*area*43560 = 305756.352 cft
 A = 17.12 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

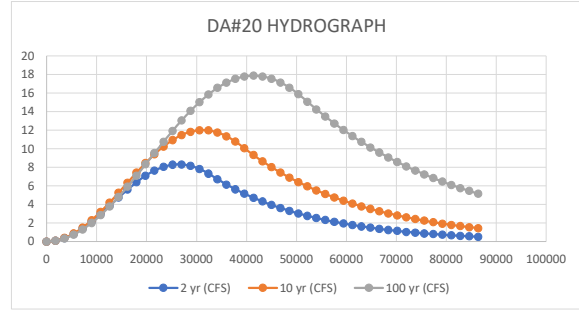
$q_i = \left(\frac{Q_p}{2}\right) \left[1 - \cos\left(\frac{\pi t_i}{T_p}\right)\right]$ $t_i \leq 1.25 T_p$
 $q_i = 1.34 Q_p e^{-1.3 t_i / T_p}$ $t_i > 1.25 T_p$

| DA#20 Existing Conditions | | | |
|---------------------------|-----------|-----------|------------|
| | 2 - Year | 10 - Year | 100 - Year |
| Qp= | 8.32 | 12.02 | 17.87 |
| TP= | 26437.517 | 31248.847 | 41423.964 |
| 1.25*TP= | 33046.896 | 39061.059 | 51779.955 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) |
|----------|-------------|-------------|--------------|
| 0 | 0 | 0 | 0 |
| 1800.00 | 0.094804085 | 0.098123301 | 0.083140218 |
| 3600.00 | 0.374895441 | 0.389288679 | 0.331013916 |
| 5400.00 | 0.827508308 | 0.86398722 | 0.739009009 |
| 7200.00 | 1.432013887 | 1.506716157 | 1.299534097 |
| 9000.00 | 2.160860548 | 2.296485169 | 2.002159717 |
| 10800.00 | 2.980829547 | 3.207501879 | 2.833812399 |
| 12600.00 | 3.854549049 | 4.210014188 | 3.77901792 |
| 14400.00 | 4.742197422 | 5.271281922 | 4.820189223 |
| 16200.00 | 5.603318197 | 6.356646065 | 5.937953656 |
| 18000.00 | 6.398663958 | 7.430660659 | 7.11151343 |
| 19800.00 | 7.091985124 | 8.458250397 | 8.319032594 |
| 21600.00 | 7.651682103 | 9.405856125 | 9.538043329 |
| 23400.00 | 8.052245511 | 10.24253082 | 10.745864 |
| 25200.00 | 8.275418817 | 10.94095024 | 11.92002116 |
| 27000.00 | 8.311030419 | 11.47830533 | 13.03866777 |
| 28800.00 | 8.157457245 | 11.83704707 | 14.08098961 |
| 30600.00 | 7.821698718 | 12.00545963 | 15.02759262 |
| 32400.00 | 7.31905775 | 11.97804298 | 15.86086375 |
| 34200.00 | 6.718561005 | 11.75569248 | 16.56529865 |
| 36000.00 | 6.14945471 | 11.34566969 | 17.1277902 |
| 37800.00 | 5.628555461 | 10.76136519 | 17.53787233 |
| 39600.00 | 5.151779803 | 10.04303204 | 17.78791483 |
| 41400.00 | 4.715390178 | 9.318449964 | 17.87326524 |
| 43200.00 | 4.315965624 | 8.646144848 | 17.79233549 |
| 45000.00 | 3.950374957 | 8.022345027 | 17.54663141 |
| 46800.00 | 3.615752222 | 7.443550955 | 17.14072471 |
| 48600.00 | 3.309474234 | 6.906515567 | 16.58216793 |
| 50400.00 | 3.029140005 | 6.40822607 | 15.88135391 |
| 52200.00 | 2.772551929 | 5.945887034 | 15.07441643 |
| 54000.00 | 2.53769855 | 5.516904716 | 14.24648187 |
| 55800.00 | 2.322738796 | 5.118872502 | 13.4640201 |
| 57600.00 | 2.125987547 | 4.749557414 | 12.72453359 |
| 59400.00 | 1.945902422 | 4.406887575 | 12.02566202 |
| 61200.00 | 1.781071692 | 4.088940591 | 11.36517469 |
| 63000.00 | 1.630203208 | 3.793932764 | 10.7409634 |
| 64800.00 | 1.492114277 | 3.520209085 | 10.15103577 |
| 66600.00 | 1.365722387 | 3.266233951 | 9.593508827 |
| 68400.00 | 1.25003672 | 3.030582549 | 9.066603025 |
| 70200.00 | 1.14415039 | 2.811932864 | 8.568636554 |
| 72000.00 | 1.047233329 | 2.60905826 | 8.098019974 |
| 73800.00 | 0.95852578 | 2.4208206 | 7.653251143 |
| 75600.00 | 0.877332344 | 2.246163862 | 7.23291042 |
| 77400.00 | 0.803016525 | 2.084108213 | 6.835656138 |
| 79200.00 | 0.734995746 | 1.933744513 | 6.460220315 |
| 81000.00 | 0.672736773 | 1.794229214 | 6.105404613 |
| 82800.00 | 0.615751545 | 1.66477963 | 5.770076511 |
| 84600.00 | 0.56359334 | 1.54466954 | 5.453165686 |
| 86400.00 | 0.515853278 | 1.433225122 | 5.153660605 |

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DA#21 EXISTING CALCULATIONS

Volume (100-yr) = 1.38*area*43560 = 951585.62 cft
 Volume (10-yr) = 0.70*area*43560 = 482688.36 cft
 Volume (2-yr) = 0.41*area*43560 = 282717.468 cft
 A = 15.83 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

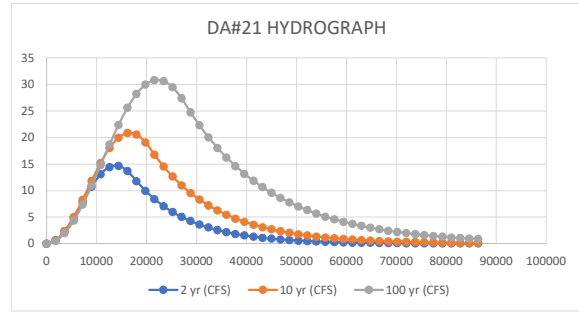
$q_i = \left(\frac{Q_p}{2}\right) \left[1 - \cos\left(\frac{\pi t_i}{T_p}\right)\right]$ $t_i \leq 1.25 T_p$
 $q_i = 4.34 Q_p e^{-1.3t_i/T_p}$ $t_i > 1.25 T_p$

| DA#21 Existing Conditions | | | |
|---------------------------|-----------|-----------|------------|
| | 2 - Year | 10 - Year | 100 - Year |
| Qp= | 14.72 | 20.90 | 30.87 |
| TP= | 13815.735 | 16618.705 | 22177.753 |
| 1.25*TP= | 17269.668 | 20773.381 | 27722.191 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) |
|----------|-------------|-------------|--------------|
| 0 | 0 | 0 | 0 |
| 1800.00 | 0.608035604 | 0.599033099 | 0.49901198 |
| 3600.00 | 2.331691444 | 2.327440299 | 1.963780341 |
| 5400.00 | 4.886209676 | 4.987022338 | 4.299588855 |
| 7200.00 | 7.849569221 | 8.272800622 | 7.355397279 |
| 9000.00 | 10.73220606 | 11.80798962 | 10.93360806 |
| 10800.00 | 13.05789205 | 15.18720346 | 14.80284358 |
| 12600.00 | 14.44241049 | 18.02294221 | 18.71290769 |
| 14400.00 | 14.657031 | 19.9900271 | 22.41096416 |
| 16200.00 | 13.66629703 | 20.8628893 | 25.65788579 |
| 18000.00 | 11.74572689 | 20.54143629 | 28.24371708 |
| 19800.00 | 9.915680597 | 19.06252961 | 30.0012506 |
| 21600.00 | 8.370765186 | 16.73915559 | 30.81683904 |
| 23400.00 | 7.06655756 | 14.54061002 | 30.63774408 |
| 25200.00 | 5.965549044 | 12.6308247 | 29.47554651 |
| 27000.00 | 5.036084993 | 10.97187342 | 27.40539744 |
| 28800.00 | 4.251436351 | 9.530811267 | 24.76502485 |
| 30600.00 | 3.589040112 | 8.279020356 | 22.28516545 |
| 32400.00 | 3.029848705 | 7.191641523 | 20.05362813 |
| 34200.00 | 2.557782273 | 6.247080642 | 18.04554703 |
| 36000.00 | 2.159266285 | 5.42657979 | 16.23854624 |
| 37800.00 | 1.822841193 | 4.713844738 | 14.61249047 |
| 39600.00 | 1.538832907 | 4.094721368 | 13.14926068 |
| 41400.00 | 1.299074612 | 3.55691458 | 11.83255222 |
| 43200.00 | 1.096671926 | 3.089744135 | 10.64769309 |
| 45000.00 | 0.925804647 | 2.68393255 | 9.581480475 |
| 46800.00 | 0.781559393 | 2.331420862 | 8.622033649 |
| 48600.00 | 0.659788311 | 2.025208582 | 7.75866156 |
| 50400.00 | 0.556989808 | 1.759214678 | 6.981743711 |
| 52200.00 | 0.470207854 | 1.528156809 | 6.282622959 |
| 54000.00 | 0.396946986 | 1.327446424 | 5.653509048 |
| 55800.00 | 0.335100549 | 1.153097638 | 5.087391805 |
| 57600.00 | 0.282890114 | 1.001648081 | 4.577963024 |
| 59400.00 | 0.23881434 | 0.870090134 | 4.119546175 |
| 61200.00 | 0.201605804 | 0.755811204 | 3.70703315 |
| 63000.00 | 0.170194555 | 0.656541837 | 3.335827343 |
| 64800.00 | 0.143677344 | 0.570310657 | 3.001792435 |
| 66600.00 | 0.121291655 | 0.495405208 | 2.701206296 |
| 68400.00 | 0.102393775 | 0.430337952 | 2.430719515 |
| 70200.00 | 0.086440284 | 0.373816726 | 2.187318078 |
| 72000.00 | 0.072972431 | 0.324719082 | 1.968289777 |
| 73800.00 | 0.061602941 | 0.282069995 | 1.771193996 |
| 75600.00 | 0.052004877 | 0.245022503 | 1.59383451 |
| 77400.00 | 0.043902243 | 0.212840884 | 1.434235013 |
| 79200.00 | 0.037062041 | 0.184886046 | 1.2906171 |
| 81000.00 | 0.03128758 | 0.160602838 | 1.161380446 |
| 82800.00 | 0.026412809 | 0.139509022 | 1.045084975 |
| 84600.00 | 0.022297554 | 0.1211857 | 0.940434815 |
| 86400.00 | 0.018823477 | 0.10526899 | 0.846263857 |

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DA#22 EXISTING CALCULATIONS

Volume (100-yr) = 1.38*area*43560 = 3064550.54 cft
 Volume (10-yr) = 0.70*area*43560 = 1554482.16 cft
 Volume (2-yr) = 0.41*area*43560 = 910482.408 cft
 A = 50.98 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

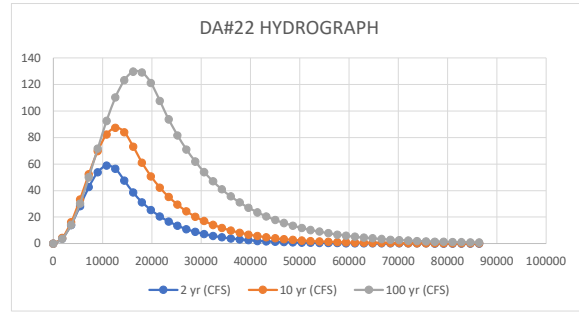
$q_i = \left(\frac{Q_p}{2}\right) \left[1 - \cos\left(\frac{\pi t_i}{T_p}\right)\right]$ $t_i \leq 1.25 T_p$
 $q_i = 4.34 Q_p e^{-1.3t_i/T_p}$ $t_i > 1.25 T_p$

| DA#22 Existing Conditions | | | |
|---------------------------|-----------|-----------|------------|
| | 2 - Year | 10 - Year | 100 - Year |
| Qp= | 58.88 | 87.43 | 130.25 |
| TP= | 11124.358 | 12791.073 | 16926.270 |
| 1.25*TP= | 13905.447 | 15988.842 | 21157.837 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) |
|----------|-------------|-------------|--------------|
| 0 | 0 | 0 | 0 |
| 1800.00 | 3.722584919 | 4.202906209 | 3.600889147 |
| 3600.00 | 13.94895439 | 16.0034684 | 14.00536804 |
| 5400.00 | 28.09301465 | 33.13261377 | 30.062903 |
| 7200.00 | 42.57794732 | 52.29666211 | 49.9978419 |
| 9000.00 | 53.74073256 | 69.81065161 | 71.6057669 |
| 10800.00 | 58.75847126 | 82.30690225 | 92.49726033 |
| 12600.00 | 56.36225337 | 87.38257066 | 110.362128 |
| 14400.00 | 47.49451827 | 84.06168122 | 123.2248617 |
| 16200.00 | 38.48486609 | 73.13156533 | 129.6630926 |
| 18000.00 | 31.18433395 | 60.90528796 | 128.964877 |
| 19800.00 | 25.26870384 | 50.72302343 | 121.2074241 |
| 21600.00 | 20.47526155 | 42.24304969 | 107.5978015 |
| 23400.00 | 16.59112941 | 35.18077446 | 93.7051892 |
| 25200.00 | 13.4438124 | 29.29918414 | 81.60633734 |
| 27000.00 | 10.89353759 | 24.40088954 | 71.06964247 |
| 28800.00 | 8.8270468 | 20.32150135 | 61.89340492 |
| 30600.00 | 7.15256679 | 16.92411322 | 53.90196769 |
| 32400.00 | 5.795733596 | 14.09470705 | 46.94235395 |
| 34200.00 | 4.696290003 | 11.7383265 | 40.88133864 |
| 36000.00 | 3.805409519 | 9.775890239 | 35.6028982 |
| 37800.00 | 3.083527976 | 8.14153789 | 31.00598959 |
| 39600.00 | 2.498586481 | 6.780419746 | 27.00261605 |
| 41400.00 | 2.024607673 | 5.646855982 | 23.51614263 |
| 43200.00 | 1.640542068 | 4.702803613 | 20.47982918 |
| 45000.00 | 1.329333239 | 3.916579755 | 17.83555279 |
| 46800.00 | 1.077160345 | 3.261798332 | 15.53269515 |
| 48600.00 | 0.872824342 | 2.716484541 | 13.52717358 |
| 50400.00 | 0.707250629 | 2.262337371 | 11.78059721 |
| 52200.00 | 0.573086047 | 1.884115408 | 10.25953203 |
| 54000.00 | 0.464372323 | 1.569125328 | 8.93486091 |
| 55800.00 | 0.37628146 | 1.306795903 | 7.781226202 |
| 57600.00 | 0.304901326 | 1.088323222 | 6.776544349 |
| 59400.00 | 0.247061917 | 0.906375228 | 5.901583134 |
| 61200.00 | 0.200194572 | 0.754845654 | 5.139593529 |
| 63000.00 | 0.162217906 | 0.628649089 | 4.475989077 |
| 64800.00 | 0.131445367 | 0.523550311 | 3.898066667 |
| 66600.00 | 0.106510342 | 0.436022152 | 3.394763365 |
| 68400.00 | 0.08630546 | 0.36312712 | 2.95644464 |
| 70200.00 | 0.069933419 | 0.302418822 | 2.574719934 |
| 72000.00 | 0.056667135 | 0.251859855 | 2.242282048 |
| 73800.00 | 0.045917449 | 0.209753434 | 1.952767256 |
| 75600.00 | 0.037206965 | 0.174686447 | 1.700633495 |
| 77400.00 | 0.030148849 | 0.145482027 | 1.481054271 |
| 79200.00 | 0.024429649 | 0.121160059 | 1.289826268 |
| 81000.00 | 0.019795374 | 0.100904284 | 1.123288885 |
| 82800.00 | 0.016040216 | 0.08403491 | 0.978254166 |
| 84600.00 | 0.012997407 | 0.06998579 | 0.851945769 |
| 86400.00 | 0.010531814 | 0.05828543 | 0.741945824 |

ti (hrs)

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DA#23 DRAINAGE CALCULATIONS

Time of Concentration:

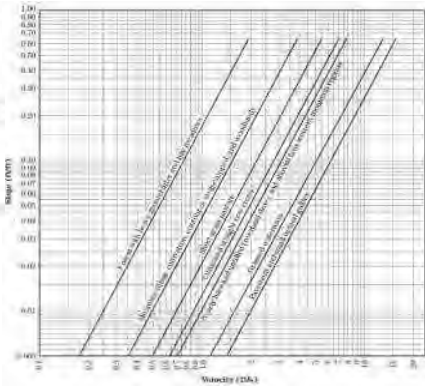
$T_c = T_{OL} + T_1 + \dots + T_n$

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Table 2.1 (continued) Long-term Conditions for Gravel Shell Flow

| Surface | n |
|-------------------------------------------------------|-------|
| Asphalt Surface (asphalt, asphalt gravel, surf. seal) | 0.012 |
| Polished Stone Course | 0.009 |
| Concrete Slab, Residue Cover in 20% | 0.008 |
| Concrete Slab, Residue Cover in 50% | 0.010 |
| Grass, Short (3-6 in) | 0.20 |
| Grass, Dense (6-12 in) | 0.25 |
| Grass, Shrubland (12-36 in) | 0.30 |
| Grass, Pasture (36-72 in) | 0.35 |
| Grass, Tall (72-144 in) | 0.40 |
| Grass, Very Tall (144-360 in) | 0.50 |
| Wooded Slope (unimproved) | 0.40 |
| Wooded Slope (improved) | 0.30 |

Source: SCS TR-55 (1975, 1980)



| | | |
|------------|-----------------------------------------------------------------------------|-------------|
| $T_{OL} =$ | $T_t = T_{OL}$; multiply by 60 to convert hrs. to min. ($L = \max 300'$) | $T =$ |
| $n =$ | 0.8 | $D =$ |
| $L =$ | 100 (ft) | $S =$ |
| $P_2 =$ | 4.89 (in) | $V =$ |
| $S =$ | 0.0081 (ft/ft) | |
| $T_{OL} =$ | 43.42 (min) | $T_1 =$ |
| | | 45.07 (min) |

$T_c = 88.48$ (min)

Intensity:

SEE FIG. 2.1-2.1a

| | |
|---------------|-------------|
| I (100-YR)= | 3.9 (in/hr) |
| I (10-YR)= | 2.5 (in/hr) |
| I (2-YR)= | 1.6 (in/hr) |

Peak Flow Rate:

$Q = CIA$

$C =$ 0.18 Woodlands; basin slope <1%

| | | |
|--------------|-------------|------------|
| i (100-YR) | i (10-YR) | i (2-YR) |
| 3.9 | 2.5 | 1.6 |
| $A =$ | 13.48 (Ac) | |

| | |
|---------------|------------|
| Q (100-YR)= | 9.46 (cfs) |
| Q (10-YR)= | 6.07 (cfs) |
| Q (2-YR)= | 3.88 (cfs) |

DA#23 EXISTING CALCULATIONS

Volume (100-yr) = 1.38*area*43560 = 810320.54 cft
 Volume (10-yr) = 0.70*area*43560 = 411032.16 cft
 Volume (2-yr) = 0.41*area*43560 = 240747.408 cft
 A = 13.48 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

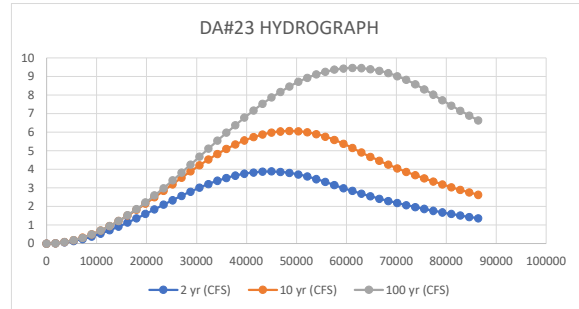
$q_i = \left(\frac{Q_p}{2}\right) \left[1 - \cos\left(\frac{\pi t_i}{T_p}\right)\right]$ $t_i \leq 1.25 T_p$
 $q_i = 1.34 Q_p e^{-1.3t_i/T_p}$ $t_i > 1.25 T_p$

| DA#23 Existing Conditions | | | |
|---------------------------|-----------|-----------|------------|
| | 2 - Year | 10 - Year | 100 - Year |
| Qp= | 3.88 | 6.07 | 9.46 |
| TP= | 44613.309 | 48748.201 | 61604.870 |
| 1.25*TP= | 55766.637 | 60935.252 | 77006.087 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) |
|----------|-------------|-------------|--------------|
| 0 | 0 | 0 | 0 |
| 1800.00 | 0.015572442 | 0.020383695 | 0.019919421 |
| 3600.00 | 0.062039912 | 0.081260798 | 0.079509964 |
| 5400.00 | 0.138656848 | 0.181813043 | 0.178269879 |
| 7200.00 | 0.244193948 | 0.320688888 | 0.315367613 |
| 9000.00 | 0.376957888 | 0.496021639 | 0.489648808 |
| 10800.00 | 0.534818498 | 0.705454625 | 0.699646025 |
| 12600.00 | 0.715242936 | 0.946172791 | 0.943591097 |
| 14400.00 | 0.915336328 | 1.214940578 | 1.219430019 |
| 16200.00 | 1.131888215 | 1.508145404 | 1.524840238 |
| 18000.00 | 1.361424066 | 1.821846222 | 1.857250216 |
| 19800.00 | 1.600261022 | 2.151826492 | 2.213861075 |
| 21600.00 | 1.844566992 | 2.493650859 | 2.59167017 |
| 23400.00 | 2.090422137 | 2.842724766 | 2.987496363 |
| 25200.00 | 2.333881758 | 3.194356216 | 3.398006818 |
| 27000.00 | 2.571039595 | 3.543818832 | 3.819745056 |
| 28800.00 | 2.798090498 | 3.88641539 | 4.249160059 |
| 30600.00 | 3.011391479 | 4.217540957 | 4.682636175 |
| 32400.00 | 3.207520167 | 4.532744782 | 5.116523552 |
| 34200.00 | 3.383329716 | 4.827790123 | 5.547168881 |
| 36000.00 | 3.535999297 | 5.098711194 | 5.970946148 |
| 37800.00 | 3.663079357 | 5.341866471 | 6.384287166 |
| 39600.00 | 3.762530922 | 5.553987635 | 6.783711626 |
| 41400.00 | 3.83275831 | 5.732223509 | 7.165856389 |
| 43200.00 | 3.872634738 | 5.874178374 | 7.527503817 |
| 45000.00 | 3.881520396 | 5.977944175 | 7.865608853 |
| 46800.00 | 3.859272715 | 6.042126169 | 8.17732467 |
| 48600.00 | 3.806248656 | 6.065861667 | 8.460026634 |
| 50400.00 | 3.723298978 | 6.048831633 | 8.711334409 |
| 52200.00 | 3.611754592 | 5.991264974 | 8.929131993 |
| 54000.00 | 3.473405207 | 5.893935458 | 9.111585543 |
| 55800.00 | 3.314525485 | 5.758151318 | 9.257158806 |
| 57600.00 | 3.145156832 | 5.585737667 | 9.364626064 |
| 59400.00 | 2.984442734 | 5.379011963 | 9.433082447 |
| 61200.00 | 2.831940951 | 5.147512277 | 9.461951555 |
| 63000.00 | 2.687231844 | 4.906259181 | 9.450990311 |
| 64800.00 | 2.549917215 | 4.676313112 | 9.40029101 |
| 66600.00 | 2.419619214 | 4.457144133 | 9.310280536 |
| 68400.00 | 2.2959793 | 4.248247144 | 9.181716773 |
| 70200.00 | 2.178657251 | 4.049140717 | 9.015682224 |
| 72000.00 | 2.067330231 | 3.859365992 | 8.81357489 |
| 73800.00 | 1.961691901 | 3.678485609 | 8.577096506 |
| 75600.00 | 1.861451576 | 3.50608271 | 8.308238209 |
| 77400.00 | 1.766333421 | 3.341759973 | 8.02069968 |
| 79200.00 | 1.676075702 | 3.185138698 | 7.721148605 |
| 81000.00 | 1.590430054 | 3.035857933 | 7.433368538 |
| 82800.00 | 1.509160805 | 2.893573644 | 7.156314514 |
| 84600.00 | 1.432044327 | 2.757957922 | 6.889586755 |
| 86400.00 | 1.358868417 | 2.628698223 | 6.632800384 |

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DA#24 DRAINAGE CALCULATIONS

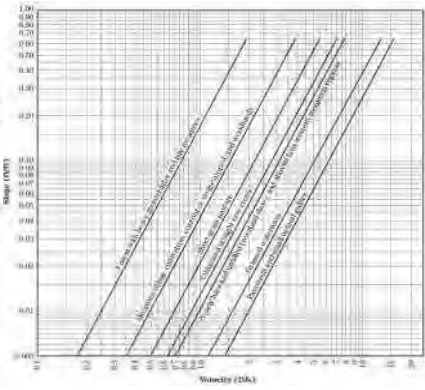
Time of Concentration:

$T_c = T_{OL} + T_1 + \dots + T_n$

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Table 2.1 Manning's Roughness Coefficients for Gravel and Shell Flow

| Surface | n |
|---------------------------------------------------------|-------|
| Smooth Surface (sandstone, asphalt, gravel, surf, well) | 0.012 |
| Polished metal | 0.009 |
| Concrete (smooth) | 0.012 |
| Concrete (rough) | 0.015 |
| Concrete (very rough) | 0.018 |
| Concrete (extremely rough) | 0.022 |
| Concrete (open channel) | 0.025 |
| Concrete (rough) | 0.030 |
| Concrete (very rough) | 0.035 |
| Concrete (extremely rough) | 0.040 |
| Concrete (open channel) | 0.045 |
| Concrete (rough) | 0.050 |
| Concrete (very rough) | 0.055 |
| Concrete (extremely rough) | 0.060 |
| Concrete (open channel) | 0.065 |
| Concrete (rough) | 0.070 |
| Concrete (very rough) | 0.075 |
| Concrete (extremely rough) | 0.080 |
| Concrete (open channel) | 0.085 |
| Concrete (rough) | 0.090 |
| Concrete (very rough) | 0.095 |
| Concrete (extremely rough) | 0.100 |
| Concrete (open channel) | 0.105 |
| Concrete (rough) | 0.110 |
| Concrete (very rough) | 0.115 |
| Concrete (extremely rough) | 0.120 |
| Concrete (open channel) | 0.125 |
| Concrete (rough) | 0.130 |
| Concrete (very rough) | 0.135 |
| Concrete (extremely rough) | 0.140 |
| Concrete (open channel) | 0.145 |
| Concrete (rough) | 0.150 |
| Concrete (very rough) | 0.155 |
| Concrete (extremely rough) | 0.160 |
| Concrete (open channel) | 0.165 |
| Concrete (rough) | 0.170 |
| Concrete (very rough) | 0.175 |
| Concrete (extremely rough) | 0.180 |
| Concrete (open channel) | 0.185 |
| Concrete (rough) | 0.190 |
| Concrete (very rough) | 0.195 |
| Concrete (extremely rough) | 0.200 |
| Concrete (open channel) | 0.205 |
| Concrete (rough) | 0.210 |
| Concrete (very rough) | 0.215 |
| Concrete (extremely rough) | 0.220 |
| Concrete (open channel) | 0.225 |
| Concrete (rough) | 0.230 |
| Concrete (very rough) | 0.235 |
| Concrete (extremely rough) | 0.240 |
| Concrete (open channel) | 0.245 |
| Concrete (rough) | 0.250 |
| Concrete (very rough) | 0.255 |
| Concrete (extremely rough) | 0.260 |
| Concrete (open channel) | 0.265 |
| Concrete (rough) | 0.270 |
| Concrete (very rough) | 0.275 |
| Concrete (extremely rough) | 0.280 |
| Concrete (open channel) | 0.285 |
| Concrete (rough) | 0.290 |
| Concrete (very rough) | 0.295 |
| Concrete (extremely rough) | 0.300 |
| Concrete (open channel) | 0.305 |
| Concrete (rough) | 0.310 |
| Concrete (very rough) | 0.315 |
| Concrete (extremely rough) | 0.320 |
| Concrete (open channel) | 0.325 |
| Concrete (rough) | 0.330 |
| Concrete (very rough) | 0.335 |
| Concrete (extremely rough) | 0.340 |
| Concrete (open channel) | 0.345 |
| Concrete (rough) | 0.350 |
| Concrete (very rough) | 0.355 |
| Concrete (extremely rough) | 0.360 |
| Concrete (open channel) | 0.365 |
| Concrete (rough) | 0.370 |
| Concrete (very rough) | 0.375 |
| Concrete (extremely rough) | 0.380 |
| Concrete (open channel) | 0.385 |
| Concrete (rough) | 0.390 |
| Concrete (very rough) | 0.395 |
| Concrete (extremely rough) | 0.400 |
| Concrete (open channel) | 0.405 |
| Concrete (rough) | 0.410 |
| Concrete (very rough) | 0.415 |
| Concrete (extremely rough) | 0.420 |
| Concrete (open channel) | 0.425 |
| Concrete (rough) | 0.430 |
| Concrete (very rough) | 0.435 |
| Concrete (extremely rough) | 0.440 |
| Concrete (open channel) | 0.445 |
| Concrete (rough) | 0.450 |
| Concrete (very rough) | 0.455 |
| Concrete (extremely rough) | 0.460 |
| Concrete (open channel) | 0.465 |
| Concrete (rough) | 0.470 |
| Concrete (very rough) | 0.475 |
| Concrete (extremely rough) | 0.480 |
| Concrete (open channel) | 0.485 |
| Concrete (rough) | 0.490 |
| Concrete (very rough) | 0.495 |
| Concrete (extremely rough) | 0.500 |
| Concrete (open channel) | 0.505 |
| Concrete (rough) | 0.510 |
| Concrete (very rough) | 0.515 |
| Concrete (extremely rough) | 0.520 |
| Concrete (open channel) | 0.525 |
| Concrete (rough) | 0.530 |
| Concrete (very rough) | 0.535 |
| Concrete (extremely rough) | 0.540 |
| Concrete (open channel) | 0.545 |
| Concrete (rough) | 0.550 |
| Concrete (very rough) | 0.555 |
| Concrete (extremely rough) | 0.560 |
| Concrete (open channel) | 0.565 |
| Concrete (rough) | 0.570 |
| Concrete (very rough) | 0.575 |
| Concrete (extremely rough) | 0.580 |
| Concrete (open channel) | 0.585 |
| Concrete (rough) | 0.590 |
| Concrete (very rough) | 0.595 |
| Concrete (extremely rough) | 0.600 |
| Concrete (open channel) | 0.605 |
| Concrete (rough) | 0.610 |
| Concrete (very rough) | 0.615 |
| Concrete (extremely rough) | 0.620 |
| Concrete (open channel) | 0.625 |
| Concrete (rough) | 0.630 |
| Concrete (very rough) | 0.635 |
| Concrete (extremely rough) | 0.640 |
| Concrete (open channel) | 0.645 |
| Concrete (rough) | 0.650 |
| Concrete (very rough) | 0.655 |
| Concrete (extremely rough) | 0.660 |
| Concrete (open channel) | 0.665 |
| Concrete (rough) | 0.670 |
| Concrete (very rough) | 0.675 |
| Concrete (extremely rough) | 0.680 |
| Concrete (open channel) | 0.685 |
| Concrete (rough) | 0.690 |
| Concrete (very rough) | 0.695 |
| Concrete (extremely rough) | 0.700 |
| Concrete (open channel) | 0.705 |
| Concrete (rough) | 0.710 |
| Concrete (very rough) | 0.715 |
| Concrete (extremely rough) | 0.720 |
| Concrete (open channel) | 0.725 |
| Concrete (rough) | 0.730 |
| Concrete (very rough) | 0.735 |
| Concrete (extremely rough) | 0.740 |
| Concrete (open channel) | 0.745 |
| Concrete (rough) | 0.750 |
| Concrete (very rough) | 0.755 |
| Concrete (extremely rough) | 0.760 |
| Concrete (open channel) | 0.765 |
| Concrete (rough) | 0.770 |
| Concrete (very rough) | 0.775 |
| Concrete (extremely rough) | 0.780 |
| Concrete (open channel) | 0.785 |
| Concrete (rough) | 0.790 |
| Concrete (very rough) | 0.795 |
| Concrete (extremely rough) | 0.800 |
| Concrete (open channel) | 0.805 |
| Concrete (rough) | 0.810 |
| Concrete (very rough) | 0.815 |
| Concrete (extremely rough) | 0.820 |
| Concrete (open channel) | 0.825 |
| Concrete (rough) | 0.830 |
| Concrete (very rough) | 0.835 |
| Concrete (extremely rough) | 0.840 |
| Concrete (open channel) | 0.845 |
| Concrete (rough) | 0.850 |
| Concrete (very rough) | 0.855 |
| Concrete (extremely rough) | 0.860 |
| Concrete (open channel) | 0.865 |
| Concrete (rough) | 0.870 |
| Concrete (very rough) | 0.875 |
| Concrete (extremely rough) | 0.880 |
| Concrete (open channel) | 0.885 |
| Concrete (rough) | 0.890 |
| Concrete (very rough) | 0.895 |
| Concrete (extremely rough) | 0.900 |
| Concrete (open channel) | 0.905 |
| Concrete (rough) | 0.910 |
| Concrete (very rough) | 0.915 |
| Concrete (extremely rough) | 0.920 |
| Concrete (open channel) | 0.925 |
| Concrete (rough) | 0.930 |
| Concrete (very rough) | 0.935 |
| Concrete (extremely rough) | 0.940 |
| Concrete (open channel) | 0.945 |
| Concrete (rough) | 0.950 |
| Concrete (very rough) | 0.955 |
| Concrete (extremely rough) | 0.960 |
| Concrete (open channel) | 0.965 |
| Concrete (rough) | 0.970 |
| Concrete (very rough) | 0.975 |
| Concrete (extremely rough) | 0.980 |
| Concrete (open channel) | 0.985 |
| Concrete (rough) | 0.990 |
| Concrete (very rough) | 0.995 |
| Concrete (extremely rough) | 1.000 |



| | | |
|------------|--------------------------------------------------------------------------|------------|
| $T_{OL} =$ | $Tt = T_0t$; multiply by 60 to convert hrs. to min. ($L = \max 300'$) | $T =$ |
| $n =$ | 0.8 | $D =$ |
| $L =$ | 100 (ft) | $S =$ |
| $P_2 =$ | 4.89 (in) | $V =$ |
| $S =$ | 0.0280 (ft/ft) | |
| $T_{OL} =$ | 26.44 (min) | $T_1 =$ |
| | | 6.87 (min) |

$T_c = 33.30$ (min)

Intensity:

SEE FIG. 2.1-2.1a

| | |
|---------------|-------------|
| I (100-YR)= | 6.4 (in/hr) |
| I (10-YR)= | 4.3 (in/hr) |
| I (2-YR)= | 3 (in/hr) |

Peak Flow Rate:

$Q = CIA$

$C =$ 0.2 Woodlands; basin slope 1-3.5%

| i (100-YR) | i (10-YR) | i (2-YR) |
|--------------|-------------|------------|
| 6.4 | 4.3 | 3 |

$A =$ 7.98 (Ac)

| | |
|---------------|-------------|
| Q (100-YR)= | 10.21 (cfs) |
| Q (10-YR)= | 6.86 (cfs) |
| Q (2-YR)= | 4.79 (cfs) |

DA#24 EXISTING CALCULATIONS

Volume (100-yr) = 1.38*area*43560 = 479700.14 cft
 Volume (10-yr) = 0.70*area*43560 = 243326.16 cft
 Volume (2-yr) = 0.41*area*43560 = 142519.608 cft
 A = 7.98 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

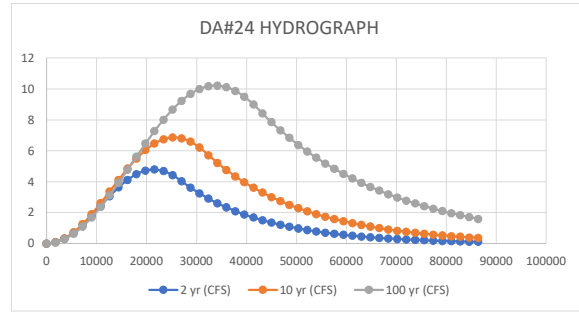
$q_i = \left(\frac{Q_p}{2}\right) \left[1 - \cos\left(\frac{\pi t_i}{T_p}\right)\right]$ $t_i \leq 1.25 T_p$
 $q_i = 1.34 Q_p e^{-1.3t_i/T_p}$ $t_i > 1.25 T_p$

| DA#24 Existing Conditions | | | |
|---------------------------|-----------|-----------|------------|
| | 2 - Year | 10 - Year | 100 - Year |
| Qp= | 4.79 | 6.86 | 10.21 |
| TP= | 21414.388 | 25507.780 | 33786.421 |
| 1.25*TP= | 26767.986 | 31884.725 | 42233.026 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) |
|----------|-------------|-------------|--------------|
| 0 | 0 | 0 | 0 |
| 1800.00 | 0.082985534 | 0.083977194 | 0.071367287 |
| 3600.00 | 0.326188919 | 0.331798402 | 0.283474595 |
| 5400.00 | 0.712749369 | 0.731333689 | 0.63039401 |
| 7200.00 | 1.215867446 | 1.263027274 | 1.102429926 |
| 9000.00 | 1.800663017 | 1.900854715 | 1.686390018 |
| 10800.00 | 2.426593413 | 2.61359671 | 2.365953934 |
| 12600.00 | 3.050264175 | 3.366367162 | 3.122129417 |
| 14400.00 | 3.628437499 | 4.122320732 | 3.933783088 |
| 16200.00 | 4.121029825 | 4.844456278 | 4.778231082 |
| 18000.00 | 4.493890747 | 5.497427925 | 5.631873005 |
| 19800.00 | 4.721170588 | 6.049275117 | 6.470851516 |
| 21600.00 | 4.787112506 | 6.472986966 | 7.271719082 |
| 23400.00 | 4.687144885 | 6.747824339 | 8.012093284 |
| 25200.00 | 4.428198273 | 6.860334959 | 8.671282355 |
| 27000.00 | 4.03458027 | 6.805011846 | 9.230863464 |
| 28800.00 | 3.616945734 | 6.584562862 | 9.6751976 |
| 30600.00 | 3.242542115 | 6.209778172 | 9.991866637 |
| 32400.00 | 2.906894419 | 5.712912416 | 10.1720204 |
| 34200.00 | 2.605990876 | 5.212148919 | 10.210624 |
| 36000.00 | 2.336234986 | 4.755279684 | 10.10659856 |
| 37800.00 | 2.09440254 | 4.338457176 | 9.862851346 |
| 39600.00 | 1.877603078 | 3.95817111 | 9.486194542 |
| 41400.00 | 1.683245341 | 3.611218896 | 8.987154843 |
| 43200.00 | 1.509006303 | 3.294678668 | 8.410379394 |
| 45000.00 | 1.352803401 | 3.00588467 | 7.847601874 |
| 46800.00 | 1.212769647 | 2.742404818 | 7.32248241 |
| 48600.00 | 1.087231312 | 2.502020207 | 6.832501127 |
| 50400.00 | 0.974687921 | 2.282706432 | 6.375306765 |
| 52200.00 | 0.873794319 | 2.082616535 | 5.9487054 |
| 54000.00 | 0.783344592 | 1.900065454 | 5.550649912 |
| 55800.00 | 0.702257655 | 1.733515829 | 5.179230165 |
| 57600.00 | 0.629564331 | 1.581565057 | 4.832663836 |
| 59400.00 | 0.564395766 | 1.442933482 | 4.509287869 |
| 61200.00 | 0.505973044 | 1.316453612 | 4.207550489 |
| 63000.00 | 0.453597876 | 1.201060295 | 3.926003758 |
| 64800.00 | 0.406644259 | 1.095781742 | 3.663296625 |
| 66600.00 | 0.364550986 | 0.999731346 | 3.418168445 |
| 68400.00 | 0.326814947 | 0.912100217 | 3.18944293 |
| 70200.00 | 0.292985106 | 0.832150367 | 2.976022501 |
| 72000.00 | 0.262657119 | 0.759208494 | 2.776883023 |
| 73800.00 | 0.235468495 | 0.692660318 | 2.591068891 |
| 75600.00 | 0.211094268 | 0.631945401 | 2.417688446 |
| 77400.00 | 0.189243109 | 0.576552431 | 2.255909691 |
| 79200.00 | 0.169653845 | 0.526014913 | 2.104956303 |
| 81000.00 | 0.152092339 | 0.479907245 | 1.964103907 |
| 82800.00 | 0.13634869 | 0.43784113 | 1.832676599 |
| 84600.00 | 0.122234726 | 0.399462307 | 1.710043702 |
| 86400.00 | 0.109581751 | 0.364447567 | 1.595616741 |

ti (hrs)

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DA#25 DRAINAGE CALCULATIONS

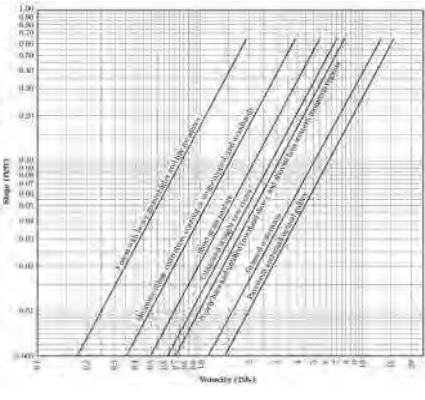
Time of Concentration:

$T_c = T_{OL} + T_1 + \dots + T_n$

Section 2.1
 1. ...
 2. ...
 3. ...
 4. ...
 5. ...
 6. ...
 7. ...
 8. ...
 9. ...
 10. ...

Table 2.1 (continued) Long-term Conditions for Ground Shell Flow

| Parameter | Value |
|-----------------|-------|
| Soil Type | 0.012 |
| Surface Slope | 0.009 |
| Substrate Slope | 0.008 |
| Substrate Slope | 0.007 |
| Substrate Slope | 0.006 |
| Substrate Slope | 0.005 |
| Substrate Slope | 0.004 |
| Substrate Slope | 0.003 |
| Substrate Slope | 0.002 |
| Substrate Slope | 0.001 |
| Substrate Slope | 0.000 |



| | | | |
|------------|----------------------------------------------------------------------|---------|----------------|
| $T_{OL} =$ | $T_t = T_{OL}$; multiply by 60 to convert hrs. to min. (L=max 300') | $T =$ | |
| n= | 0.8 | D= | 763.95 (ft) |
| L= | 100 (ft) | S= | 0.0126 (ft/ft) |
| $P_2 =$ | 4.89 (in) | V= | 0.55 (ft/s) |
| S= | 0.0126 (ft/ft) | | |
| $T_{OL} =$ | 36.38 (min) | $T_1 =$ | 23.15 (min) |

$T_c = 59.53$ (min)

Intensity:

SEE FIG. 2.1-2.1a

| | |
|-------------|-------------|
| I (100-YR)= | 4.6 (in/hr) |
| I (10-YR)= | 3.1 (in/hr) |
| I (2-YR)= | 2.2 (in/hr) |

Peak Flow Rate:

$Q = CIA$

C= 0.2 Woodlands; basin slope 1-3.5%

| | | |
|---------------|-----------|----------|
| i (100-YR) | i (10-YR) | i (2-YR) |
| 4.6 | 3.1 | 2.2 |
| A= 30.31 (Ac) | | |

| | |
|-------------|-------------|
| Q (100-YR)= | 27.89 (cfs) |
| Q (10-YR)= | 18.79 (cfs) |
| Q (2-YR)= | 13.34 (cfs) |

DA#25 EXISTING CALCULATIONS

Volume (100-yr) = 1.38*area*43560 = 1822018.97 cft
 Volume (10-yr) = 0.70*area*43560 = 924212.52 cft
 Volume (2-yr) = 0.41*area*43560 = 541324.476 cft
 A = 30.31 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

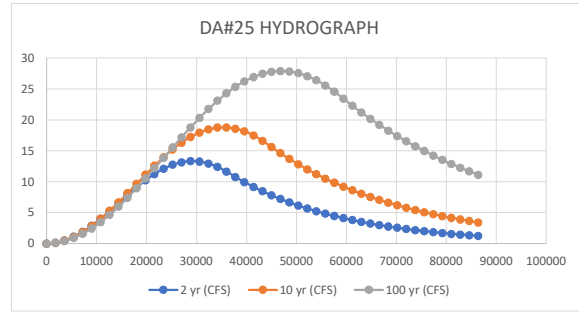
$q_i = \left(\frac{Q_p}{2}\right) \left[1 - \cos\left(\frac{\pi t_i}{T_p}\right)\right]$ $t_i \leq 1.25 T_p$
 $q_i = 1.34 Q_p e^{-1.3t_i/T_p}$ $t_i > 1.25 T_p$

| DA#25 Existing Conditions | | | |
|---------------------------|-----------|-----------|------------|
| | 2 - Year | 10 - Year | 100 - Year |
| Qp= | 13.34 | 18.79 | 27.89 |
| TP= | 29201.439 | 35381.759 | 47007.194 |
| 1.25*TP= | 36501.799 | 44227.199 | 58758.993 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) |
|----------|-------------|-------------|--------------|
| 0 | 0 | 0 | 0 |
| 1800.00 | 0.12463995 | 0.119750928 | 0.100764154 |
| 3600.00 | 0.493900335 | 0.475951322 | 0.401600155 |
| 5400.00 | 1.093976952 | 1.059521814 | 0.898159678 |
| 7200.00 | 1.902436906 | 1.855587484 | 1.583265381 |
| 9000.00 | 2.889057224 | 2.843857021 | 2.447014651 |
| 10800.00 | 4.016954697 | 3.999139931 | 3.476922732 |
| 12600.00 | 5.2439647 | 5.291988635 | 4.658103189 |
| 14400.00 | 6.524217441 | 6.689449071 | 5.973483072 |
| 16200.00 | 7.809852738 | 8.155900675 | 7.404049696 |
| 18000.00 | 9.052809189 | 9.653964336 | 8.929125448 |
| 19800.00 | 10.20662087 | 11.14545517 | 10.52666667 |
| 21600.00 | 11.281544 | 12.59235581 | 12.17358227 |
| 23400.00 | 12.07922139 | 13.95778551 | 13.8460675 |
| 25200.00 | 12.72800607 | 15.20694014 | 15.51994803 |
| 27000.00 | 13.15025468 | 16.30797938 | 17.17102935 |
| 28800.00 | 13.33018214 | 17.2328383 | 18.7754465 |
| 30600.00 | 13.26106214 | 17.9579427 | 20.31000899 |
| 32400.00 | 12.94547862 | 18.46481005 | 21.75253607 |
| 34200.00 | 12.39522917 | 18.74052054 | 23.08217722 |
| 36000.00 | 11.63088397 | 18.77804646 | 24.27971364 |
| 37800.00 | 10.75722579 | 18.5764313 | 25.32783595 |
| 39600.00 | 9.928849972 | 18.14081411 | 26.21139446 |
| 41400.00 | 9.164264436 | 17.48229856 | 26.91761809 |
| 43200.00 | 8.458556922 | 16.61766988 | 27.43629897 |
| 45000.00 | 7.807193441 | 15.61015877 | 27.75994003 |
| 46800.00 | 7.205989153 | 14.61116748 | 27.8838633 |
| 48600.00 | 6.651081476 | 13.67610786 | 27.80627759 |
| 50400.00 | 6.138905271 | 12.80088854 | 27.52830433 |
| 52200.00 | 5.66616994 | 11.98167995 | 27.05396137 |
| 54000.00 | 5.229838282 | 11.21489762 | 26.39010496 |
| 55800.00 | 4.827106977 | 10.49718646 | 25.54633055 |
| 57600.00 | 4.455388582 | 9.825406118 | 24.53483418 |
| 59400.00 | 4.112294903 | 9.196617181 | 23.41186997 |
| 61200.00 | 3.795621652 | 8.608068365 | 22.27496814 |
| 63000.00 | 3.503334285 | 8.057184454 | 21.19327531 |
| 64800.00 | 3.233554932 | 7.541555035 | 20.16411047 |
| 66600.00 | 2.98455033 | 7.058923954 | 19.18492281 |
| 68400.00 | 2.754720691 | 6.607179443 | 18.2532854 |
| 70200.00 | 2.542589416 | 6.184344876 | 17.36688916 |
| 72000.00 | 2.34679362 | 5.788570127 | 16.52353713 |
| 73800.00 | 2.166075363 | 5.41812347 | 15.72113905 |
| 75600.00 | 1.999273579 | 5.071384001 | 14.95770615 |
| 77400.00 | 1.845316608 | 4.746834551 | 14.23134625 |
| 79200.00 | 1.703215319 | 4.443055042 | 13.54025906 |
| 81000.00 | 1.572056745 | 4.158716275 | 12.88273169 |
| 82800.00 | 1.450998229 | 3.892574117 | 12.25713445 |
| 84600.00 | 1.339261999 | 3.643464054 | 11.66191678 |
| 86400.00 | 1.236130181 | 3.410296095 | 11.09560343 |

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DA RP1 401 EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 372177.15 cft
 Volume (100-yr) = 1.38*area*43560 = 251766.90 cft
 Volume (10-yr) = 0.70*area*43560 = 127707.8464 cft
 Volume (2-yr) = 0.41*area*43560 = 74800.31005 cft
 A= 4.19 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Qp}$

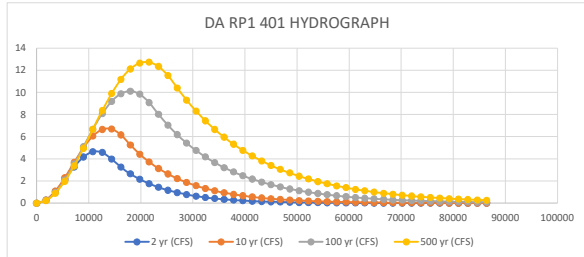
$Q_i = \frac{Q_p}{2} \left[2 - \cos \left(\frac{\pi t_i}{T_p} \right) \right]$ $t_i = 1.25 T_p$

$Q_i = 4.34 Q_p \left(\frac{t_i - T_p}{T_p} \right)^2$ $t_i = 1.25 T_p$

| DA RP1 401 Existing Conditions | | | | |
|--------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 4.69 | 6.74 | 10.11 | 12.75 |
| TP= | 11471.994 | 13625.274 | 17907.503 | 20995.003 |
| 1.25*TP= | 14339.992 | 17031.592 | 22384.378 | 26243.754 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.279219089 | 0.286225949 | 0.250064244 | 0.229903052 |
| 3600.00 | 1.050394902 | 1.096305566 | 0.97552753 | 0.903034269 |
| 5400.00 | 2.129912166 | 2.292695641 | 2.104647074 | 1.970855249 |
| 7200.00 | 3.260740181 | 3.672261412 | 3.525761569 | 3.356367146 |
| 9000.00 | 4.173631272 | 5.000766762 | 5.098333636 | 4.959662937 |
| 10800.00 | 4.651228067 | 6.052645111 | 6.666847897 | 6.665131553 |
| 12600.00 | 4.579815815 | 6.649298305 | 8.076190259 | 8.349794411 |
| 14400.00 | 3.981600381 | 6.689420752 | 9.186987516 | 9.892173194 |
| 16200.00 | 3.246926444 | 6.166200071 | 9.889390296 | 11.18104946 |
| 18000.00 | 2.647812518 | 5.254015724 | 10.11393632 | 12.12348443 |
| 19800.00 | 2.159245444 | 4.424923608 | 9.83841971 | 12.65152063 |
| 21600.00 | 1.760827421 | 3.726635359 | 9.090086946 | 12.72708224 |
| 23400.00 | 1.435924394 | 3.138590067 | 8.02952319 | 12.34472062 |
| 25200.00 | 1.17097158 | 2.643315516 | 7.045954765 | 11.53200726 |
| 27000.00 | 0.954907128 | 2.226196084 | 6.182867573 | 10.40024865 |
| 28800.00 | 0.778710295 | 1.874898768 | 5.425503384 | 9.303350672 |
| 30600.00 | 0.635024816 | 1.579036732 | 4.760911765 | 8.322140807 |
| 32400.00 | 0.517851785 | 1.329862201 | 4.177728633 | 7.444417613 |
| 34200.00 | 0.4222992 | 1.120007811 | 3.665981936 | 6.659266514 |
| 36000.00 | 0.344377715 | 0.94326878 | 3.21692114 | 5.956924075 |
| 37800.00 | 0.280834087 | 0.794419452 | 2.822867597 | 5.328656597 |
| 39600.00 | 0.229015355 | 0.669058788 | 2.47708325 | 4.766651508 |
| 41400.00 | 0.186758072 | 0.563480237 | 2.173655411 | 4.263920218 |
| 43200.00 | 0.152297987 | 0.474562151 | 1.907395662 | 3.814211212 |
| 45000.00 | 0.124196382 | 0.399675482 | 1.673751135 | 3.411932312 |
| 46800.00 | 0.101280008 | 0.336606049 | 1.468726661 | 3.05208114 |
| 48600.00 | 0.082592099 | 0.283489074 | 1.288816456 | 2.730182909 |
| 50400.00 | 0.067352433 | 0.238754043 | 1.130944171 | 2.442234781 |
| 52200.00 | 0.054924747 | 0.201078272 | 0.992410294 | 2.184656093 |
| 54000.00 | 0.044790184 | 0.169347798 | 0.870845986 | 1.954243827 |
| 55800.00 | 0.036525623 | 0.142624443 | 0.764172577 | 1.748132783 |
| 57600.00 | 0.029786015 | 0.120118077 | 0.67056602 | 1.563759948 |
| 59400.00 | 0.024289982 | 0.101163252 | 0.588425705 | 1.398832629 |
| 61200.00 | 0.019808061 | 0.085199528 | 0.516347086 | 1.251299936 |
| 63000.00 | 0.016153132 | 0.071754906 | 0.453097665 | 1.119327286 |
| 64800.00 | 0.013172601 | 0.060431867 | 0.397595919 | 1.001273586 |
| 66600.00 | 0.010742029 | 0.050895621 | 0.348892804 | 0.895670824 |
| 68400.00 | 0.008759939 | 0.04286421 | 0.306155529 | 0.801205821 |
| 70200.00 | 0.007143579 | 0.036100169 | 0.268653313 | 0.716703895 |
| 72000.00 | 0.005825466 | 0.030403504 | 0.235744894 | 0.641114254 |
| 73800.00 | 0.004750567 | 0.025605783 | 0.206867558 | 0.573496935 |
| 75600.00 | 0.003874005 | 0.021565149 | 0.181527523 | 0.513011109 |
| 77400.00 | 0.003159185 | 0.018162134 | 0.159291491 | 0.458904629 |
| 79200.00 | 0.002576261 | 0.01529612 | 0.139779239 | 0.410504674 |
| 81000.00 | 0.002100896 | 0.012882368 | 0.12265712 | 0.367209387 |
| 82800.00 | 0.001713244 | 0.010849509 | 0.107632359 | 0.328480387 |
| 84600.00 | 0.001397121 | 0.009137439 | 0.094448041 | 0.293836073 |
| 86400.00 | 0.001139328 | 0.007695537 | 0.082878722 | 0.262845642 |

ti (hrs)
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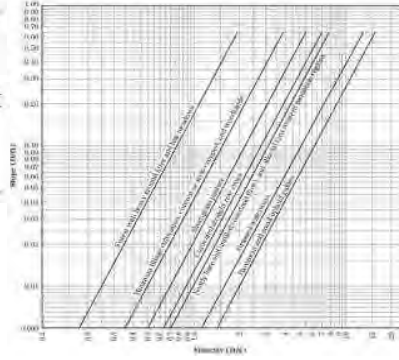
DA RP1 402 DRAINAGE CALCULATIONS

Time of Concentration:

$$T_c = T_{OL} + T_1 + \dots + T_n$$

Equation 3.3
 $T_{OL} = \frac{L}{V}$
 where:
 T_{OL} = travel time (min)
 L = length of travel (ft)
 V = average flow velocity (ft/s)
 T_1 = time of entry to storm sewer (min)
 T_n = time of entry to storm sewer (min)
 (The following is a list of the various methods for determining the time of entry to a storm sewer.)

Table 3.3 Intensity Duration Coefficient for Overland Flow
 Intensity (in/hr)
 Duration (min)
 Coefficient (C)



| | |
|------------------------------------------------------------------------------|----------------------|
| $T_{OL} = \frac{L}{V}$; multiply by 60 to convert hrs. to min. (L=max 300') | $T =$ |
| $n = 0.15$ | $D = 929$ (ft) |
| $L = 100$ (ft) | $S = 0.0035$ (ft/ft) |
| $P_2 = 4.89$ (in) | $V = 0.5$ (ft/s) |
| $S = 0.0035$ (ft/ft) | |
| $T_{OL} = 15.92$ (min) | $T_1 = 30.97$ (min) |

$T_c = 46.88$ (min)

Intensity:

SEE FIG. 2.1-2.1a

| | |
|-------------|--------------|
| I (500-YR)= | 7.25 (in/hr) |
| I (100-YR)= | 5.3 (in/hr) |
| I (10-YR)= | 4.5 (in/hr) |
| I (2-YR)= | 2.4 (in/hr) |

Peak Flow Rate:

$$Q = CIA$$

$C = 0.35$ Mixed use area. Residential lots b/w 1/4 and 1/2 acres; sub-basin slope <1%; and golf course

| | | | |
|--------------------------------|------------|-----------|----------|
| i (500-YR) | i (100-YR) | i (10-YR) | i (2-YR) |
| 7.25 | 5.3 | 4.5 | 2.4 |
| A RP1 402= 9.36 (Ac) | | | |
| Q (500-YR)= 23.74 (cfs) | | | |
| Q (100-YR)= 17.36 (cfs) | | | |
| Q (10-YR)= 14.74 (cfs) | | | |
| Q (2-YR)= 7.86 (cfs) | | | |

DA RP1 402 EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 831752.06 cft
 Volume (100-yr) = 1.38*area*43560 = 562655.81 cft
 Volume (10-yr) = 0.70*area*43560 = 285405.12 cft
 Volume (2-yr) = 0.41*area*43560 = 167165.856 cft
 A= 9.36 Ac

TP = time to Qp in seconds

$T_p = \frac{V}{1.39 Q_p}$

$Q_i = \frac{Q_p}{2} \left[2 - \cos \left(\frac{\pi t_i}{T_p} \right) \right]$
 $t_i = 1.25 T_p$

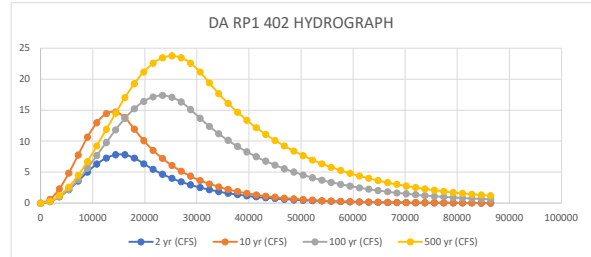
$Q_i = 4.34 Q_p \left(\frac{t_i}{T_p} \right)^{-1.81}$
 $t_i = 1.25 T_p$

| DA RP1 402 Existing Conditions | | | | |
|--------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 7.86 | 14.74 | 17.36 | 23.74 |
| Tp= | 15295.992 | 13928.058 | 23313.541 | 25200.714 |
| 1.25*Tp= | 19119.990 | 17410.072 | 29141.926 | 31500.893 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.265602729 | 0.599219691 | 0.254131045 | 0.2976475 |
| 3600.00 | 1.026521207 | 2.29945257 | 1.0016458 | 1.175665555 |
| 5400.00 | 2.179935927 | 4.824260428 | 2.198780192 | 2.590029157 |
| 7200.00 | 3.569991122 | 7.763138696 | 3.775446675 | 4.46982021 |
| 9000.00 | 5.008854855 | 10.63825975 | 5.639337579 | 6.720783462 |
| 10800.00 | 6.302099912 | 12.98216214 | 7.681329367 | 9.230052585 |
| 12600.00 | 7.274975878 | 14.41375443 | 9.781871387 | 11.87180945 |
| 14400.00 | 7.796022378 | 14.70027628 | 11.8179851 | 14.5135928 |
| 16200.00 | 7.794832732 | 13.79514255 | 13.670464 | 17.02294007 |
| 18000.00 | 7.271567691 | 11.92352009 | 15.23085267 | 19.27402922 |
| 19800.00 | 6.341862277 | 10.07953095 | 16.40779645 | 21.15398759 |
| 21600.00 | 5.442242532 | 8.520717328 | 17.13238987 | 22.56855155 |
| 23400.00 | 4.670237619 | 7.202976421 | 17.36221081 | 23.44679295 |
| 25200.00 | 4.007744838 | 6.089025996 | 17.08380415 | 23.74467559 |
| 27000.00 | 3.439229435 | 5.14734957 | 16.31346953 | 23.44726324 |
| 28800.00 | 2.951360324 | 4.351304727 | 15.09630701 | 22.56946854 |
| 30600.00 | 2.532697492 | 3.678369337 | 13.67952018 | 21.1553053 |
| 32400.00 | 2.173423738 | 3.10950435 | 12.37315225 | 19.37244033 |
| 34200.00 | 1.865114471 | 2.628615133 | 11.19153995 | 17.65461006 |
| 36000.00 | 1.600540166 | 2.22029611 | 10.12276936 | 16.08910654 |
| 37800.00 | 1.373496835 | 1.878445824 | 9.15606431 | 14.66242235 |
| 39600.00 | 1.178660552 | 1.587941538 | 8.28167737 | 13.36224785 |
| 41400.00 | 1.011462613 | 1.342364148 | 7.490793404 | 12.17736492 |
| 43200.00 | 0.867982402 | 1.134765646 | 6.775437007 | 11.09755021 |
| 45000.00 | 0.74485546 | 0.959272545 | 6.128395773 | 10.11348691 |
| 46800.00 | 0.639194591 | 0.810919698 | 5.543145736 | 9.216684355 |
| 48600.00 | 0.548522159 | 0.685509827 | 5.013785954 | 8.399404803 |
| 50400.00 | 0.470711992 | 0.579494769 | 4.534979016 | 7.654596634 |
| 52200.00 | 0.403939523 | 0.489875089 | 4.101897221 | 6.975833527 |
| 54000.00 | 0.346639008 | 0.414115218 | 3.710173907 | 6.357259006 |
| 55800.00 | 0.297466812 | 0.350071718 | 3.355859418 | 5.793535915 |
| 57600.00 | 0.255269898 | 0.295932635 | 3.035381283 | 5.279800361 |
| 59400.00 | 0.219058793 | 0.250166237 | 2.745508194 | 4.811619754 |
| 61200.00 | 0.187984385 | 0.211477677 | 2.48331743 | 4.384954558 |
| 63000.00 | 0.161318012 | 0.178772357 | 2.24616538 | 3.996123438 |
| 64800.00 | 0.138434376 | 0.151124961 | 2.031660896 | 3.641771499 |
| 66600.00 | 0.11879688 | 0.127753273 | 1.837641179 | 3.318841336 |
| 68400.00 | 0.101945044 | 0.10799605 | 1.662149972 | 3.024546657 |
| 70200.00 | 0.087483712 | 0.091294309 | 1.503417839 | 2.756348242 |
| 72000.00 | 0.075073781 | 0.077175516 | 1.35984432 | 2.511932032 |
| 73800.00 | 0.064424251 | 0.065240214 | 1.229981797 | 2.289189166 |
| 75600.00 | 0.055285401 | 0.055150723 | 1.112520895 | 2.086197784 |
| 77400.00 | 0.047442935 | 0.046621586 | 1.006277284 | 1.901206443 |
| 79200.00 | 0.040712956 | 0.039411493 | 0.910179735 | 1.732619011 |
| 81000.00 | 0.034937652 | 0.03331645 | 0.823259316 | 1.578980887 |
| 82800.00 | 0.0299816 | 0.028164014 | 0.744639631 | 1.438966459 |
| 84600.00 | 0.025728584 | 0.02380841 | 0.673527975 | 1.311367659 |
| 86400.00 | 0.022078877 | 0.020126406 | 0.609207346 | 1.195083545 |

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DA RP1 403 EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 76421.66 cft
 Volume (100-yr) = 1.38*area*43560 = 51697.01 cft
 Volume (10-yr) = 0.70*area*43560 = 26223.12 cft
 Volume (2-yr) = 0.41*area*43560 = 15359.256 cft
 A= 0.86 Ac

TP = time to Qp in seconds

$Tp = \frac{V}{1.39 Qp}$

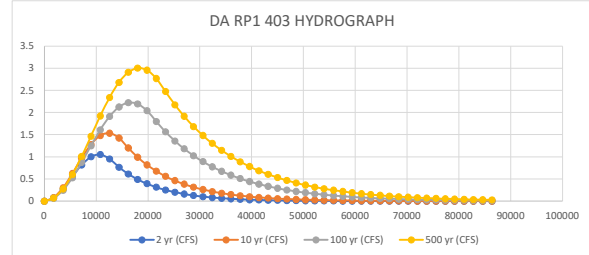
$Qp = \frac{Qp}{2} \left[1 - \cos \left(\frac{\pi t_i}{Tp} \right) \right]$
 $t_i = 1.25 Tp$
 $Qp = 4.34 Qp \left(\frac{t_i - Tp}{Tp} \right)^2$
 $t_i = 1.25 Tp$

| DA RP1 403 Existing Conditions | | | | |
|--------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 1.05 | 1.54 | 2.23 | 3.01 |
| TP= | 10488.680 | 12289.463 | 16697.536 | 18294.740 |
| 1.25*TP= | 13110.850 | 15361.828 | 20871.920 | 22868.425 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.074719208 | 0.079832437 | 0.063259144 | 0.071211025 |
| 3600.00 | 0.277679072 | 0.302723095 | 0.245850226 | 0.278094483 |
| 5400.00 | 0.551300093 | 0.622306514 | 0.527030575 | 0.601041282 |
| 7200.00 | 0.817956279 | 0.972103318 | 0.874857609 | 1.00944146 |
| 9000.00 | 1.001997553 | 1.279349174 | 1.249817559 | 1.464585508 |
| 10800.00 | 1.051211601 | 1.480131151 | 1.609314315 | 1.923333375 |
| 12600.00 | 0.951636449 | 1.532682811 | 1.912508408 | 2.34220343 |
| 14400.00 | 0.767367854 | 1.426072419 | 2.124956455 | 2.681493793 |
| 16200.00 | 0.613922455 | 1.200582254 | 2.222523981 | 2.909045408 |
| 18000.00 | 0.491160503 | 0.992428435 | 2.194127144 | 3.003290183 |
| 19800.00 | 0.392946434 | 0.820363783 | 2.042991873 | 2.955295291 |
| 21600.00 | 0.314371573 | 0.678131251 | 1.798627911 | 2.769609843 |
| 23400.00 | 0.2515088 | 0.560558625 | 1.563432409 | 2.47304504 |
| 25200.00 | 0.201216273 | 0.463370433 | 1.358991975 | 2.176122409 |
| 27000.00 | 0.160980406 | 0.383032477 | 1.181284959 | 1.914849372 |
| 28800.00 | 0.128790235 | 0.316623305 | 1.026815596 | 1.684945709 |
| 30600.00 | 0.103036916 | 0.261727983 | 0.89254524 | 1.482645102 |
| 32400.00 | 0.082433316 | 0.216350268 | 0.775832592 | 1.304633343 |
| 34200.00 | 0.065949679 | 0.178840023 | 0.674381739 | 1.147994475 |
| 36000.00 | 0.052762164 | 0.147833207 | 0.58619699 | 1.010162154 |
| 37800.00 | 0.042211668 | 0.122202271 | 0.509543618 | 0.888878473 |
| 39600.00 | 0.033770884 | 0.10101516 | 0.442913735 | 0.782156546 |
| 41400.00 | 0.027017947 | 0.083501415 | 0.384996632 | 0.688248034 |
| 43200.00 | 0.02161535 | 0.069024158 | 0.334652992 | 0.605614514 |
| 45000.00 | 0.017293073 | 0.05705693 | 0.29089248 | 0.53290227 |
| 46800.00 | 0.013835094 | 0.047164548 | 0.252854261 | 0.468920118 |
| 48600.00 | 0.011068583 | 0.038987282 | 0.219790065 | 0.412619892 |
| 50400.00 | 0.008855273 | 0.032227769 | 0.191049471 | 0.363079272 |
| 52200.00 | 0.007084543 | 0.026640202 | 0.166067108 | 0.319486677 |
| 54000.00 | 0.005667895 | 0.022021393 | 0.144351534 | 0.281127964 |
| 55800.00 | 0.004534524 | 0.018203382 | 0.125475572 | 0.247374735 |
| 57600.00 | 0.003627785 | 0.015047327 | 0.109067904 | 0.21767404 |
| 59400.00 | 0.002902362 | 0.012438461 | 0.094805766 | 0.191539316 |
| 61200.00 | 0.002321996 | 0.010281913 | 0.082408599 | 0.168542421 |
| 63000.00 | 0.001857682 | 0.008499262 | 0.071632534 | 0.148306615 |
| 64800.00 | 0.001486214 | 0.007025682 | 0.062265588 | 0.130500393 |
| 66600.00 | 0.001189026 | 0.005807587 | 0.054123501 | 0.114832049 |
| 68400.00 | 0.000951264 | 0.004800683 | 0.047046103 | 0.101044903 |
| 70200.00 | 0.000761046 | 0.003968353 | 0.040894174 | 0.08891309 |
| 72000.00 | 0.000608865 | 0.00328033 | 0.035546695 | 0.078237867 |
| 73800.00 | 0.000487114 | 0.002711595 | 0.030898472 | 0.068844349 |
| 75600.00 | 0.000389709 | 0.002241466 | 0.026858069 | 0.06057865 |
| 77400.00 | 0.000311782 | 0.001852846 | 0.023346005 | 0.053305361 |
| 79200.00 | 0.000249437 | 0.001531605 | 0.020293191 | 0.046905329 |
| 81000.00 | 0.000199559 | 0.001266059 | 0.017639576 | 0.041273707 |
| 82800.00 | 0.000159654 | 0.001046553 | 0.015332957 | 0.036318238 |
| 84600.00 | 0.000127729 | 0.000865104 | 0.013327961 | 0.031957741 |
| 86400.00 | 0.000102188 | 0.000715115 | 0.011585145 | 0.02812078 |

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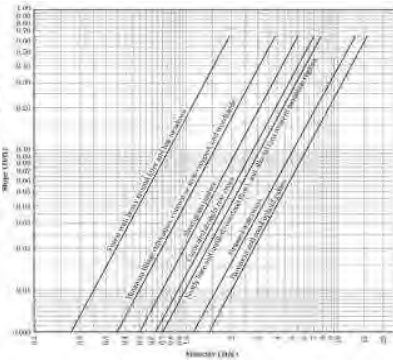
DA RP1 404 DRAINAGE CALCULATIONS

Time of Concentration:

$$T_c = T_{OL} + T_1 + \dots + T_n$$

Equation 3.3
 $T_c = T_{OL} + \sum_{i=1}^n T_i$
 where:
 T_c = time of concentration
 T_{OL} = time of overland flow
 T_i = time of travel in pipe or conduit
 T_n = time of travel in stream
 T_{OL} = time of overland flow
 T_i = time of travel in pipe or conduit
 T_n = time of travel in stream
 (The following is a summary of the following calculations)
 1) Determine the overland flow time
 2) Determine the travel time in pipe or conduit
 3) Determine the travel time in stream
 4) Determine the time of concentration
 5) Determine the time of travel in stream
 6) Determine the time of travel in stream
 7) Determine the time of travel in stream
 8) Determine the time of travel in stream
 9) Determine the time of travel in stream
 10) Determine the time of travel in stream

| Parameter | Value |
|--------------------------------|-------|
| Subarea | 0.15 |
| Runoff Coefficient | 0.5 |
| Time of Concentration (min) | 15.92 |
| Time of Travel in Pipe (min) | 0.0 |
| Time of Travel in Stream (min) | 0.0 |
| Time of Concentration (min) | 15.92 |
| Time of Travel in Pipe (min) | 0.0 |
| Time of Travel in Stream (min) | 0.0 |
| Time of Concentration (min) | 15.92 |
| Time of Travel in Pipe (min) | 0.0 |
| Time of Travel in Stream (min) | 0.0 |



| Parameter | Value | Parameter | Value |
|----------------|-------|-------------|-------|
| T_{OL} (min) | 15.92 | T_1 (min) | 32.13 |
| T_c (min) | 48.05 | | |

$T_c = 48.05$ (min)

Intensity:

SEE FIG. 2.1-2.1a

| | |
|-------------|--------------|
| I (500-YR)= | 7.15 (in/hr) |
| I (100-YR)= | 5.2 (in/hr) |
| I (10-YR)= | 3.4 (in/hr) |
| I (2-YR)= | 2.4 (in/hr) |

Peak Flow Rate:

$$Q = CIA$$

C = 0.35 Mixed use area. Residential lots b/w 1/4 and 1/2 acres; sub-basin slope <1%; and golf course

| i (500-YR) | i (100-YR) | i (10-YR) | i (2-YR) |
|----------------------|------------|-----------|----------|
| 7.15 | 5.2 | 3.4 | 2.4 |
| A RP1 404= 3.62 (Ac) | | | |
| Q (500-YR)= | 9.06 (cfs) | | |
| Q (100-YR)= | 6.59 (cfs) | | |
| Q (10-YR)= | 4.31 (cfs) | | |
| Q (2-YR)= | 3.04 (cfs) | | |

DA RP1 404 EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 321681.89 cft
 Volume (100-yr) = 1.38*area*43560 = 217608.34 cft
 Volume (10-yr) = 0.70*area*43560 = 110381.04 cft
 Volume (2-yr) = 0.41*area*43560 = 64651.752 cft
 A= 3.62 Ac

TP = time to Qp in seconds

$T_p = \frac{V}{1.39 Q_p}$

$Q_p = \frac{Q_p}{2} \left[2 - \cos \left(\frac{\pi t_i}{T_p} \right) \right]$
 $t_i = 1.25 T_p$

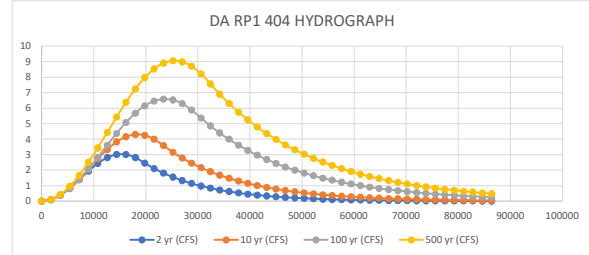
$Q_p = 4.34 Q_{ps} \left(\frac{t_i}{T_p} \right)^{-1.81}$
 $t_i = 1.25 T_p$

| DA RP1 404 Existing Conditions | | | | |
|--------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 3.04 | 4.31 | 6.59 | 9.06 |
| Tp= | 15295.992 | 18434.194 | 23761.878 | 25554.458 |
| 1.25*Tp= | 19119.990 | 23042.742 | 29702.348 | 31943.073 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.102722423 | 0.100550371 | 0.09284372 | 0.110413862 |
| 3600.00 | 0.39700927 | 0.392813511 | 0.366141467 | 0.43627074 |
| 5400.00 | 0.843094878 | 0.849502018 | 0.804487996 | 0.961679117 |
| 7200.00 | 1.380701695 | 1.427976774 | 1.383174592 | 1.661015671 |
| 9000.00 | 1.937185318 | 2.074227982 | 2.069581853 | 2.50017488 |
| 10800.00 | 2.437350607 | 2.727917837 | 2.825018382 | 3.438232296 |
| 12600.00 | 2.813612466 | 3.328014019 | 3.606901736 | 4.429440365 |
| 14400.00 | 3.015128313 | 3.818488027 | 4.371158721 | 5.42545946 |
| 16200.00 | 3.014668215 | 4.15354633 | 5.074709705 | 6.377715328 |
| 18000.00 | 2.812294342 | 4.301905919 | 5.677896931 | 7.239767979 |
| 19800.00 | 2.452728787 | 4.249715073 | 6.146719947 | 7.969576489 |
| 21600.00 | 2.104798928 | 4.001846634 | 6.45475214 | 8.531549268 |
| 23400.00 | 1.806224378 | 3.5898394 | 6.584630353 | 8.898279806 |
| 25200.00 | 1.55000388 | 3.161888418 | 6.529033613 | 9.051883243 |
| 27000.00 | 1.330129333 | 2.784954214 | 6.291095797 | 8.984868585 |
| 28800.00 | 1.141444912 | 2.452954991 | 5.88422898 | 8.700504031 |
| 30600.00 | 0.979526167 | 2.160533971 | 5.360594065 | 8.212657583 |
| 32400.00 | 0.840576275 | 1.902972969 | 4.857858674 | 7.561558037 |
| 34200.00 | 0.721337007 | 1.67611626 | 4.402271579 | 6.899908218 |
| 36000.00 | 0.619012329 | 1.476303533 | 3.989411046 | 6.29615394 |
| 37800.00 | 0.531202836 | 1.300310828 | 3.615270028 | 5.745229237 |
| 39600.00 | 0.455849487 | 1.145298518 | 3.276217273 | 5.242511429 |
| 41400.00 | 0.391185327 | 1.008765495 | 2.968962079 | 4.783782326 |
| 43200.00 | 0.335694048 | 0.88850881 | 2.690522359 | 4.365192838 |
| 45000.00 | 0.288074441 | 0.782588134 | 2.438195696 | 3.983230677 |
| 46800.00 | 0.247209874 | 0.689294445 | 2.209533117 | 3.634690887 |
| 48600.00 | 0.212142117 | 0.607122458 | 2.00231532 | 3.316648949 |
| 50400.00 | 0.182048869 | 0.534746337 | 1.814531137 | 3.026436249 |
| 52200.00 | 0.156224474 | 0.470998298 | 1.644358017 | 2.761617678 |
| 54000.00 | 0.134063377 | 0.414849774 | 1.490144331 | 2.519971205 |
| 55800.00 | 0.115045925 | 0.365394813 | 1.350393347 | 2.299469228 |
| 57600.00 | 0.098726179 | 0.321835463 | 1.223748703 | 2.098261569 |
| 59400.00 | 0.084721456 | 0.283468899 | 1.10898124 | 1.914659938 |
| 61200.00 | 0.072703363 | 0.24967608 | 1.004977074 | 1.747123777 |
| 63000.00 | 0.062390086 | 0.219911761 | 0.910726784 | 1.59424733 |
| 64800.00 | 0.053539791 | 0.193695699 | 0.825315619 | 1.454747844 |
| 66600.00 | 0.045944947 | 0.170604899 | 0.747914614 | 1.327454813 |
| 68400.00 | 0.039427464 | 0.150266793 | 0.677772547 | 1.211300148 |
| 70200.00 | 0.033834513 | 0.132353228 | 0.614208651 | 1.105309224 |
| 72000.00 | 0.029034945 | 0.116575717 | 0.556606 | 1.008592695 |
| 73800.00 | 0.024916217 | 0.102678042 | 0.504405529 | 0.920339035 |
| 75600.00 | 0.021381747 | 0.090437614 | 0.457100602 | 0.839807728 |
| 77400.00 | 0.018348656 | 0.079656389 | 0.414232098 | 0.766323053 |
| 79200.00 | 0.015745823 | 0.070160413 | 0.375383953 | 0.699268419 |
| 81000.00 | 0.013512212 | 0.061796468 | 0.340179124 | 0.638081185 |
| 82800.00 | 0.011595448 | 0.054429604 | 0.308275928 | 0.582247943 |
| 84600.00 | 0.009950585 | 0.047940957 | 0.279364725 | 0.531300209 |
| 86400.00 | 0.008539053 | 0.042225832 | 0.253164918 | 0.484810493 |

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DA RP1 405 DRAINAGE CALCULATIONS

Time of Concentration:

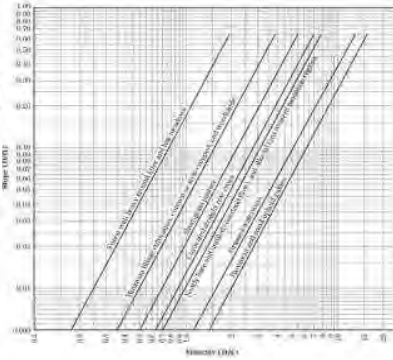
$T_c = T_{OL} + T_1 + \dots + T_n$

Equation 3.1
 $T_c = T_{OL} + \sum_{i=1}^n \left(\frac{L_i}{V_i} \right)$
 where:
 T_c = time of concentration
 T_{OL} = time of overland flow
 L_i = length of pipe section (feet)
 V_i = velocity of flow in pipe section (feet per second)
 n = number of pipe sections
 (The following is a list of the various pipe materials and their roughness coefficients.)
 1) Cast Iron (Standard)
 2) Concrete (Standard)
 3) Steel (Standard)
 4) Aluminum (Standard)
 5) Copper (Standard)
 6) Brass (Standard)
 7) Cast Steel (Standard)
 8) Cast Aluminum (Standard)
 9) Cast Bronze (Standard)
 10) Cast Iron (Standard)
 11) Cast Steel (Standard)
 12) Cast Aluminum (Standard)
 13) Cast Bronze (Standard)
 14) Cast Iron (Standard)
 15) Cast Steel (Standard)
 16) Cast Aluminum (Standard)
 17) Cast Bronze (Standard)
 18) Cast Iron (Standard)
 19) Cast Steel (Standard)
 20) Cast Aluminum (Standard)
 21) Cast Bronze (Standard)
 22) Cast Iron (Standard)
 23) Cast Steel (Standard)
 24) Cast Aluminum (Standard)
 25) Cast Bronze (Standard)

| Material | n |
|--------------------------|-------|
| Cast Iron (Standard) | 0.013 |
| Cast Steel (Standard) | 0.013 |
| Cast Aluminum (Standard) | 0.013 |
| Cast Bronze (Standard) | 0.013 |
| Cast Iron (Standard) | 0.013 |
| Cast Steel (Standard) | 0.013 |
| Cast Aluminum (Standard) | 0.013 |
| Cast Bronze (Standard) | 0.013 |
| Cast Iron (Standard) | 0.013 |
| Cast Steel (Standard) | 0.013 |
| Cast Aluminum (Standard) | 0.013 |
| Cast Bronze (Standard) | 0.013 |
| Cast Iron (Standard) | 0.013 |
| Cast Steel (Standard) | 0.013 |
| Cast Aluminum (Standard) | 0.013 |
| Cast Bronze (Standard) | 0.013 |
| Cast Iron (Standard) | 0.013 |
| Cast Steel (Standard) | 0.013 |
| Cast Aluminum (Standard) | 0.013 |
| Cast Bronze (Standard) | 0.013 |

| T_{OL} = | $T =$ |
|--------------------------------|------------------------------|
| $n = 0.15$ | $D = 835 \text{ (ft)}$ |
| $L = 100 \text{ (ft)}$ | $S = 0.0035 \text{ (ft/ft)}$ |
| $P_2 = 4.89 \text{ (in)}$ | $V = 0.5 \text{ (ft/s)}$ |
| $S = 0.0035 \text{ (ft/ft)}$ | |
| $T_{OL} = 15.92 \text{ (min)}$ | $T_1 = 27.83 \text{ (min)}$ |

$T_c = 43.75 \text{ (min)}$



Intensity:

SEE FIG. 2.1-2.1a

| | |
|-------------|--------------|
| I (500-YR)= | 7.52 (in/hr) |
| I (100-YR)= | 5.5 (in/hr) |
| I (10-YR)= | 3.7 (in/hr) |
| I (2-YR)= | 2.5 (in/hr) |

Peak Flow Rate:

$Q = CIA$

$C = 0.35$ Mixed use area. Residential lots b/w 1/4 and 1/2 acres; sub-basin slope <1%; and golf course

| i (500-YR) | i (100-YR) | i (10-YR) | i (2-YR) |
|--------------------------------|------------|-----------|----------|
| 7.52 | 5.5 | 3.7 | 2.5 |
| A RP1 405= 5.62 (Ac) | | | |
| Q (500-YR)= 14.79 (cfs) | | | |
| Q (100-YR)= 10.82 (cfs) | | | |
| Q (10-YR)= 7.28 (cfs) | | | |
| Q (2-YR)= 4.92 (cfs) | | | |

DA RP1 405 EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 499406.69 cft
 Volume (100-yr) = 1.38*area*43560 = 337833.94 cft
 Volume (10-yr) = 0.70*area*43560 = 171365.04 cft
 Volume (2-yr) = 0.41*area*43560 = 100370.952 cft
 A= 5.62 Ac

TP = time to Qp in seconds
 TP = $\frac{V}{1.39 Qp}$

$$Q_t = \frac{Q_p}{2} \left[2 - \cos \left(\frac{\pi t_i}{TP} \right) \right] \quad t_i = 1.25 TP$$

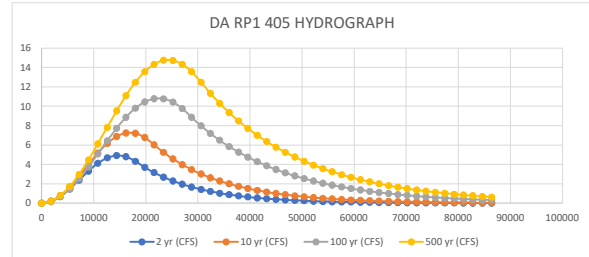
$$Q_t = 4.34 Q_p \left(\frac{t_i}{TP} \right)^{-1.81} \quad t_i = 1.25 TP$$

| DA RP1 405 Existing Conditions | | | | |
|--------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 4.92 | 7.28 | 10.82 | 14.79 |
| TP= | 14684.152 | 16939.529 | 22465.776 | 24297.392 |
| 1.25*TP= | 18355.190 | 21174.412 | 28082.220 | 30371.741 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|--------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.180076693 | 0.200886732 | 0.170456964 | 0.199335248 |
| 3600.00 | 0.693929454 | 0.781367191 | 0.671084935 | 0.786592448 |
| 5400.00 | 1.466290033 | 1.677351007 | 1.47033221 | 1.730105742 |
| 7200.00 | 2.384024406 | 2.789913349 | 2.517826827 | 2.978999122 |
| 9000.00 | 3.312704453 | 3.996217126 | 3.747551224 | 4.465930067 |
| 10800.00 | 4.11629875 | 5.163075334 | 5.082002941 | 6.110720616 |
| 12600.00 | 4.677098214 | 6.161656123 | 6.437079159 | 7.824680739 |
| 14400.00 | 4.912957924 | 6.881707013 | 7.727377215 | 9.515390658 |
| 16200.00 | 4.789329563 | 7.243727778 | 8.871577039 | 11.09168429 |
| 18000.00 | 4.324321997 | 7.207748006 | 9.797566295 | 12.46856507 |
| 19800.00 | 3.697897518 | 6.7774740193 | 10.4469852 | 13.57178915 |
| 21600.00 | 3.153172053 | 6.019809114 | 10.77890463 | 14.34186872 |
| 23400.00 | 2.688688355 | 5.243121989 | 10.77240559 | 14.73727972 |
| 25200.00 | 2.292626267 | 4.566644502 | 10.42789769 | 14.73670088 |
| 27000.00 | 1.954906818 | 3.977447416 | 9.767093275 | 14.34016342 |
| 28800.00 | 1.666935743 | 3.46426965 | 8.869310553 | 13.56904935 |
| 30600.00 | 1.421384766 | 3.017303046 | 7.991980755 | 12.48352297 |
| 32400.00 | 1.212005119 | 2.628004917 | 7.201434203 | 11.3373545 |
| 34200.00 | 1.033468518 | 2.288934767 | 6.48908652 | 10.29642091 |
| 36000.00 | 0.881231574 | 1.993612086 | 5.847202471 | 9.351060134 |
| 37800.00 | 0.751420167 | 1.736392495 | 5.268811971 | 8.492497185 |
| 39600.00 | 0.640730864 | 1.512359861 | 4.747634398 | 7.712762768 |
| 41400.00 | 0.546346848 | 1.317232339 | 4.278010394 | 7.004619279 |
| 43200.00 | 0.46586624 | 1.147280539 | 3.854840411 | 6.361493633 |
| 45000.00 | 0.397240973 | 0.99925624 | 3.473529334 | 5.77741625 |
| 46800.00 | 0.338724675 | 0.870330316 | 3.129936585 | 5.246965642 |
| 48600.00 | 0.288828225 | 0.758038657 | 2.820331163 | 4.765218093 |
| 50400.00 | 0.246281863 | 0.66023508 | 2.541351128 | 4.327701957 |
| 52200.00 | 0.210002869 | 0.575050305 | 2.289967093 | 3.90356148 |
| 54000.00 | 0.179068017 | 0.50085623 | 2.063449332 | 3.569492447 |
| 55800.00 | 0.15269008 | 0.436234815 | 1.859338135 | 3.241761268 |
| 57600.00 | 0.130197792 | 0.379950976 | 1.675417103 | 2.944120565 |
| 59400.00 | 0.111018772 | 0.330928985 | 1.509689075 | 2.673807595 |
| 61200.00 | 0.094664951 | 0.288231903 | 1.360354444 | 2.428313277 |
| 63000.00 | 0.08072016 | 0.251043679 | 1.225791619 | 2.205358897 |
| 64800.00 | 0.068829531 | 0.21865355 | 1.104539408 | 2.002874964 |
| 66600.00 | 0.058690473 | 0.190442457 | 0.995281159 | 1.818981992 |
| 68400.00 | 0.050044967 | 0.165871212 | 0.896830461 | 1.651973063 |
| 70200.00 | 0.042673003 | 0.144470195 | 0.808118257 | 1.500297975 |
| 72000.00 | 0.036386979 | 0.125830378 | 0.72818124 | 1.36254886 |
| 73800.00 | 0.031026929 | 0.109595506 | 0.656151391 | 1.237447112 |
| 75600.00 | 0.026456452 | 0.095455287 | 0.591246552 | 1.123831519 |
| 77400.00 | 0.022559236 | 0.083139466 | 0.532761937 | 1.020647486 |
| 79200.00 | 0.019236107 | 0.072412655 | 0.480062471 | 0.926937243 |
| 81000.00 | 0.016402498 | 0.063069838 | 0.432575904 | 0.84183096 |
| 82800.00 | 0.013986298 | 0.054932448 | 0.389786588 | 0.764538668 |
| 84600.00 | 0.011926021 | 0.04784496 | 0.351229883 | 0.694342929 |
| 86400.00 | 0.010169237 | 0.041671913 | 0.316487111 | 0.630592177 |

ti (hrs)

0
0.5
1
1.5
2
2.5
3
3.5
4
4.5
5
5.5
6
6.5
7
7.5
8
8.5
9
9.5
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23.5
24



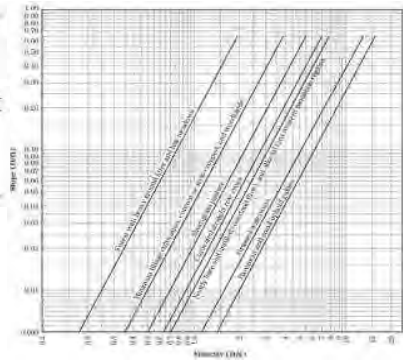
DA RP1 406 DRAINAGE CALCULATIONS

Time of Concentration:

$T_c = T_{OL} + T_1 + \dots + T_n$

Equation 3.1
 $T_c = T_{OL} + \sum_{i=1}^n T_i$
 where:
 T_c = Time of Concentration
 T_{OL} = Time of Overland Flow
 T_i = Time of Travel in Pipe or Channel
 n = Number of Pipe or Channel Segments
 L_i = Length of Pipe or Channel Segment (feet)
 V_i = Velocity of Flow in Pipe or Channel Segment (feet per second)
 $T_i = L_i / V_i$
 (The following is a summary of the steps to calculate the time of concentration for a drainage area.)
 1. Determine the time of overland flow (T_{OL}).
 2. Determine the length of each pipe or channel segment (L_i).
 3. Determine the velocity of flow in each pipe or channel segment (V_i).
 4. Calculate the time of travel in each pipe or channel segment ($T_i = L_i / V_i$).
 5. Sum the times of travel in all pipe or channel segments to determine the total time of travel ($\sum T_i$).
 6. Add the time of overland flow (T_{OL}) to the total time of travel ($\sum T_i$) to determine the time of concentration (T_c).

| Parameter | Value |
|------------------------------------|--------------|
| Drainage Area (Acres) | 4.02 |
| Length of Overland Flow (ft) | 100 |
| Velocity of Overland Flow (ft/s) | 0.5 |
| Time of Overland Flow (min) | 15.92 |
| Length of Pipe (ft) | 905 |
| Velocity of Pipe Flow (ft/s) | 0.0035 |
| Time of Pipe Flow (min) | 30.17 |
| Time of Concentration (min) | 46.08 |



| T_{OL} = | T_c = |
|--------------------------------------------------------------------------------|------------------------------------|
| $T_{OL} = T_{OL}$; multiply by 60 to convert hrs. to min. ($L = \max 300'$) | $T_c = T_{OL} + T_1 + \dots + T_n$ |
| $n = 0.15$ | $D = 905$ (ft) |
| $L = 100$ (ft) | $S = 0.0035$ (ft/ft) |
| $P_2 = 4.89$ (in) | $V = 0.5$ (ft/s) |
| $S = 0.0035$ (ft/ft) | |
| $T_{OL} = 15.92$ (min) | $T_c = 46.08$ (min) |

$T_c = 46.08$ (min)

Intensity:

SEE FIG. 2.1-2.1a

| | |
|-------------|--------------|
| I (500-YR)= | 7.32 (in/hr) |
| I (100-YR)= | 5.4 (in/hr) |
| I (10-YR)= | 3.6 (in/hr) |
| I (2-YR)= | 2.5 (in/hr) |

Peak Flow Rate:

$Q = CIA$

$C = 0.35$ Mixed use area. Residential lots b/w 1/4 and 1/2 acres; sub-basin slope <1%; and golf course

| i (500-YR) | i (100-YR) | i (10-YR) | i (2-YR) |
|--------------------------------|--------------|-------------|------------|
| 7.32 | 5.4 | 3.6 | 2.5 |
| A RP1 406= 4.02 (Ac) | | | |
| Q (500-YR)= 10.29 (cfs) | | | |
| Q (100-YR)= 7.60 (cfs) | | | |
| Q (10-YR)= 5.07 (cfs) | | | |
| Q (2-YR)= 3.52 (cfs) | | | |

DA RP1 406 EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 357226.85 cft
 Volume (100-yr) = 1.38*area*43560 = 241653.46 cft
 Volume (10-yr) = 0.70*area*43560 = 122577.84 cft
 Volume (2-yr) = 0.41*area*43560 = 71795.592 cft
 A= 4.02 Ac

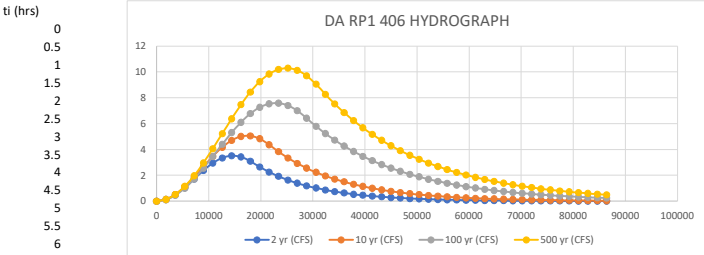
TP = time to Qp in seconds

$T_p = \frac{V}{1.39 Q_p}$

$Q_p = \frac{Q_p}{2} \left[1 - \cos \left(\frac{\pi t_i}{T_p} \right) \right]$
 $t_i = 1.25 T_p$
 $Q_p = 4.34 Q_{ps} \left(\frac{t_i}{T_p} \right)^{0.5}$
 $t_i = 1.25 T_p$

| DA RP1 406 Existing Conditions | | | | |
|--------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 3.52 | 5.07 | 7.60 | 10.29 |
| Tp= | 14684.152 | 17410.072 | 22881.809 | 24963.753 |
| 1.25*Tp= | 18355.190 | 21762.590 | 28602.261 | 31204.692 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.128809307 | 0.132421583 | 0.115419824 | 0.131500237 |
| 3600.00 | 0.496369467 | 0.515838526 | 0.454665827 | 0.519282118 |
| 5400.00 | 1.048840913 | 1.110155529 | 0.997123777 | 1.143532442 |
| 7200.00 | 1.705298596 | 1.853222708 | 1.709831269 | 1.972355969 |
| 9000.00 | 2.369585747 | 2.667334834 | 2.549480749 | 2.963405059 |
| 10800.00 | 2.94439875 | 3.46735725 | 3.465051022 | 4.066043375 |
| 12600.00 | 3.345540004 | 4.169628711 | 4.400907584 | 5.23933076 |
| 14400.00 | 3.514251042 | 4.700710144 | 5.300183236 | 6.377913325 |
| 16200.00 | 3.425819367 | 5.005064437 | 6.108233613 | 7.469023032 |
| 18000.00 | 3.093198297 | 5.050864159 | 6.775957643 | 8.441513396 |
| 19800.00 | 2.645115307 | 4.833319866 | 7.262781166 | 9.245696312 |
| 21600.00 | 2.255471824 | 4.375180955 | 7.539122414 | 9.840483121 |
| 23400.00 | 1.923225478 | 3.83053128 | 7.58818955 | 10.19548398 |
| 25200.00 | 1.63992128 | 3.348788204 | 7.407001015 | 10.29256059 |
| 27000.00 | 1.398349717 | 2.927631082 | 7.006566707 | 10.12675296 |
| 28800.00 | 1.192363289 | 2.55944038 | 6.420518003 | 9.706532801 |
| 30600.00 | 1.016720064 | 2.237554826 | 5.796383321 | 9.053370705 |
| 32400.00 | 0.866950281 | 1.956150899 | 5.232920396 | 8.266989578 |
| 34200.00 | 0.739242606 | 1.710137466 | 4.724231361 | 7.527285772 |
| 36000.00 | 0.63034714 | 1.495063675 | 4.264991681 | 6.853768299 |
| 37800.00 | 0.537492717 | 1.307038433 | 3.850394413 | 6.240515017 |
| 39600.00 | 0.458316383 | 1.142660003 | 3.476099895 | 5.682133678 |
| 41400.00 | 0.390803261 | 0.998954469 | 3.138190321 | 5.173714517 |
| 43200.00 | 0.333235282 | 0.873321923 | 2.833128733 | 4.710787077 |
| 45000.00 | 0.284147457 | 0.763489433 | 2.557721999 | 4.289280905 |
| 46800.00 | 0.242290604 | 0.66746992 | 2.309087386 | 3.905489759 |
| 48600.00 | 0.206599549 | 0.583526208 | 2.084622394 | 3.556039017 |
| 50400.00 | 0.17616603 | 0.510139597 | 1.881977509 | 3.237856011 |
| 52200.00 | 0.150215575 | 0.445982382 | 1.699031611 | 2.948143004 |
| 54000.00 | 0.128087799 | 0.389893837 | 1.533869773 | 2.68435259 |
| 55800.00 | 0.109219594 | 0.340859215 | 1.384763218 | 2.4441653 |
| 57600.00 | 0.093130805 | 0.297991384 | 1.250151221 | 2.2254692 |
| 59400.00 | 0.079412004 | 0.260514785 | 1.128624775 | 2.026341329 |
| 61200.00 | 0.067714075 | 0.227751394 | 1.018911841 | 1.845030783 |
| 63000.00 | 0.057739331 | 0.199108459 | 0.919864036 | 1.679943326 |
| 64800.00 | 0.049233935 | 0.174067776 | 0.830444608 | 1.529627366 |
| 66600.00 | 0.041981441 | 0.15217631 | 0.749717589 | 1.392761198 |
| 68400.00 | 0.035797289 | 0.133038003 | 0.676837994 | 1.268141377 |
| 70200.00 | 0.030524105 | 0.116306606 | 0.611042981 | 1.15467214 |
| 72000.00 | 0.026027697 | 0.101679418 | 0.551643862 | 1.051355767 |
| 73800.00 | 0.02219364 | 0.088891804 | 0.498018895 | 0.957283813 |
| 75600.00 | 0.018924366 | 0.077712412 | 0.449606778 | 0.871629117 |
| 77400.00 | 0.016136678 | 0.067938985 | 0.405900775 | 0.79363853 |
| 79200.00 | 0.013759635 | 0.059394704 | 0.366443405 | 0.722626291 |
| 81000.00 | 0.011732748 | 0.051924987 | 0.330821663 | 0.657968 |
| 82800.00 | 0.010004434 | 0.045394691 | 0.298662689 | 0.599095126 |
| 84600.00 | 0.008530713 | 0.039685671 | 0.269629869 | 0.545490009 |
| 86400.00 | 0.007274081 | 0.034694641 | 0.243419312 | 0.496681306 |



DA RP1 406L DRAINAGE CALCULATIONS

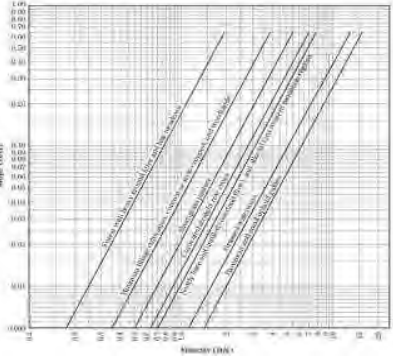
Time of Concentration:

$T_c = T_{OL} + T_1 + \dots + T_n$

Equation 2.1
 $T_{OL} = \frac{L}{V}$
 where:
 T_{OL} = travel time (min)
 L = length of overland flow (ft)
 V = velocity (ft/min)
 $V = 4.47 \sqrt{S}$
 S = slope (ft/ft)
 (The following is a summary of the following calculations)
 1) Slope = 0.0035 (ft/ft)
 2) Velocity = 0.15 (ft/min)
 3) Length = 100 (ft)
 4) Travel time = 15.92 (min)

Table 2.1 Manning's Roughness Coefficients Overland Flow

| Surface | n |
|--------------------|------|
| Grass (medium) | 0.05 |
| Grass (long) | 0.06 |
| Grass (short) | 0.07 |
| Grass (very short) | 0.08 |
| Grass (bare) | 0.09 |
| Grass (matted) | 0.10 |
| Grass (clipped) | 0.11 |
| Grass (matted) | 0.12 |
| Grass (matted) | 0.13 |
| Grass (matted) | 0.14 |
| Grass (matted) | 0.15 |
| Grass (matted) | 0.16 |
| Grass (matted) | 0.17 |
| Grass (matted) | 0.18 |
| Grass (matted) | 0.19 |
| Grass (matted) | 0.20 |
| Grass (matted) | 0.21 |
| Grass (matted) | 0.22 |
| Grass (matted) | 0.23 |
| Grass (matted) | 0.24 |
| Grass (matted) | 0.25 |
| Grass (matted) | 0.26 |
| Grass (matted) | 0.27 |
| Grass (matted) | 0.28 |
| Grass (matted) | 0.29 |
| Grass (matted) | 0.30 |
| Grass (matted) | 0.31 |
| Grass (matted) | 0.32 |
| Grass (matted) | 0.33 |
| Grass (matted) | 0.34 |
| Grass (matted) | 0.35 |
| Grass (matted) | 0.36 |
| Grass (matted) | 0.37 |
| Grass (matted) | 0.38 |
| Grass (matted) | 0.39 |
| Grass (matted) | 0.40 |
| Grass (matted) | 0.41 |
| Grass (matted) | 0.42 |
| Grass (matted) | 0.43 |
| Grass (matted) | 0.44 |
| Grass (matted) | 0.45 |
| Grass (matted) | 0.46 |
| Grass (matted) | 0.47 |
| Grass (matted) | 0.48 |
| Grass (matted) | 0.49 |
| Grass (matted) | 0.50 |
| Grass (matted) | 0.51 |
| Grass (matted) | 0.52 |
| Grass (matted) | 0.53 |
| Grass (matted) | 0.54 |
| Grass (matted) | 0.55 |
| Grass (matted) | 0.56 |
| Grass (matted) | 0.57 |
| Grass (matted) | 0.58 |
| Grass (matted) | 0.59 |
| Grass (matted) | 0.60 |
| Grass (matted) | 0.61 |
| Grass (matted) | 0.62 |
| Grass (matted) | 0.63 |
| Grass (matted) | 0.64 |
| Grass (matted) | 0.65 |
| Grass (matted) | 0.66 |
| Grass (matted) | 0.67 |
| Grass (matted) | 0.68 |
| Grass (matted) | 0.69 |
| Grass (matted) | 0.70 |
| Grass (matted) | 0.71 |
| Grass (matted) | 0.72 |
| Grass (matted) | 0.73 |
| Grass (matted) | 0.74 |
| Grass (matted) | 0.75 |
| Grass (matted) | 0.76 |
| Grass (matted) | 0.77 |
| Grass (matted) | 0.78 |
| Grass (matted) | 0.79 |
| Grass (matted) | 0.80 |
| Grass (matted) | 0.81 |
| Grass (matted) | 0.82 |
| Grass (matted) | 0.83 |
| Grass (matted) | 0.84 |
| Grass (matted) | 0.85 |
| Grass (matted) | 0.86 |
| Grass (matted) | 0.87 |
| Grass (matted) | 0.88 |
| Grass (matted) | 0.89 |
| Grass (matted) | 0.90 |
| Grass (matted) | 0.91 |
| Grass (matted) | 0.92 |
| Grass (matted) | 0.93 |
| Grass (matted) | 0.94 |
| Grass (matted) | 0.95 |
| Grass (matted) | 0.96 |
| Grass (matted) | 0.97 |
| Grass (matted) | 0.98 |
| Grass (matted) | 0.99 |
| Grass (matted) | 1.00 |



| T_{OL} | T_1 | T_n | T_c |
|-------------|-------------|-------|-------------|
| 15.92 (min) | 25.93 (min) | | 41.85 (min) |

$T_c = 41.85$ (min)

Intensity:

SEE FIG. 2.1-2.1a

| | |
|-------------|--------------|
| I (500-YR)= | 7.68 (in/hr) |
| I (100-YR)= | 5.6 (in/hr) |
| I (10-YR)= | 3.8 (in/hr) |
| I (2-YR)= | 2.6 (in/hr) |

Peak Flow Rate:

$Q = CIA$
 $C = 0.35$ Mixed use area. Residential lots b/w 1/4 and 1/2 acres; sub-basin slope <1%; and golf course

| i (500-YR) | i (100-YR) | i (10-YR) | i (2-YR) |
|-----------------------|-------------------|-----------|----------|
| 7.68 | 5.6 | 3.8 | 2.6 |
| A RP1 406L= 3.02 (Ac) | | | |
| Q (500-YR)= | 8.12 (cfs) | | |
| Q (100-YR)= | 5.92 (cfs) | | |
| Q (10-YR)= | 4.02 (cfs) | | |
| Q (2-YR)= | 2.75 (cfs) | | |

DA RP1 406L EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 268364.45 cft
 Volume (100-yr) = 1.38*area*43560 = 181540.66 cft
 Volume (10-yr) = 0.70*area*43560 = 92085.84 cft
 Volume (2-yr) = 0.41*area*43560 = 53935.992 cft
 A= 3.02 Ac

TP = time to Qp in seconds

$Tp = \frac{V}{1.39 Qp}$

$Qp = \frac{Qp}{2} \left[2 - \cos \left(\frac{\pi t_i}{Tp} \right) \right]$
 $t_i = 1.25 Tp$

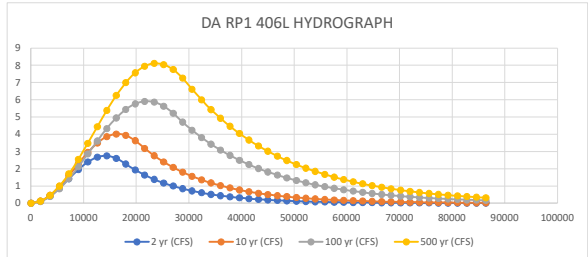
$Qp = 4.34 Qp^{0.8} \left(\frac{-1.8 t_i}{Tp} \right)^{0.5}$
 $t_i = 1.25 Tp$

| DA RP1 406L Existing Conditions | | | | |
|---------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 2.75 | 4.02 | 5.92 | 8.12 |
| TP= | 14119.377 | 16493.752 | 22064.601 | 23780.503 |
| 1.25*TP= | 17649.221 | 20617.190 | 27580.752 | 29725.629 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.108739932 | 0.116881593 | 0.096666759 | 0.114231109 |
| 3600.00 | 0.417749374 | 0.453921525 | 0.380352358 | 0.450495491 |
| 5400.00 | 0.878121165 | 0.971888841 | 0.83252526 | 0.989868138 |
| 7200.00 | 1.416991907 | 1.610492902 | 1.423647629 | 1.701993075 |
| 9000.00 | 1.949074114 | 2.295401127 | 2.115104867 | 2.546791806 |
| 10800.00 | 2.390154726 | 2.946891201 | 2.861728078 | 3.476718931 |
| 12600.00 | 2.670423576 | 3.48913063 | 3.614744695 | 4.439438013 |
| 14400.00 | 2.745522297 | 3.859003538 | 4.324964505 | 5.380767078 |
| 16200.00 | 2.603564957 | 4.013457257 | 4.945992963 | 6.247727986 |
| 18000.00 | 2.273961772 | 3.934513601 | 5.43726188 | 6.991528048 |
| 19800.00 | 1.92667148 | 3.631361496 | 5.766679502 | 7.570306084 |
| 21600.00 | 1.632421019 | 3.176713945 | 5.912726887 | 7.951488381 |
| 23400.00 | 1.383109893 | 2.756537632 | 5.865863603 | 8.113621942 |
| 25200.00 | 1.171874751 | 2.391937029 | 5.629150959 | 8.047581866 |
| 27000.00 | 0.992900448 | 2.075561271 | 5.218052019 | 7.757084898 |
| 28800.00 | 0.841259954 | 1.801031774 | 4.707891313 | 7.258480252 |
| 30600.00 | 0.71277872 | 1.562813633 | 4.234172366 | 6.614416383 |
| 32400.00 | 0.603919753 | 1.356104033 | 3.808120118 | 5.994555441 |
| 34200.00 | 0.511686247 | 1.176735414 | 3.424938235 | 5.432783915 |
| 36000.00 | 0.433539082 | 1.021091451 | 3.080313003 | 4.923658036 |
| 37800.00 | 0.367326925 | 0.886034141 | 2.770364762 | 4.462244189 |
| 39600.00 | 0.311227005 | 0.768840536 | 2.491604231 | 4.040471107 |
| 41400.00 | 0.263694931 | 0.667147847 | 2.240893232 | 3.66508654 |
| 43200.00 | 0.223422183 | 0.578905806 | 2.015409356 | 3.321617992 |
| 45000.00 | 0.189300082 | 0.502335328 | 1.81261419 | 3.010337126 |
| 46800.00 | 0.16038927 | 0.435892642 | 1.630224744 | 2.728227519 |
| 48600.00 | 0.135893855 | 0.378238171 | 1.466187748 | 2.472555426 |
| 50400.00 | 0.115139497 | 0.328209518 | 1.318565635 | 2.240843292 |
| 52200.00 | 0.097554844 | 0.284798034 | 1.185970255 | 2.030845742 |
| 54000.00 | 0.082655803 | 0.247128483 | 1.066635176 | 1.840527824 |
| 55800.00 | 0.070032214 | 0.214441393 | 0.95930787 | 1.688045288 |
| 57600.00 | 0.05933656 | 0.186077746 | 0.862780086 | 1.511726716 |
| 59400.00 | 0.050274398 | 0.16146569 | 0.775965152 | 1.370057324 |
| 61200.00 | 0.042596252 | 0.140109011 | 0.697885738 | 1.241664285 |
| 63000.00 | 0.036090749 | 0.121577129 | 0.627662855 | 1.125303423 |
| 64800.00 | 0.030578798 | 0.105496415 | 0.564505963 | 1.019847159 |
| 66600.00 | 0.025908658 | 0.091542658 | 0.507704063 | 0.924273584 |
| 68400.00 | 0.021951764 | 0.079434531 | 0.456617702 | 0.837656555 |
| 70200.00 | 0.018599186 | 0.068927916 | 0.410671769 | 0.759156722 |
| 72000.00 | 0.015758629 | 0.059810987 | 0.369349023 | 0.688013393 |
| 73800.00 | 0.013351896 | 0.051899931 | 0.332184267 | 0.623537163 |
| 75600.00 | 0.011312731 | 0.045035252 | 0.298759116 | 0.565103235 |
| 77400.00 | 0.009584997 | 0.039078548 | 0.26869728 | 0.512145362 |
| 79200.00 | 0.00812113 | 0.033909722 | 0.241660336 | 0.464150363 |
| 81000.00 | 0.006880833 | 0.029424565 | 0.217343913 | 0.42065315 |
| 82800.00 | 0.005829959 | 0.025532648 | 0.195474264 | 0.381232218 |
| 84600.00 | 0.00493958 | 0.022155506 | 0.17580519 | 0.345505564 |
| 86400.00 | 0.004185184 | 0.019225051 | 0.158115264 | 0.313126985 |

ti (hrs)

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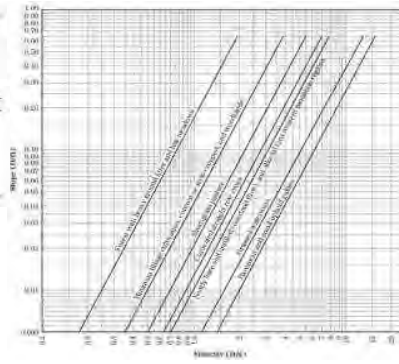
DA RP1 407 DRAINAGE CALCULATIONS

Time of Concentration:

$T_c = T_{OL} + T_1 + \dots + T_n$

Equation 2.1
 $T_c = T_{OL} + T_1 + \dots + T_n$
 where:
 T_c = Time of Concentration
 T_{OL} = Time of Overland Flow
 T_1 = Time of Flow in Pipe
 T_2 = Time of Flow in Channel
 T_n = Time of Flow in Reservoir
 (The following is a summary of the methods used to calculate the time of concentration for each component.)

| Parameter | Value |
|----------------------------------------------------|--------------------|
| Overland Flow Time (T _{OL}) | 15.92 (min) |
| Pipe Flow Time (T ₁) | 11.97 (min) |
| Channel Flow Time (T ₂) | 0 (min) |
| Reservoir Flow Time (T _n) | 0 (min) |
| Total Time of Concentration (T_c) | 27.88 (min) |



| T _{OL} = T _{OL} ; multiply by 60 to convert hrs. to min. (L = max 300') | | T ₁ = | |
|-------------------------------------------------------------------------------------------|--------------------|------------------------|--------------------|
| n = | 0.15 | D = | 359 (ft) |
| L = | 100 (ft) | S = | 0.0035 (ft/ft) |
| P ₂ = | 4.89 (in) | V = | 0.5 (ft/s) |
| S = | 0.0035 (ft/ft) | | |
| T_{OL} = | 15.92 (min) | T₁ = | 11.97 (min) |

T_c = 27.88 (min)

Intensity:

SEE FIG. 2.1-2.1a

| | |
|--------------|--------------|
| I (500-YR) = | 9.21 (in/hr) |
| I (100-YR) = | 7 (in/hr) |
| I (10-YR) = | 4.7 (in/hr) |
| I (2-YR) = | 3.3 (in/hr) |

Peak Flow Rate:

$Q = CIA$

C = 0.35 Mixed use area. Residential lots b/w 1/4 and 1/2 acres; sub-basin slope <1%; and golf course

| i (500-YR) | i (100-YR) | i (10-YR) | i (2-YR) |
|------------|------------|-----------|----------|
| 9.21 | 7 | 4.7 | 3.3 |

A RP1 407 = 1.96 (Ac)

Q (500-YR) = 6.32 (cfs)

Q (100-YR) = 4.80 (cfs)

Q (10-YR) = 3.22 (cfs)

Q (2-YR) = 2.26 (cfs)

DA RP1 407 EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 174170.30 cft
 Volume (100-yr) = 1.38*area*43560 = 117821.09 cft
 Volume (10-yr) = 0.70*area*43560 = 59764.32 cft
 Volume (2-yr) = 0.41*area*43560 = 35004.816 cft
 A= 1.96 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Qp}$

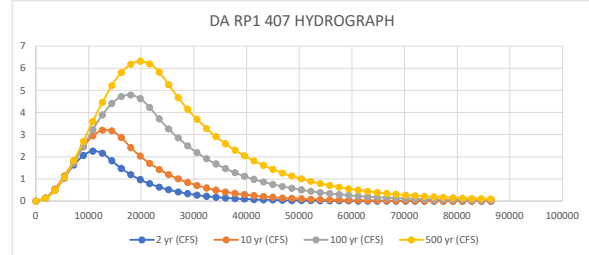
$Q_i = \frac{Q_p}{2} \left[1 - \cos \left(\frac{\pi t_i}{T_p} \right) \right]$ $t_i = 1.25 T_p$
 $Q_i = 4.34 Q_p \left(\frac{t_i}{T_p} \right)^{-1.81}$ $t_i = 1.25 T_p$

| DA RP1 407 Existing Conditions | | | | |
|--------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 2.26 | 3.22 | 4.80 | 6.32 |
| TP= | 11124.358 | 13335.374 | 17651.681 | 19836.504 |
| 1.25*TP= | 13905.447 | 16669.218 | 22064.601 | 24795.629 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.143120173 | 0.14278372 | 0.122156703 | 0.127469286 |
| 3600.00 | 0.536287772 | 0.545842168 | 0.476196775 | 0.499588055 |
| 5400.00 | 1.080076672 | 1.137777559 | 1.02609492 | 1.086319558 |
| 7200.00 | 1.636970905 | 1.813734441 | 1.715896332 | 1.840303895 |
| 9000.00 | 2.066140365 | 2.453973792 | 2.475410368 | 2.700680823 |
| 10800.00 | 2.259054603 | 2.945083595 | 3.227352788 | 3.598002284 |
| 12600.00 | 2.166928533 | 3.200068647 | 3.8952098 | 4.459838122 |
| 14400.00 | 1.825995602 | 3.173760886 | 4.41102371 | 5.216622516 |
| 16200.00 | 1.479606464 | 2.870820472 | 4.72230795 | 5.807269209 |
| 18000.00 | 1.198926923 | 2.420145835 | 4.797387836 | 6.184102275 |
| 19800.00 | 0.971491948 | 2.030647403 | 4.628623626 | 6.316704433 |
| 21600.00 | 0.787201111 | 1.703834875 | 4.233187896 | 6.194372281 |
| 23400.00 | 0.637870021 | 1.429619577 | 3.719384662 | 5.826980245 |
| 25200.00 | 0.516866856 | 1.199536508 | 3.257607284 | 5.257100302 |
| 27000.00 | 0.418817844 | 1.006483023 | 2.853161526 | 4.672130903 |
| 28800.00 | 0.33936861 | 0.844499578 | 2.498929423 | 4.152252368 |
| 30600.00 | 0.274990799 | 0.70858576 | 2.188676738 | 3.690222189 |
| 32400.00 | 0.22282538 | 0.594545921 | 1.91694324 | 3.279602584 |
| 34200.00 | 0.180555677 | 0.498859661 | 1.678946608 | 2.914673813 |
| 36000.00 | 0.146304485 | 0.418573154 | 1.470498267 | 2.590351489 |
| 37800.00 | 0.118550703 | 0.351207963 | 1.287929671 | 2.302117241 |
| 39600.00 | 0.096061779 | 0.29468453 | 1.128027741 | 2.045955468 |
| 41400.00 | 0.077838977 | 0.247257982 | 0.987978313 | 1.818297392 |
| 43200.00 | 0.063073018 | 0.207464266 | 0.865316616 | 1.615971343 |
| 45000.00 | 0.051108143 | 0.174074953 | 0.757883889 | 1.43615857 |
| 46800.00 | 0.041412991 | 0.146059319 | 0.66378939 | 1.276353969 |
| 48600.00 | 0.033556997 | 0.122525222 | 0.581377123 | 1.134331187 |
| 50400.00 | 0.027191276 | 0.102828911 | 0.509196687 | 1.008111599 |
| 52200.00 | 0.022033124 | 0.086279619 | 0.445977759 | 0.89593675 |
| 54000.00 | 0.017853467 | 0.072393772 | 0.390607729 | 0.796243848 |
| 55800.00 | 0.014466686 | 0.060742713 | 0.342112123 | 0.707644001 |
| 57600.00 | 0.011722373 | 0.050966777 | 0.299637452 | 0.628902858 |
| 59400.00 | 0.009498654 | 0.042764181 | 0.262436192 | 0.55892342 |
| 61200.00 | 0.007696771 | 0.03588171 | 0.229853626 | 0.496730751 |
| 63000.00 | 0.006236703 | 0.030106906 | 0.201316324 | 0.441458401 |
| 64800.00 | 0.005053608 | 0.025261498 | 0.176322048 | 0.39233633 |
| 66600.00 | 0.004094944 | 0.021195911 | 0.154430918 | 0.348680182 |
| 68400.00 | 0.003318139 | 0.01778464 | 0.135257665 | 0.309881753 |
| 70200.00 | 0.002688692 | 0.014922379 | 0.118464852 | 0.275400512 |
| 72000.00 | 0.00217865 | 0.01252077 | 0.103756938 | 0.244756076 |
| 73800.00 | 0.001765363 | 0.010505676 | 0.090875075 | 0.217521516 |
| 75600.00 | 0.001430476 | 0.008814892 | 0.079592549 | 0.193317407 |
| 77400.00 | 0.001159116 | 0.007396223 | 0.069710796 | 0.171806543 |
| 79200.00 | 0.000939233 | 0.006205874 | 0.061055905 | 0.152689242 |
| 81000.00 | 0.000761062 | 0.0052071 | 0.053475556 | 0.135699166 |
| 82800.00 | 0.000616689 | 0.004369069 | 0.046836339 | 0.120599614 |
| 84600.00 | 0.000499704 | 0.003665911 | 0.041021409 | 0.107180223 |
| 86400.00 | 0.000404911 | 0.003075919 | 0.035928427 | 0.095254038 |

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DA RP1 408 EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 103969.01 cft
 Volume (100-yr) = 1.38*area*43560 = 70331.98 cft
 Volume (10-yr) = 0.70*area*43560 = 35675.64 cft
 Volume (2-yr) = 0.41*area*43560 = 20895.732 cft
 A= 1.17 Ac

TP = time to Qp in seconds
 TP = $\frac{V}{1.39 Qp}$

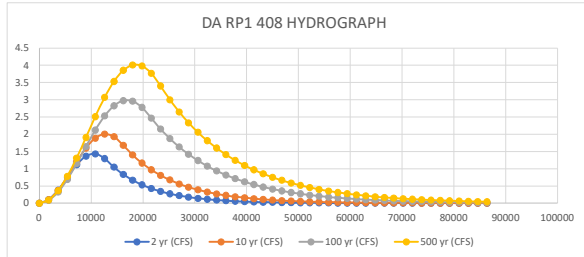
$$Q_t = \frac{Q_p}{2} \left[2 - \cos \left(\frac{\pi t}{TP} \right) \right] \quad t_1 = 1.25 TP$$

$$Q_t = 4.34 Q_p \left(\frac{t}{TP} \right)^{-1.81} \quad t_1 = 1.25 TP$$

| DA RP1 408 Existing Conditions | | | | |
|--------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 1.43 | 2.01 | 2.99 | 4.02 |
| TP= | 10488.680 | 12791.073 | 16926.270 | 18607.849 |
| 1.25*TP= | 13110.850 | 15988.842 | 21157.837 | 23259.812 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.101652876 | 0.096457439 | 0.082641042 | 0.092095916 |
| 3600.00 | 0.37777269 | 0.367282425 | 0.321425669 | 0.359943558 |
| 5400.00 | 0.750024545 | 0.760399335 | 0.689948931 | 0.778996106 |
| 7200.00 | 1.112800985 | 1.200217628 | 1.147459298 | 1.310849607 |
| 9000.00 | 1.363182718 | 1.602166779 | 1.643364992 | 1.906762495 |
| 10800.00 | 1.430136713 | 1.888957937 | 2.122828454 | 2.512122502 |
| 12600.00 | 1.294668193 | 2.005445423 | 2.53283032 | 3.071451582 |
| 14400.00 | 1.043977197 | 1.929230424 | 2.828032331 | 3.533490176 |
| 16200.00 | 0.835220084 | 1.678382335 | 2.975790866 | 3.85589489 |
| 18000.00 | 0.66820673 | 1.397787111 | 2.959766694 | 4.009119032 |
| 19800.00 | 0.534589916 | 1.164102342 | 2.78173178 | 3.979120421 |
| 21600.00 | 0.427691559 | 0.969485448 | 2.469388539 | 3.76864827 |
| 23400.00 | 0.342168949 | 0.807404985 | 2.150550635 | 3.401736306 |
| 25200.00 | 0.273747721 | 0.672421449 | 1.872879849 | 2.999760934 |
| 27000.00 | 0.219008227 | 0.560004723 | 1.631060841 | 2.645286068 |
| 28800.00 | 0.175214622 | 0.466382044 | 1.420464569 | 2.332698684 |
| 30600.00 | 0.14017813 | 0.388411386 | 1.237059674 | 2.057049033 |
| 32400.00 | 0.11214765 | 0.323476015 | 1.07733531 | 1.81397227 |
| 34200.00 | 0.089722237 | 0.269396665 | 0.938233939 | 1.599619329 |
| 36000.00 | 0.071781084 | 0.224358407 | 0.817092799 | 1.410595984 |
| 37800.00 | 0.057427502 | 0.186849732 | 0.711592935 | 1.243909094 |
| 39600.00 | 0.04594411 | 0.15561183 | 0.619714805 | 1.096919211 |
| 41400.00 | 0.036756975 | 0.129596342 | 0.539699625 | 0.967298785 |
| 43200.00 | 0.029406929 | 0.107930173 | 0.470015695 | 0.852995307 |
| 45000.00 | 0.023526623 | 0.089886197 | 0.409329085 | 0.752198809 |
| 46800.00 | 0.018822162 | 0.074858848 | 0.356478096 | 0.663313202 |
| 48600.00 | 0.015058421 | 0.0623438 | 0.310451022 | 0.584931003 |
| 50400.00 | 0.012047289 | 0.051921042 | 0.270366786 | 0.515811049 |
| 52200.00 | 0.009638274 | 0.043240781 | 0.235458071 | 0.454858841 |
| 54000.00 | 0.007710973 | 0.036011703 | 0.205056635 | 0.401109215 |
| 55800.00 | 0.006169061 | 0.029991197 | 0.178580515 | 0.35371106 |
| 57600.00 | 0.004935476 | 0.02497721 | 0.155522889 | 0.311913836 |
| 59400.00 | 0.003948562 | 0.020801471 | 0.135442375 | 0.275055694 |
| 61200.00 | 0.003158994 | 0.017323841 | 0.117954579 | 0.242552993 |
| 63000.00 | 0.002527311 | 0.014427608 | 0.10272474 | 0.213891063 |
| 64800.00 | 0.002021942 | 0.012015572 | 0.089461318 | 0.188616047 |
| 66600.00 | 0.001617628 | 0.010006785 | 0.077910419 | 0.166327721 |
| 68400.00 | 0.001294162 | 0.008333832 | 0.067850926 | 0.146673156 |
| 70200.00 | 0.001035377 | 0.006940565 | 0.059090277 | 0.129341126 |
| 72000.00 | 0.000828339 | 0.005780228 | 0.051460769 | 0.114057182 |
| 73800.00 | 0.000662702 | 0.004813878 | 0.044816353 | 0.100579306 |
| 75600.00 | 0.000530186 | 0.004009085 | 0.039029839 | 0.088694081 |
| 77400.00 | 0.000424168 | 0.003338838 | 0.033990457 | 0.078213305 |
| 79200.00 | 0.00033935 | 0.002780645 | 0.029601741 | 0.068971018 |
| 81000.00 | 0.000271493 | 0.002315771 | 0.025779678 | 0.060820871 |
| 82800.00 | 0.000217204 | 0.001928616 | 0.022451106 | 0.053633808 |
| 84600.00 | 0.000173771 | 0.001606186 | 0.019552306 | 0.047296024 |
| 86400.00 | 0.000139023 | 0.001337661 | 0.017027788 | 0.041707162 |

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 16.5
 17
 17.5
 18
 18.5
 19
 19.5
 20
 20.5
 21
 21.5
 22
 22.5
 23
 23.5
 24



DA RP1 409 DRAINAGE CALCULATIONS

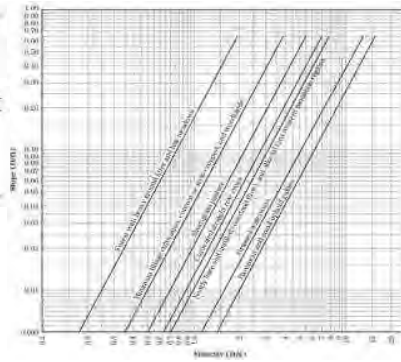
Time of Concentration:

$T_c = T_{OL} + T_1 + \dots + T_n$

Equation 2.1
 $T_{OL} = \frac{L}{V}$
 where:
 T_{OL} = travel time (min)
 L = length of overland flow (ft)
 V = velocity (ft/min)
 $V = 4.47 \sqrt{S}$ (ft/min) (Manning's equation)
 n = Manning's roughness coefficient
 S = slope (ft/ft)
 (The velocity of flow in a pipe or channel is given by the Manning equation: $V = \frac{1.49 R^{2/3} S^{1/2}}{n}$)
 where:
 V = velocity (ft/s)
 R = hydraulic radius (ft)
 S = slope (ft/ft)
 n = Manning's roughness coefficient
 (The velocity of flow in a pipe or channel is given by the Manning equation: $V = \frac{1.49 R^{2/3} S^{1/2}}{n}$)
 where:
 V = velocity (ft/s)
 R = hydraulic radius (ft)
 S = slope (ft/ft)
 n = Manning's roughness coefficient

Table 2.1 Manning's Roughness Coefficients Overland Flow

| Surface | n |
|-------------------------------------------|-------|
| Grass (smooth, mowed) | 0.05 |
| Grass (rough, mowed) | 0.055 |
| Grass (smooth, unmowed) | 0.06 |
| Grass (rough, unmowed) | 0.065 |
| Grass (smooth, mowed) - 1/4 to 1/2 acre | 0.07 |
| Grass (rough, mowed) - 1/4 to 1/2 acre | 0.075 |
| Grass (smooth, unmowed) - 1/4 to 1/2 acre | 0.08 |
| Grass (rough, unmowed) - 1/4 to 1/2 acre | 0.085 |
| Grass (smooth, mowed) - 1/2 to 1 acre | 0.09 |
| Grass (rough, mowed) - 1/2 to 1 acre | 0.095 |
| Grass (smooth, unmowed) - 1/2 to 1 acre | 0.10 |
| Grass (rough, unmowed) - 1/2 to 1 acre | 0.105 |
| Grass (smooth, mowed) - 1 to 2 acres | 0.11 |
| Grass (rough, mowed) - 1 to 2 acres | 0.115 |
| Grass (smooth, unmowed) - 1 to 2 acres | 0.12 |
| Grass (rough, unmowed) - 1 to 2 acres | 0.125 |
| Grass (smooth, mowed) - 2+ acres | 0.13 |
| Grass (rough, mowed) - 2+ acres | 0.135 |
| Grass (smooth, unmowed) - 2+ acres | 0.14 |
| Grass (rough, unmowed) - 2+ acres | 0.145 |



| T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | $T_$ |
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DA RP1 409 EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 250591.97 cft
 Volume (100-yr) = 1.38*area*43560 = 169518.10 cft
 Volume (10-yr) = 0.70*area*43560 = 85987.44 cft
 Volume (2-yr) = 0.41*area*43560 = 50364.072 cft
 A= 2.82 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Qp}$

$Qp = \frac{Qp}{2} \left[2 - \cos\left(\frac{\pi t_i}{TP}\right) \right]$ $t_i = 1.25 TP$

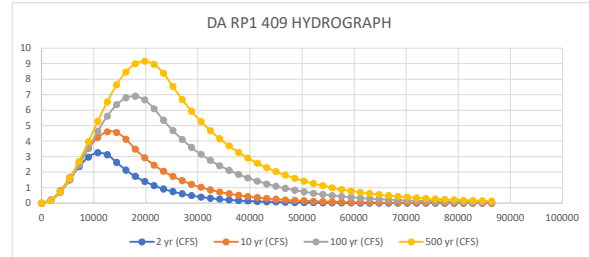
$Qp = 4.34 Qp \left(\frac{t_i}{TP} \right)^{-1.81}$ $t_i = 1.25 TP$

| DA RP1 409 Existing Conditions | | | | |
|--------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 3.26 | 4.64 | 6.91 | 9.16 |
| TP= | 11124.358 | 13335.374 | 17651.681 | 19682.601 |
| 1.25*TP= | 13905.447 | 16669.218 | 22064.601 | 24603.252 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.205917801 | 0.20543372 | 0.175756073 | 0.187715545 |
| 3600.00 | 0.771597713 | 0.785344344 | 0.685140259 | 0.73547388 |
| 5400.00 | 1.553987864 | 1.637006488 | 1.476320243 | 1.59837159 |
| 7200.00 | 2.355233649 | 2.609556695 | 2.468789621 | 2.705671178 |
| 9000.00 | 2.972712158 | 3.530717394 | 3.561559816 | 3.966599887 |
| 10800.00 | 3.250272439 | 4.237314152 | 4.643436154 | 5.277790957 |
| 12600.00 | 3.117723706 | 4.6041804 | 5.604332467 | 6.531757283 |
| 14400.00 | 2.627197754 | 4.566329438 | 6.346472889 | 7.625702856 |
| 16200.00 | 2.128821545 | 4.130466189 | 6.79434103 | 8.46994964 |
| 18000.00 | 1.724986695 | 3.482046558 | 6.902364131 | 8.995289077 |
| 19800.00 | 1.397758824 | 2.921645754 | 6.659550318 | 9.158655579 |
| 21600.00 | 1.13260568 | 2.451435892 | 6.090607075 | 8.946656902 |
| 23400.00 | 0.917751764 | 2.056901637 | 5.351359565 | 8.376671994 |
| 25200.00 | 0.743655374 | 1.725863751 | 4.686965582 | 7.525124729 |
| 27000.00 | 0.602584857 | 1.448103124 | 4.10505893 | 6.681621258 |
| 28800.00 | 0.488275245 | 1.215045311 | 3.595398456 | 5.932667463 |
| 30600.00 | 0.395650026 | 1.019495838 | 3.149014491 | 5.267665117 |
| 32400.00 | 0.320595699 | 0.85541811 | 2.758050988 | 4.677203965 |
| 34200.00 | 0.259779086 | 0.717747063 | 2.415627262 | 4.152928565 |
| 36000.00 | 0.21049931 | 0.602232803 | 2.115716894 | 3.687420047 |
| 37800.00 | 0.170567848 | 0.505309416 | 1.85304167 | 3.274091136 |
| 39600.00 | 0.138211335 | 0.423984885 | 1.622978688 | 2.907092935 |
| 41400.00 | 0.111992814 | 0.355748729 | 1.421479002 | 2.581232159 |
| 43200.00 | 0.090747914 | 0.298494505 | 1.244996356 | 2.291897648 |
| 45000.00 | 0.073533145 | 0.25045478 | 1.090424779 | 2.034995113 |
| 46800.00 | 0.059583997 | 0.210146571 | 0.955043918 | 1.8068892 |
| 48600.00 | 0.048280986 | 0.176325568 | 0.836471166 | 1.604352051 |
| 50400.00 | 0.039122142 | 0.147947719 | 0.732619724 | 1.42451762 |
| 52200.00 | 0.031700719 | 0.124137003 | 0.641661878 | 1.264841123 |
| 54000.00 | 0.025687131 | 0.104158386 | 0.561996835 | 1.123063024 |
| 55800.00 | 0.020814314 | 0.087395128 | 0.492222545 | 0.997177063 |
| 57600.00 | 0.016865864 | 0.073329751 | 0.431111029 | 0.885401864 |
| 59400.00 | 0.01366643 | 0.061528056 | 0.377586766 | 0.786155729 |
| 61200.00 | 0.011073925 | 0.051625726 | 0.330707768 | 0.698034254 |
| 63000.00 | 0.008973215 | 0.043317078 | 0.289648996 | 0.619790459 |
| 64800.00 | 0.007271007 | 0.036345625 | 0.253687845 | 0.550317139 |
| 66600.00 | 0.005891706 | 0.030496158 | 0.222191423 | 0.488631195 |
| 68400.00 | 0.004774056 | 0.025588104 | 0.194605416 | 0.43385973 |
| 70200.00 | 0.003868424 | 0.021469953 | 0.170444328 | 0.385227687 |
| 72000.00 | 0.003134588 | 0.018014577 | 0.149282942 | 0.342046889 |
| 73800.00 | 0.002539961 | 0.01511531 | 0.130748832 | 0.303706297 |
| 75600.00 | 0.002058133 | 0.012682651 | 0.11451581 | 0.269663364 |
| 77400.00 | 0.001667708 | 0.010641504 | 0.100298186 | 0.239436359 |
| 79200.00 | 0.001351346 | 0.00892886 | 0.087845741 | 0.212597548 |
| 81000.00 | 0.001094997 | 0.007491849 | 0.07693932 | 0.188767143 |
| 82800.00 | 0.000887278 | 0.00628611 | 0.067386977 | 0.167607927 |
| 84600.00 | 0.000718962 | 0.005274423 | 0.059020598 | 0.148820482 |
| 86400.00 | 0.000582576 | 0.004425557 | 0.051692941 | 0.132138952 |

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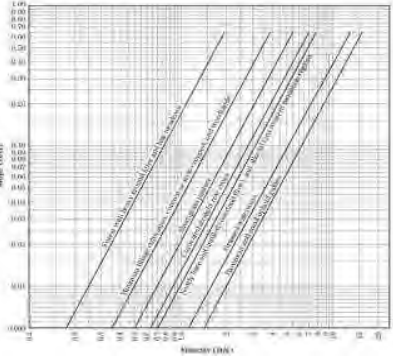
DA RP1 409A DRAINAGE CALCULATIONS

Time of Concentration:

$T_c = T_{OL} + T_1 + \dots + T_n$

Equation 3.3
 $T_{OL} = \frac{L}{V}$
 where:
 T_{OL} = travel time (min)
 L = length of overland flow (ft)
 V = velocity (ft/min)
 $V = 4.47 \sqrt{S}$
 S = slope (ft/ft)
 (The following is a summary of the following calculations:
 1) Slope = 0.0026 (ft/ft)
 2) Velocity = 0.026 (ft/s)
 3) Length = 100 (ft)
 4) Travel time = 17.93 (min)

| Parameter | Value |
|-----------------------------------|--------|
| Subsidence | 0 |
| Design Rainfall Intensity (in/hr) | 4.89 |
| Design Rainfall Depth (in) | 0.24 |
| Design Rainfall Duration (hr) | 0.25 |
| Design Rainfall Intensity (ft/hr) | 0.1245 |
| Design Rainfall Depth (ft) | 0.024 |
| Design Rainfall Duration (min) | 15 |
| Design Rainfall Intensity (in/hr) | 4.89 |
| Design Rainfall Depth (in) | 0.24 |
| Design Rainfall Duration (hr) | 0.25 |
| Design Rainfall Intensity (ft/hr) | 0.1245 |
| Design Rainfall Depth (ft) | 0.024 |
| Design Rainfall Duration (min) | 15 |



| T _{OL} = T _{OL} ; multiply by 60 to convert hrs. to min. (L = max 300') | | T = | |
|-------------------------------------------------------------------------------------------|----------------|------------------|----------------|
| n = | 0.15 | D = | 142 (ft) |
| L = | 100 (ft) | S = | 0.0026 (ft/ft) |
| P ₂ = | 4.89 (in) | V = | 0.5 (ft/s) |
| S = | 0.0026 (ft/ft) | | |
| T _{OL} = | 17.93 (min) | T ₁ = | 4.73 (min) |

T_c = 22.66 (min)

Intensity:

SEE FIG. 2.1-2.1a

| | |
|--------------|---------------|
| I (500-YR) = | 10.46 (in/hr) |
| I (100-YR) = | 7 (in/hr) |
| I (10-YR) = | 5.3 (in/hr) |
| I (2-YR) = | 3.7 (in/hr) |

Peak Flow Rate:

Q = CIA
 C = 0.35 Mixed use area. Residential lots b/w 1/4 and 1/2 acres; sub-basin slope <1%; and golf course

| i (500-YR) | i (100-YR) | i (10-YR) | i (2-YR) |
|--------------|------------|-----------|----------|
| 10.46 | 7 | 5.3 | 3.7 |
| A RP1 409A = | 0.69 (Ac) | | |
| Q (500-YR) = | 2.53 (cfs) | | |
| Q (100-YR) = | 1.69 (cfs) | | |
| Q (10-YR) = | 1.28 (cfs) | | |
| Q (2-YR) = | 0.89 (cfs) | | |

DA RP1 409A EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 61315.06 cft
 Volume (100-yr) = 1.38*area*43560 = 41477.83 cft
 Volume (10-yr) = 0.70*area*43560 = 21039.48 cft
 Volume (2-yr) = 0.41*area*43560 = 12323.124 cft
 A= 0.69 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

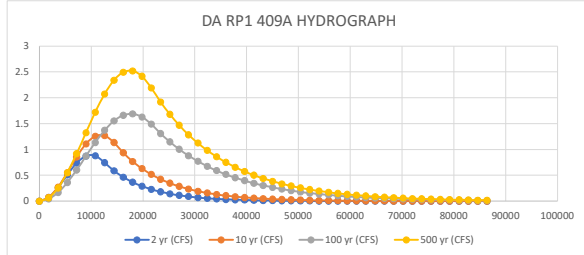
$Q_t = \frac{Q_p}{2} \left[2 - \cos \left(\frac{\pi t_i}{T_p} \right) \right]$
 $t_i = 1.25 T_p$
 $Q_t = 4.34 Q_p e^{-1.8 t_i / T_p}$
 $t_i = 1.25 T_p$

| DA RP1 409A Existing Conditions | | | | |
|---------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 0.89 | 1.28 | 1.69 | 2.53 |
| TP= | 9921.724 | 11825.709 | 17651.681 | 17459.365 |
| 1.25*TP= | 12402.155 | 14782.137 | 22064.601 | 21824.206 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.070622151 | 0.071784729 | 0.043004146 | 0.065682833 |
| 3600.00 | 0.260161981 | 0.271035014 | 0.167640702 | 0.255901033 |
| 5400.00 | 0.508698007 | 0.553051834 | 0.361227293 | 0.55087397 |
| 7200.00 | 0.737657576 | 0.854568654 | 0.604065546 | 0.919927665 |
| 9000.00 | 0.874656972 | 1.107944382 | 0.871445487 | 1.324684541 |
| 10800.00 | 0.876384945 | 1.256337713 | 1.13615991 | 1.723054279 |
| 12600.00 | 0.744084009 | 1.266458672 | 1.371272838 | 2.073610752 |
| 14400.00 | 0.587753619 | 1.136036765 | 1.552860388 | 2.339899896 |
| 16200.00 | 0.464267895 | 0.935971418 | 1.662445146 | 2.49423053 |
| 18000.00 | 0.366726246 | 0.767939514 | 1.68887633 | 2.520553946 |
| 19800.00 | 0.28967788 | 0.630073832 | 1.62946444 | 2.416132794 |
| 21600.00 | 0.228817203 | 0.516958726 | 1.490254923 | 2.19182574 |
| 23400.00 | 0.180743219 | 0.424150808 | 1.309375213 | 1.920121435 |
| 25200.00 | 0.142769472 | 0.348004393 | 1.146810728 | 1.679276318 |
| 27000.00 | 0.112773925 | 0.285528297 | 1.004429313 | 1.468640942 |
| 28800.00 | 0.089080375 | 0.234268331 | 0.879725154 | 1.284426031 |
| 30600.00 | 0.070364787 | 0.192210899 | 0.770503546 | 1.123317607 |
| 32400.00 | 0.055581302 | 0.157703902 | 0.674842263 | 0.982417373 |
| 34200.00 | 0.043903794 | 0.129391834 | 0.591057734 | 0.859190569 |
| 36000.00 | 0.034679705 | 0.106162539 | 0.51767541 | 0.751420379 |
| 37800.00 | 0.027393576 | 0.087103523 | 0.453403813 | 0.657168043 |
| 39600.00 | 0.021638247 | 0.071466111 | 0.397111807 | 0.574737989 |
| 41400.00 | 0.0170921 | 0.058636033 | 0.347808692 | 0.50264732 |
| 43200.00 | 0.013501088 | 0.048109297 | 0.304626768 | 0.439599145 |
| 45000.00 | 0.010664539 | 0.039472391 | 0.266806063 | 0.384459243 |
| 46800.00 | 0.008423943 | 0.032386041 | 0.233680959 | 0.336235662 |
| 48600.00 | 0.006654092 | 0.026571881 | 0.204668477 | 0.294060873 |
| 50400.00 | 0.005256082 | 0.021801517 | 0.179258017 | 0.257176161 |
| 52200.00 | 0.004151791 | 0.017887562 | 0.157002374 | 0.224917981 |
| 54000.00 | 0.003279509 | 0.014676266 | 0.137509864 | 0.196706017 |
| 55800.00 | 0.002590491 | 0.012041484 | 0.120437431 | 0.172032742 |
| 57600.00 | 0.002046235 | 0.009879715 | 0.105484613 | 0.150454292 |
| 59400.00 | 0.001616325 | 0.008106042 | 0.092388251 | 0.131582474 |
| 61200.00 | 0.001276739 | 0.006650791 | 0.080917858 | 0.115077791 |
| 63000.00 | 0.001008499 | 0.005456796 | 0.070871563 | 0.100643326 |
| 64800.00 | 0.000796616 | 0.004477155 | 0.062072558 | 0.088019409 |
| 66600.00 | 0.000629248 | 0.003673386 | 0.054365987 | 0.076978938 |
| 68400.00 | 0.000497045 | 0.003013915 | 0.047616219 | 0.067323298 |
| 70200.00 | 0.000392617 | 0.002472837 | 0.041704463 | 0.058878787 |
| 72000.00 | 0.000310129 | 0.002028896 | 0.036526677 | 0.051493489 |
| 73800.00 | 0.000244971 | 0.001664655 | 0.031991735 | 0.045034546 |
| 75600.00 | 0.000193504 | 0.001365805 | 0.028019826 | 0.039385762 |
| 77400.00 | 0.000152849 | 0.001120607 | 0.024541046 | 0.034445518 |
| 79200.00 | 0.000120736 | 0.000919428 | 0.021494171 | 0.03012494 |
| 81000.00 | 9.53694E-05 | 0.000754366 | 0.018825578 | 0.026346302 |
| 82800.00 | 7.53325E-05 | 0.000618937 | 0.016488303 | 0.023041626 |
| 84600.00 | 5.95053E-05 | 0.000507821 | 0.01444121 | 0.020151464 |
| 86400.00 | 4.70034E-05 | 0.000416654 | 0.012648273 | 0.017623821 |

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DA RP1 501 DRAINAGE CALCULATIONS

Time of Concentration:

$$T_c = T_{OL} + T_1 + \dots + T_n$$

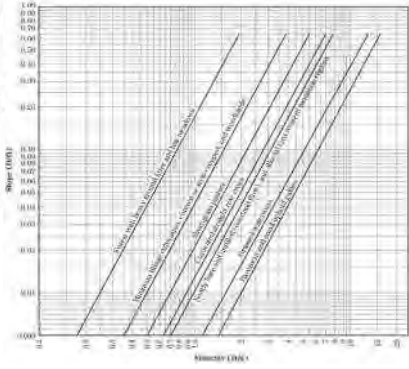
Equation 5.3
 T_{OL} = (L/n) / 4.83
 T₁ = (S/P₁) / 4.83
 T₂ = (S/P₂) / 4.83
 T_n = (S/P_n) / 4.83
 T_c = T_{OL} + T₁ + T₂ + ... + T_n

Table 5.3 Manning's Roughness Coefficients for Open Channel Flow

| Surface | n |
|-----------------------------------|-------|
| Smoothed Concrete (finished) | 0.012 |
| Cast-in-place concrete (finished) | 0.012 |
| Asphalt (finished) | 0.016 |
| Gravel (finished) | 0.017 |
| Grass (finished) | 0.022 |
| Earth (finished) | 0.024 |
| Rock (finished) | 0.035 |
| Wood (finished) | 0.040 |
| Unfinished concrete | 0.015 |
| Unfinished asphalt | 0.018 |
| Unfinished gravel | 0.020 |
| Unfinished grass | 0.025 |
| Unfinished earth | 0.028 |
| Unfinished rock | 0.040 |
| Unfinished wood | 0.045 |

| | | |
|-------------------|-----------------------------------------------------------------------|------------------|
| $T_{OL} =$ | $Tt = T_{OL}$; multiply by 60 to convert hrs. to min. (L = max 300') | $T =$ |
| n = | 0.15 | D = |
| L = | 100 (ft) | S = |
| P ₁ = | 4.89 (in) | V = |
| S = | 0.0026 (ft/ft) | |
| T _{OL} = | 17.93 (min) | T ₁ = |
| | | 19.47 (min) |

T_c = 37.39 (min)



Intensity:

SEE FIG. 2.1-2.1a

| | |
|--------------|--------------|
| I (500-YR) = | 8.06 (in/hr) |
| I (100-YR) = | 6 (in/hr) |
| I (10-YR) = | 4.1 (in/hr) |
| I (2-YR) = | 2.8 (in/hr) |

Peak Flow Rate:

Q=CIA
 C = 0.35 Mixed use area; lots 1/4-1/2 acre; MOSTLY golf course; basin slope <1%

| | | | | | | | |
|---------------------|------|------------|---|--------------------|-----|----------|-----|
| i (500-YR) | 8.06 | i (100-YR) | 6 | i (10-YR) | 4.1 | i (2-YR) | 2.8 |
| A = | | | | 9.47 (Ac) | | | |
| Q (500-YR) = | | | | 26.73 (cfs) | | | |
| Q (100-YR) = | | | | 19.89 (cfs) | | | |
| Q (10-YR) = | | | | 13.59 (cfs) | | | |
| Q (2-YR) = | | | | 9.28 (cfs) | | | |

DA RP1 501 EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 841526.93 cft
 Volume (100-yr) = 1.38*area*43560 = 569268.22 cft
 Volume (10-yr) = 0.70*area*43560 = 288759.24 cft
 Volume (2-yr) = 0.41*area*43560 = 169130.412 cft
 A= 9.47 Ac

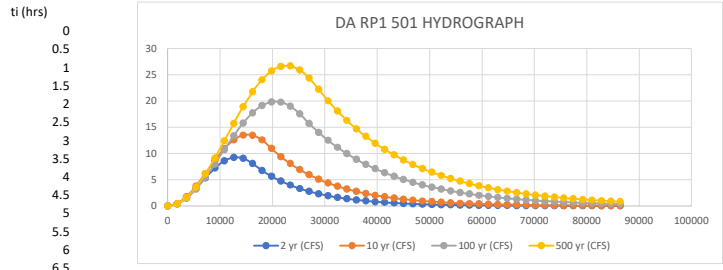
TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

$Q_1 = \frac{Q_p}{2} \left[1 - \cos \left(\frac{\pi t_i}{T_p} \right) \right]$
 $t_i = 1.25 T_p$
 $q_1 = 4.34 Q_p \left(\frac{-1.25}{T_p} \right)^2$
 $t_i = 1.25 T_p$

| DA RP1 501 Existing Conditions | | | | |
|--------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 9.28 | 13.59 | 19.89 | 26.73 |
| TP= | 13110.850 | 15286.892 | 20593.628 | 22650.163 |
| 1.25*TP= | 16388.563 | 19108.616 | 25742.035 | 28312.703 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.424967772 | 0.459610813 | 0.372526979 | 0.414349689 |
| 3600.00 | 1.622032324 | 1.776264988 | 1.462194939 | 1.631705915 |
| 5400.00 | 3.371934619 | 3.771839497 | 3.187356429 | 3.576583307 |
| 7200.00 | 5.35415569 | 6.176363851 | 5.418747265 | 6.128384632 |
| 9000.00 | 7.205624154 | 8.664542942 | 7.989172138 | 9.128878745 |
| 10800.00 | 8.587217787 | 10.89976447 | 10.70603234 | 12.39201212 |
| 12600.00 | 9.245878482 | 12.57963739 | 13.36575695 | 15.71544561 |
| 14400.00 | 9.060963362 | 13.47690078 | 15.76905616 | 18.89310098 |
| 16200.00 | 8.066342206 | 13.47016871 | 17.73585375 | 21.72793937 |
| 18000.00 | 6.75997542 | 12.56035195 | 19.11878008 | 24.04417916 |
| 19800.00 | 5.655005739 | 10.95036348 | 19.8142142 | 25.69819583 |
| 21600.00 | 4.730651804 | 9.396152866 | 19.77004811 | 26.58742773 |
| 23400.00 | 3.957390588 | 8.062534989 | 18.98959112 | 26.6567357 |
| 25200.00 | 3.310524832 | 6.918200606 | 17.53132189 | 25.90182211 |
| 27000.00 | 2.76939423 | 5.936284269 | 15.69794626 | 24.36949736 |
| 28800.00 | 2.316715564 | 5.093733607 | 14.01183755 | 22.21245827 |
| 30600.00 | 1.938030688 | 4.370768124 | 12.50683295 | 20.03223644 |
| 32400.00 | 1.62124475 | 3.750414817 | 11.16348016 | 18.06601016 |
| 34200.00 | 1.356239897 | 3.2181097 | 9.964416232 | 16.2927751 |
| 36000.00 | 1.134552114 | 2.76135589 | 8.894143172 | 14.69358857 |
| 37800.00 | 0.949100894 | 2.369430212 | 7.938827617 | 13.25136717 |
| 39600.00 | 0.793963095 | 2.03313146 | 7.086122037 | 11.95070429 |
| 41400.00 | 0.664183755 | 1.744564373 | 6.325005145 | 10.77770551 |
| 43200.00 | 0.555617841 | 1.496954285 | 5.645639445 | 9.719840209 |
| 45000.00 | 0.464797856 | 1.284488074 | 5.039244081 | 8.765807676 |
| 46800.00 | 0.388823091 | 1.102177688 | 4.497981346 | 7.905416401 |
| 48600.00 | 0.325266984 | 0.94574304 | 4.014855376 | 7.129475205 |
| 50400.00 | 0.272099608 | 0.811511526 | 3.58362173 | 6.42969505 |
| 52200.00 | 0.227622846 | 0.696331804 | 3.198706677 | 5.798600492 |
| 54000.00 | 0.190416151 | 0.597499808 | 2.855135162 | 5.229449827 |
| 55800.00 | 0.159291175 | 0.512695267 | 2.548466495 | 4.716163069 |
| 57600.00 | 0.133253814 | 0.439927233 | 2.274736959 | 4.253257003 |
| 59400.00 | 0.111472459 | 0.377487336 | 2.030408578 | 3.835786605 |
| 61200.00 | 0.093251433 | 0.323909678 | 1.812323389 | 3.459292225 |
| 63000.00 | 0.078008773 | 0.277936423 | 1.617662622 | 3.119751939 |
| 64800.00 | 0.065257643 | 0.238488258 | 1.443910274 | 2.813538588 |
| 66600.00 | 0.054590782 | 0.204639064 | 1.288820579 | 2.537381029 |
| 68400.00 | 0.045667501 | 0.175594165 | 1.150388993 | 2.288329193 |
| 70200.00 | 0.038202799 | 0.150671676 | 1.026826276 | 2.063722568 |
| 72000.00 | 0.031958259 | 0.129286493 | 0.916535369 | 1.861161783 |
| 73800.00 | 0.026734437 | 0.11093656 | 0.818090755 | 1.678482968 |
| 75600.00 | 0.022364489 | 0.095191076 | 0.730220028 | 1.513734646 |
| 77400.00 | 0.018708842 | 0.081680384 | 0.651787453 | 1.365156885 |
| 79200.00 | 0.015650739 | 0.070087297 | 0.581779282 | 1.231162493 |
| 81000.00 | 0.013092506 | 0.060139644 | 0.519290655 | 1.110320067 |
| 82800.00 | 0.010952436 | 0.051603884 | 0.463513901 | 1.0013387 |
| 84600.00 | 0.009162176 | 0.044279624 | 0.4137281 | 0.903054194 |
| 86400.00 | 0.007664549 | 0.037994914 | 0.369289768 | 0.814416617 |



DA RP1 416 DRAINAGE CALCULATIONS

Time of Concentration:

$$T_c = T_{OL} + T_1 + \dots + T_n$$

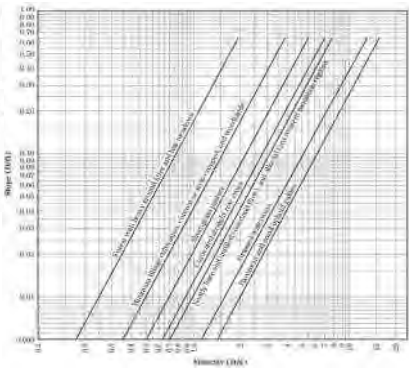
Equation 2.1
 T_{OL} = (L/n)^{0.77}
 T₁ = 0.01185 L^{0.0167} S^{-0.0141} P₂^{0.486}
 T_n = 0.01185 L^{0.0167} S^{-0.0141} P_n^{0.486}

Table 2.3 Manning's Roughness Coefficients for Open Channel Flow

| Surface | n |
|------------------------------------------------|-------|
| Smoothed Corrugated Metal (12 in. corrugation) | 0.12 |
| Cast Iron Pipe (new) | 0.013 |
| Concrete Pipe (new) | 0.012 |
| Concrete Pipe (old) | 0.015 |
| Concrete Pipe (rough) | 0.018 |
| Concrete Pipe (very rough) | 0.020 |
| Concrete Pipe (extremely rough) | 0.025 |
| Concrete Pipe (extremely rough) | 0.030 |
| Concrete Pipe (extremely rough) | 0.035 |
| Concrete Pipe (extremely rough) | 0.040 |
| Concrete Pipe (extremely rough) | 0.045 |
| Concrete Pipe (extremely rough) | 0.050 |
| Concrete Pipe (extremely rough) | 0.055 |
| Concrete Pipe (extremely rough) | 0.060 |
| Concrete Pipe (extremely rough) | 0.065 |
| Concrete Pipe (extremely rough) | 0.070 |
| Concrete Pipe (extremely rough) | 0.075 |
| Concrete Pipe (extremely rough) | 0.080 |
| Concrete Pipe (extremely rough) | 0.085 |
| Concrete Pipe (extremely rough) | 0.090 |
| Concrete Pipe (extremely rough) | 0.095 |
| Concrete Pipe (extremely rough) | 0.100 |

| | | | |
|---------------------------------------------------------------|----------------|------------------|----------------|
| Tt=Total; multiply by 60 to convert hrs. to min. (L=max 300') | | T= | |
| n= | 0.15 | D= | 509 (ft) |
| L= | 100 (ft) | S= | 0.0026 (ft/ft) |
| P ₂ = | 4.89 (in) | V= | 0.5 (ft/s) |
| S= | 0.0026 (ft/ft) | | |
| T _{OL} = | 17.93 (min) | T ₁ = | 16.97 (min) |

Tc = 34.89 (min)



Intensity:

SEE FIG. 2.1-2.1a

| | |
|-------------|--------------|
| I (500-YR)= | 8.28 (in/hr) |
| I (100-YR)= | 6.2 (in/hr) |
| I (10-YR)= | 4.2 (in/hr) |
| I (2-YR)= | 3 (in/hr) |

Peak Flow Rate:

Q=CIA
 C= 0.35 Mixed use area; lots 1/4-1/2 acre; MOSTLY golf course; basin slope <1%

| | | | | | | | |
|-------------|------|------------|-----|-----------|-----|----------|---|
| i (500-YR) | 8.28 | i (100-YR) | 6.2 | i (10-YR) | 4.2 | i (2-YR) | 3 |
| A= | | 3.02 (Ac) | | | | | |
| Q (500-YR)= | | 8.75 (cfs) | | | | | |
| Q (100-YR)= | | 6.55 (cfs) | | | | | |
| Q (10-YR)= | | 4.44 (cfs) | | | | | |
| Q (2-YR)= | | 3.17 (cfs) | | | | | |

DA RP1 416 EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 268364.45 cft
 Volume (100-yr) = 1.38*area*43560 = 181540.66 cft
 Volume (10-yr) = 0.70*area*43560 = 92085.84 cft
 Volume (2-yr) = 0.41*area*43560 = 53935.992 cft
 A= 3.02 Ac

TP = time to Qp in seconds

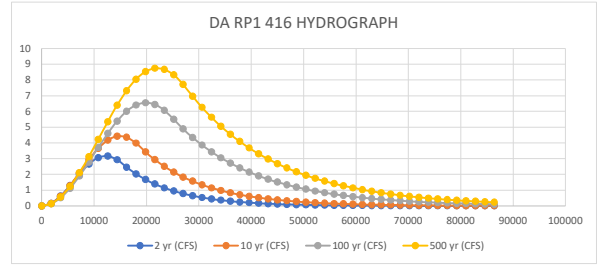
$T_p = \frac{V}{1.39 Q_p}$

$Q_p = \frac{Q_p}{L} \left[1 - \cos \left(\frac{\pi T_p}{L} \right) \right]$
 $T_p = 1.25 T_p$
 $Q_p = 4.34 Q_{ps} \left(\frac{-1.25 T_p}{T_p} \right)$
 $T_p = 1.25 T_p$

| DA RP1 416 Existing Conditions | | | | |
|--------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 3.17 | 4.44 | 6.55 | 8.75 |
| Tp= | 12236.793 | 14922.919 | 19929.317 | 22061.971 |
| 1.25*Tp= | 15295.992 | 18653.649 | 24911.647 | 27577.464 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.16630417 | 0.15747021 | 0.131023988 | 0.142949623 |
| 3600.00 | 0.630329166 | 0.6075383 | 0.513617554 | 0.562458205 |
| 5400.00 | 1.294731195 | 1.286346707 | 1.11718349 | 1.231115183 |
| 7200.00 | 2.020131098 | 2.097583225 | 1.893452734 | 2.105230711 |
| 9000.00 | 2.6543535 | 2.926146188 | 2.780344601 | 3.127690344 |
| 10800.00 | 3.064350365 | 3.654475578 | 3.706931566 | 4.231686876 |
| 12600.00 | 3.164111995 | 4.179232945 | 4.599111563 | 5.345085507 |
| 14400.00 | 2.93271026 | 4.425963494 | 5.38553416 | 6.395137105 |
| 16200.00 | 2.461774026 | 4.359660051 | 6.003306675 | 7.313231616 |
| 18000.00 | 2.03291018 | 3.98973003 | 6.403023901 | 8.039381019 |
| 19800.00 | 1.679387434 | 3.43327625 | 6.552719199 | 8.526138933 |
| 21600.00 | 1.387082384 | 2.935049031 | 6.440420966 | 8.74170074 |
| 23400.00 | 1.145654363 | 2.509085574 | 6.075110044 | 8.671981699 |
| 25200.00 | 0.946247991 | 2.144942163 | 5.496155835 | 8.321537229 |
| 27000.00 | 0.781549208 | 1.83364686 | 4.887270408 | 7.713265267 |
| 28800.00 | 0.645517001 | 1.567529822 | 4.345839667 | 6.958913235 |
| 30600.00 | 0.53316182 | 1.34003433 | 3.86439072 | 6.258612097 |
| 32400.00 | 0.440362571 | 1.145555243 | 3.436278551 | 5.628784849 |
| 34200.00 | 0.363715455 | 0.979300892 | 3.055594307 | 5.062339443 |
| 36000.00 | 0.30040912 | 0.837175024 | 2.717083737 | 4.552897529 |
| 37800.00 | 0.248121541 | 0.715675872 | 2.416074679 | 4.094722637 |
| 39600.00 | 0.204934854 | 0.611809884 | 2.14841257 | 3.682655576 |
| 41400.00 | 0.169265007 | 0.523017959 | 1.910403106 | 3.312056346 |
| 43200.00 | 0.13980366 | 0.4471124 | 1.698761252 | 2.978751884 |
| 45000.00 | 0.115470195 | 0.382223009 | 1.510565902 | 2.678989082 |
| 46800.00 | 0.09537208 | 0.326751011 | 1.343219562 | 2.409392517 |
| 48600.00 | 0.078772134 | 0.27932966 | 1.194412497 | 2.16692645 |
| 50400.00 | 0.065061485 | 0.238790566 | 1.062090856 | 1.948860639 |
| 52200.00 | 0.053737236 | 0.204134908 | 0.944428318 | 1.752739596 |
| 54000.00 | 0.044384025 | 0.174508824 | 0.839800891 | 1.576354937 |
| 55800.00 | 0.036658783 | 0.14918237 | 0.746764497 | 1.417720518 |
| 57600.00 | 0.030278154 | 0.127531544 | 0.664035034 | 1.275050067 |
| 59400.00 | 0.025008103 | 0.1090229 | 0.590470661 | 1.14673707 |
| 61200.00 | 0.020655329 | 0.093200414 | 0.525056035 | 1.031336684 |
| 63000.00 | 0.017060174 | 0.079674245 | 0.466888294 | 0.927549465 |
| 64800.00 | 0.014090773 | 0.068111127 | 0.415164601 | 0.834206737 |
| 66600.00 | 0.01163821 | 0.058226164 | 0.369171059 | 0.750257432 |
| 68400.00 | 0.009612526 | 0.049775805 | 0.328272859 | 0.674756256 |
| 70200.00 | 0.007939422 | 0.042551846 | 0.291905521 | 0.606853042 |
| 72000.00 | 0.00655753 | 0.0363763 | 0.259567097 | 0.545783179 |
| 73800.00 | 0.005416162 | 0.03109701 | 0.230811249 | 0.490859002 |
| 75600.00 | 0.004473454 | 0.026583903 | 0.205241085 | 0.441462048 |
| 77400.00 | 0.003694829 | 0.022725783 | 0.182503683 | 0.397036092 |
| 79200.00 | 0.003051727 | 0.019427592 | 0.162285218 | 0.357080884 |
| 81000.00 | 0.00252056 | 0.016608067 | 0.144306633 | 0.321146516 |
| 82800.00 | 0.002081845 | 0.014197739 | 0.128319785 | 0.288828356 |
| 84600.00 | 0.00171949 | 0.012137222 | 0.114104023 | 0.259762492 |
| 86400.00 | 0.001420205 | 0.010375748 | 0.101463137 | 0.233621633 |

ti (hrs)
 0
 0.5
 1
 1.5
 2
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 24



DA RP1 415A EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 269253.07 cft
 Volume (100-yr) = 1.38*area*43560 = 182141.78 cft
 Volume (10-yr) = 0.70*area*43560 = 92390.76 cft
 Volume (2-yr) = 0.41*area*43560 = 54114.588 cft
 A= 3.03 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

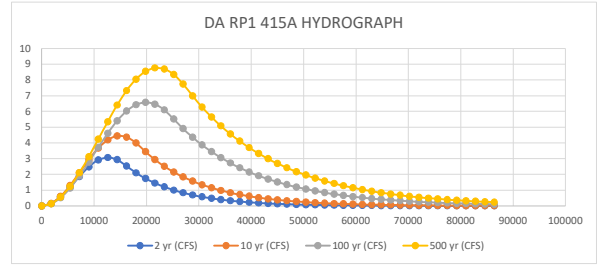
$$Q_1 = \frac{Q_p}{2} \left[1 - \cos \left(\frac{\pi t_i}{T_p} \right) \right] \quad t_i = 1.25 T_p$$

$$Q_1 = 1.34 Q_p \left(\frac{t_i - 1.25 T_p}{T_p} \right)^2 \quad t_i = 1.25 T_p$$

| DA RP1 415A Existing Conditions | | | | |
|---------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 3.08 | 4.45 | 6.58 | 8.77 |
| TP= | 12658.752 | 14922.919 | 19929.317 | 22084.911 |
| 1.25*TP= | 15823.440 | 18653.649 | 24911.647 | 27606.139 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.150895912 | 0.157991634 | 0.131457843 | 0.142978119 |
| 3600.00 | 0.57396902 | 0.609550016 | 0.515318274 | 0.56258962 |
| 5400.00 | 1.18618757 | 1.290606133 | 1.120882773 | 1.231473832 |
| 7200.00 | 1.86739838 | 2.104528865 | 1.899722445 | 2.106016315 |
| 9000.00 | 2.483907939 | 2.935835413 | 2.78955104 | 3.129192727 |
| 10800.00 | 2.914720917 | 3.666576491 | 3.719206174 | 4.234287086 |
| 12600.00 | 3.075286544 | 4.193071465 | 4.61434041 | 5.34924197 |
| 14400.00 | 2.934092426 | 4.440619002 | 5.403367055 | 6.401357003 |
| 16200.00 | 2.528571314 | 4.374096012 | 6.023185173 | 7.322029266 |
| 18000.00 | 2.101816765 | 4.002941057 | 6.424225967 | 8.051226537 |
| 19800.00 | 1.747086859 | 3.444666259 | 6.574416944 | 8.541401677 |
| 21600.00 | 1.45222578 | 2.944767737 | 6.461746863 | 8.760592927 |
| 23400.00 | 1.207129289 | 2.517393805 | 6.095226302 | 8.694507973 |
| 25200.00 | 1.003398465 | 2.152044621 | 5.514355027 | 8.34745587 |
| 27000.00 | 0.834051903 | 1.839718538 | 4.903453423 | 7.74206607 |
| 28800.00 | 0.693286467 | 1.572720318 | 4.360229864 | 6.987009284 |
| 30600.00 | 0.576278435 | 1.34447153 | 3.877186715 | 6.284573096 |
| 32400.00 | 0.479018199 | 1.149348473 | 3.447656957 | 5.652756049 |
| 34200.00 | 0.398172863 | 0.982543611 | 3.065712169 | 5.084458476 |
| 36000.00 | 0.330972037 | 0.839947126 | 2.726080703 | 4.573294473 |
| 37800.00 | 0.275112896 | 0.71804566 | 2.424074926 | 4.113520139 |
| 39600.00 | 0.228681269 | 0.613835744 | 2.155526519 | 3.699969034 |
| 41400.00 | 0.190086047 | 0.524749806 | 1.916728944 | 3.327994125 |
| 43200.00 | 0.158004656 | 0.448592904 | 1.704386289 | 2.993415564 |
| 45000.00 | 0.131337737 | 0.383488648 | 1.515567776 | 2.692473725 |
| 46800.00 | 0.109171474 | 0.327832968 | 1.347667309 | 2.421786954 |
| 48600.00 | 0.090746278 | 0.280254593 | 1.198367506 | 2.17831357 |
| 50400.00 | 0.075430757 | 0.239581263 | 1.065607713 | 1.959317685 |
| 52200.00 | 0.062700082 | 0.204810852 | 0.947555564 | 1.762338464 |
| 54000.00 | 0.052118002 | 0.175086667 | 0.842581689 | 1.58516247 |
| 55800.00 | 0.04332189 | 0.149676352 | 0.749237227 | 1.425798794 |
| 57600.00 | 0.036010325 | 0.127953834 | 0.666233825 | 1.282456681 |
| 59400.00 | 0.029932755 | 0.109383903 | 0.592425862 | 1.153525411 |
| 61200.00 | 0.024880914 | 0.093509025 | 0.526794631 | 1.037556194 |
| 63000.00 | 0.020681688 | 0.079938067 | 0.468434282 | 0.93245896 |
| 64800.00 | 0.017191178 | 0.068336661 | 0.416539318 | 0.839422393 |
| 66600.00 | 0.014289771 | 0.058418966 | 0.37039348 | 0.755031398 |
| 68400.00 | 0.011878044 | 0.049940626 | 0.329359856 | 0.679124618 |
| 70200.00 | 0.009873351 | 0.042692746 | 0.292872095 | 0.610849095 |
| 72000.00 | 0.008206996 | 0.036496751 | 0.26042659 | 0.549437625 |
| 73800.00 | 0.006821876 | 0.03119998 | 0.231575524 | 0.494200133 |
| 75600.00 | 0.005670528 | 0.026671929 | 0.205920691 | 0.44451592 |
| 77400.00 | 0.004713496 | 0.022801034 | 0.183107999 | 0.399826689 |
| 79200.00 | 0.003917985 | 0.019491922 | 0.162822586 | 0.359630273 |
| 81000.00 | 0.003256735 | 0.01666306 | 0.14478447 | 0.323474987 |
| 82800.00 | 0.002707086 | 0.014244752 | 0.128744685 | 0.290954558 |
| 84600.00 | 0.002250203 | 0.012177412 | 0.114481851 | 0.261703558 |
| 86400.00 | 0.00187043 | 0.010410105 | 0.101799108 | 0.235393295 |

ti (hrs)
0
0.5
1
1.5
2
2.5
3
3.5
4
4.5
5
5.5
6
6.5
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17.5
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18.5
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19.5
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20.5
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21.5
22
22.5
23
23.5
24



DA RP1 415 EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 81753.41 cft
 Volume (100-yr) = 1.38*area*43560 = 55303.78 cft
 Volume (10-yr) = 0.70*area*43560 = 28052.64 cft
 Volume (2-yr) = 0.41*area*43560 = 16430.832 cft
 A= 0.92 Ac

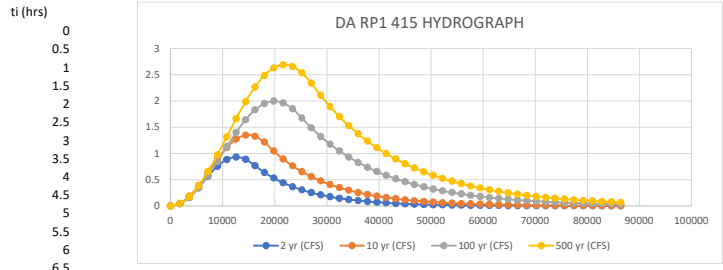
TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

$Q_1 = \frac{Q_p}{2} \left[1 - \cos \left(\frac{\pi t_i}{T_p} \right) \right]$ $t_i = 1.25 T_p$
 $q_1 = 4.34 Q_p \left(\frac{-1.3 t_i}{T_p} \right)^{1.5}$ $t_i = 1.25 T_p$

| DA RP1 415 Existing Conditions | | | | |
|--------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 0.93 | 1.35 | 2.00 | 2.69 |
| TP= | 12658.752 | 14922.919 | 19929.317 | 21880.148 |
| 1.25*TP= | 15823.440 | 18653.649 | 24911.647 | 27350.185 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.04581658 | 0.047971057 | 0.039914592 | 0.044638163 |
| 3600.00 | 0.174274422 | 0.185077893 | 0.156466275 | 0.175587602 |
| 5400.00 | 0.360162563 | 0.391867209 | 0.340334043 | 0.384150123 |
| 7200.00 | 0.566998848 | 0.638998863 | 0.576813416 | 0.656472153 |
| 9000.00 | 0.754189869 | 0.891408772 | 0.846992395 | 0.974464955 |
| 10800.00 | 0.88499777 | 1.113283951 | 1.129263921 | 1.317006152 |
| 12600.00 | 0.93375037 | 1.273143811 | 1.401053854 | 1.661342763 |
| 14400.00 | 0.890879549 | 1.34830676 | 1.6406263 | 1.984602548 |
| 16200.00 | 0.767751026 | 1.32810836 | 1.828821901 | 2.265313275 |
| 18000.00 | 0.638175387 | 1.215414446 | 1.950590063 | 2.484828996 |
| 19800.00 | 0.530468617 | 1.045914376 | 1.996192604 | 2.628568582 |
| 21600.00 | 0.440939841 | 0.894120897 | 1.961982546 | 2.686984264 |
| 23400.00 | 0.366521104 | 0.764357195 | 1.850695775 | 2.656195835 |
| 25200.00 | 0.30466224 | 0.65342609 | 1.674325619 | 2.538248388 |
| 27000.00 | 0.253243482 | 0.558594408 | 1.488837343 | 2.340976473 |
| 28800.00 | 0.210502822 | 0.477525641 | 1.323898177 | 2.107617582 |
| 30600.00 | 0.17497563 | 0.40822379 | 1.17723161 | 1.893850281 |
| 32400.00 | 0.14544447 | 0.348977094 | 1.046813333 | 1.701764551 |
| 34200.00 | 0.120897371 | 0.298330073 | 0.930843299 | 1.529161315 |
| 36000.00 | 0.10049316 | 0.255033451 | 0.827720873 | 1.374064541 |
| 37800.00 | 0.083532628 | 0.218020464 | 0.73602275 | 1.234698619 |
| 39600.00 | 0.069434577 | 0.18637917 | 0.654483299 | 1.10946803 |
| 41400.00 | 0.057715895 | 0.159329974 | 0.581977105 | 0.996939083 |
| 43200.00 | 0.047975011 | 0.136206426 | 0.517503428 | 0.895823502 |
| 45000.00 | 0.039878125 | 0.116438797 | 0.460172394 | 0.804963673 |
| 46800.00 | 0.033147774 | 0.099540043 | 0.409192714 | 0.723319397 |
| 48600.00 | 0.027553325 | 0.085093804 | 0.363860761 | 0.649955976 |
| 50400.00 | 0.022903068 | 0.072744146 | 0.323550857 | 0.584033517 |
| 52200.00 | 0.019037649 | 0.062186793 | 0.28770664 | 0.524797311 |
| 54000.00 | 0.015824608 | 0.053161628 | 0.255833384 | 0.471569199 |
| 55800.00 | 0.013153841 | 0.045446285 | 0.227491171 | 0.423739804 |
| 57600.00 | 0.010933828 | 0.038850669 | 0.202288818 | 0.380761554 |
| 59400.00 | 0.009088493 | 0.033212274 | 0.17987848 | 0.342142418 |
| 61200.00 | 0.007554601 | 0.028392179 | 0.159950845 | 0.307440268 |
| 63000.00 | 0.006279588 | 0.024271624 | 0.142230871 | 0.27625782 |
| 64800.00 | 0.005219763 | 0.020749085 | 0.126473984 | 0.248238084 |
| 66600.00 | 0.004338808 | 0.017737772 | 0.112462707 | 0.223060279 |
| 68400.00 | 0.003606535 | 0.01516349 | 0.100003653 | 0.200436158 |
| 70200.00 | 0.00297849 | 0.012962814 | 0.088924861 | 0.180106713 |
| 72000.00 | 0.002491893 | 0.011081522 | 0.07907342 | 0.161839203 |
| 73800.00 | 0.002071329 | 0.009473261 | 0.070313361 | 0.145424493 |
| 75600.00 | 0.001721744 | 0.008098408 | 0.062523774 | 0.130674663 |
| 77400.00 | 0.00143116 | 0.006923086 | 0.055597148 | 0.11742085 |
| 79200.00 | 0.001189619 | 0.005918339 | 0.049437881 | 0.105511318 |
| 81000.00 | 0.000988844 | 0.005059411 | 0.043960961 | 0.094809723 |
| 82800.00 | 0.000821954 | 0.004325139 | 0.039090796 | 0.085193549 |
| 84600.00 | 0.00068323 | 0.003697432 | 0.034760166 | 0.076552705 |
| 86400.00 | 0.000567919 | 0.003160824 | 0.0309093 | 0.068788267 |



DA RP1 414 DRAINAGE CALCULATIONS

Time of Concentration:

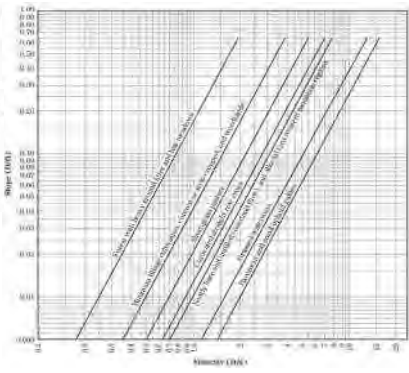
$$T_c = T_{OL} + T_1 + \dots + T_n$$

Equation 5.3
 T_{OL} = 0.0114 L^{0.77} / S^{0.047}
 T₁ = 0.00007 L^{1.48} / S^{0.016}
 T_n = 0.00007 L^{1.48} / S^{0.016}

| Material | n |
|----------|-------|
| Gravel | 0.15 |
| Asphalt | 0.015 |
| Concrete | 0.012 |
| Clay | 0.013 |
| Earth | 0.04 |
| Grass | 0.05 |
| Shrub | 0.05 |
| Forest | 0.05 |
| Water | 0.01 |

| | | | |
|-------------------|-------------------------------------------------------------|------------------|----------------|
| T _{OL} = | Tt=Tol; multiply by 60 to convert hrs. to min. (L=max 300') | T = | |
| n = | 0.15 | D = | 892 (ft) |
| L = | 100 (ft) | S = | 0.0026 (ft/ft) |
| P ₂ = | 4.89 (in) | V = | 0.5 (ft/s) |
| S = | 0.0026 (ft/ft) | | |
| T _{OL} = | 17.93 (min) | T ₁ = | 29.73 (min) |

T_c = 47.66 (min)



Intensity:

SEE FIG. 2.1-2.1a

| | |
|--------------|--------------|
| I (500-YR) = | 7.18 (in/hr) |
| I (100-YR) = | 5.2 (in/hr) |
| I (10-YR) = | 3.5 (in/hr) |
| I (2-YR) = | 2.4 (in/hr) |

Peak Flow Rate:

Q=CIA

C = 0.35 Mixed use area; lots 1/4-1/2 acre; MOSTLY golf course; basin slope <1%

| | | | |
|------------|------------|-----------|----------|
| i (500-YR) | i (100-YR) | i (10-YR) | i (2-YR) |
| 7.18 | 5.2 | 3.5 | 2.4 |

| | |
|--------------|-------------|
| A = | 4.63 (Ac) |
| Q (500-YR) = | 11.64 (cfs) |
| Q (100-YR) = | 8.43 (cfs) |
| Q (10-YR) = | 5.67 (cfs) |
| Q (2-YR) = | 3.89 (cfs) |

DA RP1 414 EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 411432.91 cft
 Volume (100-yr) = 1.38*area*43560 = 278322.26 cft
 Volume (10-yr) = 0.70*area*43560 = 141177.96 cft
 Volume (2-yr) = 0.41*area*43560 = 82689.948 cft
 A= 4.63 Ac

TP = time to Qp in seconds

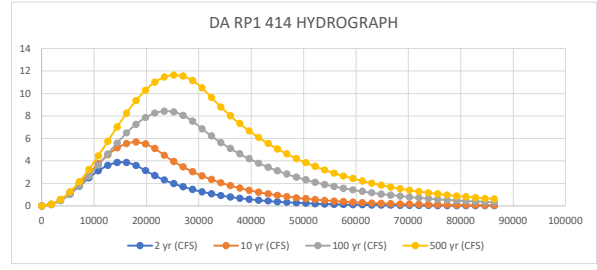
TP = $\frac{V}{1.39 Q_p}$

$Q_1 = \frac{Q_p}{2} \left[1 - \cos \left(\frac{\pi t_i}{T_p} \right) \right]$ $t_i = 1.25 T_p$
 $q_1 = 4.34 Q_p \left(\frac{-1.8 t_i}{T_p} \right)^{1.4}$ $t_i = 1.25 T_p$

| DA RP1 414 Existing Conditions | | | | |
|--------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 3.89 | 5.67 | 8.43 | 11.64 |
| TP= | 15295.992 | 17907.503 | 23761.878 | 25434.971 |
| 1.25*TP= | 19119.990 | 22384.378 | 29702.348 | 31793.713 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.131382546 | 0.140223199 | 0.118747631 | 0.143214053 |
| 3600.00 | 0.50777705 | 0.547025793 | 0.46829696 | 0.565806387 |
| 5400.00 | 1.078323007 | 1.180178108 | 1.028944591 | 1.246974565 |
| 7200.00 | 1.765925095 | 1.977066212 | 1.769087945 | 2.153187548 |
| 9000.00 | 2.477670724 | 2.858883952 | 2.647006625 | 3.239836292 |
| 10800.00 | 3.117384892 | 3.738426283 | 3.613214118 | 4.453429661 |
| 12600.00 | 3.598625888 | 4.528713178 | 4.613247248 | 5.734227572 |
| 14400.00 | 3.85636577 | 5.151591295 | 5.590736154 | 7.019181742 |
| 16200.00 | 3.85777302 | 5.54546274 | 6.490581749 | 8.245039296 |
| 18000.00 | 3.596940001 | 5.671376632 | 7.262061544 | 9.351456435 |
| 19800.00 | 3.137053669 | 5.51688105 | 7.861688772 | 10.28396891 |
| 21600.00 | 2.692049458 | 5.097254426 | 8.255663648 | 10.99667306 |
| 23400.00 | 2.310170959 | 4.50254468 | 8.421778601 | 11.45448547 |
| 25200.00 | 1.982463526 | 3.951009966 | 8.350670063 | 11.63486996 |
| 27000.00 | 1.701242765 | 3.467034946 | 8.046346281 | 11.52894696 |
| 28800.00 | 1.459914349 | 3.042343962 | 7.525961376 | 11.14193063 |
| 30600.00 | 1.252819379 | 2.669675077 | 6.856229426 | 10.49287213 |
| 32400.00 | 1.075101699 | 2.342655894 | 6.213228084 | 9.641761251 |
| 34200.00 | 0.922594017 | 2.0556946 | 5.630529672 | 8.79430607 |
| 36000.00 | 0.791720189 | 1.803884343 | 5.102478769 | 8.02133731 |
| 37800.00 | 0.679411362 | 1.582919332 | 4.62395034 | 7.316308043 |
| 39600.00 | 0.583034012 | 1.389021209 | 4.190299993 | 6.673246782 |
| 41400.00 | 0.500328194 | 1.218874443 | 3.797318902 | 6.086706894 |
| 43200.00 | 0.429354543 | 1.069569635 | 3.441192961 | 5.551720479 |
| 45000.00 | 0.368448801 | 0.938553771 | 3.118465766 | 5.063756282 |
| 46800.00 | 0.316182794 | 0.823586564 | 2.826005064 | 4.618681323 |
| 48600.00 | 0.27133094 | 0.72270215 | 2.560972356 | 4.212725885 |
| 50400.00 | 0.232841509 | 0.634175472 | 2.320795349 | 3.842451587 |
| 52200.00 | 0.199811965 | 0.556492781 | 2.103142988 | 3.504722263 |
| 54000.00 | 0.1714678 | 0.488325754 | 1.905902832 | 3.196677399 |
| 55800.00 | 0.147144374 | 0.428508778 | 1.727160552 | 2.9157079 |
| 57600.00 | 0.126271328 | 0.376019023 | 1.565181352 | 2.659434 |
| 59400.00 | 0.108359211 | 0.329958949 | 1.418393133 | 2.425685096 |
| 61200.00 | 0.092988003 | 0.289540957 | 1.285371229 | 2.212481372 |
| 63000.00 | 0.079797265 | 0.254073926 | 1.164824589 | 2.018017026 |
| 64800.00 | 0.068477688 | 0.222951394 | 1.055583236 | 1.840644973 |
| 66600.00 | 0.058763841 | 0.195641186 | 0.956586923 | 1.678862901 |
| 68400.00 | 0.050427944 | 0.171676314 | 0.866874832 | 1.531300539 |
| 70200.00 | 0.043274529 | 0.150646996 | 0.785576258 | 1.396708057 |
| 72000.00 | 0.037135855 | 0.132193642 | 0.711902149 | 1.273945478 |
| 73800.00 | 0.031867979 | 0.116000714 | 0.645137459 | 1.161973021 |
| 75600.00 | 0.027347372 | 0.101791323 | 0.584634196 | 1.059842297 |
| 77400.00 | 0.023468033 | 0.089322496 | 0.529805142 | 0.966688275 |
| 79200.00 | 0.020138994 | 0.078381026 | 0.48011815 | 0.881721953 |
| 81000.00 | 0.017282193 | 0.068779821 | 0.435090979 | 0.804223681 |
| 82800.00 | 0.014830642 | 0.060354705 | 0.394286614 | 0.73353706 |
| 84600.00 | 0.012726853 | 0.052961616 | 0.357309027 | 0.669063385 |
| 86400.00 | 0.010921496 | 0.046474136 | 0.323799328 | 0.610256574 |

ti (hrs)



DA RP1 412 EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 175947.55 cft
 Volume (100-yr) = 1.38*area*43560 = 119023.34 cft
 Volume (10-yr) = 0.70*area*43560 = 60374.16 cft
 Volume (2-yr) = 0.41*area*43560 = 35362.008 cft
 A= 1.98 Ac

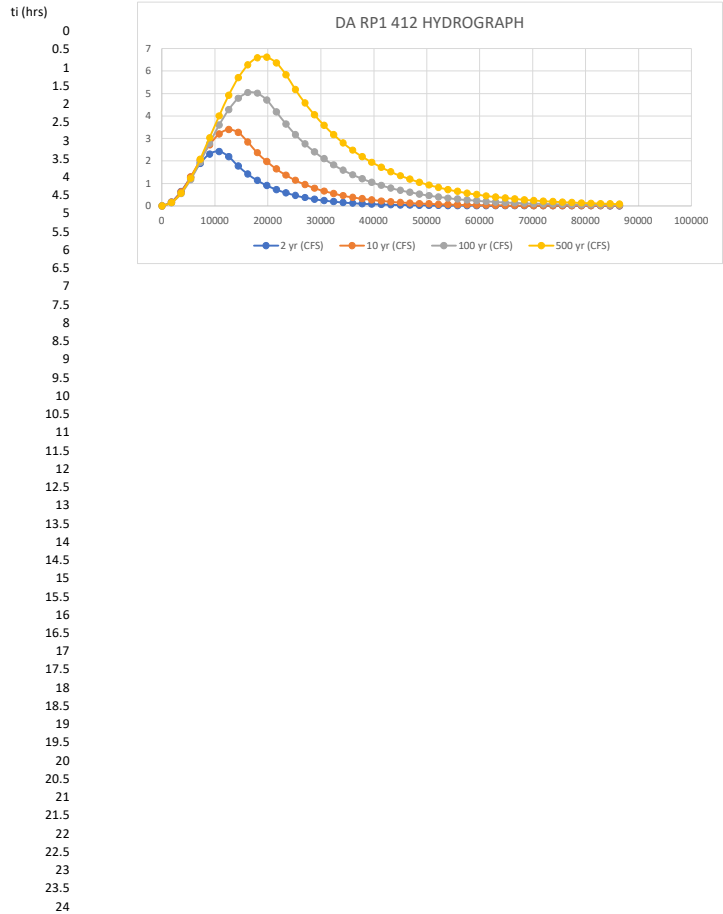
TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

$Q_1 = \frac{Q_p}{2} \left[1 - \cos \left(\frac{\pi t_i}{T_p} \right) \right]$ $t_i = 1.25 T_p$
 $Q_1 = 0.34 Q_p \left(1 - \cos \left(\frac{\pi t_i}{T_p} \right) \right)$ $t_i = 1.25 T_p$

| DA RP1 412 Existing Conditions | | | | |
|--------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 2.43 | 3.40 | 5.06 | 6.63 |
| TP= | 10488.680 | 12791.073 | 16926.270 | 19078.774 |
| 1.25*TP= | 13110.850 | 15988.842 | 21157.837 | 23848.468 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.172027944 | 0.163235667 | 0.13985407 | 0.144650531 |
| 3600.00 | 0.63930763 | 0.621554873 | 0.543951132 | 0.565987274 |
| 5400.00 | 1.269272307 | 1.286829644 | 1.167605883 | 1.227265808 |
| 7200.00 | 1.883201667 | 2.031137524 | 1.941854197 | 2.070816593 |
| 9000.00 | 2.3069246 | 2.711359164 | 2.781079216 | 3.02307428 |
| 10800.00 | 2.420231361 | 3.196698047 | 3.592478922 | 4.000993281 |
| 12600.00 | 2.190976941 | 3.393830716 | 4.286328234 | 4.91290111 |
| 14400.00 | 1.76673064 | 3.264851487 | 4.785900867 | 5.697880879 |
| 16200.00 | 1.413449373 | 2.840339336 | 5.035953772 | 6.268865346 |
| 18000.00 | 1.13081139 | 2.36548588 | 5.008835945 | 6.582448438 |
| 19800.00 | 0.904690627 | 1.970019349 | 4.70754609 | 6.611282841 |
| 21600.00 | 0.723785715 | 1.640667681 | 4.17896522 | 6.352853931 |
| 23400.00 | 0.579055144 | 1.366377666 | 3.639393382 | 5.829699073 |
| 25200.00 | 0.463265374 | 1.13794399 | 3.169488975 | 5.171116863 |
| 27000.00 | 0.370629307 | 0.9477003 | 2.760256808 | 4.574234238 |
| 28800.00 | 0.296517052 | 0.78926192 | 2.403863118 | 4.046247535 |
| 30600.00 | 0.237224527 | 0.657311577 | 2.093485603 | 3.579204357 |
| 32400.00 | 0.189788331 | 0.547420948 | 1.823182833 | 3.166070222 |
| 34200.00 | 0.151837632 | 0.455902049 | 1.587780512 | 2.800622611 |
| 36000.00 | 0.12147568 | 0.379683458 | 1.382772429 | 2.477357246 |
| 37800.00 | 0.097185004 | 0.316207239 | 1.204234197 | 2.191405191 |
| 39600.00 | 0.077751571 | 0.263343097 | 1.048748132 | 1.938459508 |
| 41400.00 | 0.062204111 | 0.219316886 | 0.913337827 | 1.714710397 |
| 43200.00 | 0.049765573 | 0.182651062 | 0.795411177 | 1.516787807 |
| 45000.00 | 0.039814285 | 0.152115102 | 0.69271076 | 1.341710679 |
| 46800.00 | 0.03185289 | 0.126684204 | 0.603270624 | 1.186842048 |
| 48600.00 | 0.025483481 | 0.105504892 | 0.525378652 | 1.049849321 |
| 50400.00 | 0.020387721 | 0.087866379 | 0.457543791 | 0.928669152 |
| 52200.00 | 0.016310925 | 0.073176707 | 0.398467505 | 0.821476354 |
| 54000.00 | 0.013049339 | 0.060942883 | 0.347018921 | 0.72665642 |
| 55800.00 | 0.01043995 | 0.050754333 | 0.302213179 | 0.642781195 |
| 57600.00 | 0.008352343 | 0.042269125 | 0.263192582 | 0.568587372 |
| 59400.00 | 0.006682181 | 0.03520249 | 0.229210173 | 0.502957464 |
| 61200.00 | 0.00534599 | 0.029317269 | 0.199615441 | 0.44490297 |
| 63000.00 | 0.004276989 | 0.024415951 | 0.173841867 | 0.393549489 |
| 64800.00 | 0.003421748 | 0.020334045 | 0.151396077 | 0.348123548 |
| 66600.00 | 0.002737524 | 0.01693456 | 0.131848401 | 0.307940952 |
| 68400.00 | 0.00219012 | 0.014103407 | 0.114824645 | 0.272396483 |
| 70200.00 | 0.001752176 | 0.011745572 | 0.09999893 | 0.240954779 |
| 72000.00 | 0.001401805 | 0.009781925 | 0.087087455 | 0.213142272 |
| 73800.00 | 0.001121496 | 0.008146563 | 0.075843059 | 0.188540059 |
| 75600.00 | 0.000897238 | 0.006784605 | 0.066050497 | 0.166775787 |
| 77400.00 | 0.000717823 | 0.005650342 | 0.057522312 | 0.147527076 |
| 79200.00 | 0.000574285 | 0.004705706 | 0.050095253 | 0.130498579 |
| 81000.00 | 0.000459449 | 0.003918997 | 0.043627148 | 0.115435617 |
| 82800.00 | 0.000367576 | 0.003263812 | 0.037994179 | 0.102111317 |
| 84600.00 | 0.000294074 | 0.002718161 | 0.033088518 | 0.09032499 |
| 86400.00 | 0.00023527 | 0.002263734 | 0.028816256 | 0.079899116 |



DA RP1 411 BOX EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 925946.21 cft
 Volume (100-yr) = 1.38*area*43560 = 626375.38 cft
 Volume (10-yr) = 0.70*area*43560 = 317726.64 cft
 Volume (2-yr) = 0.41*area*43560 = 186097.032 cft
 A= 10.42 Ac

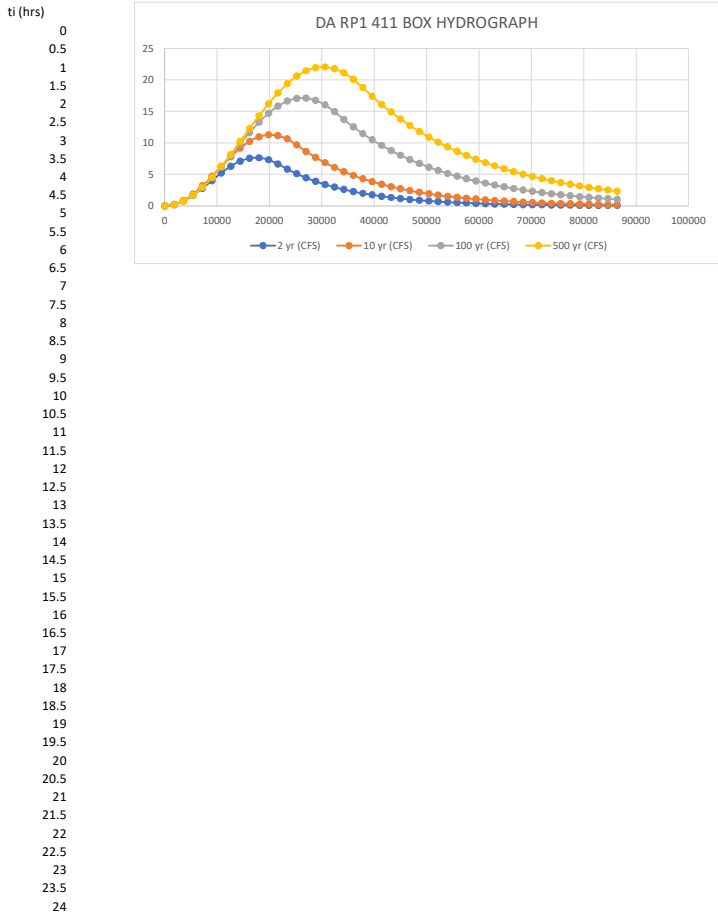
TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

$Q_1 = \frac{Q_p}{2} \left[1 - \cos \left(\frac{\pi t_i}{T_p} \right) \right]$ $t_i = 1.25 T_p$
 $q_1 = 4.34 Q_p \left(\frac{-1.25}{T_p} \right)^2$ $t_i = 1.25 T_p$

| DA RP1 411 BOX Existing Conditions | | | | |
|------------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 7.66 | 11.31 | 17.14 | 22.06 |
| TP= | 17481.133 | 20218.148 | 26289.738 | 30201.932 |
| 1.25*TP= | 21851.417 | 25272.685 | 32862.172 | 37752.415 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.198614166 | 0.219667832 | 0.197501668 | 0.19274469 |
| 3600.00 | 0.773853906 | 0.861598893 | 0.780904002 | 0.764241417 |
| 5400.00 | 1.66604812 | 1.875902738 | 1.723318635 | 1.694513657 |
| 7200.00 | 2.782647206 | 3.183748359 | 2.98131058 | 2.951043977 |
| 9000.00 | 4.007823468 | 4.683490883 | 4.496900284 | 4.489910678 |
| 10800.00 | 5.214486217 | 6.25857134 | 6.200235757 | 6.25732306 |
| 12600.00 | 6.277465221 | 7.786575546 | 8.012811997 | 8.191501669 |
| 14400.00 | 7.086494932 | 9.14874805 | 9.851089207 | 10.22483778 |
| 16200.00 | 7.557652615 | 10.23922173 | 11.63034306 | 12.28625663 |
| 18000.00 | 7.642063872 | 10.97324572 | 13.26856954 | 14.30370186 |
| 19800.00 | 7.330972504 | 11.29377216 | 14.69026447 | 16.20665417 |
| 21600.00 | 6.656648822 | 11.17588996 | 15.82990336 | 17.92859634 |
| 23400.00 | 5.833136466 | 10.62876085 | 16.63496143 | 19.40933831 |
| 25200.00 | 5.102324631 | 9.694907319 | 17.06833435 | 20.59712113 |
| 27000.00 | 4.463073476 | 8.646177553 | 17.11004841 | 21.45042614 |
| 28800.00 | 3.903911705 | 7.701227398 | 16.75818106 | 21.93942629 |
| 30600.00 | 3.41480522 | 6.859551875 | 16.0289495 | 22.04702868 |
| 32400.00 | 2.986977055 | 6.109863985 | 14.95596327 | 21.76947212 |
| 34200.00 | 2.61274988 | 5.442110301 | 13.71085135 | 21.11645852 |
| 36000.00 | 2.285408227 | 4.847336144 | 12.54320988 | 20.1108138 |
| 37800.00 | 1.999077984 | 4.317565501 | 11.47500692 | 18.81082714 |
| 39600.00 | 1.748620986 | 3.845694069 | 10.4977741 | 17.40842228 |
| 41400.00 | 1.529542808 | 3.425393979 | 9.603764236 | 16.11057101 |
| 43200.00 | 1.337912114 | 3.051028943 | 8.785889905 | 14.90947853 |
| 45000.00 | 1.170290113 | 2.717578669 | 8.037667266 | 13.79793117 |
| 46800.00 | 1.023668845 | 2.420571539 | 7.353164651 | 12.76925309 |
| 48600.00 | 0.895417207 | 2.156024641 | 6.726955545 | 11.81726611 |
| 50400.00 | 0.783233737 | 1.920390362 | 6.154075565 | 10.93625267 |
| 52200.00 | 0.685105314 | 1.710508809 | 5.629983104 | 10.1209215 |
| 54000.00 | 0.599271033 | 1.52356544 | 5.150523327 | 9.366375756 |
| 55800.00 | 0.524190609 | 1.357053315 | 4.711895231 | 8.668083717 |
| 57600.00 | 0.458516729 | 1.208739481 | 4.310621515 | 8.021851491 |
| 59400.00 | 0.401070884 | 1.076635028 | 3.943521012 | 7.423797859 |
| 61200.00 | 0.350822214 | 0.958968414 | 3.607683467 | 6.870330959 |
| 63000.00 | 0.306869012 | 0.854161712 | 3.300446468 | 6.358126715 |
| 64800.00 | 0.268422542 | 0.760809449 | 3.01937434 | 5.884108868 |
| 66600.00 | 0.234792887 | 0.677659757 | 2.762238835 | 5.445430505 |
| 68400.00 | 0.205376565 | 0.603597584 | 2.527001466 | 5.039456959 |
| 70200.00 | 0.179645704 | 0.537629747 | 2.311797345 | 4.663749987 |
| 72000.00 | 0.157138566 | 0.478871607 | 2.114920406 | 4.316053122 |
| 73800.00 | 0.137451263 | 0.426535208 | 1.934809872 | 3.994278124 |
| 75600.00 | 0.120230509 | 0.379918711 | 1.770037883 | 3.696492439 |
| 77400.00 | 0.105167278 | 0.338396982 | 1.619298182 | 3.420907591 |
| 79200.00 | 0.091991264 | 0.301413207 | 1.481395753 | 3.165868438 |
| 81000.00 | 0.080466023 | 0.26847143 | 1.35523735 | 2.929843236 |
| 82800.00 | 0.070384736 | 0.239129895 | 1.23982283 | 2.711414437 |
| 84600.00 | 0.061566496 | 0.212995129 | 1.134237224 | 2.509270175 |
| 86400.00 | 0.05385306 | 0.189716659 | 1.037643484 | 2.322196387 |



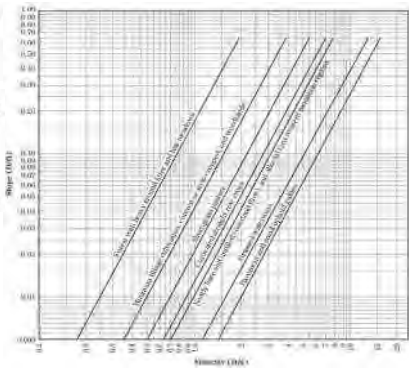
DA RP1 707A DRAINAGE CALCULATIONS

Time of Concentration:

$$T_c = T_{OL} + T_1 + \dots + T_n$$

Equation 5.3
 T_{OL} = (L / V) * 4.83
 T₁ = (L / V) * 4.83
 T_n = (L / V) * 4.83
 T_c = T_{OL} + T₁ + ... + T_n

| Parameter | Value |
|------------------|--------|
| Basin Area | 11.00 |
| Basin Length | 100 |
| Basin Width | 100 |
| Basin Slope | 0.0026 |
| Basin Depth | 4.89 |
| Basin Volume | 530.00 |
| Basin Time | 30.67 |
| Basin Loss | 0.00 |
| Basin Gain | 0.00 |
| Basin Net Change | 0.00 |
| Basin Status | Empty |



| Parameter | Value | Parameter | Value |
|-------------------|----------------|------------------|----------------|
| n = | 0.15 | D = | 920 (ft) |
| L = | 100 (ft) | S = | 0.0026 (ft/ft) |
| P ₂ = | 4.89 (in) | V = | 0.5 (ft/s) |
| S = | 0.0026 (ft/ft) | | |
| T _{OL} = | 17.93 (min) | T ₁ = | 30.67 (min) |

T_c = 48.59 (min)

Intensity:

SEE FIG. 2.1-2.1a

| | |
|--------------|--------------|
| I (500-YR) = | 7.10 (in/hr) |
| I (100-YR) = | 5.2 (in/hr) |
| I (10-YR) = | 3.5 (in/hr) |
| I (2-YR) = | 2.4 (in/hr) |

Peak Flow Rate:

Q=CIA
 C = 0.35 Mixed use area; lots 1/4-1/2 acre; MOSTLY golf course; basin slope <1%

| i (500-YR) | i (100-YR) | i (10-YR) | i (2-YR) |
|---------------|-------------|-----------|----------|
| 7.10 | 5.2 | 3.5 | 2.4 |
| A = 6.39 (Ac) | | | |
| Q (500-YR) = | 15.88 (cfs) | | |
| Q (100-YR) = | 11.63 (cfs) | | |
| Q (10-YR) = | 7.83 (cfs) | | |
| Q (2-YR) = | 5.37 (cfs) | | |

DA RP1 707A EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 567830.74 cft
 Volume (100-yr) = 1.38*area*43560 = 384120.79 cft
 Volume (10-yr) = 0.70*area*43560 = 194843.88 cft
 Volume (2-yr) = 0.41*area*43560 = 114122.844 cft

A= #REF! Ac from DA#15D
 A= 6.39 Ac from DA RP1 707A

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

$q_1 = \frac{Q_p}{L} \left[1 - \cos \left(\frac{\pi t_1}{T_p} \right) \right]$
 $t_1 = 1.25 T_p$

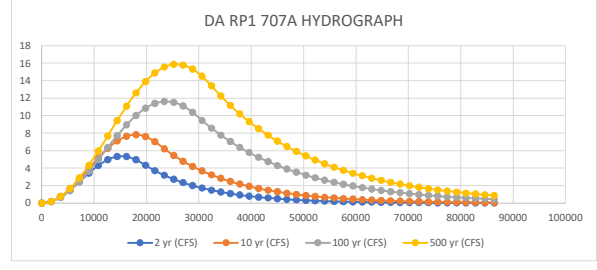
$q_1 = 4.34 Q_p \left(\frac{t_1 - T_p}{T_p} \right)^{-1.81}$
 $t_1 = 1.25 T_p$

| DA RP1 707A Existing Conditions | | | | |
|---------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 5.37 | 7.83 | 11.63 | 15.88 |
| TP= | 15295.992 | 17907.503 | 23761.878 | 25722.475 |
| 1.25*TP= | 19119.990 | 22384.378 | 29702.348 | 32153.093 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.18132494 | 0.193526187 | 0.16388712 | 0.19111764 |
| 3600.00 | 0.700798132 | 0.754966483 | 0.646310491 | 0.755270935 |
| 5400.00 | 1.488225489 | 1.628798728 | 1.420076877 | 1.665303838 |
| 7200.00 | 2.437205477 | 2.72860758 | 2.441570619 | 2.877411063 |
| 9000.00 | 3.41950668 | 3.945630336 | 3.653212167 | 4.33246694 |
| 10800.00 | 4.302395132 | 5.159512731 | 4.986703718 | 5.962732722 |
| 12600.00 | 4.96657007 | 6.25021106 | 6.366879031 | 7.68743231 |
| 14400.00 | 5.322284508 | 7.109863579 | 7.715940394 | 9.424325431 |
| 16200.00 | 5.321472346 | 7.653457215 | 8.957843926 | 11.08980511 |
| 18000.00 | 4.964243328 | 7.827234704 | 10.02258602 | 12.60370192 |
| 19800.00 | 4.329540593 | 7.614010779 | 10.8501493 | 13.89314302 |
| 21600.00 | 3.715377113 | 7.034871659 | 11.39388568 | 14.89605997 |
| 23400.00 | 3.188335297 | 6.214095141 | 11.62314584 | 15.56417641 |
| 25200.00 | 2.736056572 | 5.452905763 | 11.52500685 | 15.86533193 |
| 27000.00 | 2.347935479 | 4.784957517 | 11.10500059 | 15.78503013 |
| 28800.00 | 2.014870991 | 4.198828924 | 10.38680198 | 15.32713641 |
| 30600.00 | 1.729053096 | 3.684497568 | 9.462485104 | 14.51369193 |
| 32400.00 | 1.483779667 | 3.233168718 | 8.575059925 | 13.40396204 |
| 34200.00 | 1.273299302 | 2.837124945 | 7.770860606 | 12.23840929 |
| 36000.00 | 1.092676459 | 2.489594158 | 7.04208193 | 11.17420816 |
| 37800.00 | 0.937675724 | 2.184633808 | 6.381650686 | 10.20254552 |
| 39600.00 | 0.804662492 | 1.917029271 | 5.783157009 | 9.315374632 |
| 41400.00 | 0.690517745 | 1.682204685 | 5.240792177 | 8.505348427 |
| 43200.00 | 0.592564909 | 1.476144702 | 4.74929223 | 7.765758729 |
| 45000.00 | 0.508507093 | 1.295325831 | 4.303886878 | 7.090480673 |
| 46800.00 | 0.43637323 | 1.136656187 | 3.900253209 | 6.473921986 |
| 48600.00 | 0.374471859 | 0.997422622 | 3.534473727 | 5.910976676 |
| 50400.00 | 0.321351456 | 0.875244334 | 3.202998333 | 5.396982747 |
| 52200.00 | 0.275766405 | 0.768032154 | 2.902609869 | 4.927683591 |
| 54000.00 | 0.236647785 | 0.673952822 | 2.630392893 | 4.499192736 |
| 55800.00 | 0.203078305 | 0.591397644 | 2.383705384 | 4.107961663 |
| 57600.00 | 0.174270796 | 0.51895498 | 2.160153098 | 3.750750415 |
| 59400.00 | 0.149549753 | 0.455386108 | 1.957566332 | 3.424600771 |
| 61200.00 | 0.128335494 | 0.399604042 | 1.773978867 | 3.126811742 |
| 63000.00 | 0.110130566 | 0.350654944 | 1.607608882 | 2.854917207 |
| 64800.00 | 0.094508084 | 0.307701816 | 1.456841659 | 2.60666549 |
| 66600.00 | 0.081101716 | 0.27001019 | 1.320213917 | 2.380000708 |
| 68400.00 | 0.069597098 | 0.236935561 | 1.196399607 | 2.173045753 |
| 70200.00 | 0.059724458 | 0.207912376 | 1.084197038 | 1.984086739 |
| 72000.00 | 0.051252293 | 0.182444357 | 0.982517221 | 1.811558814 |
| 73800.00 | 0.04398194 | 0.160096018 | 0.890373296 | 1.6540332 |
| 75600.00 | 0.037742918 | 0.140485216 | 0.806870953 | 1.510205358 |
| 77400.00 | 0.032388927 | 0.12327662 | 0.731199753 | 1.378884186 |
| 79200.00 | 0.027794422 | 0.108175973 | 0.662625265 | 1.258982156 |
| 81000.00 | 0.023851666 | 0.094925066 | 0.600481934 | 1.149506308 |
| 82800.00 | 0.020468208 | 0.083297314 | 0.544166623 | 1.049550024 |
| 84600.00 | 0.017564707 | 0.073093893 | 0.493132761 | 0.958285522 |
| 86400.00 | 0.015073079 | 0.06414033 | 0.446885034 | 0.874957002 |

ti (hrs)

0
0.5
1
1.5
2
2.5
3
3.5
4
4.5
5
5.5
6
6.5
7
7.5
8
8.5
9
9.5
10
10.5
11
11.5
12
12.5
13
13.5
14
14.5
15
15.5
16
16.5
17
17.5
18
18.5
19
19.5
20
20.5
21
21.5
22
22.5
23
23.5
24



DA RP1 702 DRAINAGE CALCULATIONS

Time of Concentration:

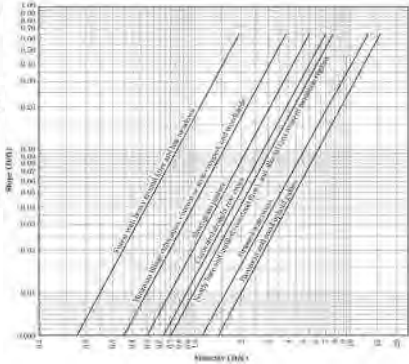
$$T_c = T_{OL} + T_1 + \dots + T_n$$

Equation 2.1
 T_{OL} = (L / V) * 4.83
 T₁ = (L / V) * 4.83 * (S / 0.0026)^{0.58}
 T_n = (L / V) * 4.83 * (S / 0.0026)^{0.58}

| Material | n |
|----------|-------|
| Gravel | 0.15 |
| Asphalt | 0.015 |
| Concrete | 0.015 |
| Brick | 0.015 |
| Stucco | 0.015 |
| Shingles | 0.015 |
| Clay | 0.015 |
| Wood | 0.015 |
| Paint | 0.015 |
| Other | 0.015 |

| | |
|-------------------------------------------------------------|------------------------------|
| Tt=ToL; multiply by 60 to convert hrs. to min. (L=max 300') | T= |
| n= 0.15 | D= 329 (ft) |
| L= 100 (ft) | S= 0.0026 (ft/ft) |
| P ₂ = 4.89 (in) | V= 0.5 (ft/s) |
| S= 0.0026 (ft/ft) | |
| T _{OL} = 17.93 (min) | T ₁ = 10.97 (min) |

Tc = 28.89 (min)



Intensity:

SEE FIG. 2.1-2.1a

| | |
|-------------|--------------|
| I (500-YR)= | 8.97 (in/hr) |
| I (100-YR)= | 6.9 (in/hr) |
| I (10-YR)= | 4.7 (in/hr) |
| I (2-YR)= | 3.3 (in/hr) |

Peak Flow Rate:

Q=CIA
 C= 0.35 Mixed use area; lots 1/4-1/2 acre; MOSTLY golf course; basin slope <1%

| | | | |
|------------|------------|-----------|----------|
| i (500-YR) | i (100-YR) | i (10-YR) | i (2-YR) |
| 8.97 | 6.9 | 4.7 | 3.3 |

| | |
|-------------|------------|
| A= | 2.19 (Ac) |
| Q (500-YR)= | 6.87 (cfs) |
| Q (100-YR)= | 5.29 (cfs) |
| Q (10-YR)= | 3.60 (cfs) |
| Q (2-YR)= | 2.53 (cfs) |

DA RP1 702 EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 194608.66 cft
 Volume (100-yr) = 1.38*area*43560 = 131647.03 cft
 Volume (10-yr) = 0.70*area*43560 = 66777.48 cft
 Volume (2-yr) = 0.41*area*43560 = 39112.524 cft
 A= 2.19 Ac

TP = time to Qp in seconds

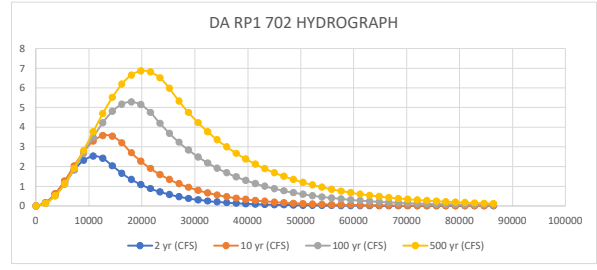
TP = $\frac{V}{1.39 Q_p}$

$Q_1 = \frac{Q_p}{2} \left[1 - \cos \left(\frac{\pi t_i}{T_p} \right) \right]$ $t_i = 1.25 T_p$
 $q_1 = 4.34 Q_p \left(\frac{-1.25 t_i}{T_p} \right)$ $t_i = 1.25 T_p$

| DA RP1 702 Existing Conditions | | | | |
|--------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 2.53 | 3.60 | 5.29 | 6.87 |
| TP= | 11124.358 | 13335.374 | 17907.503 | 20372.567 |
| 1.25*TP= | 13905.447 | 16669.218 | 22384.378 | 25465.709 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.159914888 | 0.159538953 | 0.130756727 | 0.131523896 |
| 3600.00 | 0.5992195 | 0.609895076 | 0.510096066 | 0.516027014 |
| 5400.00 | 1.206820363 | 1.271292273 | 1.100504251 | 1.124074432 |
| 7200.00 | 1.82906443 | 2.026570625 | 1.843594417 | 1.909118204 |
| 9000.00 | 2.308595612 | 2.741940104 | 2.665880617 | 2.81106076 |
| 10800.00 | 2.524147745 | 3.29068014 | 3.486045021 | 3.760855558 |
| 12600.00 | 2.421210963 | 3.575586906 | 4.222979626 | 4.685792815 |
| 14400.00 | 2.040270596 | 3.546192011 | 4.803807223 | 5.515065674 |
| 16200.00 | 1.653233753 | 3.207702466 | 5.171088396 | 6.185190686 |
| 18000.00 | 1.339617327 | 2.70414254 | 5.288501838 | 6.644867673 |
| 19800.00 | 1.085493554 | 2.26893766 | 5.144436257 | 6.858906915 |
| 21600.00 | 0.879576751 | 1.903774682 | 4.753138638 | 6.810923033 |
| 23400.00 | 0.712722115 | 1.597381058 | 4.198577763 | 6.504589345 |
| 25200.00 | 0.577519599 | 1.340298445 | 3.684277173 | 5.973465385 |
| 27000.00 | 0.467964836 | 1.124590724 | 3.23297532 | 5.325288471 |
| 28800.00 | 0.379192477 | 0.943599018 | 2.836955237 | 4.747444821 |
| 30600.00 | 0.307260127 | 0.79173613 | 2.489445238 | 4.232302615 |
| 32400.00 | 0.248973256 | 0.664314064 | 2.18450313 | 3.773058162 |
| 34200.00 | 0.201743333 | 0.557399315 | 1.916914601 | 3.363646031 |
| 36000.00 | 0.163472869 | 0.467691432 | 1.682104061 | 2.998658948 |
| 37800.00 | 0.132462265 | 0.392421142 | 1.476056404 | 2.673276381 |
| 39600.00 | 0.107334335 | 0.329264857 | 1.295248349 | 2.383200868 |
| 41400.00 | 0.086973143 | 0.276272949 | 1.136588196 | 2.124601264 |
| 43200.00 | 0.070474443 | 0.231809562 | 0.99736296 | 1.894062138 |
| 45000.00 | 0.057105528 | 0.194502116 | 0.87519198 | 1.688538665 |
| 46800.00 | 0.046272679 | 0.163198933 | 0.767986212 | 1.505316413 |
| 48600.00 | 0.037494808 | 0.136933686 | 0.673912508 | 1.341975491 |
| 50400.00 | 0.030382089 | 0.114895569 | 0.591362269 | 1.196358587 |
| 52200.00 | 0.024618643 | 0.096404269 | 0.518923938 | 1.066542481 |
| 54000.00 | 0.019948517 | 0.080888959 | 0.455358868 | 0.950812638 |
| 55800.00 | 0.016164308 | 0.067870685 | 0.399580139 | 0.847640566 |
| 57600.00 | 0.013097958 | 0.056947572 | 0.350633969 | 0.755663629 |
| 59400.00 | 0.010613291 | 0.047782426 | 0.307683411 | 0.673667051 |
| 61200.00 | 0.008599963 | 0.040092319 | 0.269994039 | 0.60056787 |
| 63000.00 | 0.006968561 | 0.033639859 | 0.236921388 | 0.535400634 |
| 64800.00 | 0.005646633 | 0.028225858 | 0.20789994 | 0.477304653 |
| 66600.00 | 0.004575474 | 0.023683186 | 0.182433444 | 0.42551263 |
| 68400.00 | 0.003707512 | 0.019871613 | 0.160086442 | 0.379340526 |
| 70200.00 | 0.003004201 | 0.016673474 | 0.140476813 | 0.338178528 |
| 72000.00 | 0.002434308 | 0.013990044 | 0.123269246 | 0.301482992 |
| 73800.00 | 0.001972523 | 0.011738485 | 0.108169503 | 0.268769265 |
| 75600.00 | 0.001598338 | 0.009849293 | 0.094919387 | 0.239605284 |
| 77400.00 | 0.001295135 | 0.008264147 | 0.083292332 | 0.213605868 |
| 79200.00 | 0.001049449 | 0.006934115 | 0.073089521 | 0.190427631 |
| 81000.00 | 0.00085037 | 0.005818138 | 0.064136493 | 0.169764451 |
| 82800.00 | 0.000689056 | 0.004881766 | 0.056280157 | 0.151343419 |
| 84600.00 | 0.00058343 | 0.004096094 | 0.049386176 | 0.134921241 |
| 86400.00 | 0.000452426 | 0.003436869 | 0.043336665 | 0.120281023 |

ti (hrs)



DA RP1 705 DRAINAGE CALCULATIONS

Time of Concentration:

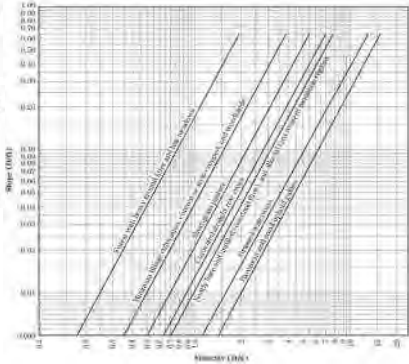
$$T_c = T_{OL} + T_1 + \dots + T_n$$

Equation 5.3
 The time of concentration is the time required for runoff to travel from the most hydraulically distant point in the watershed to the outlet point.
 It is the sum of the travel time through the overland flow area and the travel time through the pipe network.

| Item | Value |
|------------------------------------------|--------------|
| Overland Flow Time (min) | 17.93 |
| Pipe Flow Time (min) | 13.20 |
| Total Time of Concentration (min) | 31.13 |

| | |
|---------------------------------------------------------------------------|---------------------|
| $T_{OL} = Tt = Tol$; multiply by 60 to convert hrs. to min. (L=max 300') | $T =$ |
| n= 0.15 | D= 396 (ft) |
| L= 100 (ft) | S= 0.0026 (ft/ft) |
| $P_s = 4.89$ (in) | V= 0.5 (ft/s) |
| S= 0.0026 (ft/ft) | |
| $T_{OL} = 17.93$ (min) | $T_1 = 13.20$ (min) |

Tc = 31.13 (min)



Intensity:

SEE FIG. 2.1-2.1a

| | |
|-------------|--------------|
| I (500-YR)= | 8.60 (in/hr) |
| I (100-YR)= | 6.7 (in/hr) |
| I (10-YR)= | 4.6 (in/hr) |
| I (2-YR)= | 3.2 (in/hr) |

Peak Flow Rate:

Q=CIA
 C= 0.35 Mixed use area; lots 1/4-1/2 acre; MOSTLY golf course; basin slope <1%

| | | | | | | | |
|-------------|------|------------|-----|-----------|-----|----------|-----|
| i (500-YR) | 8.60 | i (100-YR) | 6.7 | i (10-YR) | 4.6 | i (2-YR) | 3.2 |
| A= | | 2.08 (Ac) | | | | | |
| Q (500-YR)= | | 6.26 (cfs) | | | | | |
| Q (100-YR)= | | 4.88 (cfs) | | | | | |
| Q (10-YR)= | | 3.35 (cfs) | | | | | |
| Q (2-YR)= | | 2.33 (cfs) | | | | | |

DA RP1 705 EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 184833.79 cft
 Volume (100-yr) = 1.38*area*43560 = 125034.62 cft
 Volume (10-yr) = 0.70*area*43560 = 63423.36 cft
 Volume (2-yr) = 0.41*area*43560 = 37147.968 cft
 A= 2.08 Ac

TP = time to Qp in seconds

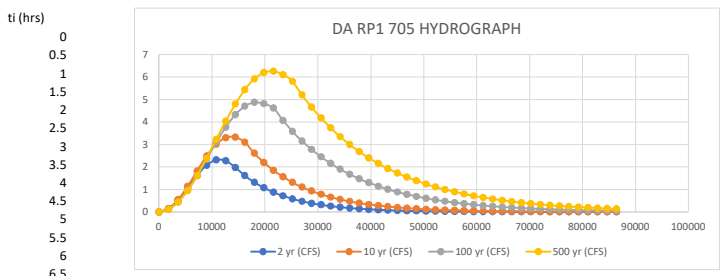
TP = $\frac{V}{1.39 Q_p}$

$$q_1 = \frac{Q_p}{2} \left[1 - \cos \left(\frac{\pi t_i}{T_p} \right) \right] \quad t_i = 1.25 T_p$$

$$q_1 = 1.34 Q_p \left(\frac{t_i - T_p}{T_p} \right)^2 \quad t_i = 1.25 T_p$$

| DA RP1 705 Existing Conditions | | | | |
|--------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 2.33 | 3.35 | 4.88 | 6.26 |
| TP= | 11471.994 | 13625.274 | 18442.055 | 21231.277 |
| 1.25*TP= | 14339.992 | 17031.592 | 23052.569 | 26539.097 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.138668166 | 0.142147972 | 0.113754062 | 0.110421602 |
| 3600.00 | 0.521656076 | 0.544456621 | 0.444404481 | 0.433899275 |
| 5400.00 | 1.057775147 | 1.138618065 | 0.961105902 | 0.94762078 |
| 7200.00 | 1.619376602 | 1.823749786 | 1.615656844 | 1.615357537 |
| 9000.00 | 2.072744362 | 2.483523445 | 2.34699627 | 2.390019526 |
| 10800.00 | 2.309932556 | 3.005916243 | 3.086899782 | 3.216976164 |
| 12600.00 | 2.274467195 | 3.302231241 | 3.766344066 | 4.037908956 |
| 14400.00 | 1.977376343 | 3.322157192 | 4.321945863 | 4.794924217 |
| 16200.00 | 1.612516306 | 3.098194108 | 4.701874795 | 5.34635845 |
| 18000.00 | 1.314979238 | 2.609294104 | 4.870688466 | 5.911930203 |
| 19800.00 | 1.07234289 | 2.197543306 | 4.812638769 | 6.19314762 |
| 21600.00 | 0.874477133 | 1.850767444 | 4.617810822 | 6.258456128 |
| 23400.00 | 0.713121021 | 1.55871337 | 4.067533664 | 6.103250052 |
| 25200.00 | 0.581537894 | 1.312745898 | 3.582829775 | 5.80979686 |
| 27000.00 | 0.474234123 | 1.105592488 | 3.155885177 | 5.203496753 |
| 28800.00 | 0.386729749 | 0.931128218 | 2.779817037 | 4.660469051 |
| 30600.00 | 0.315371441 | 0.784194691 | 2.44856271 | 4.174110758 |
| 32400.00 | 0.257179971 | 0.66044751 | 2.156781998 | 3.738507955 |
| 34200.00 | 0.209725831 | 0.556227832 | 1.899771065 | 3.348363888 |
| 36000.00 | 0.171027798 | 0.468454187 | 1.673386602 | 2.998934565 |
| 37800.00 | 0.13947022 | 0.394531365 | 1.473979035 | 2.685971067 |
| 39600.00 | 0.113735559 | 0.332273682 | 1.298333686 | 2.405667886 |
| 41400.00 | 0.092749387 | 0.279840362 | 1.143618952 | 2.154616647 |
| 43200.00 | 0.075635525 | 0.235681103 | 1.007340657 | 1.929764671 |
| 45000.00 | 0.061679467 | 0.198490247 | 0.887301839 | 1.728377849 |
| 46800.00 | 0.050298541 | 0.167168167 | 0.781567336 | 1.548007399 |
| 48600.00 | 0.041017593 | 0.140788762 | 0.688432587 | 1.38646009 |
| 50400.00 | 0.03344914 | 0.118572069 | 0.606396154 | 1.241771571 |
| 52200.00 | 0.027277196 | 0.099861206 | 0.534135517 | 1.11218249 |
| 54000.00 | 0.022244083 | 0.084102948 | 0.470485752 | 0.996117096 |
| 55800.00 | 0.018139666 | 0.070831368 | 0.414420752 | 0.892164081 |
| 57600.00 | 0.014792585 | 0.059654064 | 0.365036686 | 0.799059418 |
| 59400.00 | 0.012063098 | 0.050240557 | 0.321537427 | 0.715670993 |
| 61200.00 | 0.009837248 | 0.042312516 | 0.283221717 | 0.640984836 |
| 63000.00 | 0.008022106 | 0.035635533 | 0.249471863 | 0.574092794 |
| 64800.00 | 0.006541889 | 0.030012189 | 0.219743779 | 0.514181487 |
| 66600.00 | 0.005334798 | 0.025276217 | 0.193558215 | 0.460522418 |
| 68400.00 | 0.004350436 | 0.02128759 | 0.170493029 | 0.412463115 |
| 70200.00 | 0.003547705 | 0.017928374 | 0.150176385 | 0.369419195 |
| 72000.00 | 0.002893093 | 0.015099248 | 0.132280755 | 0.330867262 |
| 73800.00 | 0.002359267 | 0.012716562 | 0.116517641 | 0.296338541 |
| 75600.00 | 0.001923942 | 0.010709868 | 0.102632924 | 0.265413176 |
| 77400.00 | 0.001568941 | 0.009019834 | 0.090402766 | 0.237715127 |
| 79200.00 | 0.001279444 | 0.00759649 | 0.079630004 | 0.212907597 |
| 81000.00 | 0.001043365 | 0.006397751 | 0.070140968 | 0.190688938 |
| 82800.00 | 0.000850846 | 0.005388176 | 0.061782685 | 0.170788978 |
| 84600.00 | 0.00069385 | 0.004537913 | 0.054420408 | 0.152965743 |
| 86400.00 | 0.000565823 | 0.003821823 | 0.047935451 | 0.137002509 |



DA RP1 707 DRAINAGE CALCULATIONS

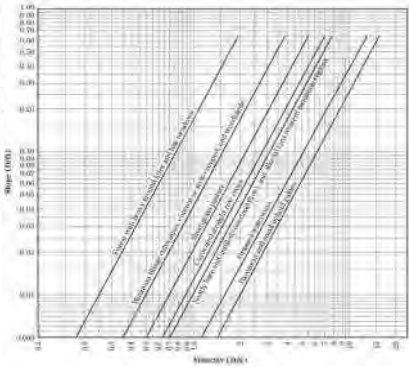
Time of Concentration:

$$T_c = T_{OL} + T_1 + \dots + T_n$$

Equation 2.1
 T_{OL} = 0.0114 L^{0.77} / S^{0.385}
 T₁ = 0.0114 L₁^{0.77} / S₁^{0.385}
 T₂ = 0.0114 L₂^{0.77} / S₂^{0.385}
 T_n = 0.0114 L_n^{0.77} / S_n^{0.385}
 T_c = T_{OL} + T₁ + T₂ + ... + T_n

Table 2.3 Manning's Roughness Coefficients for Open Channel Flow

| Surface | n |
|------------------------|-------------|
| Smoothed Concrete | 0.012 |
| Cast-in-place concrete | 0.012-0.015 |
| Asphalt concrete | 0.016 |
| Gravel | 0.020-0.025 |
| Grass | 0.030-0.040 |
| Earth | 0.022-0.035 |
| Wood | 0.012-0.018 |



| | | |
|----------------------------|-----------------------------------------------------------------------|-------|
| $T_{OL} =$ | $Tt = T_{OL}$; multiply by 60 to convert hrs. to min. (L = max 300') | $T =$ |
| n = 0.15 | D = 242 (ft) | |
| L = 100 (ft) | S = 0.0026 (ft/ft) | |
| P ₂ = 4.89 (in) | V = 0.5 (ft/s) | |
| S = 0.0026 (ft/ft) | | |
| $T_{OL} = 17.93$ (min) | $T_1 = 8.07$ (min) | |

$T_c = 25.99$ (min)

Intensity:

SEE FIG. 2.1-2.1a

| | |
|--------------|--------------|
| I (500-YR) = | 9.66 (in/hr) |
| I (100-YR) = | 7.3 (in/hr) |
| I (10-YR) = | 4.9 (in/hr) |
| I (2-YR) = | 3.5 (in/hr) |

Peak Flow Rate:

Q = CIA

C = 0.35 Mixed use area; lots 1/4-1/2 acre; MOSTLY golf course; basin slope <1%

| | | | | | | | |
|---------------|------------|------------|-----|-----------|-----|----------|-----|
| i (500-YR) | 9.66 | i (100-YR) | 7.3 | i (10-YR) | 4.9 | i (2-YR) | 3.5 |
| A = 2.16 (Ac) | | | | | | | |
| Q (500-YR) = | 7.30 (cfs) | | | | | | |
| Q (100-YR) = | 5.52 (cfs) | | | | | | |
| Q (10-YR) = | 3.70 (cfs) | | | | | | |
| Q (2-YR) = | 2.65 (cfs) | | | | | | |

DA RP1 707 EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 191942.78 cft
 Volume (100-yr) = 1.38*area*43560 = 129843.65 cft
 Volume (10-yr) = 0.70*area*43560 = 65862.72 cft
 Volume (2-yr) = 0.41*area*43560 = 38576.736 cft
 A= 2.16 Ac

TP = time to Qp in seconds

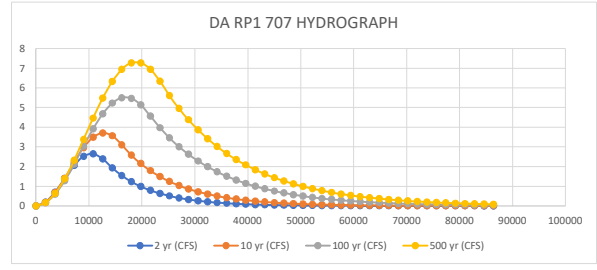
TP = $\frac{V}{1.39 Q_p}$

$Q_1 = \frac{Q_p}{2} \left[1 - \cos \left(\frac{\pi t_i}{T_p} \right) \right]$ $t_i = 1.25 T_p$
 $q_1 = 4.34 Q_p \left(\frac{-1.3 t_i}{T_p} \right)^{1.4}$ $t_i = 1.25 T_p$

| DA RP1 707 Existing Conditions | | | | |
|--------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 2.65 | 3.70 | 5.52 | 7.30 |
| TP= | 10488.680 | 12791.073 | 16926.270 | 18905.004 |
| 1.25*TP= | 13110.850 | 15988.842 | 21157.837 | 23631.256 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.187666848 | 0.178075273 | 0.152568077 | 0.162170127 |
| 3600.00 | 0.697426505 | 0.678059862 | 0.593401235 | 0.634278551 |
| 5400.00 | 1.384660699 | 1.403814158 | 1.273751873 | 1.374398408 |
| 7200.00 | 2.054401818 | 2.21578639 | 2.118386397 | 2.316801351 |
| 9000.00 | 2.516645018 | 2.957846361 | 3.0339046 | 3.377794741 |
| 10800.00 | 2.640252393 | 3.487306961 | 3.919067915 | 4.463154188 |
| 12600.00 | 2.390156663 | 3.702360781 | 4.675994437 | 5.476491414 |
| 14400.00 | 1.927342517 | 3.561656168 | 5.220982765 | 6.327814266 |
| 16200.00 | 1.541944771 | 3.098552003 | 5.493767752 | 6.941518716 |
| 18000.00 | 1.233612425 | 2.580530051 | 5.464184667 | 7.263103081 |
| 19800.00 | 0.986935229 | 2.149112017 | 5.135504825 | 7.264008192 |
| 21600.00 | 0.789584416 | 1.789819289 | 4.558871149 | 6.944153668 |
| 23400.00 | 0.631696521 | 1.490593818 | 3.970247326 | 6.331945055 |
| 25200.00 | 0.505380408 | 1.241393443 | 3.457624336 | 5.60392229 |
| 27000.00 | 0.40432288 | 1.033854872 | 3.011189245 | 4.951497281 |
| 28800.00 | 0.323473148 | 0.861013003 | 2.622396128 | 4.375029497 |
| 30600.00 | 0.258790394 | 0.717067174 | 2.283802476 | 3.865675778 |
| 32400.00 | 0.207041816 | 0.597186489 | 1.988926727 | 3.415622507 |
| 34200.00 | 0.165641054 | 0.49734769 | 1.732124195 | 3.017965753 |
| 36000.00 | 0.132518924 | 0.414200136 | 1.508479014 | 2.666605361 |
| 37800.00 | 0.106020004 | 0.344953351 | 1.313710034 | 2.356151372 |
| 39600.00 | 0.084819896 | 0.287283379 | 1.144088871 | 2.081841344 |
| 41400.00 | 0.06785903 | 0.239254785 | 0.996368538 | 1.839467291 |
| 43200.00 | 0.054289716 | 0.199255704 | 0.867721283 | 1.625311133 |
| 45000.00 | 0.043433766 | 0.165943748 | 0.755684465 | 1.436087662 |
| 46800.00 | 0.034748607 | 0.138200949 | 0.658113408 | 1.268894139 |
| 48600.00 | 0.027800161 | 0.115096246 | 0.573140348 | 1.121165776 |
| 50400.00 | 0.02224115 | 0.095854231 | 0.499138681 | 0.99063638 |
| 52200.00 | 0.017793736 | 0.079829135 | 0.434691824 | 0.875303597 |
| 54000.00 | 0.014235642 | 0.066483145 | 0.378566096 | 0.773398195 |
| 55800.00 | 0.011389036 | 0.055368363 | 0.329687105 | 0.683356917 |
| 57600.00 | 0.009111647 | 0.046111772 | 0.28711918 | 0.603798507 |
| 59400.00 | 0.007289652 | 0.038402717 | 0.250047461 | 0.533502521 |
| 61200.00 | 0.005831989 | 0.031982476 | 0.217762299 | 0.471390598 |
| 63000.00 | 0.004665806 | 0.026635583 | 0.189645673 | 0.416509927 |
| 64800.00 | 0.003732816 | 0.022182595 | 0.165159357 | 0.368018624 |
| 66600.00 | 0.00298639 | 0.018474065 | 0.143834619 | 0.325172821 |
| 68400.00 | 0.002389221 | 0.015385535 | 0.125263249 | 0.287315251 |
| 70200.00 | 0.001911465 | 0.012813351 | 0.109089742 | 0.253865169 |
| 72000.00 | 0.001529242 | 0.01067119 | 0.095004496 | 0.224309445 |
| 73800.00 | 0.00122345 | 0.00888716 | 0.082737883 | 0.198194684 |
| 75600.00 | 0.000978805 | 0.007401387 | 0.072055087 | 0.175120279 |
| 77400.00 | 0.00078308 | 0.006164009 | 0.062751613 | 0.154732265 |
| 79200.00 | 0.000626493 | 0.005133498 | 0.054649367 | 0.136717882 |
| 81000.00 | 0.000501217 | 0.00427527 | 0.047593252 | 0.120800787 |
| 82800.00 | 0.000400992 | 0.003560522 | 0.041448195 | 0.106736806 |
| 84600.00 | 0.000320808 | 0.002965267 | 0.036096565 | 0.094310195 |
| 86400.00 | 0.000256658 | 0.002469528 | 0.031435916 | 0.083330327 |

ti (hrs)
0
0.5
1
1.5
2
2.5
3
3.5
4
4.5
5
5.5
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6.5
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17
17.5
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18.5
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19.5
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20.5
21
21.5
22
22.5
23
23.5
24



DA RP1 708 EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 550058.26 cft
 Volume (100-yr) = 1.38*area*43560 = 372098.23 cft
 Volume (10-yr) = 0.70*area*43560 = 188745.48 cft
 Volume (2-yr) = 0.41*area*43560 = 110550.924 cft
 A= 6.19 Ac

TP = time to Qp in seconds

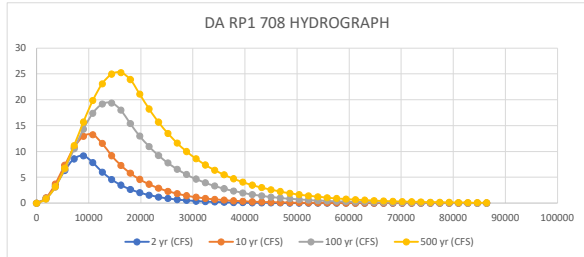
TP = $\frac{V}{1.39 Q_p}$

$Q_p = \frac{Q_p}{2} \left[1 - \cos \left(\frac{\pi t_i}{T_p} \right) \right]$
 $t_i = 1.25 T_p$
 $Q_p = 4.34 Q_{ps} \left(\frac{t_i}{T_p} \right)^{-1.81}$
 $t_i = 1.25 T_p$

| DA RP1 708 Existing Conditions | | | | |
|--------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 9.19 | 13.37 | 19.50 | 25.35 |
| TP= | 8652.278 | 10155.875 | 13729.085 | 15609.995 |
| 1.25*TP= | 10815.348 | 12694.844 | 17161.357 | 19512.494 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.947166479 | 1.009821909 | 0.815368838 | 0.822651102 |
| 3600.00 | 3.398278752 | 3.734213656 | 3.125090226 | 3.183821866 |
| 5400.00 | 6.343078554 | 7.350118196 | 6.542821657 | 6.777025364 |
| 7200.00 | 8.567827789 | 10.76514648 | 10.49688599 | 11.13585318 |
| 9000.00 | 9.155566705 | 12.94759554 | 14.32589473 | 15.69451661 |
| 10800.00 | 7.864050951 | 13.23813284 | 17.3893772 | 19.86128768 |
| 12600.00 | 6.007935577 | 11.54898512 | 19.17491078 | 23.09530723 |
| 14400.00 | 4.584276011 | 9.185715844 | 19.38383281 | 24.97678997 |
| 16200.00 | 3.497971353 | 7.295379125 | 17.98119731 | 25.2615139 |
| 18000.00 | 2.669080911 | 5.794056499 | 15.39128099 | 23.91252101 |
| 19800.00 | 2.036606989 | 4.601692405 | 12.97935618 | 21.10491455 |
| 21600.00 | 1.554006105 | 3.65470599 | 10.94539739 | 18.20754248 |
| 23400.00 | 1.185763864 | 2.90260076 | 9.230174623 | 15.67288232 |
| 25200.00 | 0.904781479 | 2.305271941 | 7.783739643 | 13.49107056 |
| 27000.00 | 0.690381576 | 1.830867957 | 6.563971464 | 11.61298739 |
| 28800.00 | 0.526786557 | 1.454091995 | 5.535349762 | 9.996350959 |
| 30600.00 | 0.401957535 | 1.154853096 | 4.667920504 | 8.604765436 |
| 32400.00 | 0.306708396 | 0.91719484 | 3.936423671 | 7.40690163 |
| 34200.00 | 0.234029797 | 0.72844489 | 3.319557672 | 6.375791666 |
| 36000.00 | 0.17857335 | 0.578537243 | 2.799359027 | 5.488221851 |
| 37800.00 | 0.13625804 | 0.459479544 | 2.360679263 | 4.724210052 |
| 39600.00 | 0.1039699 | 0.364922836 | 1.990743785 | 4.06655584 |
| 41400.00 | 0.079332861 | 0.289825037 | 1.678779866 | 3.500453244 |
| 43200.00 | 0.060533894 | 0.230181683 | 1.415702945 | 3.013157422 |
| 45000.00 | 0.046189589 | 0.182812387 | 1.193852076 | 2.593697735 |
| 46800.00 | 0.035244357 | 0.145191262 | 1.006766839 | 2.232630758 |
| 48600.00 | 0.026892742 | 0.115312222 | 0.84899921 | 1.921827681 |
| 50400.00 | 0.020520152 | 0.091582016 | 0.715954906 | 1.654291298 |
| 52200.00 | 0.015657631 | 0.072735271 | 0.603759605 | 1.423998481 |
| 54000.00 | 0.011947349 | 0.057767014 | 0.509146117 | 1.225764578 |
| 55800.00 | 0.009116267 | 0.045879088 | 0.429359246 | 1.055126687 |
| 57600.00 | 0.006956047 | 0.036437589 | 0.362075554 | 0.908243187 |
| 59400.00 | 0.00530772 | 0.028939065 | 0.305335701 | 0.781807243 |
| 61200.00 | 0.004049886 | 0.022983669 | 0.257487393 | 0.672972364 |
| 63000.00 | 0.003090288 | 0.018253839 | 0.21713726 | 0.579288319 |
| 64800.00 | 0.002358004 | 0.014497365 | 0.183110284 | 0.498645968 |
| 66600.00 | 0.001799244 | 0.011513939 | 0.154415581 | 0.429229787 |
| 68400.00 | 0.001372889 | 0.009144475 | 0.130217545 | 0.369476987 |
| 70200.00 | 0.001047565 | 0.007262626 | 0.109811516 | 0.318042336 |
| 72000.00 | 0.000799331 | 0.005768043 | 0.092603259 | 0.273767869 |
| 73800.00 | 0.000609919 | 0.004581033 | 0.07809166 | 0.235656822 |
| 75600.00 | 0.00046539 | 0.003638298 | 0.065854133 | 0.202851189 |
| 77400.00 | 0.00035511 | 0.002889569 | 0.055534315 | 0.174612406 |
| 79200.00 | 0.000270962 | 0.002294922 | 0.046831687 | 0.150304727 |
| 81000.00 | 0.000206754 | 0.001822648 | 0.039492824 | 0.129380903 |
| 82800.00 | 0.000157761 | 0.001447564 | 0.033304013 | 0.111369872 |
| 84600.00 | 0.000120377 | 0.001149668 | 0.028085034 | 0.095866144 |
| 86400.00 | 9.18524E-05 | 0.000913077 | 0.023683907 | 0.082520681 |

ti (hrs)
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DA RP1 711 DRAINAGE CALCULATIONS

Time of Concentration:

$$T_c = T_{01} + T_1 + \dots + T_n$$

Table 2.1.1 (partial) showing drainage calculation parameters:

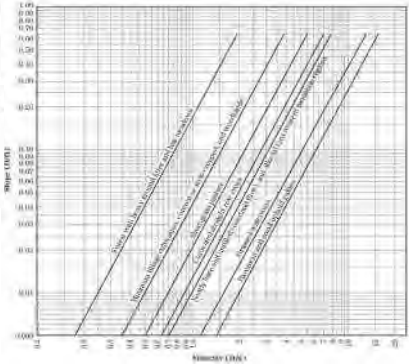
- Area: 22.51 ac
- Peak runoff rate: 7.68 in/hr
- Peak runoff rate: 5.6 in/hr
- Peak runoff rate: 3.8 in/hr
- Peak runoff rate: 2.6 in/hr

Table 2.1.2 (partial) showing drainage calculation parameters:

- Runoff coefficient: 0.45
- Peak runoff rate: 7.68 in/hr
- Peak runoff rate: 5.6 in/hr
- Peak runoff rate: 3.8 in/hr
- Peak runoff rate: 2.6 in/hr

| | | |
|-----------------------|-----------------------------------------------------------------------|----------------------|
| $T_{01} =$ | $T_t = T_{01}$; multiply by 60 to convert hrs. to min. (L= max 300') | $T =$ |
| $n = 0.15$ | | $D = 1557$ (ft) |
| $L = 100$ (ft) | | $S = 0.0128$ (ft/ft) |
| $P_2 = 4.89$ (in) | | $V = 0.8$ (ft/s) |
| $S = 0.0128$ (ft/ft) | | |
| $T_{01} = 9.48$ (min) | | $T_1 = 32.44$ (min) |

$T_c = 41.91$ (min)



Intensity:

SEE FIG. 2.1-2.1a

| | |
|-------------|--------------|
| I (500-YR)= | 7.68 (in/hr) |
| I (100-YR)= | 5.6 (in/hr) |
| I (10-YR)= | 3.8 (in/hr) |
| I (2-YR)= | 2.6 (in/hr) |

Peak Flow Rate:

Q=CIA

C= 0.45 Single family residential district; lots 1/4-1/2 acre; basin slope 1-3.5%

| | | | |
|------------|------------|-----------|----------|
| i (500-YR) | i (100-YR) | i (10-YR) | i (2-YR) |
| 7.68 | 5.6 | 3.8 | 2.6 |

A= 22.51 (Ac)

| | |
|-------------|-------------|
| Q (500-YR)= | 77.75 (cfs) |
| Q (100-YR)= | 56.73 (cfs) |
| Q (10-YR)= | 38.49 (cfs) |
| Q (2-YR)= | 26.34 (cfs) |

DA RP1 711 EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 2000292.62 cft
 Volume (100-yr) = 1.38*area*43560 = 1353139.13 cft
 Volume (10-yr) = 0.70*area*43560 = 686374.92 cft
 Volume (2-yr) = 0.41*area*43560 = 402019.596 cft
 A= 22.51 Ac

TP = time to Qp in seconds

$$T_p = \frac{V}{1.39 Q_p}$$

$$Q_i = \frac{Q_p}{2} \left[2 - \cos \left(\frac{\pi t_i}{T_p} \right) \right] \quad t_i = 1.25 T_p$$

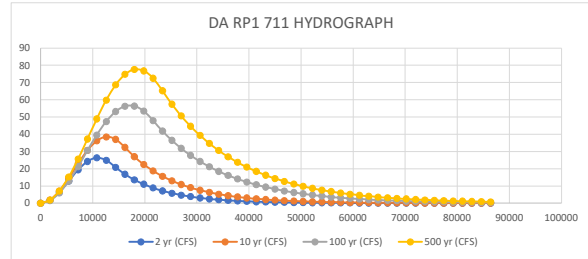
$$Q_i = 4.34 Q_p \left(\frac{t_i}{T_p} \right)^{-1.81} \quad t_i = 1.25 T_p$$

| DA RP1 711 Existing Conditions | | | | |
|--------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 26.34 | 38.49 | 56.73 | 77.75 |
| TP= | 10981.738 | 12828.474 | 17161.357 | 18509.007 |
| 1.25*TP= | 13727.172 | 16035.593 | 21451.696 | 23136.259 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 1.707600817 | 1.839766216 | 1.525894261 | 1.800252029 |
| 3600.00 | 6.387538284 | 7.007331418 | 5.939392285 | 7.034271491 |
| 5400.00 | 12.82607415 | 14.514741 | 12.76560592 | 15.21729141 |
| 7200.00 | 19.353379 | 22.92670008 | 21.27004115 | 25.59141283 |
| 9000.00 | 24.27660125 | 30.6349786 | 30.53762889 | 37.1958003 |
| 10800.00 | 26.31890692 | 36.16587879 | 39.57118562 | 48.95567297 |
| 12600.00 | 24.95062558 | 38.4619823 | 47.39870929 | 59.7818492 |
| 14400.00 | 20.78412544 | 37.08431138 | 53.17796589 | 68.67162488 |
| 16200.00 | 16.79545751 | 32.35170767 | 56.28711295 | 74.80164243 |
| 18000.00 | 13.57225223 | 26.95746025 | 56.39160924 | 77.60414886 |
| 19800.00 | 10.96761017 | 22.46263692 | 53.48021105 | 76.81958028 |
| 21600.00 | 8.862823269 | 18.71726983 | 47.93560871 | 72.52060223 |
| 23400.00 | 7.161964646 | 15.59639641 | 41.82548189 | 65.22466838 |
| 25200.00 | 5.78751669 | 12.99589007 | 36.49418423 | 57.47860633 |
| 27000.00 | 4.676838143 | 10.82898601 | 31.84244203 | 50.65246429 |
| 28800.00 | 3.77930919 | 9.023386431 | 27.78363556 | 44.63699283 |
| 30600.00 | 3.054024433 | 7.518848263 | 24.24218608 | 39.33591695 |
| 32400.00 | 2.467928599 | 6.265173241 | 21.15214852 | 34.66439525 |
| 34200.00 | 1.994310034 | 5.220533034 | 18.45598353 | 30.54766207 |
| 36000.00 | 1.611583298 | 4.350073671 | 16.10348603 | 26.91983089 |
| 37800.00 | 1.3023054 | 3.624752649 | 14.05085033 | 23.72283985 |
| 39600.00 | 1.052380822 | 3.020369943 | 12.25985445 | 20.90552251 |
| 41400.00 | 0.850419106 | 2.516760584 | 10.69714841 | 18.42278893 |
| 43200.00 | 0.687215731 | 2.097121861 | 9.333633162 | 16.23490404 |
| 45000.00 | 0.555332609 | 1.747452709 | 8.143918797 | 14.30685171 |
| 46800.00 | 0.448759091 | 1.456086567 | 7.105851732 | 12.60777429 |
| 48600.00 | 0.362638027 | 1.213302127 | 6.200102199 | 11.1104788 |
| 50400.00 | 0.2930444 | 1.010998993 | 5.409804303 | 9.791001672 |
| 52200.00 | 0.236806441 | 0.842427406 | 4.720241966 | 8.628225251 |
| 54000.00 | 0.191361071 | 0.701963047 | 4.118574901 | 7.603539809 |
| 55800.00 | 0.154637093 | 0.584919385 | 3.593599509 | 6.700545702 |
| 57600.00 | 0.12496079 | 0.487391306 | 3.135540264 | 5.904790905 |
| 59400.00 | 0.100979646 | 0.40612483 | 2.735867679 | 5.203539709 |
| 61200.00 | 0.081600708 | 0.338408534 | 2.387139481 | 4.585568894 |
| 63000.00 | 0.06594077 | 0.281983093 | 2.082862027 | 4.040988108 |
| 64800.00 | 0.05328612 | 0.234965897 | 1.817369391 | 3.561081573 |
| 66600.00 | 0.043060015 | 0.195788238 | 1.585717854 | 3.138168594 |
| 68400.00 | 0.034796396 | 0.163142969 | 1.383593849 | 2.765480633 |
| 70200.00 | 0.028118642 | 0.135940895 | 1.207233642 | 2.437052983 |
| 72000.00 | 0.022722412 | 0.113274431 | 1.053353242 | 2.147629302 |
| 73800.00 | 0.018361769 | 0.09438732 | 0.919087253 | 1.89257749 |
| 75600.00 | 0.014837974 | 0.078649401 | 0.80193552 | 1.667815555 |
| 77400.00 | 0.011990428 | 0.065535585 | 0.699716567 | 1.46974628 |
| 79200.00 | 0.009689353 | 0.054608336 | 0.610526984 | 1.295199653 |
| 81000.00 | 0.007829875 | 0.045503071 | 0.532705978 | 1.141382131 |
| 82800.00 | 0.006327249 | 0.037915996 | 0.46480445 | 1.005831931 |
| 84600.00 | 0.005112991 | 0.031593973 | 0.40555801 | 0.886379633 |
| 86400.00 | 0.00413176 | 0.026326068 | 0.353863436 | 0.781113454 |

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DA RP2 107 EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 1553314.75 cft
 Volume (100-yr) = 1.38*area*43560 = 1050771.74 cft
 Volume (10-yr) = 0.70*area*43560 = 533000.16 cft
 Volume (2-yr) = 0.41*area*43560 = 312185.808 cft
 A= #REF! Ac from DA#15B
 A= 17.48 Ac from DA RP2 107

Tr = time to Qp in seconds

Tr = $\frac{V}{1.39 Q_p}$

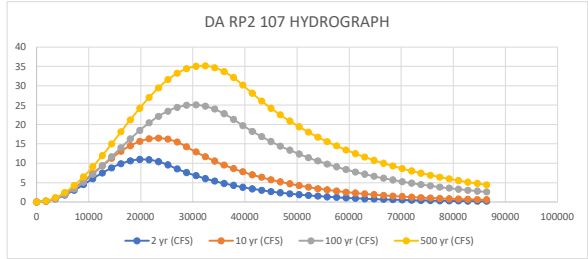
$Q_t = \frac{Q_p}{2} \left[1 - \cos \left(\frac{\pi t}{T_r} \right) \right]$ $t_r = 1.25 T_r$
 $Q_t = 0.34 Q_p \left(1 - \cos \left(\frac{\pi t}{T_r} \right) \right)$ $t_r = 1.25 T_r$

| DA#15B Existing Conditions | | | | |
|----------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 11.01 | 16.52 | 25.08 | 35.16 |
| Tr= | 20394.656 | 23213.429 | 30137.017 | 31782.025 |
| 1.25*Tr= | 25493.320 | 29016.787 | 37671.271 | 39727.531 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.210305112 | 0.243854433 | 0.220142036 | 0.277548385 |
| 3600.00 | 0.825155562 | 0.961018211 | 0.872840046 | 1.101430106 |
| 5400.00 | 1.797583861 | 2.109143055 | 1.935181031 | 2.445631563 |
| 7200.00 | 3.053307693 | 3.620432582 | 3.369871455 | 4.267710355 |
| 9000.00 | 4.496404229 | 5.405645659 | 5.126546432 | 6.510135371 |
| 10800.00 | 6.016637525 | 7.359366057 | 7.143537794 | 9.10210331 |
| 12600.00 | 7.497879277 | 9.36622725 | 9.350038951 | 11.96177425 |
| 14400.00 | 8.826979685 | 11.30772476 | 11.66859056 | 14.99885569 |
| 16200.00 | 9.902410794 | 13.06921383 | 14.01779975 | 18.1174535 |
| 18000.00 | 10.64202206 | 14.54667911 | 16.31519739 | 21.21909972 |
| 19800.00 | 10.98931571 | 15.65287679 | 18.48013323 | 24.20586161 |
| 21600.00 | 10.91776251 | 16.32248626 | 20.43660707 | 26.98343387 |
| 23400.00 | 10.4328283 | 16.51596732 | 22.1159368 | 29.46411621 |
| 25200.00 | 9.571556463 | 16.22189497 | 23.45916945 | 31.56958249 |
| 27000.00 | 8.549366219 | 15.45763408 | 24.41915077 | 33.2333538 |
| 28800.00 | 7.622628162 | 14.26831401 | 24.96218057 | 34.4028975 |
| 30600.00 | 6.796347075 | 12.9189877 | 25.06919575 | 35.04128591 |
| 32400.00 | 6.059633579 | 11.68019211 | 24.73643954 | 35.12836228 |
| 34200.00 | 5.402778684 | 10.56018404 | 23.97559337 | 34.66137721 |
| 36000.00 | 4.817125843 | 9.547573006 | 22.81336678 | 33.6507551 |
| 37800.00 | 4.294956862 | 8.632060767 | 21.3178267 | 32.14123057 |
| 39600.00 | 3.829390191 | 7.804336562 | 19.72522513 | 30.16764119 |
| 41400.00 | 3.414290225 | 7.055982437 | 18.25160285 | 28.06171416 |
| 43200.00 | 3.044186453 | 6.379387634 | 16.88807121 | 26.06985428 |
| 45000.00 | 2.714201356 | 5.767671185 | 15.6264056 | 24.21937941 |
| 46800.00 | 2.419986133 | 5.214611936 | 14.45899589 | 22.50025385 |
| 48600.00 | 2.157663384 | 4.714585275 | 13.37880043 | 20.90315423 |
| 50400.00 | 1.923776015 | 4.262505933 | 12.37930368 | 19.41941899 |
| 52200.00 | 1.715241675 | 3.853776265 | 11.45447683 | 18.04100136 |
| 54000.00 | 1.529312134 | 3.48423949 | 10.59874149 | 16.76042574 |
| 55800.00 | 1.363537067 | 3.150137421 | 9.806935997 | 15.57074719 |
| 57600.00 | 1.215731761 | 2.848072241 | 9.074284313 | 14.46551368 |
| 59400.00 | 1.083948321 | 2.574971947 | 8.396367205 | 13.43873121 |
| 61200.00 | 0.966450002 | 2.32805911 | 7.769095591 | 12.48483119 |
| 63000.00 | 0.861688319 | 2.104822628 | 7.188685872 | 11.59864034 |
| 64800.00 | 0.76828264 | 1.902992187 | 6.651637112 | 10.77532556 |
| 66600.00 | 0.685001991 | 1.72051517 | 6.154709924 | 10.0105029 |
| 68400.00 | 0.610748836 | 1.555535788 | 5.694906924 | 9.299943347 |
| 70200.00 | 0.544544609 | 1.406376201 | 5.269454657 | 8.639820308 |
| 72000.00 | 0.485516816 | 1.271519455 | 4.875786866 | 8.026553729 |
| 73800.00 | 0.432887545 | 1.149594059 | 4.511529012 | 7.456817672 |
| 75600.00 | 0.385963206 | 1.039360031 | 4.174483953 | 6.927522282 |
| 77400.00 | 0.344125392 | 0.939696291 | 3.862618687 | 6.435797021 |
| 79200.00 | 0.306822733 | 0.84958926 | 3.574052096 | 5.97897511 |
| 81000.00 | 0.273563624 | 0.76812255 | 3.307043595 | 5.55457906 |
| 82800.00 | 0.243909751 | 0.694467643 | 3.059982631 | 5.160307238 |
| 84600.00 | 0.217470311 | 0.627875471 | 2.831378974 | 4.794021383 |
| 86400.00 | 0.193896866 | 0.567668791 | 2.619853726 | 4.453735012 |

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DA RP2 202 EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 1703492.21 cft
 Volume (100-yr) = 1.38*area*43560 = 1152362.38 cft
 Volume (10-yr) = 0.70*area*43560 = 584531.64 cft
 Volume (2-yr) = 0.41*area*43560 = 342368.532 cft
 A= 19.17 Ac

TP = time to Qp in seconds

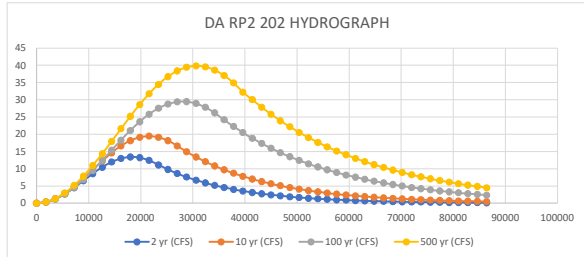
$T_p = \frac{V}{1.39 Q_p}$

$Q_p = \frac{Q_p}{2} \left[1 - \cos \left(\frac{\pi t_i}{T_p} \right) \right]$
 $t_i = 1.25 T_p$
 $Q_p = 4.34 Q_{ps} \left(\frac{t_i}{T_p} \right)^{-1.81}$
 $t_i = 1.25 T_p$

| DA RP2 202 Existing Conditions | | | | |
|--------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 13.42 | 19.46 | 29.52 | 39.84 |
| Tp= | 18355.190 | 21612.503 | 28082.220 | 30761.662 |
| 1.25*Tp= | 22943.988 | 27015.629 | 35102.775 | 38452.077 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|--------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.315899832 | 0.331118717 | 0.298261162 | 0.335627378 |
| 3600.00 | 1.233852639 | 1.301935625 | 1.180991221 | 1.331199602 |
| 5400.00 | 2.667419451 | 2.846367246 | 2.612517001 | 2.953168056 |
| 7200.00 | 4.481608535 | 4.859284165 | 4.534987212 | 5.146875939 |
| 9000.00 | 6.505586884 | 7.203667184 | 6.87071036 | 7.838400076 |
| 10800.00 | 8.5487667 | 9.719934219 | 9.525294435 | 10.93704197 |
| 12600.00 | 10.41875208 | 12.23680305 | 12.39146152 | 14.33838414 |
| 14400.00 | 11.93945596 | 14.58295048 | 15.35338312 | 17.92780876 |
| 16200.00 | 12.96768135 | 16.59867432 | 18.29136111 | 21.58436006 |
| 18000.00 | 13.40660547 | 18.1467432 | 21.08666494 | 25.18482022 |
| 19800.00 | 13.21489705 | 19.12184203 | 23.62632989 | 28.60786158 |
| 21600.00 | 12.41060832 | 19.45753393 | 25.80772218 | 31.7381351 |
| 23400.00 | 11.10337421 | 19.1309895 | 27.54268668 | 34.47015739 |
| 25200.00 | 9.774379906 | 18.1644366 | 28.76110943 | 36.71186525 |
| 27000.00 | 8.604456692 | 16.62366845 | 29.41375113 | 38.38771802 |
| 28800.00 | 7.5745649 | 14.9360677 | 29.47423701 | 39.4412431 |
| 30600.00 | 6.667943774 | 13.40339828 | 28.9401227 | 39.83693899 |
| 32400.00 | 5.869838699 | 12.02800423 | 27.832993 | 39.56147162 |
| 34200.00 | 5.16726108 | 10.79374668 | 26.19758959 | 38.62412362 |
| 36000.00 | 4.548776966 | 9.686142875 | 24.20280189 | 37.05648158 |
| 37800.00 | 4.004320968 | 8.692196189 | 22.26779939 | 34.91137163 |
| 39600.00 | 3.52503245 | 7.800243664 | 20.48749942 | 32.26107929 |
| 41400.00 | 3.103111332 | 6.999819136 | 18.84953358 | 30.0588377 |
| 43200.00 | 2.731691148 | 6.28153043 | 17.34252234 | 27.85710375 |
| 45000.00 | 2.404727298 | 5.636949152 | 15.95599592 | 25.81664125 |
| 46800.00 | 2.116898677 | 5.058511791 | 14.68032164 | 23.92563748 |
| 48600.00 | 1.863521079 | 4.539430967 | 13.50666369 | 22.17314496 |
| 50400.00 | 1.640470963 | 4.073615789 | 12.42678771 | 20.54901809 |
| 52200.00 | 1.444118347 | 3.655600386 | 11.43327194 | 19.04385441 |
| 54000.00 | 1.271267732 | 3.28047977 | 10.51918729 | 17.64894017 |
| 55800.00 | 1.119106097 | 2.943852277 | 9.678183264 | 16.35619987 |
| 57600.00 | 0.985157118 | 2.641767922 | 8.904417114 | 15.15814954 |
| 59400.00 | 0.867240873 | 2.370682052 | 8.192513201 | 14.04785336 |
| 61200.00 | 0.763438356 | 2.127413746 | 7.537525666 | 13.01888358 |
| 63000.00 | 0.672060257 | 1.909108496 | 6.934904074 | 12.06528324 |
| 64800.00 | 0.591619462 | 1.71320471 | 6.380461791 | 11.18153171 |
| 66600.00 | 0.520806853 | 1.537403654 | 5.870346905 | 10.36251275 |
| 68400.00 | 0.458470005 | 1.379642481 | 5.401015461 | 9.603484862 |
| 70200.00 | 0.403594432 | 1.238070021 | 4.969206844 | 8.900053849 |
| 72000.00 | 0.355287071 | 1.111025065 | 4.57192112 | 8.248147381 |
| 73800.00 | 0.312761755 | 0.997016869 | 4.2063982 | 7.643991415 |
| 75600.00 | 0.275326415 | 0.89470766 | 3.870098665 | 7.084088349 |
| 77400.00 | 0.242371817 | 0.802896944 | 3.560686117 | 6.565196768 |
| 79200.00 | 0.213361648 | 0.720507414 | 3.276010955 | 6.084312684 |
| 81000.00 | 0.187823788 | 0.646572313 | 3.014095437 | 5.638652146 |
| 82800.00 | 0.1658342627 | 0.580224086 | 2.77311994 | 5.225635116 |
| 84600.00 | 0.145552299 | 0.520684203 | 2.55141032 | 4.842870541 |
| 86400.00 | 0.128130732 | 0.467254025 | 2.347426278 | 4.488142504 |

ti (hrs)
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DA RP3 106 DRAINAGE CALCULATIONS

Time of Concentration:

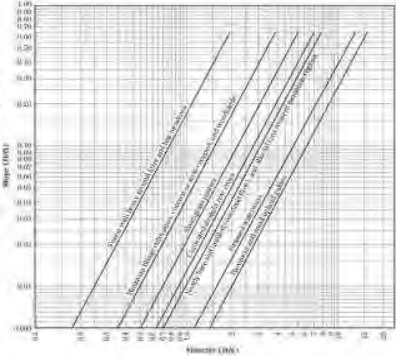
$T_c = T_{OL} + T_1 + \dots + T_n$

Equation 5.1
 $T_{OL} = 0.0114 L^{0.77} S^{-0.103} P_2^{-0.0818}$
 where:
 T_{OL} = travel time (min)
 L = Maximum length of pipe (ft)
 S = Pipe slope (ft/ft)
 P_2 = 2-year return period design rainfall (in)

Equation 5.2
 $T_1 = 0.88 L^{0.0167} S^{-0.0141} P_2^{-0.0000845}$
 where:
 T_1 = travel time (min)
 L = Maximum length of pipe (ft)
 S = Pipe slope (ft/ft)
 P_2 = 2-year return period design rainfall (in)

Table 2.1 Manning's Roughness Coefficients for Channels and Pipes

| Channel | n |
|----------------------------------------|-------|
| Concrete (finished, uncoated) (smooth) | 0.012 |
| Cast-in-place concrete (smooth) | 0.012 |
| Cast-in-place concrete (rough) | 0.015 |
| Corrugated metal (galvanized) | 0.014 |
| Steel (smooth) | 0.012 |
| Steel (rough) | 0.015 |
| Wood (finished) | 0.012 |
| Wood (rough) | 0.015 |



| | |
|------------------------|--------------------|
| T_{OL} | T_1 |
| $T_{OL} = 15.24$ (min) | $T_1 = 4.07$ (min) |

$T_c = 19.31$ (min)

Intensity:

SEE FIG. 2.1-2.1a

| | |
|-------------|---------------|
| i (500-YR)= | 11.27 (in/hr) |
| i (100-YR)= | 8.5 (in/hr) |
| i (10-YR)= | 5.8 (in/hr) |
| i (2-YR)= | 4 (in/hr) |

Peak Flow Rate:

Q=CIA

C= 0.35 Mixed use area; lots 1/4-1/2 acre; MOSTLY golf course; basin slope <1%

| i (500-YR) | i (100-YR) | i (10-YR) | i (2-YR) |
|------------|------------|-----------|----------|
| 11.27 | 8.5 | 5.8 | 4 |

A= 3.38 (Ac)

| | |
|--------------------|--------------------|
| Q (500-YR)= | 13.33 (cfs) |
| Q (100-YR)= | 10.06 (cfs) |
| Q (10-YR)= | 6.86 (cfs) |
| Q (2-YR)= | 4.73 (cfs) |

DA RP3 106 EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 300354.91 cft
 Volume (100-yr) = 1.38*area*43560 = 203181.26 cft
 Volume (10-yr) = 0.70*area*43560 = 103062.96 cft
 Volume (2-yr) = 0.41*area*43560 = 60365.448 cft
 A= 3.38 Ac

TP = time to Qp in seconds

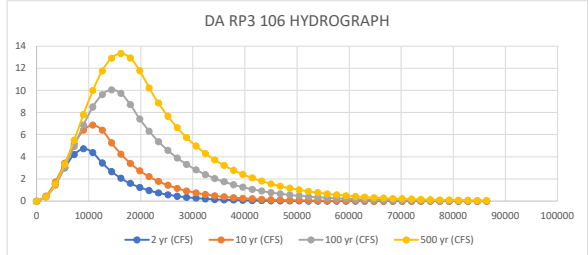
$T_p = \frac{V}{1.39 Q_p}$

$Q_t = \frac{Q_p}{2} \left[2 - \cos \left(\frac{\pi t_i}{T_p} \right) \right]$
 $t_i = 1.25 T_p$
 $Q_t = 4.34 Q_p e^{-1.8 t_i / T_p}$
 $t_i = 1.25 T_p$

| DA RP3 106 Existing Conditions | | | | |
|--------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 4.73 | 6.86 | 10.06 | 13.33 |
| Tp= | 9177.595 | 10806.252 | 14536.679 | 16213.193 |
| 1.25*Tp= | 11471.994 | 13507.814 | 18170.848 | 20266.491 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.435098792 | 0.45910719 | 0.37564227 | 0.401228669 |
| 3600.00 | 1.580368998 | 1.713550389 | 1.446437763 | 1.556598503 |
| 5400.00 | 3.01458857 | 3.427582437 | 3.052380094 | 3.326979246 |
| 7200.00 | 4.210261986 | 5.14244889 | 4.953497179 | 5.499180697 |
| 9000.00 | 4.727629262 | 6.399171977 | 6.865709684 | 7.811625187 |
| 10800.00 | 4.376406481 | 6.861394334 | 8.503280312 | 9.985846909 |
| 12600.00 | 3.446781855 | 6.405403828 | 9.62151084 | 11.76002491 |
| 14400.00 | 2.671051577 | 5.266970145 | 10.05330678 | 12.92051173 |
| 16200.00 | 2.069906604 | 4.241487146 | 9.734145907 | 13.32756091 |
| 18000.00 | 1.604054893 | 3.415666449 | 8.711719661 | 12.93215537 |
| 19800.00 | 1.243047437 | 2.750633655 | 7.428327631 | 11.78191007 |
| 21600.00 | 0.963288063 | 2.21508324 | 6.323852705 | 10.23473409 |
| 23400.00 | 0.746491135 | 1.78304888 | 5.383595746 | 8.859234236 |
| 25200.00 | 0.57848637 | 1.436496752 | 4.583140138 | 7.668595055 |
| 27000.00 | 0.448292638 | 1.156809768 | 3.901699629 | 6.637972149 |
| 28800.00 | 0.347400215 | 0.931578047 | 3.321578554 | 5.745860087 |
| 30600.00 | 0.269214569 | 0.750199109 | 2.827712315 | 4.973643667 |
| 32400.00 | 0.208625329 | 0.604134786 | 2.407276182 | 4.305209482 |
| 34200.00 | 0.161672261 | 0.486509294 | 2.049352257 | 3.726609689 |
| 36000.00 | 0.125286416 | 0.391785573 | 1.744645963 | 3.25770972 |
| 37800.00 | 0.097089544 | 0.315504631 | 1.485244679 | 2.79224261 |
| 39600.00 | 0.07523864 | 0.254075645 | 1.264412268 | 2.41697841 |
| 41400.00 | 0.058305485 | 0.204606928 | 1.076414145 | 2.092147943 |
| 43200.00 | 0.045183294 | 0.164769808 | 0.916368373 | 1.810973154 |
| 45000.00 | 0.035014374 | 0.132689004 | 0.780118878 | 1.567586928 |
| 46800.00 | 0.027134064 | 0.106854356 | 0.664127529 | 1.356910659 |
| 48600.00 | 0.021027291 | 0.086049734 | 0.565382261 | 1.174548284 |
| 50400.00 | 0.016294904 | 0.069295787 | 0.481318854 | 1.01669455 |
| 52200.00 | 0.012627584 | 0.055803845 | 0.409754347 | 0.880055611 |
| 54000.00 | 0.009785629 | 0.044938795 | 0.348830351 | 0.761780299 |
| 55800.00 | 0.007583282 | 0.036189179 | 0.29696479 | 0.65940063 |
| 57600.00 | 0.005876594 | 0.029143119 | 0.252810819 | 0.570780304 |
| 59400.00 | 0.004554012 | 0.023468932 | 0.215221846 | 0.49407013 |
| 61200.00 | 0.003529089 | 0.018899513 | 0.183221758 | 0.427669442 |
| 63000.00 | 0.002734835 | 0.015219764 | 0.155979578 | 0.370192691 |
| 64800.00 | 0.002119335 | 0.012256465 | 0.13278788 | 0.320440545 |
| 66600.00 | 0.001642359 | 0.009870122 | 0.113044421 | 0.277374851 |
| 68400.00 | 0.001272731 | 0.007948402 | 0.096236502 | 0.240096983 |
| 70200.00 | 0.000986291 | 0.006400842 | 0.081927655 | 0.207829084 |
| 72000.00 | 0.000764317 | 0.005154593 | 0.069746307 | 0.179897838 |
| 73800.00 | 0.0005923 | 0.00415099 | 0.059376134 | 0.155720419 |
| 75600.00 | 0.000458998 | 0.003342789 | 0.050547841 | 0.134792332 |
| 77400.00 | 0.000355696 | 0.002691946 | 0.043032176 | 0.11667688 |
| 79200.00 | 0.000275643 | 0.002167822 | 0.036633971 | 0.100996059 |
| 81000.00 | 0.000213607 | 0.001745745 | 0.031187079 | 0.087422666 |
| 82800.00 | 0.000165533 | 0.001405847 | 0.026550053 | 0.075673473 |
| 84600.00 | 0.000128278 | 0.001132128 | 0.02260248 | 0.065503316 |
| 86400.00 | 9.9408E-05 | 0.000911702 | 0.019241848 | 0.056699981 |

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DA RP2 204 DRAINAGE CALCULATIONS

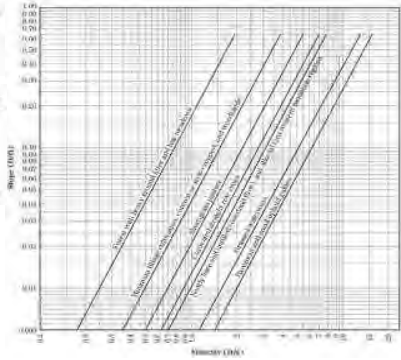
Time of Concentration:

$T_c = T_{OL} + T_1 + \dots + T_n$

Equation 2.1
 $T_{OL} = 0.0114 L^{0.77} S^{-0.103} n^{1.49}$
 where:
 T_{OL} = travel time (min)
 L = Maximum length of pipe (ft)
 S = Pipe slope (ft/ft)
 n = Manning's roughness coefficient

Table 2.1 Manning's Roughness Coefficients for Channels and Pipes

| Channel | n |
|------------------------------------------|-------|
| Smooth finished concrete (open and full) | 0.012 |
| Cast-in-place concrete (open and full) | 0.013 |
| Galvanized steel (open and full) | 0.014 |
| Corrugated metal (open and full) | 0.015 |
| Steel (open and full) | 0.016 |
| Aluminum (open and full) | 0.017 |
| Brick (open and full) | 0.018 |
| Stoneware (open and full) | 0.019 |
| Asbestos-cement (open and full) | 0.020 |
| Wood (open and full) | 0.021 |
| Earth (open and full) | 0.022 |
| Grass (open and full) | 0.023 |
| Gravel (open and full) | 0.024 |
| Rock (open and full) | 0.025 |
| Concrete (open and full) | 0.026 |
| Steel (open and full) | 0.027 |
| Aluminum (open and full) | 0.028 |
| Brick (open and full) | 0.029 |
| Stoneware (open and full) | 0.030 |
| Asbestos-cement (open and full) | 0.031 |
| Wood (open and full) | 0.032 |
| Earth (open and full) | 0.033 |
| Grass (open and full) | 0.034 |
| Gravel (open and full) | 0.035 |
| Rock (open and full) | 0.036 |
| Concrete (open and full) | 0.037 |
| Steel (open and full) | 0.038 |
| Aluminum (open and full) | 0.039 |
| Brick (open and full) | 0.040 |
| Stoneware (open and full) | 0.041 |
| Asbestos-cement (open and full) | 0.042 |
| Wood (open and full) | 0.043 |
| Earth (open and full) | 0.044 |
| Grass (open and full) | 0.045 |
| Gravel (open and full) | 0.046 |
| Rock (open and full) | 0.047 |
| Concrete (open and full) | 0.048 |
| Steel (open and full) | 0.049 |
| Aluminum (open and full) | 0.050 |
| Brick (open and full) | 0.051 |
| Stoneware (open and full) | 0.052 |
| Asbestos-cement (open and full) | 0.053 |
| Wood (open and full) | 0.054 |
| Earth (open and full) | 0.055 |
| Grass (open and full) | 0.056 |
| Gravel (open and full) | 0.057 |
| Rock (open and full) | 0.058 |
| Concrete (open and full) | 0.059 |
| Steel (open and full) | 0.060 |
| Aluminum (open and full) | 0.061 |
| Brick (open and full) | 0.062 |
| Stoneware (open and full) | 0.063 |
| Asbestos-cement (open and full) | 0.064 |
| Wood (open and full) | 0.065 |
| Earth (open and full) | 0.066 |
| Grass (open and full) | 0.067 |
| Gravel (open and full) | 0.068 |
| Rock (open and full) | 0.069 |
| Concrete (open and full) | 0.070 |
| Steel (open and full) | 0.071 |
| Aluminum (open and full) | 0.072 |
| Brick (open and full) | 0.073 |
| Stoneware (open and full) | 0.074 |
| Asbestos-cement (open and full) | 0.075 |
| Wood (open and full) | 0.076 |
| Earth (open and full) | 0.077 |
| Grass (open and full) | 0.078 |
| Gravel (open and full) | 0.079 |
| Rock (open and full) | 0.080 |
| Concrete (open and full) | 0.081 |
| Steel (open and full) | 0.082 |
| Aluminum (open and full) | 0.083 |
| Brick (open and full) | 0.084 |
| Stoneware (open and full) | 0.085 |
| Asbestos-cement (open and full) | 0.086 |
| Wood (open and full) | 0.087 |
| Earth (open and full) | 0.088 |
| Grass (open and full) | 0.089 |
| Gravel (open and full) | 0.090 |
| Rock (open and full) | 0.091 |
| Concrete (open and full) | 0.092 |
| Steel (open and full) | 0.093 |
| Aluminum (open and full) | 0.094 |
| Brick (open and full) | 0.095 |
| Stoneware (open and full) | 0.096 |
| Asbestos-cement (open and full) | 0.097 |
| Wood (open and full) | 0.098 |
| Earth (open and full) | 0.099 |
| Grass (open and full) | 0.100 |
| Gravel (open and full) | 0.101 |
| Rock (open and full) | 0.102 |
| Concrete (open and full) | 0.103 |
| Steel (open and full) | 0.104 |
| Aluminum (open and full) | 0.105 |
| Brick (open and full) | 0.106 |
| Stoneware (open and full) | 0.107 |
| Asbestos-cement (open and full) | 0.108 |
| Wood (open and full) | 0.109 |
| Earth (open and full) | 0.110 |
| Grass (open and full) | 0.111 |
| Gravel (open and full) | 0.112 |
| Rock (open and full) | 0.113 |
| Concrete (open and full) | 0.114 |
| Steel (open and full) | 0.115 |
| Aluminum (open and full) | 0.116 |
| Brick (open and full) | 0.117 |
| Stoneware (open and full) | 0.118 |
| Asbestos-cement (open and full) | 0.119 |
| Wood (open and full) | 0.120 |
| Earth (open and full) | 0.121 |
| Grass (open and full) | 0.122 |
| Gravel (open and full) | 0.123 |
| Rock (open and full) | 0.124 |
| Concrete (open and full) | 0.125 |
| Steel (open and full) | 0.126 |
| Aluminum (open and full) | 0.127 |
| Brick (open and full) | 0.128 |
| Stoneware (open and full) | 0.129 |
| Asbestos-cement (open and full) | 0.130 |
| Wood (open and full) | 0.131 |
| Earth (open and full) | 0.132 |
| Grass (open and full) | 0.133 |
| Gravel (open and full) | 0.134 |
| Rock (open and full) | 0.135 |
| Concrete (open and full) | 0.136 |
| Steel (open and full) | 0.137 |
| Aluminum (open and full) | 0.138 |
| Brick (open and full) | 0.139 |
| Stoneware (open and full) | 0.140 |
| Asbestos-cement (open and full) | 0.141 |
| Wood (open and full) | 0.142 |
| Earth (open and full) | 0.143 |
| Grass (open and full) | 0.144 |
| Gravel (open and full) | 0.145 |
| Rock (open and full) | 0.146 |
| Concrete (open and full) | 0.147 |
| Steel (open and full) | 0.148 |
| Aluminum (open and full) | 0.149 |
| Brick (open and full) | 0.150 |
| Stoneware (open and full) | 0.151 |
| Asbestos-cement (open and full) | 0.152 |
| Wood (open and full) | 0.153 |
| Earth (open and full) | 0.154 |
| Grass (open and full) | 0.155 |
| Gravel (open and full) | 0.156 |
| Rock (open and full) | 0.157 |
| Concrete (open and full) | 0.158 |
| Steel (open and full) | 0.159 |
| Aluminum (open and full) | 0.160 |
| Brick (open and full) | 0.161 |
| Stoneware (open and full) | 0.162 |
| Asbestos-cement (open and full) | 0.163 |
| Wood (open and full) | 0.164 |
| Earth (open and full) | 0.165 |
| Grass (open and full) | 0.166 |
| Gravel (open and full) | 0.167 |
| Rock (open and full) | 0.168 |
| Concrete (open and full) | 0.169 |
| Steel (open and full) | 0.170 |
| Aluminum (open and full) | 0.171 |
| Brick (open and full) | 0.172 |
| Stoneware (open and full) | 0.173 |
| Asbestos-cement (open and full) | 0.174 |
| Wood (open and full) | 0.175 |
| Earth (open and full) | 0.176 |
| Grass (open and full) | 0.177 |
| Gravel (open and full) | 0.178 |
| Rock (open and full) | 0.179 |
| Concrete (open and full) | 0.180 |
| Steel (open and full) | 0.181 |
| Aluminum (open and full) | 0.182 |
| Brick (open and full) | 0.183 |
| Stoneware (open and full) | 0.184 |
| Asbestos-cement (open and full) | 0.185 |
| Wood (open and full) | 0.186 |
| Earth (open and full) | 0.187 |
| Grass (open and full) | 0.188 |
| Gravel (open and full) | 0.189 |
| Rock (open and full) | 0.190 |
| Concrete (open and full) | 0.191 |
| Steel (open and full) | 0.192 |
| Aluminum (open and full) | 0.193 |
| Brick (open and full) | 0.194 |
| Stoneware (open and full) | 0.195 |
| Asbestos-cement (open and full) | 0.196 |
| Wood (open and full) | 0.197 |
| Earth (open and full) | 0.198 |
| Grass (open and full) | 0.199 |
| Gravel (open and full) | 0.200 |
| Rock (open and full) | 0.201 |
| Concrete (open and full) | 0.202 |
| Steel (open and full) | 0.203 |
| Aluminum (open and full) | 0.204 |
| Brick (open and full) | 0.205 |
| Stoneware (open and full) | 0.206 |
| Asbestos-cement (open and full) | 0.207 |
| Wood (open and full) | 0.208 |
| Earth (open and full) | 0.209 |
| Grass (open and full) | 0.210 |
| Gravel (open and full) | 0.211 |
| Rock (open and full) | 0.212 |
| Concrete (open and full) | 0.213 |
| Steel (open and full) | 0.214 |
| Aluminum (open and full) | 0.215 |
| Brick (open and full) | 0.216 |
| Stoneware (open and full) | 0.217 |
| Asbestos-cement (open and full) | 0.218 |
| Wood (open and full) | 0.219 |
| Earth (open and full) | 0.220 |
| Grass (open and full) | 0.221 |
| Gravel (open and full) | 0.222 |
| Rock (open and full) | 0.223 |
| Concrete (open and full) | 0.224 |
| Steel (open and full) | 0.225 |
| Aluminum (open and full) | 0.226 |
| Brick (open and full) | 0.227 |
| Stoneware (open and full) | 0.228 |
| Asbestos-cement (open and full) | 0.229 |
| Wood (open and full) | 0.230 |
| Earth (open and full) | 0.231 |
| Grass (open and full) | 0.232 |
| Gravel (open and full) | 0.233 |
| Rock (open and full) | 0.234 |
| Concrete (open and full) | 0.235 |
| Steel (open and full) | 0.236 |
| Aluminum (open and full) | 0.237 |
| Brick (open and full) | 0.238 |
| Stoneware (open and full) | 0.239 |
| Asbestos-cement (open and full) | 0.240 |
| Wood (open and full) | 0.241 |
| Earth (open and full) | 0.242 |
| Grass (open and full) | 0.243 |
| Gravel (open and full) | 0.244 |
| Rock (open and full) | 0.245 |
| Concrete (open and full) | 0.246 |
| Steel (open and full) | 0.247 |
| Aluminum (open and full) | 0.248 |
| Brick (open and full) | 0.249 |
| Stoneware (open and full) | 0.250 |
| Asbestos-cement (open and full) | 0.251 |
| Wood (open and full) | 0.252 |
| Earth (open and full) | 0.253 |
| Grass (open and full) | 0.254 |
| Gravel (open and full) | 0.255 |
| Rock (open and full) | 0.256 |
| Concrete (open and full) | 0.257 |
| Steel (open and full) | 0.258 |
| Aluminum (open and full) | 0.259 |
| Brick (open and full) | 0.260 |
| Stoneware (open and full) | 0.261 |
| Asbestos-cement (open and full) | 0.262 |
| Wood (open and full) | 0.263 |
| Earth (open and full) | 0.264 |
| Grass (open and full) | 0.265 |
| Gravel (open and full) | 0.266 |
| Rock (open and full) | 0.267 |
| Concrete (open and full) | 0.268 |
| Steel (open and full) | 0.269 |
| Aluminum (open and full) | 0.270 |
| Brick (open and full) | 0.271 |
| Stoneware (open and full) | 0.272 |
| Asbestos-cement (open and full) | 0.273 |
| Wood (open and full) | 0.274 |
| Earth (open and full) | 0.275 |
| Grass (open and full) | 0.276 |
| Gravel (open and full) | 0.277 |
| Rock (open and full) | 0.278 |
| Concrete (open and full) | 0.279 |
| Steel (open and full) | 0.280 |
| Aluminum (open and full) | 0.281 |
| Brick (open and full) | 0.282 |
| Stoneware (open and full) | 0.283 |
| Asbestos-cement (open and full) | 0.284 |
| Wood (open and full) | 0.285 |
| Earth (open and full) | 0.286 |
| Grass (open and full) | 0.287 |
| Gravel (open and full) | 0.288 |
| Rock (open and full) | 0.289 |
| Concrete (open and full) | 0.290 |
| Steel (open and full) | 0.291 |
| Aluminum (open and full) | 0.292 |
| Brick (open and full) | 0.293 |
| Stoneware (open and full) | 0.294 |
| Asbestos-cement (open and full) | 0.295 |
| Wood (open and full) | 0.296 |
| Earth (open and full) | 0.297 |
| Grass (open and full) | 0.298 |
| Gravel (open and full) | 0.299 |
| Rock (open and full) | 0.300 |



| | |
|-------------------------------------------------------------------------|---------------------|
| $T_{OL} = T_{OL}$, multiply by 60 to convert hrs. to min. (L=max 300') | $T =$ |
| n= 0.15 | D= 404 (ft) |
| L= 100 (ft) | S= 0.0040 (ft/ft) |
| $P_2 = 4.89$ (in) | V= 0.5 (ft/s) |
| S= 0.0040 (ft/ft) | |
| $T_{OL} = 15.09$ (min) | $T_1 = 13.47$ (min) |

$T_c = 28.56$ (min)

Intensity:

SEE FIG. 2.1-2.1a

| | |
|-------------|--------------|
| i (500-YR)= | 9.05 (in/hr) |
| i (100-YR)= | 7 (in/hr) |
| i (10-YR)= | 4.8 (in/hr) |
| i (2-YR)= | 3.3 (in/hr) |

Peak Flow Rate:

Q=CIA

C= 0.4 Single family residential districts; lots 1/4-1/2 acre; basin slope <1%

| | | | |
|--------------------|--------------------|-----------|----------|
| i (500-YR) | i (100-YR) | i (10-YR) | i (2-YR) |
| 9.05 | 7 | 4.8 | 3.3 |
| A= 3.16 (Ac) | | | |
| Q (500-YR)= | 11.44 (cfs) | | |
| Q (100-YR)= | 8.85 (cfs) | | |
| Q (10-YR)= | 6.07 (cfs) | | |
| Q (2-YR)= | 4.17 (cfs) | | |

DA RP2 204 EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 280805.18 cft
 Volume (100-yr) = 1.38*area*43560 = 189956.45 cft
 Volume (10-yr) = 0.70*area*43560 = 96354.72 cft
 Volume (2-yr) = 0.41*area*43560 = 56436.336 cft
 A= 3.16 Ac

TP = time to Qp in seconds

$$T_p = \frac{V}{1.39 Q_p}$$

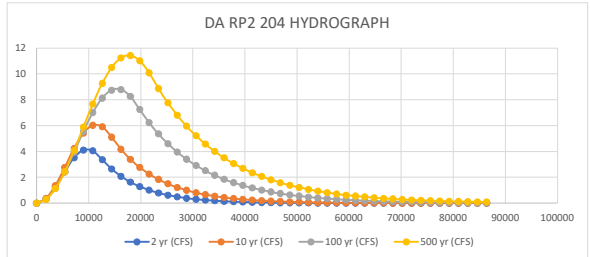
$$Q_p = \frac{Q_p}{2} \left[2 - \cos \left(\frac{\pi t_i}{T_p} \right) \right] \quad t_i = 1.25 T_p$$

$$Q_p = 4.34 Q_{ps} \left(\frac{t_i}{T_p} \right)^{-1.81} \quad t_i = 1.25 T_p$$

| DA RP2 204 Existing Conditions | | | | |
|--------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 4.17 | 6.07 | 8.85 | 11.44 |
| Tp= | 9733.813 | 11425.360 | 15445.221 | 17666.450 |
| 1.25*Tp= | 12167.266 | 14281.700 | 19306.526 | 22083.063 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.342161053 | 0.364040368 | 0.29321412 | 0.290412922 |
| 3600.00 | 1.256375141 | 1.368789774 | 1.133989154 | 1.132149729 |
| 5400.00 | 2.442672516 | 2.773102818 | 2.410875235 | 2.43970154 |
| 7200.00 | 3.511808107 | 4.239936623 | 3.954613308 | 4.080239078 |
| 9000.00 | 4.11297969 | 5.417242984 | 5.560571455 | 5.887106295 |
| 10800.00 | 4.048932277 | 6.022461879 | 7.015870109 | 7.676750335 |
| 12600.00 | 3.364516678 | 5.910337435 | 8.127600539 | 9.267367982 |
| 14400.00 | 2.645566467 | 5.115683991 | 8.748396082 | 10.49737436 |
| 16200.00 | 2.080245872 | 4.168280318 | 8.795966493 | 11.24181775 |
| 18000.00 | 1.635726391 | 3.396331916 | 8.264006025 | 11.42507293 |
| 19800.00 | 1.286194513 | 2.767345188 | 7.253839236 | 11.0285237 |
| 21600.00 | 1.011352714 | 2.254844221 | 6.234059368 | 10.09245401 |
| 23400.00 | 0.795240768 | 1.837256328 | 5.357645094 | 8.869837543 |
| 25200.00 | 0.625308925 | 1.497003999 | 4.604441386 | 7.769470608 |
| 27000.00 | 0.491689144 | 1.219765004 | 3.957126705 | 6.805612081 |
| 28800.00 | 0.386622043 | 0.993869533 | 3.400814659 | 5.961327113 |
| 30600.00 | 0.304006313 | 0.809808976 | 2.922711655 | 5.221781749 |
| 32400.00 | 0.239044411 | 0.659835678 | 2.511822688 | 4.573982288 |
| 34200.00 | 0.18796396 | 0.537636819 | 2.158698484 | 4.006546995 |
| 36000.00 | 0.147798688 | 0.438068688 | 1.855218191 | 3.509506118 |
| 37800.00 | 0.116216173 | 0.356940165 | 1.594402628 | 3.074126725 |
| 39600.00 | 0.0913824 | 0.290836312 | 1.370253781 | 2.692759266 |
| 41400.00 | 0.07185258 | 0.236974621 | 1.177616865 | 2.358703175 |
| 43200.00 | 0.056500793 | 0.193087894 | 1.01206178 | 2.066089137 |
| 45000.00 | 0.044427363 | 0.157328809 | 0.869781231 | 1.809775968 |
| 46800.00 | 0.034933856 | 0.128192159 | 0.747503171 | 1.585260285 |
| 48600.00 | 0.027468979 | 0.104451498 | 0.642415553 | 1.388597382 |
| 50400.00 | 0.021599242 | 0.085107509 | 0.552101662 | 1.216331922 |
| 52200.00 | 0.016983786 | 0.069345948 | 0.474484535 | 1.065437227 |
| 54000.00 | 0.013354588 | 0.056503363 | 0.4077792 | 0.933262101 |
| 55800.00 | 0.010500899 | 0.046039172 | 0.350451624 | 0.817484247 |
| 57600.00 | 0.008257004 | 0.037512906 | 0.301183437 | 0.716069466 |
| 59400.00 | 0.006492597 | 0.030565667 | 0.25884161 | 0.627235915 |
| 61200.00 | 0.00510522 | 0.024905034 | 0.222452402 | 0.549422803 |
| 63000.00 | 0.004014306 | 0.020292724 | 0.191178965 | 0.481262966 |
| 64800.00 | 0.003156505 | 0.016534594 | 0.1643021 | 0.421558845 |
| 66600.00 | 0.002482004 | 0.013472455 | 0.141203715 | 0.369261448 |
| 68400.00 | 0.001951634 | 0.010977412 | 0.121352612 | 0.323451918 |
| 70200.00 | 0.001534597 | 0.00894444 | 0.104292274 | 0.283325389 |
| 72000.00 | 0.001206675 | 0.007287967 | 0.089630361 | 0.248176843 |
| 73800.00 | 0.000948826 | 0.005938265 | 0.07702969 | 0.217388727 |
| 75600.00 | 0.000746075 | 0.004838523 | 0.066200483 | 0.190420097 |
| 77400.00 | 0.000586649 | 0.003942448 | 0.056893699 | 0.166797119 |
| 79200.00 | 0.00046129 | 0.003212323 | 0.048895307 | 0.14610474 |
| 81000.00 | 0.000362719 | 0.002617414 | 0.042021368 | 0.1279794 |
| 82800.00 | 0.000285211 | 0.00213268 | 0.0361138 | 0.112102638 |
| 84600.00 | 0.000224265 | 0.001737716 | 0.031036747 | 0.098195502 |
| 86400.00 | 0.000176343 | 0.001415898 | 0.026673451 | 0.086013646 |

ti (hrs)
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DA RP2 301 EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 581160.10 cft
 Volume (100-yr) = 1.38*area*43560 = 393137.71 cft
 Volume (10-yr) = 0.70*area*43560 = 199417.68 cft
 Volume (2-yr) = 0.41*area*43560 = 116801.784 cft
 A= 6.54 Ac

TP = time to Qp in seconds

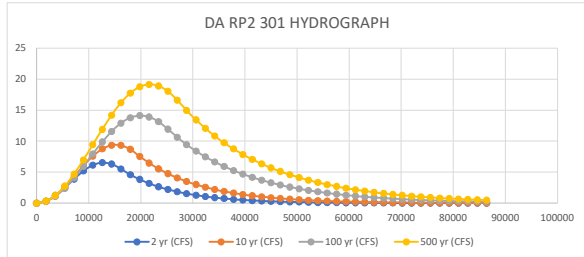
TP = $\frac{V}{1.39 Qp}$

$Qp = \frac{Qp}{2} \left[2 - \cos \left(\frac{\pi t_i}{TP} \right) \right]$
 $t_i = 1.25 TP$
 $Qp = 4.34 Qp \left(\frac{t_i}{TP} \right)^{-1.81}$
 $t_i = 1.25 TP$

| DA RP2 301 Existing Conditions | | | | |
|--------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 6.54 | 9.42 | 14.13 | 19.16 |
| TP= | 12848.633 | 15233.813 | 20021.583 | 21819.052 |
| 1.25*TP= | 16060.791 | 19042.266 | 25026.978 | 27273.815 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.311621239 | 0.32071194 | 0.279853345 | 0.319982182 |
| 3600.00 | 1.187091807 | 1.239160984 | 1.097237058 | 1.258555678 |
| 5400.00 | 2.459552241 | 2.630237729 | 2.387379488 | 2.753028944 |
| 7200.00 | 3.886479179 | 4.304452317 | 4.048046329 | 4.703579392 |
| 9000.00 | 5.195908867 | 6.033746387 | 5.947641939 | 6.979920985 |
| 10800.00 | 6.138271823 | 7.582558751 | 7.935637327 | 9.430006633 |
| 12600.00 | 6.533959293 | 8.739913103 | 9.854498468 | 11.8901841 |
| 14400.00 | 6.307555609 | 9.348156809 | 11.55216972 | 14.19612707 |
| 16200.00 | 5.510892849 | 9.324436056 | 12.89412311 | 16.19381124 |
| 18000.00 | 4.593333951 | 8.671982039 | 13.7740187 | 17.7498023 |
| 19800.00 | 3.828547817 | 7.54429836 | 14.12213123 | 18.76016862 |
| 21600.00 | 3.191097913 | 6.470068026 | 13.91087534 | 19.15742328 |
| 23400.00 | 2.659782868 | 5.548795934 | 13.1569915 | 18.91503187 |
| 25200.00 | 2.216931318 | 4.758703648 | 11.93750895 | 18.04918478 |
| 27000.00 | 1.847814169 | 4.081112494 | 10.62077064 | 16.61771585 |
| 28800.00 | 1.540154707 | 3.50000345 | 9.449272 | 14.95254894 |
| 30600.00 | 1.283720279 | 3.001638443 | 8.406992705 | 13.43194817 |
| 32400.00 | 1.069981961 | 2.57423556 | 7.479679528 | 12.06598503 |
| 34200.00 | 0.891830889 | 2.207690514 | 6.654651409 | 10.83893363 |
| 36000.00 | 0.743341817 | 1.893337767 | 5.920626039 | 9.73667328 |
| 37800.00 | 0.619576046 | 1.623745664 | 5.267565577 | 8.746496095 |
| 39600.00 | 0.51641717 | 1.392540744 | 4.686539384 | 7.857020412 |
| 41400.00 | 0.430434157 | 1.19425706 | 4.169601892 | 7.058000037 |
| 43200.00 | 0.358767242 | 1.024206962 | 3.709683951 | 6.340236108 |
| 45000.00 | 0.299032806 | 0.878370274 | 3.300496156 | 5.695465244 |
| 46800.00 | 0.249244102 | 0.753299253 | 2.93644284 | 5.116264409 |
| 48600.00 | 0.207745175 | 0.646037076 | 2.612545552 | 4.595965454 |
| 50400.00 | 0.173155783 | 0.554047946 | 2.324374978 | 4.128578347 |
| 52200.00 | 0.144325494 | 0.475157136 | 2.067990368 | 3.708722212 |
| 54000.00 | 0.120295424 | 0.407499577 | 1.839885648 | 3.331563383 |
| 55800.00 | 0.10026634 | 0.349475768 | 1.636941472 | 2.992759754 |
| 57600.00 | 0.083572081 | 0.299713962 | 1.456382568 | 2.68841079 |
| 59400.00 | 0.069657402 | 0.257037732 | 1.29573978 | 2.415012621 |
| 61200.00 | 0.058059505 | 0.220438165 | 1.15281631 | 2.169417702 |
| 63000.00 | 0.048392647 | 0.189050005 | 1.02565767 | 1.948798579 |
| 64800.00 | 0.040335313 | 0.162131201 | 0.91252496 | 1.750615338 |
| 66600.00 | 0.033619518 | 0.139045362 | 0.811871082 | 1.572586358 |
| 68400.00 | 0.028021898 | 0.119246712 | 0.722319588 | 1.412662052 |
| 70200.00 | 0.023356276 | 0.102267189 | 0.642645858 | 1.269001261 |
| 72000.00 | 0.019467476 | 0.087705378 | 0.571760347 | 1.139950067 |
| 73800.00 | 0.016226158 | 0.075217022 | 0.508693693 | 1.024022746 |
| 75600.00 | 0.013524517 | 0.064506888 | 0.452583454 | 0.919884663 |
| 77400.00 | 0.011272697 | 0.055321755 | 0.402662321 | 0.826336912 |
| 79200.00 | 0.009395802 | 0.047444498 | 0.358247619 | 0.742302508 |
| 81000.00 | 0.007831409 | 0.040688882 | 0.318731974 | 0.66681399 |
| 82800.00 | 0.006527486 | 0.034895198 | 0.283575008 | 0.599002283 |
| 84600.00 | 0.005440666 | 0.029926475 | 0.252295947 | 0.538086694 |
| 86400.00 | 0.004534799 | 0.025665249 | 0.224467047 | 0.48336592 |

ti (hrs)
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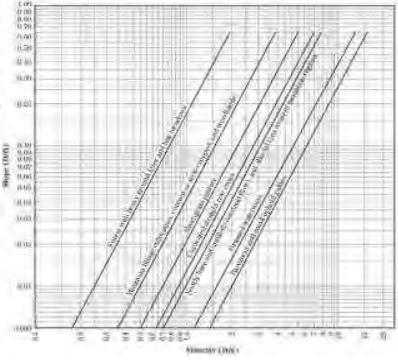
DA RP3 302 DRAINAGE CALCULATIONS

Time of Concentration:

$T_c = T_{OL} + T_1 + \dots + T_n$

Equation 5.1
 $T_{OL} = 0.06L^{0.849}$
 where:
 T_{OL} = travel time (min)
 L = Maximum length of travel (ft)
 n = Number of pipe segments
 T_1 = Travel time of first pipe segment (min)
 T_n = Travel time of last pipe segment (min)
 The following is a list of pipe segments:
 1) Pipe segment 1
 2) Pipe segment 2
 3) Pipe segment 3
 4) Pipe segment 4
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 100) Pipe segment 100

Equation 5.2
 $T_1 = \frac{L_1}{V_1}$
 where:
 T_1 = travel time (min)
 L_1 = length of pipe segment 1 (ft)
 V_1 = velocity of pipe segment 1 (ft/s)
 n = number of pipe segments
 T_n = travel time of last pipe segment (min)
 L_n = length of pipe segment n (ft)
 V_n = velocity of pipe segment n (ft/s)
 The following is a list of pipe segments:
 1) Pipe segment 1
 2) Pipe segment 2
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| | |
|-------------------------------------------------------------------------|---------------------|
| $T_{OL} = T_{OL}$; multiply by 60 to convert hrs. to min. (L=max 300') | T= |
| n= 0.15 | D= 488 (ft) |
| L= 100 (ft) | S= 0.0039 (ft/ft) |
| $P_2 = 4.89$ (in) | V= 0.5 (ft/s) |
| S= 0.0039 (ft/ft) | |
| $T_{OL} = 15.24$ (min) | $T_1 = 16.27$ (min) |

Tc= 31.51 (min)

Intensity:

SEE FIG. 2.1-2.1a

| | |
|-------------|--------------|
| i (500-YR)= | 8.57 (in/hr) |
| i (100-YR)= | 6.7 (in/hr) |
| i (10-YR)= | 4.5 (in/hr) |
| i (2-YR)= | 3.1 (in/hr) |

Peak Flow Rate:

Q=CIA
 C= 0.35 Mixed use area; lots 1/4-1/2 acre; MOSTLY golf course; basin slope <1%

| | | | |
|--------------------|--------------------|-----------|----------|
| i (500-YR) | i (100-YR) | i (10-YR) | i (2-YR) |
| 8.57 | 6.7 | 4.5 | 3.1 |
| A= 13.52 (Ac) | | | |
| Q (500-YR)= | 40.55 (cfs) | | |
| Q (100-YR)= | 31.70 (cfs) | | |
| Q (10-YR)= | 21.29 (cfs) | | |
| Q (2-YR)= | 14.67 (cfs) | | |

DA RP3 302 EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 1201419.65 cft
 Volume (100-yr) = 1.38*area*43560 = 812725.06 cft
 Volume (10-yr) = 0.70*area*43560 = 412251.84 cft
 Volume (2-yr) = 0.41*area*43560 = 241461.792 cft
 A= 13.52 Ac

TP = time to Qp in seconds

$T_p = \frac{V}{1.39 Q_p}$

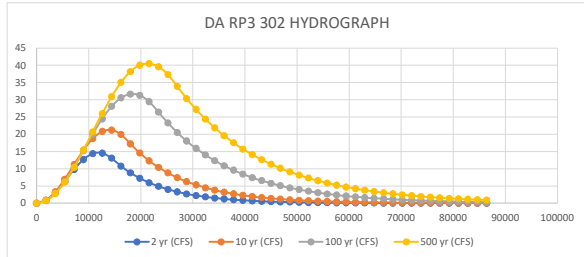
$Q_t = \frac{Q_p}{2} \left[1 - \cos \left(\frac{\pi t}{T_p} \right) \right]$
 $t_1 = 1.25 T_p$

$Q_t = 4.34 Q_p e^{-1.8 t_1 / T_p}$
 $t_1 = 1.25 T_p$

| DA RP3 302 Existing Conditions | | | | |
|--------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 14.67 | 21.29 | 31.70 | 40.55 |
| TP= | 11842.058 | 13928.058 | 18442.055 | 21312.847 |
| 1.25*TP= | 14802.573 | 17410.072 | 23052.569 | 26641.059 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.820480806 | 0.865539554 | 0.739401401 | 0.709563013 |
| 3600.00 | 3.098357999 | 3.32143149 | 2.88862913 | 2.788592423 |
| 5400.00 | 6.324004737 | 6.968376173 | 6.247188366 | 6.091584831 |
| 7200.00 | 9.77575079 | 11.21342256 | 10.50176949 | 10.3873763 |
| 9000.00 | 12.68134099 | 15.36637519 | 15.2547575 | 15.37532064 |
| 10800.00 | 14.39071098 | 18.75201197 | 20.06484858 | 20.70633051 |
| 12600.00 | 14.52142539 | 20.81986751 | 24.48123643 | 26.0073087 |
| 14400.00 | 13.04423963 | 21.23373241 | 28.09264811 | 30.90725981 |
| 16200.00 | 10.75334996 | 19.92631701 | 30.56218617 | 35.06325482 |
| 18000.00 | 8.825246588 | 17.22286235 | 31.65947503 | 38.18443135 |
| 19800.00 | 7.242857119 | 14.55932249 | 31.282152 | 40.05235008 |
| 21600.00 | 5.944194162 | 12.30770281 | 29.46541638 | 40.53628245 |
| 23400.00 | 4.878384822 | 10.40429927 | 26.43896882 | 39.60235985 |
| 25200.00 | 4.003677845 | 8.795259773 | 23.28839354 | 37.315944 |
| 27000.00 | 3.285808084 | 7.435060491 | 20.51325365 | 33.90714464 |
| 28800.00 | 2.696654222 | 6.285217939 | 18.06881074 | 30.381468 |
| 30600.00 | 2.213137167 | 5.313200153 | 15.91565762 | 27.22239243 |
| 32400.00 | 1.816315966 | 4.491506284 | 14.01908299 | 24.39179864 |
| 34200.00 | 1.49064583 | 3.796888526 | 12.34851192 | 21.85553097 |
| 36000.00 | 1.223369189 | 3.209694381 | 10.87701292 | 19.58298529 |
| 37800.00 | 1.004015939 | 2.713310635 | 9.580863727 | 17.5467397 |
| 39600.00 | 0.823993293 | 2.293693333 | 8.439168958 | 15.72222363 |
| 41400.00 | 0.676249171 | 1.938970436 | 7.433523191 | 14.08742137 |
| 43200.00 | 0.554995951 | 1.639105933 | 6.547714272 | 12.62260642 |
| 45000.00 | 0.455483746 | 1.385615898 | 5.767461953 | 11.31010343 |
| 46800.00 | 0.373814336 | 1.171328452 | 5.080187681 | 10.13407496 |
| 48600.00 | 0.306788461 | 0.990180861 | 4.474811813 | 9.080330335 |
| 50400.00 | 0.251780499 | 0.837048 | 3.941575 | 8.136154442 |
| 52200.00 | 0.206635606 | 0.70759735 | 3.471880859 | 7.290154286 |
| 54000.00 | 0.169585309 | 0.598166426 | 3.058157386 | 6.532121518 |
| 55800.00 | 0.139178226 | 0.505659148 | 2.693734888 | 5.852909261 |
| 57600.00 | 0.114223211 | 0.42745825 | 2.37273846 | 5.244321729 |
| 59400.00 | 0.093742695 | 0.361351231 | 2.089993275 | 4.699015339 |
| 61200.00 | 0.076934388 | 0.305467755 | 1.840941159 | 4.210410097 |
| 63000.00 | 0.063139854 | 0.258226738 | 1.621567107 | 3.772610197 |
| 64800.00 | 0.051818715 | 0.21829161 | 1.428334562 | 3.380332882 |
| 66600.00 | 0.042527486 | 0.184532506 | 1.258128394 | 3.028844698 |
| 68400.00 | 0.034902198 | 0.155994294 | 1.108204687 | 2.713904378 |
| 70200.00 | 0.028644144 | 0.131869558 | 0.9761465 | 2.431711661 |
| 72000.00 | 0.023508175 | 0.111475745 | 0.859824905 | 2.17886144 |
| 73800.00 | 0.019293099 | 0.094235865 | 0.757364665 | 1.952302673 |
| 75600.00 | 0.015833796 | 0.079662156 | 0.667114005 | 1.749301565 |
| 77400.00 | 0.012994756 | 0.067342291 | 0.587617981 | 1.567408582 |
| 79200.00 | 0.010664763 | 0.056927711 | 0.517595028 | 1.404428895 |
| 81000.00 | 0.008752543 | 0.048123761 | 0.455916295 | 1.258395892 |
| 82800.00 | 0.00718319 | 0.040681354 | 0.401587451 | 1.127547451 |
| 84600.00 | 0.005895225 | 0.034389925 | 0.353732654 | 1.010304677 |
| 86400.00 | 0.004838196 | 0.029071475 | 0.311580429 | 0.905252847 |

ti (hrs)
 0
 0.5
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DA RP2 306 EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 140402.59 cft
 Volume (100-yr) = 1.38*area*43560 = 94978.22 cft
 Volume (10-yr) = 0.70*area*43560 = 48177.36 cft
 Volume (2-yr) = 0.41*area*43560 = 28218.168 cft
 A= 1.58 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

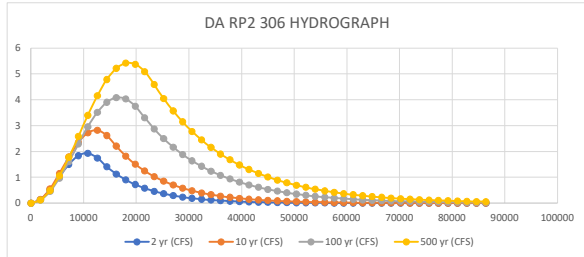
$Q_p = \frac{Q_p}{2} \left[2 - \cos \left(\frac{\pi t_i}{T_p} \right) \right]$
 $t_i = 1.25 T_p$

$Q_p = 4.34 Q_{p^*} \left(\frac{1.25 t_i}{T_p} \right)^{0.5}$
 $t_i = 1.25 T_p$

| DA RP2 306 Existing Conditions | | | | |
|--------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 1.94 | 2.82 | 4.09 | 5.43 |
| TP= | 10488.680 | 12289.463 | 16697.536 | 18589.255 |
| 1.25*TP= | 13110.850 | 15361.828 | 20871.920 | 23236.569 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.137274824 | 0.146668895 | 0.116220288 | 0.124740491 |
| 3600.00 | 0.510154573 | 0.556165686 | 0.451678322 | 0.487507454 |
| 5400.00 | 1.01285366 | 1.143307317 | 0.968265476 | 1.054989185 |
| 7200.00 | 1.502756885 | 1.785957258 | 1.607296537 | 1.775075692 |
| 9000.00 | 1.840879226 | 2.350432203 | 2.296176446 | 2.581643789 |
| 10800.00 | 1.931295732 | 2.719310719 | 2.95664723 | 3.400628966 |
| 12600.00 | 1.748355337 | 2.815859119 | 3.513678239 | 4.156826492 |
| 14400.00 | 1.409815359 | 2.619993515 | 3.903989766 | 4.780797224 |
| 16200.00 | 1.127904045 | 2.205720885 | 4.083241733 | 5.21524397 |
| 18000.00 | 0.902364644 | 1.823298754 | 4.031070799 | 5.420272907 |
| 19800.00 | 0.721924844 | 1.507179974 | 3.753403674 | 5.377056899 |
| 21600.00 | 0.577566379 | 1.245869043 | 3.304455929 | 5.089564329 |
| 23400.00 | 0.462074307 | 1.029863519 | 2.872352565 | 4.59087954 |
| 25200.00 | 0.369676409 | 0.85130847 | 2.496752699 | 4.047876648 |
| 27000.00 | 0.295754699 | 0.703710829 | 2.170267716 | 3.569099388 |
| 28800.00 | 0.236614617 | 0.581703282 | 1.886475164 | 3.146951241 |
| 30600.00 | 0.18930038 | 0.480849085 | 1.639792418 | 2.774734194 |
| 32400.00 | 0.151447254 | 0.397480725 | 1.425366856 | 2.446524265 |
| 34200.00 | 0.121163363 | 0.328566554 | 1.238980405 | 2.157168801 |
| 36000.00 | 0.096935139 | 0.271600543 | 1.076966563 | 1.902021854 |
| 37800.00 | 0.07755167 | 0.224511149 | 0.936138274 | 1.677053336 |
| 39600.00 | 0.062044183 | 0.185585992 | 0.813725234 | 1.478693783 |
| 41400.00 | 0.049637624 | 0.153409577 | 0.707319393 | 1.303795924 |
| 43200.00 | 0.039711922 | 0.126811825 | 0.61482759 | 1.149584743 |
| 45000.00 | 0.031770995 | 0.104825522 | 0.53443037 | 1.013613447 |
| 46800.00 | 0.025417963 | 0.086651146 | 0.4645462 | 0.893724648 |
| 48600.00 | 0.020335303 | 0.071627797 | 0.403800352 | 0.788016131 |
| 50400.00 | 0.016268989 | 0.059209156 | 0.350997866 | 0.694810671 |
| 52200.00 | 0.013015789 | 0.048943627 | 0.305100035 | 0.612629425 |
| 54000.00 | 0.010413109 | 0.040457909 | 0.265203981 | 0.540168462 |
| 55800.00 | 0.008330869 | 0.033443422 | 0.230524889 | 0.476278082 |
| 57600.00 | 0.006665001 | 0.027645089 | 0.200380568 | 0.419944569 |
| 59400.00 | 0.005332246 | 0.022852056 | 0.174178034 | 0.370274105 |
| 61200.00 | 0.004265992 | 0.018890026 | 0.151401845 | 0.326478595 |
| 63000.00 | 0.00341295 | 0.015614922 | 0.131603957 | 0.287863158 |
| 64800.00 | 0.002730486 | 0.012907648 | 0.114394918 | 0.253815101 |
| 66600.00 | 0.002184489 | 0.010669754 | 0.099436199 | 0.223794201 |
| 68400.00 | 0.001747671 | 0.00881986 | 0.086433539 | 0.197324132 |
| 70200.00 | 0.001398201 | 0.007290695 | 0.075131157 | 0.173984906 |
| 72000.00 | 0.001118612 | 0.006026654 | 0.065306718 | 0.153406212 |
| 73800.00 | 0.000894931 | 0.004981768 | 0.05676696 | 0.135261537 |
| 75600.00 | 0.000715978 | 0.004118042 | 0.049343894 | 0.119262989 |
| 77400.00 | 0.000572808 | 0.003404067 | 0.042891497 | 0.105156728 |
| 79200.00 | 0.000458268 | 0.002813879 | 0.03728284 | 0.092718935 |
| 81000.00 | 0.000366631 | 0.002326016 | 0.032407592 | 0.081752267 |
| 82800.00 | 0.000293318 | 0.001922737 | 0.028169851 | 0.072082722 |
| 84600.00 | 0.000234665 | 0.001589378 | 0.024486253 | 0.063556877 |
| 86400.00 | 0.000187741 | 0.001313816 | 0.021284336 | 0.056039458 |

ti (hrs)
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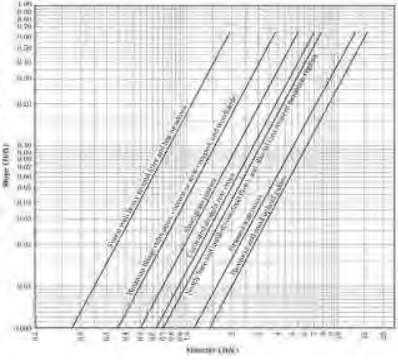
DA RP4 301 DRAINAGE CALCULATIONS

Time of Concentration:

$T_c = T_{OL} + T_1 + \dots + T_n$

Equation 2.1
 $T_{OL} = 0.0114 L^{0.77}$
 where:
 T_{OL} = travel time (min)
 L = Maximum hydraulic length (ft)
 n = Number of pipe segments
 T_1 = Time of travel along pipe (min)
 T_n = Time of travel along pipe (min)
 The following is a list of the pipe segments:
 1) Pipe segment 1 (100 ft)
 2) Pipe segment 2 (100 ft)
 3) Pipe segment 3 (100 ft)
 4) Pipe segment 4 (100 ft)
 5) Pipe segment 5 (100 ft)
 6) Pipe segment 6 (100 ft)
 7) Pipe segment 7 (100 ft)
 8) Pipe segment 8 (100 ft)
 9) Pipe segment 9 (100 ft)
 10) Pipe segment 10 (100 ft)

Equation 2.2
 $T_1 = \frac{L}{V}$
 where:
 T_1 = Time of travel along pipe (min)
 L = Length of pipe (ft)
 V = Velocity of flow (ft/s)
 The following is a list of the pipe segments:
 1) Pipe segment 1 (100 ft)
 2) Pipe segment 2 (100 ft)
 3) Pipe segment 3 (100 ft)
 4) Pipe segment 4 (100 ft)
 5) Pipe segment 5 (100 ft)
 6) Pipe segment 6 (100 ft)
 7) Pipe segment 7 (100 ft)
 8) Pipe segment 8 (100 ft)
 9) Pipe segment 9 (100 ft)
 10) Pipe segment 10 (100 ft)



| | |
|-------------------------------------------------------------------------|----------------------|
| $T_{OL} = T_{OL}$; multiply by 60 to convert hrs. to min. (L=max 300') | $T =$ |
| $n = 0.15$ | $D = 401$ (ft) |
| $L = 100$ (ft) | $S = 0.0039$ (ft/ft) |
| $P_2 = 4.89$ (in) | $V = 0.5$ (ft/s) |
| $S = 0.0039$ (ft/ft) | |
| $T_{OL} = 15.24$ (min) | $T_1 = 13.37$ (min) |

$T_c = 28.61$ (min)

Intensity:

SEE FIG. 2.1-2.1a

| | |
|---------------|--------------|
| I (500-YR)= | 9.03 (in/hr) |
| I (100-YR)= | 7 (in/hr) |
| I (10-YR)= | 4.8 (in/hr) |
| I (2-YR)= | 3.3 (in/hr) |

Peak Flow Rate:

$Q = CIA$

$C = 0.35$ Mixed use area; lots 1/4-1/2 acre; MOSTLY golf course; basin slope <1%

| | | | |
|---------------------------------|--------------------|-------------|------------|
| i (500-YR) | i (100-YR) | i (10-YR) | i (2-YR) |
| 9.03 | 7 | 4.8 | 3.3 |
| $A = 3.7$ (Ac) | | | |
| Q (500-YR)= | 11.70 (cfs) | | |
| Q (100-YR)= | 9.07 (cfs) | | |
| Q (10-YR)= | 6.22 (cfs) | | |
| Q (2-YR)= | 4.27 (cfs) | | |

DA RP4 301 EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 328790.88 cft
 Volume (100-yr) = 1.38*area*43560 = 222417.36 cft
 Volume (10-yr) = 0.70*area*43560 = 112820.4 cft
 Volume (2-yr) = 0.41*area*43560 = 66080.52 cft
 A= 3.70 Ac

TP = time to Qp in seconds

$$T_p = \frac{V}{1.39 Q_p}$$

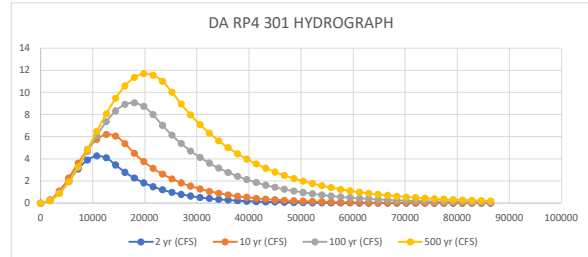
$$Q_i = \frac{Q_p}{2} \left[2 - \cos \left(\frac{\pi t_i}{T_p} \right) \right] \quad t_i = 1.25 T_p$$

$$Q_i = 4.34 Q_p e^{-1.8 t_i / T_p} \quad t_i = 1.25 T_p$$

| DA RP4 301 Existing Conditions | | | | |
|--------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 4.27 | 6.22 | 9.07 | 11.70 |
| TP= | 11124.358 | 13057.554 | 17651.681 | 20218.968 |
| 1.25*TP= | 13905.447 | 16321.942 | 22064.601 | 25273.710 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.270175838 | 0.286928539 | 0.23060194 | 0.227289828 |
| 3600.00 | 1.012379978 | 1.094736045 | 0.898942892 | 0.891495926 |
| 5400.00 | 2.038920247 | 2.27426999 | 1.937015921 | 1.941000804 |
| 7200.00 | 3.090200178 | 3.607742759 | 3.239192056 | 3.294244226 |
| 9000.00 | 3.900367016 | 4.848943676 | 4.672968552 | 4.846061506 |
| 10800.00 | 4.264541853 | 5.768699016 | 6.092451692 | 6.475856173 |
| 12600.00 | 4.090630394 | 6.197186349 | 7.353202173 | 8.056971896 |
| 14400.00 | 3.447032514 | 6.055290331 | 8.326932515 | 9.466535335 |
| 16200.00 | 2.793134652 | 5.369210459 | 8.914560926 | 10.595005 |
| 18000.00 | 2.263280416 | 4.494861455 | 9.056293364 | 11.35468406 |
| 19800.00 | 1.833938882 | 3.757403776 | 8.737707865 | 11.68653553 |
| 21600.00 | 1.486042913 | 3.140938443 | 7.991222049 | 11.56477022 |
| 23400.00 | 1.204142386 | 2.625614623 | 7.021287373 | 10.99885088 |
| 25200.00 | 0.975718044 | 2.19483835 | 6.149564771 | 10.03275684 |
| 27000.00 | 0.790625521 | 1.834738175 | 5.386070227 | 8.947531634 |
| 28800.00 | 0.640644825 | 1.533718496 | 4.717366768 | 7.969683562 |
| 30600.00 | 0.519115283 | 1.282086161 | 4.13168568 | 7.098701482 |
| 32400.00 | 0.420639747 | 1.071738346 | 3.618719382 | 6.322906342 |
| 34200.00 | 0.3408449 | 0.895901631 | 3.169440025 | 5.631895454 |
| 36000.00 | 0.276187038 | 0.748913889 | 2.775940606 | 5.01640301 |
| 37800.00 | 0.223794694 | 0.62604196 | 2.431295808 | 4.468175833 |
| 39600.00 | 0.181341114 | 0.523329239 | 2.129440123 | 3.979862709 |
| 41400.00 | 0.146940926 | 0.437468269 | 1.865061102 | 3.544915816 |
| 43200.00 | 0.119066411 | 0.365694236 | 1.633505857 | 3.157502925 |
| 45000.00 | 0.096479658 | 0.305695941 | 1.430699178 | 2.812429192 |
| 46800.00 | 0.078177585 | 0.255541376 | 1.253071808 | 2.505067499 |
| 48600.00 | 0.063347392 | 0.213615512 | 1.097497629 | 2.231296416 |
| 50400.00 | 0.051330469 | 0.178568292 | 0.961238645 | 1.987444929 |
| 52200.00 | 0.041593142 | 0.149271158 | 0.841896791 | 1.770243216 |
| 54000.00 | 0.033702974 | 0.124780712 | 0.737371734 | 1.576778808 |
| 55800.00 | 0.027309561 | 0.104308336 | 0.645823906 | 1.404457526 |
| 57600.00 | 0.02212897 | 0.087194798 | 0.56564213 | 1.250968705 |
| 59400.00 | 0.017931132 | 0.072889023 | 0.495415261 | 1.114254202 |
| 61200.00 | 0.014529618 | 0.060930352 | 0.433907355 | 0.992480805 |
| 63000.00 | 0.011773367 | 0.050933702 | 0.380035917 | 0.884015646 |
| 64800.00 | 0.009539974 | 0.042577171 | 0.332852846 | 0.787404309 |
| 66600.00 | 0.007730252 | 0.03559167 | 0.291527754 | 0.701351326 |
| 68400.00 | 0.006263833 | 0.029752257 | 0.255333347 | 0.624702808 |
| 70200.00 | 0.005075591 | 0.024870899 | 0.223632629 | 0.556430969 |
| 72000.00 | 0.004112758 | 0.020790409 | 0.19586769 | 0.495620349 |
| 73800.00 | 0.003332573 | 0.017379393 | 0.171549886 | 0.441455533 |
| 75600.00 | 0.002700388 | 0.014528011 | 0.15025124 | 0.393210222 |
| 77400.00 | 0.002188128 | 0.012144446 | 0.131596911 | 0.350237493 |
| 79200.00 | 0.001773042 | 0.010151945 | 0.115258597 | 0.31196112 |
| 81000.00 | 0.001436698 | 0.008486348 | 0.100948753 | 0.277867853 |
| 82800.00 | 0.001164158 | 0.00709402 | 0.088415537 | 0.247500535 |
| 84600.00 | 0.000943319 | 0.005930126 | 0.077438373 | 0.220451966 |
| 86400.00 | 0.000764373 | 0.004957189 | 0.067824071 | 0.196359452 |

ti (hrs)
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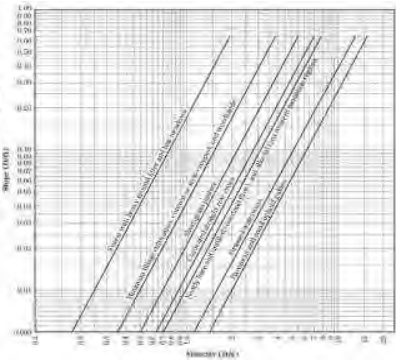
DA RP4 306 DRAINAGE CALCULATIONS

Time of Concentration:

$T_c = T_{OL} + T_1 + \dots + T_n$

Equation 2.1
 T_{OL} = Time of Overland Flow
 T₁ = Time of Flow in Pipe
 T_n = Time of Flow in Channel
 T_c = Time of Concentration
 L = Length of Overland Flow (ft)
 S = Slope of Overland Flow (ft/ft)
 n = Manning's Roughness Coefficient
 D = Diameter of Pipe (ft)
 V = Velocity of Flow in Pipe (ft/s)
 T₁ = Time of Flow in Pipe (min)
 T_n = Time of Flow in Channel (min)
 T_c = Time of Concentration (min)

Equation 2.1
 T_{OL} = Time of Overland Flow
 T₁ = Time of Flow in Pipe
 T_n = Time of Flow in Channel
 T_c = Time of Concentration
 L = Length of Overland Flow (ft)
 S = Slope of Overland Flow (ft/ft)
 n = Manning's Roughness Coefficient
 D = Diameter of Pipe (ft)
 V = Velocity of Flow in Pipe (ft/s)
 T₁ = Time of Flow in Pipe (min)
 T_n = Time of Flow in Channel (min)
 T_c = Time of Concentration (min)



| | |
|-------------------------------------------------------------------------|------------------------------|
| $T_{OL} = T_{OL}$; multiply by 60 to convert hrs. to min. (L=max 300') | T= |
| n= 0.15 | D= 346 (ft) |
| L= 100 (ft) | S= 0.0039 (ft/ft) |
| P ₂ = 4.89 (in) | V= 0.5 (ft/s) |
| S= 0.0039 (ft/ft) | |
| T _{OL} = 15.24 (min) | T ₁ = 11.53 (min) |

T_c = 26.78 (min)

Intensity:

SEE FIG. 2.1-2.1a

| | |
|-------------|--------------|
| i (500-YR)= | 9.47 (in/hr) |
| i (100-YR)= | 7.1 (in/hr) |
| i (10-YR)= | 4.9 (in/hr) |
| i (2-YR)= | 3.4 (in/hr) |

Peak Flow Rate:

Q=CIA
 C= 0.35 Mixed use area; lots 1/4-1/2 acre; MOSTLY golf course; basin slope <1%

| | | | |
|--------------------|-------------------|-----------|----------|
| i (500-YR) | i (100-YR) | i (10-YR) | i (2-YR) |
| 9.47 | 7.1 | 4.9 | 3.4 |
| A= 2.73 (Ac) | | | |
| Q (500-YR)= | 9.05 (cfs) | | |
| Q (100-YR)= | 6.78 (cfs) | | |
| Q (10-YR)= | 4.68 (cfs) | | |
| Q (2-YR)= | 3.25 (cfs) | | |

DA RP4 306 EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 242594.35 cft
 Volume (100-yr) = 1.38*area*43560 = 164107.94 cft
 Volume (10-yr) = 0.70*area*43560 = 83243.16 cft
 Volume (2-yr) = 0.41*area*43560 = 48756.708 cft
 A= 2.73 Ac

TP = time to Qp in seconds

$T_p = \frac{V}{1.39 Q_p}$

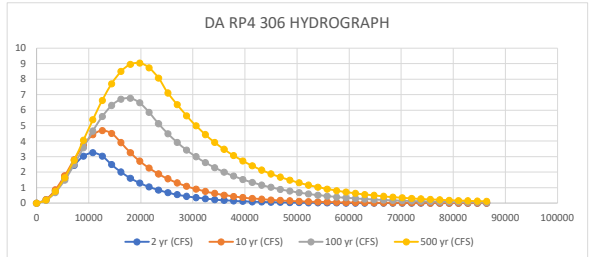
$Q_p = \frac{Q_p}{2} \left[2 - \cos \left(\frac{\pi t_i}{T_p} \right) \right]$
 $t_i = 1.25 T_p$

$Q_p = 4.34 Q_{ps} \left(\frac{t_i}{T_p} \right)^{-1.81}$
 $t_i = 1.25 T_p$

| DA RP4 306 Existing Conditions | | | | |
|--------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 3.25 | 4.68 | 6.78 | 9.05 |
| Tp= | 10797.171 | 12791.073 | 17403.066 | 19279.932 |
| 1.25*Tp= | 13496.463 | 15988.842 | 21753.832 | 24099.916 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.217733084 | 0.225067359 | 0.177499747 | 0.193294047 |
| 3600.00 | 0.812561053 | 0.856992325 | 0.69142238 | 0.756666589 |
| 5400.00 | 1.625018611 | 1.774265116 | 1.487982248 | 1.641998937 |
| 7200.00 | 2.437296923 | 2.800507798 | 2.483813705 | 2.773673225 |
| 9000.00 | 3.03163521 | 3.73838915 | 3.574695921 | 4.055031066 |
| 10800.00 | 3.24869945 | 4.40756852 | 4.646460329 | 5.376629325 |
| 12600.00 | 3.03029767 | 4.679372654 | 5.586939175 | 6.625587859 |
| 14400.00 | 2.490146942 | 4.501537657 | 6.297704672 | 7.695230818 |
| 16200.00 | 2.004948308 | 3.908258555 | 6.704370165 | 8.494198025 |
| 18000.00 | 1.614289361 | 3.261503259 | 6.764375224 | 8.95424822 |
| 19800.00 | 1.299749291 | 2.716238799 | 6.471439894 | 9.036087666 |
| 21600.00 | 1.046496533 | 2.262132712 | 5.856221936 | 8.732726306 |
| 23400.00 | 0.842589414 | 1.883944964 | 5.126795199 | 8.070074793 |
| 25200.00 | 0.678413065 | 1.56898338 | 4.481786232 | 7.104731414 |
| 27000.00 | 0.54622605 | 1.306677686 | 3.917926707 | 6.32050501 |
| 28800.00 | 0.439795329 | 1.088224768 | 3.425007103 | 5.634909072 |
| 30600.00 | 0.354102357 | 0.906293234 | 2.994102375 | 4.990875229 |
| 32400.00 | 0.285106437 | 0.754777368 | 2.617410347 | 4.42045031 |
| 34200.00 | 0.229554191 | 0.628592219 | 2.288110447 | 3.915221287 |
| 36000.00 | 0.184826156 | 0.523502949 | 2.000240209 | 3.467736691 |
| 37800.00 | 0.148813262 | 0.435982708 | 1.748587311 | 3.071396704 |
| 39600.00 | 0.119817386 | 0.36309427 | 1.5285952 | 2.720355827 |
| 41400.00 | 0.096471281 | 0.302391464 | 1.336280592 | 2.409436663 |
| 43200.00 | 0.077674104 | 0.251837071 | 1.168161342 | 2.134053559 |
| 45000.00 | 0.062539507 | 0.209734459 | 1.0211934 | 1.890144971 |
| 46800.00 | 0.050353847 | 0.174670644 | 0.892715691 | 1.674113565 |
| 48600.00 | 0.040542532 | 0.145468866 | 0.780401935 | 1.482773158 |
| 50400.00 | 0.032642925 | 0.121149098 | 0.682218523 | 1.313301729 |
| 52200.00 | 0.026282536 | 0.100895156 | 0.596387697 | 1.163199793 |
| 54000.00 | 0.021161453 | 0.084027308 | 0.521355363 | 1.030253542 |
| 55800.00 | 0.017038199 | 0.069979459 | 0.455762947 | 0.912502193 |
| 57600.00 | 0.01371835 | 0.058280157 | 0.3984228 | 0.808209065 |
| 59400.00 | 0.011045366 | 0.048536767 | 0.348296694 | 0.71583597 |
| 61200.00 | 0.008893205 | 0.040422296 | 0.304477021 | 0.634020525 |
| 63000.00 | 0.007160387 | 0.033664418 | 0.266170359 | 0.56155606 |
| 64800.00 | 0.005765204 | 0.028036335 | 0.23268311 | 0.497373816 |
| 66600.00 | 0.004641869 | 0.023349166 | 0.203408937 | 0.44052719 |
| 68400.00 | 0.003737413 | 0.019445607 | 0.177817786 | 0.390177767 |
| 70200.00 | 0.003009188 | 0.016194652 | 0.155446292 | 0.345582959 |
| 72000.00 | 0.002422856 | 0.013487199 | 0.135889386 | 0.306085051 |
| 73800.00 | 0.001950768 | 0.011232383 | 0.118792961 | 0.271101499 |
| 75600.00 | 0.001570666 | 0.009354531 | 0.103847459 | 0.240116343 |
| 77400.00 | 0.001264626 | 0.007790622 | 0.090782271 | 0.21267259 |
| 79200.00 | 0.001018217 | 0.006488171 | 0.079360832 | 0.188365482 |
| 81000.00 | 0.00081982 | 0.005403466 | 0.06937634 | 0.166836519 |
| 82800.00 | 0.00066008 | 0.004500104 | 0.06064801 | 0.147768179 |
| 84600.00 | 0.000531465 | 0.003747768 | 0.053017802 | 0.130879227 |
| 86400.00 | 0.000427911 | 0.003121209 | 0.046347562 | 0.115920574 |

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DA RP4 602 DRAINAGE CALCULATIONS

Time of Concentration:

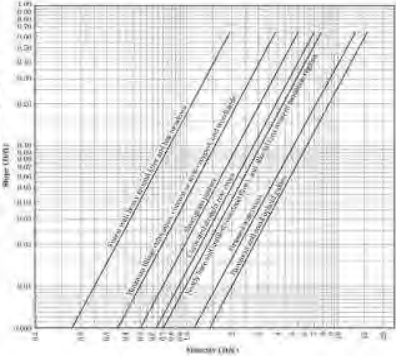
$T_c = T_{OL} + T_1 + \dots + T_n$

Equation 5.3
 $T_{OL} = 0.0114 L^{0.77} S^{-0.103} P_2^{-0.432}$
 where:
 T_{OL} = travel time (min)
 L = Maximum length of travel (ft)
 S = Slope (ft/ft)
 P_2 = 2-year return period design rainfall (in)

Equation 5.4
 $T_1 = 0.88 L^{0.0167} S^{-0.000042} P_2^{-0.000087}$
 where:
 T_1 = travel time (min)
 L = Maximum length of travel (ft)
 S = Slope (ft/ft)
 P_2 = 2-year return period design rainfall (in)

Table 2.3 Manning's Roughness Coefficients for Channels and Pipes

| Surface | n |
|-----------------------------------------|-------|
| Smooth finished concrete (open channel) | 0.012 |
| Cast-in-place concrete (open channel) | 0.013 |
| Cast-in-place concrete (pipes) | 0.013 |
| Corrugated metal (open channel) | 0.014 |
| Galvanized steel (open channel) | 0.014 |
| Asphalt (open channel) | 0.014 |
| Gravel (open channel) | 0.017 |
| Concrete (pipes) | 0.013 |
| Wood (open channel) | 0.015 |
| Wood (pipes) | 0.015 |



| | |
|-------------------------------------------------------------------------|---------------------|
| $T_{OL} = T_{OL}$; multiply by 60 to convert hrs. to min. (L=max 300') | $T =$ |
| n= 0.15 | D= 557 (ft) |
| L= 100 (ft) | S= 0.0039 (ft/ft) |
| $P_2 = 4.89$ (in) | V= 0.5 (ft/s) |
| S= 0.0039 (ft/ft) | |
| $T_{OL} = 15.24$ (min) | $T_1 = 18.57$ (min) |

$T_c = 33.81$ (min)

Intensity:

SEE FIG. 2.1-2.1a

| | |
|-------------|--------------|
| I (500-YR)= | 8.37 (in/hr) |
| I (100-YR)= | 6.3 (in/hr) |
| I (10-YR)= | 4.3 (in/hr) |
| I (2-YR)= | 3 (in/hr) |

Peak Flow Rate:

Q=CIA

C= 0.35 Mixed use area; lots 1/4-1/2 acre; MOSTLY golf course; basin slope <1%

| | | | |
|------------|------------|-----------|----------|
| i (500-YR) | i (100-YR) | i (10-YR) | i (2-YR) |
| 8.37 | 6.3 | 4.3 | 3 |

| | |
|--------------------|--------------------|
| A= | 5.52 (Ac) |
| Q (500-YR)= | 16.18 (cfs) |
| Q (100-YR)= | 12.17 (cfs) |
| Q (10-YR)= | 8.31 (cfs) |
| Q (2-YR)= | 5.80 (cfs) |

DA RP4 602 EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 490520.45 cft
 Volume (100-yr) = 1.38*area*43560 = 331822.66 cft
 Volume (10-yr) = 0.70*area*43560 = 168315.84 cft
 Volume (2-yr) = 0.41*area*43560 = 98584.992 cft
 A= 5.52 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

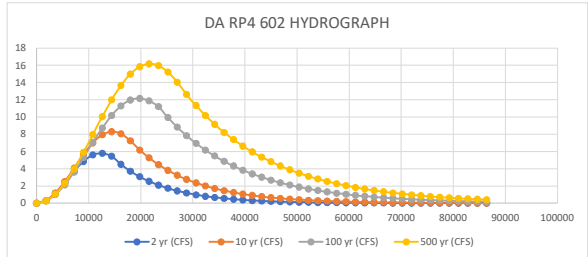
$Q_t = \frac{Q_p}{2} \left[2 - \cos \left(\frac{\pi t_i}{T_p} \right) \right]$ $t_i = 1.25 T_p$

$Q_t = 4.34 Q_p \left(\frac{t_i - T_p}{T_p} \right)^2$ $t_i = 1.25 T_p$

| DA RP4 602 Existing Conditions | | | | |
|--------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 5.80 | 8.31 | 12.17 | 16.18 |
| TP= | 12236.793 | 14575.874 | 19612.979 | 21816.365 |
| 1.25*TP= | 15295.992 | 18219.843 | 24516.224 | 27270.457 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.303973185 | 0.308700267 | 0.251208684 | 0.270176125 |
| 3600.00 | 1.152124833 | 1.188917369 | 0.984096031 | 1.062653802 |
| 5400.00 | 2.366528542 | 2.509820137 | 2.138158027 | 2.324486918 |
| 7200.00 | 3.692425053 | 4.075076038 | 3.618120297 | 3.971371321 |
| 9000.00 | 4.851666 | 5.652033084 | 5.301803548 | 5.893277252 |
| 10800.00 | 5.601064244 | 7.006300086 | 7.050210159 | 7.961800529 |
| 12600.00 | 5.783410004 | 7.936585415 | 8.718999233 | 10.03874134 |
| 14400.00 | 5.447897938 | 8.304616004 | 10.17040275 | 11.98533748 |
| 16200.00 | 4.499666431 | 8.055689585 | 11.2845991 | 13.67153521 |
| 18000.00 | 3.716478947 | 7.240226892 | 11.96960505 | 14.98467819 |
| 19800.00 | 3.069608819 | 6.166388217 | 12.16886946 | 15.83703424 |
| 21600.00 | 2.535329391 | 5.251816581 | 11.86594193 | 16.1716567 |
| 23400.00 | 2.094043736 | 4.472890196 | 11.2005846 | 15.96618916 |
| 25200.00 | 1.729565864 | 3.809490754 | 9.940896657 | 15.23435909 |
| 27000.00 | 1.42852703 | 3.244483805 | 8.822881118 | 14.04818534 |
| 28800.00 | 1.179885379 | 2.763276207 | 7.830604613 | 12.61938724 |
| 30600.00 | 0.974520942 | 2.353439208 | 6.949925742 | 11.33590783 |
| 32400.00 | 0.804901123 | 2.004387434 | 6.168293537 | 10.1829672 |
| 34200.00 | 0.664804408 | 1.707105487 | 5.474568588 | 9.147288649 |
| 36000.00 | 0.549092166 | 1.453915094 | 4.858864294 | 8.216945805 |
| 37800.00 | 0.453520168 | 1.238276789 | 4.312405964 | 7.381225296 |
| 39600.00 | 0.374582912 | 1.05462101 | 3.827405763 | 6.630503373 |
| 41400.00 | 0.309385046 | 0.898204251 | 3.396951724 | 5.956135087 |
| 43200.00 | 0.255535167 | 0.764986538 | 3.014909244 | 5.350354745 |
| 45000.00 | 0.211058104 | 0.651527093 | 2.675833655 | 4.806186474 |
| 46800.00 | 0.174322478 | 0.554895454 | 2.374892632 | 4.317363899 |
| 48600.00 | 0.143980855 | 0.472595796 | 2.107797323 | 3.878257978 |
| 50400.00 | 0.11892033 | 0.402502461 | 1.870741226 | 3.483812182 |
| 52200.00 | 0.098221703 | 0.342805063 | 1.660345943 | 3.129484265 |
| 54000.00 | 0.081125767 | 0.291961721 | 1.473613033 | 2.81119396 |
| 55800.00 | 0.067005457 | 0.24865924 | 1.307881276 | 2.525275992 |
| 57600.00 | 0.055342852 | 0.211779193 | 1.160788751 | 2.268437869 |
| 59400.00 | 0.045710176 | 0.180369032 | 1.030239173 | 2.037721969 |
| 61200.00 | 0.037754111 | 0.153617489 | 0.914372019 | 1.830471479 |
| 63000.00 | 0.031182835 | 0.130833617 | 0.811536011 | 1.644299805 |
| 64800.00 | 0.025755321 | 0.111428949 | 0.720265585 | 1.477063085 |
| 66600.00 | 0.021272489 | 0.094902297 | 0.639260004 | 1.326835501 |
| 68400.00 | 0.017569916 | 0.080826805 | 0.567364817 | 1.191887107 |
| 70200.00 | 0.014511792 | 0.068838928 | 0.503555414 | 1.070663903 |
| 72000.00 | 0.011985948 | 0.05862904 | 0.446922416 | 0.961769941 |
| 73800.00 | 0.009899739 | 0.049933438 | 0.39665872 | 0.863951252 |
| 75600.00 | 0.008176644 | 0.04252753 | 0.352047995 | 0.776081404 |
| 77400.00 | 0.006753462 | 0.036220033 | 0.312454471 | 0.69714853 |
| 79200.00 | 0.005577991 | 0.030848037 | 0.277313883 | 0.626243678 |
| 81000.00 | 0.004607116 | 0.026272791 | 0.246125426 | 0.562550343 |
| 82800.00 | 0.003805227 | 0.022376126 | 0.218444618 | 0.505335063 |
| 84600.00 | 0.00314291 | 0.019057397 | 0.193876967 | 0.453938974 |
| 86400.00 | 0.002595872 | 0.016230888 | 0.172072348 | 0.407770225 |

ti (hrs)
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DA RP4 603 DRAINAGE CALCULATIONS

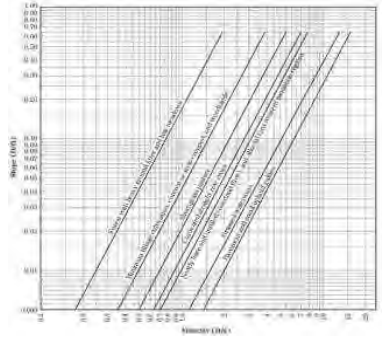
Time of Concentration:

$T_c = T_{c1} + T_1 + \dots + T_n$

The screenshot shows a software interface with various input fields and a table of Manning's roughness coefficients. The table lists materials like concrete, asphalt, and grass with their corresponding roughness values.

| | | |
|------------------------------------------------------------------------------------|-----------------------------|----|
| Tt=To; multiply by T _{oc} = 60 to convert hrs. to min. (L=max 300') | | T= |
| n= 0.15 | D= 138 (ft) | |
| L= 100 (ft) | S= 0.0076 (ft/ft) | |
| P ₂ = 4.89 (in) | V= 1.75 (ft/s) | |
| S= 0.0076 (ft/ft) | | |
| T _{oc} = 11.67 (min) | T ₁ = 1.31 (min) | |

T_c = 12.99 (min)



Intensity:

SEE FIG. 2.1-2.1a

| | |
|-------------|---------------|
| i (500-YR)= | 13.27 (in/hr) |
| i (100-YR)= | 10.2 (in/hr) |
| i (10-YR)= | 7 (in/hr) |
| i (2-YR)= | 4.8 (in/hr) |

Peak Flow Rate:

Q=CIA
C= 0.18 Mixed use area. Lots 1/4-1/2 acre; golf course; and MOSTLY woodlands; basin slope <1%

| | | | |
|--------------|------------|-----------|----------|
| i (500-YR) | i (100-YR) | i (10-YR) | i (2-YR) |
| 13.27 | 10.2 | 7 | 4.8 |
| A= 0.68 (Ac) | | | |
| Q (500-YR)= | 1.62 (cfs) | | |
| Q (100-YR)= | 1.25 (cfs) | | |
| Q (10-YR)= | 0.86 (cfs) | | |
| Q (2-YR)= | 0.59 (cfs) | | |

DA RP4 603 EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 60426.43 cft
 Volume (100-yr) = 1.38*area*43560 = 40876.70 cft
 Volume (10-yr) = 0.70*area*43560 = 20734.56 cft
 Volume (2-yr) = 0.41*area*43560 = 12144.528 cft
 A= 0.68 Ac

TP = time to Qp in seconds

$$TP = \frac{V}{1.39 Qp}$$

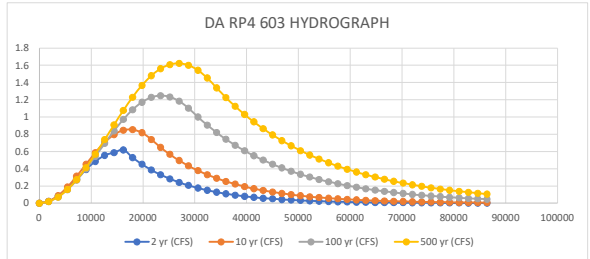
$$Qp = \frac{Qp}{2} \left[2 - \cos \left(\frac{\pi t_i}{TP} \right) \right] \quad t_i = 1.25 TP$$

$$Qp = 4.34 Qp \left(\frac{t_i - 1.25 TP}{TP} \right)^2 \quad t_i = 1.25 TP$$

| DA RP4 603 Existing Conditions | | | | |
|--------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 0.59 | 0.86 | 1.25 | 1.62 |
| TP= | 14871.103 | 17410.072 | 23554.803 | 26771.361 |
| 1.25*TP= | 18588.879 | 21762.590 | 29443.504 | 33464.202 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.020983677 | 0.022399671 | 0.017902782 | 0.018045553 |
| 3600.00 | 0.080936924 | 0.087256268 | 0.070584247 | 0.071380055 |
| 5400.00 | 0.171294656 | 0.187787502 | 0.155022658 | 0.157632697 |
| 7200.00 | 0.279148121 | 0.313480458 | 0.266374742 | 0.272969402 |
| 9000.00 | 0.389089078 | 0.451190967 | 0.398253494 | 0.412263254 |
| 10800.00 | 0.485411064 | 0.586518142 | 0.543094527 | 0.569322405 |
| 12600.00 | 0.554353256 | 0.705310329 | 0.692589954 | 0.737165307 |
| 14400.00 | 0.586066385 | 0.795144999 | 0.838164921 | 0.908331054 |
| 16200.00 | 0.618696791 | 0.846627815 | 0.971469442 | 1.075211037 |
| 18000.00 | 0.528616475 | 0.854375032 | 1.084857353 | 1.230387154 |
| 19800.00 | 0.451651571 | 0.817576495 | 1.171824874 | 1.366961562 |
| 21600.00 | 0.385892516 | 0.740080361 | 1.227383666 | 1.478863295 |
| 23400.00 | 0.329707774 | 0.647950565 | 1.248346952 | 1.56111813 |
| 25200.00 | 0.281703354 | 0.566461686 | 1.233512307 | 1.610069697 |
| 27000.00 | 0.240688228 | 0.495221178 | 1.183730626 | 1.623542016 |
| 28800.00 | 0.205644775 | 0.432940164 | 1.101857317 | 1.600936219 |
| 30600.00 | 0.17570354 | 0.378491861 | 1.000974109 | 1.543257174 |
| 32400.00 | 0.150121654 | 0.330891197 | 0.906314267 | 1.453068811 |
| 34200.00 | 0.128264411 | 0.289276984 | 0.82060619 | 1.339015479 |
| 36000.00 | 0.109589515 | 0.252896343 | 0.743003331 | 1.226945553 |
| 37800.00 | 0.093633624 | 0.221091078 | 0.672739197 | 1.124255405 |
| 39600.00 | 0.080000862 | 0.193285772 | 0.609119783 | 1.030159988 |
| 41400.00 | 0.068352987 | 0.168977373 | 0.551516712 | 0.943939959 |
| 43200.00 | 0.058401006 | 0.147726096 | 0.499361032 | 0.864936181 |
| 45000.00 | 0.049898002 | 0.129147466 | 0.452137596 | 0.792544685 |
| 46800.00 | 0.042633009 | 0.11290536 | 0.409379973 | 0.72621205 |
| 48600.00 | 0.036425777 | 0.098705926 | 0.370665841 | 0.665431177 |
| 50400.00 | 0.031122298 | 0.08629227 | 0.335612816 | 0.609737405 |
| 52200.00 | 0.026590989 | 0.075439806 | 0.303874676 | 0.558704966 |
| 54000.00 | 0.022719424 | 0.065952191 | 0.27513794 | 0.511943726 |
| 55800.00 | 0.019411547 | 0.057657778 | 0.249118771 | 0.469096203 |
| 57600.00 | 0.016585286 | 0.050406503 | 0.225560176 | 0.429834837 |
| 59400.00 | 0.014170521 | 0.044067177 | 0.204229464 | 0.393859481 |
| 61200.00 | 0.012107337 | 0.038525111 | 0.184915949 | 0.36089511 |
| 63000.00 | 0.010344547 | 0.033680038 | 0.167428868 | 0.330689718 |
| 64800.00 | 0.008838413 | 0.0294443 | 0.151595501 | 0.303012388 |
| 66600.00 | 0.00751568 | 0.025741266 | 0.13725946 | 0.277651535 |
| 68400.00 | 0.006452083 | 0.022503941 | 0.124279145 | 0.254413277 |
| 70200.00 | 0.00551268 | 0.019673754 | 0.11252635 | 0.233119963 |
| 72000.00 | 0.004710051 | 0.017199504 | 0.101884989 | 0.213608809 |
| 73800.00 | 0.004024282 | 0.015036425 | 0.092249957 | 0.195730656 |
| 75600.00 | 0.00343836 | 0.013145383 | 0.083526089 | 0.179348829 |
| 77400.00 | 0.002937745 | 0.011492167 | 0.075627217 | 0.164338091 |
| 79200.00 | 0.002510019 | 0.010046865 | 0.068475323 | 0.150583689 |
| 81000.00 | 0.002144568 | 0.008783331 | 0.061999768 | 0.137980472 |
| 82800.00 | 0.001832325 | 0.007678704 | 0.056136591 | 0.12643209 |
| 84600.00 | 0.001565545 | 0.006712999 | 0.050827881 | 0.11585026 |
| 86400.00 | 0.001337606 | 0.005868745 | 0.046021204 | 0.106154083 |

ti (hrs)
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DA RP4 604 EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 908173.73 cft
 Volume (100-yr) = 1.38*area*43560 = 614352.82 cft
 Volume (10-yr) = 0.70*area*43560 = 311628.24 cft
 Volume (2-yr) = 0.41*area*43560 = 182525.112 cft
 A= 10.22 Ac

TP = time to Qp in seconds

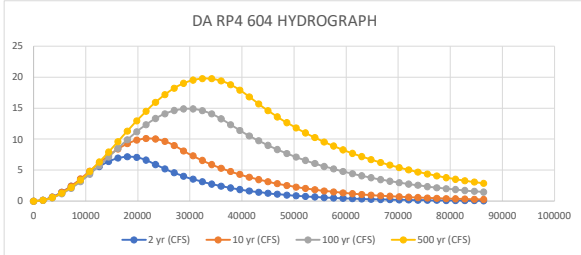
$T_p = \frac{V}{1.39 Q_p}$

$Q_p = \frac{Q_p}{2} \left[2 - \cos \left(\frac{\pi t_i}{T_p} \right) \right]$
 $t_i = 1.25 T_p$
 $Q_p = 4.34 Q_{ps} \left(\frac{t_i}{T_p} \right)^{-1.81}$
 $t_i = 1.25 T_p$

| DA RP4 604 Existing Conditions | | | | |
|--------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 7.17 | 10.12 | 14.90 | 19.79 |
| TP= | 18302.896 | 22158.273 | 29661.604 | 33013.567 |
| 1.25*TP= | 22878.620 | 27697.842 | 37077.005 | 41266.959 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.169853972 | 0.163847814 | 0.13498581 | 0.144810291 |
| 3600.00 | 0.6633308 | 0.644777841 | 0.5350519 | 0.575002812 |
| 5400.00 | 1.433698476 | 1.411637326 | 1.185701495 | 1.277986551 |
| 7200.00 | 2.408003565 | 2.41475213 | 2.063357686 | 2.23186358 |
| 9000.00 | 3.493979862 | 3.589144425 | 3.136217764 | 3.412645144 |
| 10800.00 | 4.588785954 | 4.857841701 | 4.365405623 | 4.781842134 |
| 12600.00 | 5.588744249 | 6.141304444 | 5.706380469 | 6.30070324 |
| 14400.00 | 6.399159198 | 7.353753287 | 7.110550799 | 7.924773954 |
| 16200.00 | 6.943284908 | 8.417550568 | 8.527035165 | 9.60652046 |
| 18000.00 | 7.169592947 | 9.263787685 | 9.904505904 | 11.29672087 |
| 19800.00 | 7.056652056 | 9.83764873 | 11.19304905 | 12.94590586 |
| 21600.00 | 6.615157681 | 10.10196124 | 12.34597302 | 14.5080658 |
| 23400.00 | 5.908352383 | 10.0396041 | 13.32150051 | 15.93076733 |
| 25200.00 | 5.199270819 | 9.654616549 | 14.08428235 | 17.17908194 |
| 27000.00 | 4.575288558 | 8.971936571 | 14.60667842 | 18.21421433 |
| 28800.00 | 4.02619254 | 8.105219682 | 14.8697592 | 19.00586791 |
| 30600.00 | 3.542995412 | 7.292922543 | 14.86399169 | 19.53087233 |
| 32400.00 | 3.117788423 | 6.562033024 | 14.58958491 | 19.77386158 |
| 34200.00 | 2.743611978 | 5.904392533 | 14.05648223 | 19.72772378 |
| 36000.00 | 2.414341727 | 5.312660125 | 13.28400114 | 19.3938093 |
| 37800.00 | 2.124588325 | 4.780230556 | 12.33695659 | 18.78189127 |
| 39600.00 | 1.869609218 | 4.301160555 | 11.401096 | 17.90987948 |
| 41400.00 | 1.645231026 | 3.870102477 | 10.53622821 | 16.82471326 |
| 43200.00 | 1.447781227 | 3.482244616 | 9.736967822 | 15.67346073 |
| 45000.00 | 1.274028054 | 3.133257488 | 8.998337969 | 14.60098413 |
| 46800.00 | 1.121127593 | 2.819245507 | 8.315739324 | 13.60189311 |
| 48600.00 | 0.986577238 | 2.536703497 | 7.684921453 | 12.67116617 |
| 50400.00 | 0.868174732 | 2.282477569 | 7.101956355 | 11.80412542 |
| 52200.00 | 0.763982115 | 2.053729914 | 6.563214 | 10.99641304 |
| 54000.00 | 0.67229401 | 1.847907123 | 6.065339726 | 10.24396941 |
| 55800.00 | 0.591609708 | 1.66271169 | 5.605233349 | 9.543012695 |
| 57600.00 | 0.520608605 | 1.496076361 | 5.180029861 | 8.890019843 |
| 59400.00 | 0.458128587 | 1.346141061 | 4.787081588 | 8.281708862 |
| 61200.00 | 0.403147009 | 1.211232128 | 4.423941703 | 7.715022339 |
| 63000.00 | 0.354763959 | 1.089843637 | 4.088348994 | 7.187112065 |
| 64800.00 | 0.312187524 | 0.98062058 | 3.778213779 | 6.695324728 |
| 66600.00 | 0.274720832 | 0.882343751 | 3.491604894 | 6.237188568 |
| 68400.00 | 0.241750646 | 0.793916129 | 3.226737673 | 5.810400961 |
| 70200.00 | 0.212737325 | 0.714350636 | 2.98196283 | 5.412816842 |
| 72000.00 | 0.187205991 | 0.642759118 | 2.755756191 | 5.042437925 |
| 73800.00 | 0.16473876 | 0.578342432 | 2.546709204 | 4.697402659 |
| 75600.00 | 0.144967899 | 0.520381522 | 2.353520166 | 4.375976873 |
| 77400.00 | 0.127569806 | 0.468229398 | 2.174986121 | 4.076545057 |
| 79200.00 | 0.112259717 | 0.421303909 | 2.00995365 | 3.797602247 |
| 81000.00 | 0.098787045 | 0.379081246 | 1.857520528 | 3.537746455 |
| 82800.00 | 0.086931274 | 0.341090097 | 1.716612174 | 3.295671628 |
| 84600.00 | 0.076498355 | 0.306906383 | 1.586392888 | 3.07016108 |
| 86400.00 | 0.067317526 | 0.276148527 | 1.466051816 | 2.860081381 |

ti (hrs)



DA RP4 605 DRAINAGE CALCULATIONS

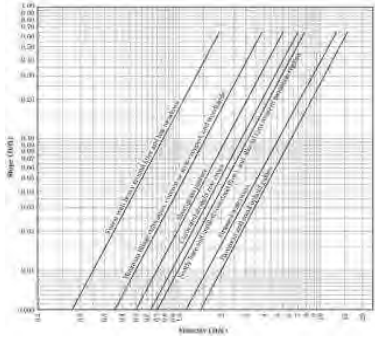
Time of Concentration:

$T_c = T_{c1} + T_1 + \dots + T_n$

The screenshot shows a software interface with various input fields and a table of Manning's roughness coefficients. The table lists materials like concrete, asphalt, and grass with their corresponding roughness values.

| | | |
|------------------------|-------------------------------------------------------------------|-------|
| $T_{c1} =$ | $T_t = T_o$; multiply by 60 to convert hrs. to min. (L=max 300') | $T =$ |
| $n = 0.15$ | $D = 220$ (ft) | |
| $L = 100$ (ft) | $S = 0.0076$ (ft/ft) | |
| $P_2 = 4.89$ (in) | $V = 1.75$ (ft/s) | |
| $S = 0.0076$ (ft/ft) | $T_1 = 2.10$ (min) | |
| $T_{c1} = 11.67$ (min) | | |

$T_c = 13.77$ (min)



Intensity:

SEE FIG. 2.1-2.1a

| | |
|---------------|---------------|
| i (500-YR)= | 12.89 (in/hr) |
| i (100-YR)= | 10 (in/hr) |
| i (10-YR)= | 6.8 (in/hr) |
| i (2-YR)= | 4.7 (in/hr) |

Peak Flow Rate:

$Q = CIA$

$C = 0.18$ Mixed use area. Lots 1/4-1/2 acre; golf course; and MOSTLY woodlands; basin slope <1%

| | | | |
|---------------------------------|-------------------|-------------|------------|
| i (500-YR) | i (100-YR) | i (10-YR) | i (2-YR) |
| 12.89 | 10 | 6.8 | 4.7 |
| $A = 2.97$ (Ac) | | | |
| Q (500-YR)= | 6.89 (cfs) | | |
| Q (100-YR)= | 5.35 (cfs) | | |
| Q (10-YR)= | 3.64 (cfs) | | |
| Q (2-YR)= | 2.51 (cfs) | | |

DA RP4 605 EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 263921.33 cft
 Volume (100-yr) = 1.38*area*43560 = 178535.02 cft
 Volume (10-yr) = 0.70*area*43560 = 90561.24 cft
 Volume (2-yr) = 0.41*area*43560 = 53043.012 cft
 A= 2.97 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

$Q_t = \frac{Q_p}{2} \left[2 - \cos \left(\frac{\pi t_i}{T_p} \right) \right]$ $t_i = 1.25 T_p$

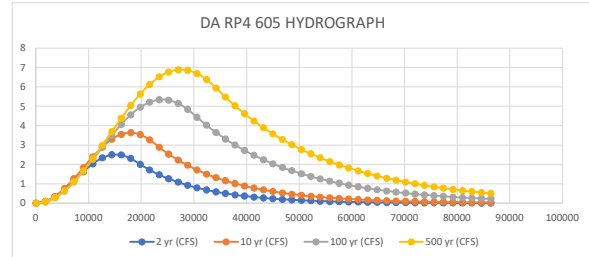
$Q_t = 4.34 Q_p e^{-1.8 t_i / T_p}$ $t_i = 1.25 T_p$

| DA RP4 605 Existing Conditions | | | | |
|--------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 2.51 | 3.64 | 5.35 | 6.89 |
| TP= | 15187.510 | 17922.133 | 24025.899 | 27549.799 |
| 1.25*TP= | 18984.387 | 22402.666 | 30032.374 | 34437.249 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.086082582 | 0.089729907 | 0.073696796 | 0.072337552 |
| 3600.00 | 0.332533541 | 0.350060385 | 0.290723422 | 0.286313197 |
| 5400.00 | 0.70557915 | 0.755288404 | 0.639112676 | 0.632943407 |
| 7200.00 | 1.154097109 | 1.26540486 | 1.099653803 | 1.097675302 |
| 9000.00 | 1.616622358 | 1.830044772 | 1.646951813 | 1.660997635 |
| 10800.00 | 2.029770275 | 2.393459932 | 2.250827798 | 2.29925995 |
| 12600.00 | 2.336922924 | 2.900023055 | 2.877983049 | 2.98566552 |
| 14400.00 | 2.495987998 | 3.299719988 | 3.493835199 | 3.691396378 |
| 16200.00 | 2.485167164 | 3.553087725 | 4.064425154 | 4.386823205 |
| 18000.00 | 2.305943312 | 3.635110683 | 4.55828965 | 5.042749286 |
| 19800.00 | 2.002480444 | 3.537690545 | 4.948196191 | 5.631636301 |
| 21600.00 | 1.716543468 | 3.270445825 | 5.212644693 | 6.12876049 |
| 23400.00 | 1.471435832 | 2.889888338 | 5.337053032 | 6.513250651 |
| 25200.00 | 1.261327456 | 2.536164872 | 5.31456113 | 6.768964396 |
| 27000.00 | 1.081220749 | 2.225737297 | 5.146409226 | 6.885165871 |
| 28800.00 | 0.92683173 | 1.953306178 | 4.841869491 | 6.856976487 |
| 30600.00 | 0.794488134 | 1.714220736 | 4.43048787 | 6.685579744 |
| 32400.00 | 0.681042065 | 1.504399445 | 4.01932834 | 6.378171542 |
| 34200.00 | 0.583795119 | 1.320260363 | 3.646325366 | 5.947658069 |
| 36000.00 | 0.500434199 | 1.158659977 | 3.307937932 | 5.471126027 |
| 37800.00 | 0.428976502 | 1.016839541 | 3.000953635 | 5.025612576 |
| 39600.00 | 0.367722349 | 0.892377982 | 2.722458191 | 4.616377258 |
| 41400.00 | 0.315214761 | 0.783150567 | 2.469807769 | 4.240465946 |
| 43200.00 | 0.270204806 | 0.687292631 | 2.240603891 | 3.895165069 |
| 45000.00 | 0.231621885 | 0.603167743 | 2.032670663 | 3.577982021 |
| 46800.00 | 0.198548273 | 0.529339775 | 1.84403412 | 3.286627168 |
| 48600.00 | 0.170197288 | 0.464548379 | 1.672903485 | 3.018997323 |
| 50400.00 | 0.14589458 | 0.407687475 | 1.51765417 | 2.77316056 |
| 52200.00 | 0.125062089 | 0.357786368 | 1.37681235 | 2.547342269 |
| 54000.00 | 0.107204299 | 0.313993176 | 1.249040977 | 2.339912347 |
| 55800.00 | 0.091896448 | 0.275560288 | 1.133127083 | 2.149373431 |
| 57600.00 | 0.078774426 | 0.241831601 | 1.027970266 | 1.974350087 |
| 59400.00 | 0.067526115 | 0.212231318 | 0.932572246 | 1.813578882 |
| 61200.00 | 0.057883967 | 0.186254122 | 0.846027383 | 1.665899267 |
| 63000.00 | 0.049618635 | 0.163456544 | 0.767514083 | 1.530245194 |
| 64800.00 | 0.042533521 | 0.143449399 | 0.696287 | 1.405637423 |
| 66600.00 | 0.0364601 | 0.125891136 | 0.631669955 | 1.291176456 |
| 68400.00 | 0.031253911 | 0.110482012 | 0.573049521 | 1.186036038 |
| 70200.00 | 0.026791122 | 0.09695897 | 0.519869199 | 1.089457197 |
| 72000.00 | 0.02296558 | 0.085091154 | 0.471624134 | 1.000742766 |
| 73800.00 | 0.019686293 | 0.074675964 | 0.427856322 | 0.919252345 |
| 75600.00 | 0.01687526 | 0.065535596 | 0.388150265 | 0.844397684 |
| 77400.00 | 0.014465618 | 0.057514014 | 0.352129022 | 0.775638433 |
| 79200.00 | 0.012400052 | 0.050474276 | 0.319450634 | 0.712478244 |
| 81000.00 | 0.010629431 | 0.044296205 | 0.289804875 | 0.654461185 |
| 82800.00 | 0.00911164 | 0.038874332 | 0.262910312 | 0.601168452 |
| 84600.00 | 0.007810576 | 0.034116098 | 0.238511627 | 0.552215342 |
| 86400.00 | 0.006695293 | 0.029940275 | 0.216377196 | 0.507248481 |

ti (hrs)

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DA RP4 CVTR 2B EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 2313976.90 cft
 Volume (100-yr) = 1.38*area*43560 = 1565337.31 cft
 Volume (10-yr) = 0.70*area*43560 = 794011.68 cft
 Volume (2-yr) = 0.41*area*43560 = 465063.984 cft
 A= 26.04 Ac

TP = time to Qp in seconds

$$T_p = \frac{V}{1.39 Q_p}$$

$$Q_t = \frac{Q_p}{2} \left[2 - \cos \left(\frac{\pi t}{T_p} \right) \right] \quad t_1 = 1.25 T_p$$

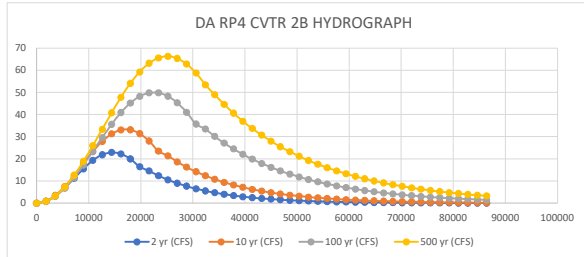
$$Q_t = 4.34 Q_p e^{-1.25 t / T_p} \quad t_1 = 1.25 T_p$$

| DA RP4 CVTR 2B Existing Conditions | | | | |
|------------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 22.92 | 33.33 | 50.00 | 66.32 |
| Tp= | 14600.719 | 17138.040 | 22524.281 | 25100.842 |
| 1.25*Tp= | 18250.899 | 21422.549 | 28155.351 | 31376.052 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.848641684 | 0.899020478 | 0.783687298 | 0.837966189 |
| 3600.00 | 3.268852328 | 3.499087167 | 3.085612785 | 3.309514399 |
| 5400.00 | 6.902111535 | 7.519680528 | 6.761448043 | 7.289733931 |
| 7200.00 | 11.21020272 | 12.52702131 | 11.58072189 | 12.57746666 |
| 9000.00 | 15.55494235 | 17.98087071 | 17.24127069 | 18.90547344 |
| 10800.00 | 19.29271795 | 23.29281639 | 23.38818371 | 25.95394027 |
| 12600.00 | 21.8698303 | 27.88975591 | 29.63605568 | 33.36664147 |
| 14400.00 | 22.90451619 | 31.27572842 | 35.5931513 | 40.76894315 |
| 16200.00 | 22.24350137 | 33.08542349 | 40.88596663 | 47.78673702 |
| 18000.00 | 19.98470595 | 33.12359427 | 45.18264748 | 54.0653476 |
| 19800.00 | 16.46273891 | 31.38612255 | 48.21379627 | 59.28745733 |
| 21600.00 | 14.53387148 | 28.06046303 | 49.78936301 | 63.18914363 |
| 23400.00 | 12.38165342 | 23.50541901 | 49.81056124 | 65.57321739 |
| 25200.00 | 10.54814208 | 21.38802216 | 48.27606185 | 66.31918882 |
| 27000.00 | 8.986142451 | 18.65832977 | 45.28207643 | 65.38935694 |
| 28800.00 | 7.655448279 | 16.27702024 | 41.01632485 | 62.83071494 |
| 30600.00 | 6.52180718 | 14.19963047 | 35.74626545 | 58.7725752 |
| 32400.00 | 5.556038959 | 12.38737205 | 33.44329499 | 53.42003389 |
| 34200.00 | 4.733284512 | 10.80640701 | 30.14332263 | 48.96652052 |
| 36000.00 | 4.032365942 | 9.427216037 | 27.16897062 | 44.60798351 |
| 37800.00 | 3.435241438 | 8.224047284 | 24.48810882 | 40.63740229 |
| 39600.00 | 2.926540871 | 7.174435535 | 22.07177747 | 37.02024469 |
| 41400.00 | 2.493170167 | 6.258782747 | 19.89387437 | 33.72505229 |
| 43200.00 | 2.12397426 | 5.459992118 | 17.93087295 | 30.72316677 |
| 45000.00 | 1.809449959 | 4.763148863 | 16.16156807 | 27.98848075 |
| 46800.00 | 1.541501334 | 4.15524173 | 14.56684698 | 25.49721064 |
| 48600.00 | 1.313231323 | 3.624920054 | 13.12948285 | 23.22768985 |
| 50400.00 | 1.1187642 | 3.162281824 | 11.83394871 | 21.16018036 |
| 52200.00 | 0.953094335 | 2.758688795 | 10.66624966 | 19.27670103 |
| 54000.00 | 0.811957348 | 2.406605195 | 9.613771757 | 17.56087124 |
| 55800.00 | 0.691720336 | 2.099457023 | 8.6651457 | 15.9977684 |
| 57600.00 | 0.589288372 | 1.831509299 | 7.810124048 | 14.57379821 |
| 59400.00 | 0.502024832 | 1.597758979 | 7.039470514 | 13.27657639 |
| 61200.00 | 0.427683532 | 1.393841548 | 6.344860185 | 12.094821 |
| 63000.00 | 0.364350907 | 1.215949518 | 5.718789601 | 11.01825431 |
| 64800.00 | 0.310396763 | 1.060761342 | 5.154495693 | 10.03751341 |
| 66600.00 | 0.264432305 | 0.925379391 | 4.645882731 | 9.144068807 |
| 68400.00 | 0.225274399 | 0.807275853 | 4.187456472 | 8.330150197 |
| 70200.00 | 0.191915109 | 0.704245533 | 3.774264811 | 7.588678932 |
| 72000.00 | 0.16349576 | 0.61436468 | 3.401844283 | 6.913206433 |
| 73800.00 | 0.139284831 | 0.535955065 | 3.066171853 | 6.297858114 |
| 75600.00 | 0.118659127 | 0.467552645 | 2.76362145 | 5.737282289 |
| 77400.00 | 0.101087738 | 0.407880232 | 2.490924804 | 5.226603627 |
| 79200.00 | 0.086118371 | 0.355823639 | 2.245136133 | 4.761380754 |
| 81000.00 | 0.073365711 | 0.31041088 | 2.023600331 | 4.337567627 |
| 82800.00 | 0.062501503 | 0.270794023 | 1.823924278 | 3.951478339 |
| 84600.00 | 0.053246098 | 0.236233353 | 1.643950991 | 3.599755072 |
| 86400.00 | 0.045361261 | 0.206803562 | 1.481736328 | 3.279338887 |

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DA RP4 202A EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 455864.11 cft
 Volume (100-yr) = 1.38*area*43560 = 308378.66 cft
 Volume (10-yr) = 0.70*area*43560 = 156423.96 cft
 Volume (2-yr) = 0.41*area*43560 = 91619.748 cft
 A= 5.13 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

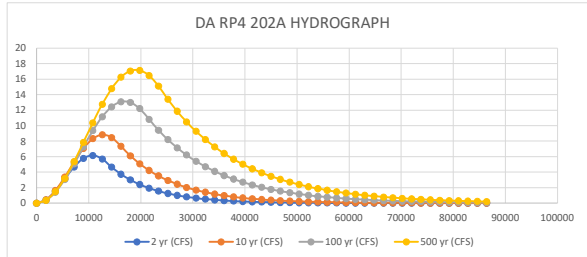
$Q_i = \frac{Q_p}{2} \left[2 - \cos \left(\frac{\pi t_i}{T_p} \right) \right]$ $t_i = 1.25 T_p$

$Q_i = 4.34 Q_p \left(\frac{t_i - T_p}{T_p} \right)^2$ $t_i = 1.25 T_p$

| DA RP4 202A Existing Conditions | | | | |
|---------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 6.16 | 8.82 | 13.13 | 17.19 |
| Tp= | 10707.194 | 12753.890 | 16893.210 | 19079.353 |
| 1.25*Tp= | 13383.993 | 15942.362 | 21116.513 | 23849.191 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.419385753 | 0.426597945 | 0.364467337 | 0.374742449 |
| 3600.00 | 1.563258145 | 1.623892209 | 1.417409905 | 1.466290791 |
| 5400.00 | 3.119905816 | 3.360338627 | 3.041940773 | 3.179457751 |
| 7200.00 | 4.665133927 | 5.300126656 | 5.057721113 | 5.364848485 |
| 9000.00 | 5.777859532 | 7.068121618 | 7.240979578 | 7.831888392 |
| 10800.00 | 6.154858936 | 8.322411814 | 9.349353106 | 10.36544196 |
| 12600.00 | 5.69339778 | 8.820430662 | 11.1487916 | 12.74457344 |
| 14400.00 | 4.650358801 | 8.465866536 | 12.43953977 | 14.76181328 |
| 16200.00 | 3.737435682 | 7.345173106 | 13.07831194 | 16.24125029 |
| 18000.00 | 3.003730696 | 6.113931023 | 12.99419815 | 17.05387179 |
| 19800.00 | 2.414061101 | 5.089077141 | 12.19653584 | 17.12881401 |
| 21600.00 | 1.940150961 | 4.23601543 | 10.81334494 | 16.45954171 |
| 23400.00 | 1.559275261 | 3.525949052 | 9.414620242 | 15.10441803 |
| 25200.00 | 1.253170185 | 2.93490827 | 8.196822984 | 13.39818503 |
| 27000.00 | 1.007157332 | 2.442941298 | 7.136549887 | 11.85172686 |
| 28800.00 | 0.809439855 | 2.033440788 | 6.213424932 | 10.48376547 |
| 30600.00 | 0.65053677 | 1.692583216 | 5.409707772 | 9.273698235 |
| 32400.00 | 0.522828333 | 1.40886224 | 4.709952803 | 8.203300539 |
| 34200.00 | 0.420190646 | 1.172700279 | 4.100712339 | 7.256451313 |
| 36000.00 | 0.33770201 | 0.976125207 | 3.570278172 | 6.418890227 |
| 37800.00 | 0.271406916 | 0.81250123 | 3.108456573 | 5.67800292 |
| 39600.00 | 0.218126372 | 0.676304888 | 2.70637239 | 5.022631019 |
| 41400.00 | 0.175305459 | 0.562938596 | 2.356298485 | 4.442904082 |
| 43200.00 | 0.140890823 | 0.468575444 | 2.051507239 | 3.930090944 |
| 45000.00 | 0.113232207 | 0.39003001 | 1.786141262 | 3.476468216 |
| 46800.00 | 0.09100332 | 0.324650835 | 1.55510083 | 3.075203966 |
| 48600.00 | 0.073138239 | 0.27023091 | 1.353945873 | 2.720254823 |
| 50400.00 | 0.058780296 | 0.22493318 | 1.178810655 | 2.406274961 |
| 52200.00 | 0.047240995 | 0.187228523 | 1.026329477 | 2.128535583 |
| 54000.00 | 0.037967001 | 0.155844156 | 0.893572001 | 1.882853707 |
| 55800.00 | 0.030513608 | 0.129720621 | 0.777986931 | 1.66552916 |
| 57600.00 | 0.024523408 | 0.107976071 | 0.677352989 | 1.473288855 |
| 59400.00 | 0.019709159 | 0.089876473 | 0.589736219 | 1.303237495 |
| 61200.00 | 0.015840007 | 0.074810838 | 0.513452829 | 1.152813966 |
| 63000.00 | 0.012730417 | 0.062270595 | 0.447036826 | 1.019752767 |
| 64800.00 | 0.010231278 | 0.051832424 | 0.389211847 | 0.902049884 |
| 66600.00 | 0.008222751 | 0.043143961 | 0.338866627 | 0.797932617 |
| 68400.00 | 0.006608523 | 0.035911911 | 0.295033649 | 0.705832873 |
| 70200.00 | 0.005311188 | 0.029892141 | 0.256870541 | 0.624363554 |
| 72000.00 | 0.004268536 | 0.02488144 | 0.223643896 | 0.552297665 |
| 73800.00 | 0.003430569 | 0.020710664 | 0.194715175 | 0.488549834 |
| 75600.00 | 0.002757106 | 0.017239018 | 0.169528433 | 0.432159966 |
| 77400.00 | 0.002215852 | 0.01434931 | 0.14759964 | 0.382278784 |
| 79200.00 | 0.001780853 | 0.011943992 | 0.128507374 | 0.338155035 |
| 81000.00 | 0.001431249 | 0.009941868 | 0.111884725 | 0.29912418 |
| 82800.00 | 0.001150277 | 0.008275353 | 0.097412244 | 0.264598382 |
| 84600.00 | 0.000924464 | 0.006888188 | 0.084811803 | 0.234057654 |
| 86400.00 | 0.00074298 | 0.005733549 | 0.073841251 | 0.207042027 |

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DA RP4 CVTR 7 EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 459418.61 cft
 Volume (100-yr) = 1.38*area*43560 = 310783.18 cft
 Volume (10-yr) = 0.70*area*43560 = 157643.64 cft
 Volume (2-yr) = 0.41*area*43560 = 92334.132 cft
 A= 5.17 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

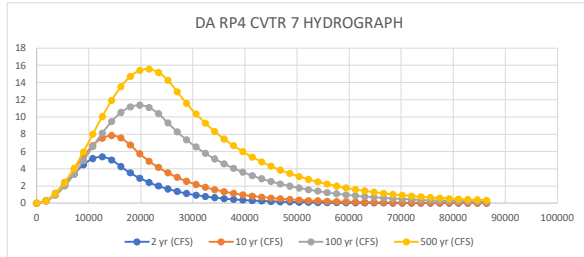
$Q_t = \frac{Q_p}{2} \left[2 - \cos \left(\frac{\pi t_i}{T_p} \right) \right]$ $t_i = 1.25 T_p$

$Q_t = 4.34 Q_p e^{-1.8 t_i / T_p}$ $t_i = 1.25 T_p$

| DA RP4 CVTR 7 Existing Conditions | | | | |
|-----------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 5.38 | 7.86 | 11.37 | 15.57 |
| TP= | 12354.455 | 14432.033 | 19657.554 | 21221.755 |
| 1.25*TP= | 15443.069 | 18040.042 | 24571.942 | 26527.193 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.276736149 | 0.297783296 | 0.233691019 | 0.274829559 |
| 3600.00 | 1.049971754 | 1.145996825 | 0.915558346 | 1.079919457 |
| 5400.00 | 2.160517524 | 2.41607303 | 1.989563202 | 2.358442617 |
| 7200.00 | 3.379740695 | 3.915500725 | 3.367439263 | 4.02015479 |
| 9000.00 | 4.456634629 | 5.417004881 | 4.935946768 | 5.947764422 |
| 10800.00 | 5.169494607 | 6.692995731 | 6.566179047 | 8.005211649 |
| 12600.00 | 5.371561127 | 7.550065578 | 8.124156624 | 10.04727206 |
| 14400.00 | 5.021233896 | 7.858304474 | 9.481838222 | 11.9298073 |
| 16200.00 | 4.24207603 | 7.570991257 | 10.52764375 | 13.51993908 |
| 18000.00 | 3.511046466 | 6.740028943 | 11.17562442 | 14.70542833 |
| 19800.00 | 2.905218986 | 5.731199834 | 11.37252641 | 15.40259757 |
| 21600.00 | 2.403926418 | 4.873369509 | 11.10216747 | 15.56223729 |
| 23400.00 | 1.98913137 | 4.143936881 | 10.38676685 | 15.17307935 |
| 25200.00 | 1.645908785 | 3.523683736 | 9.324725076 | 14.26259237 |
| 27000.00 | 1.361908905 | 2.996268386 | 8.27824736 | 12.92989968 |
| 28800.00 | 1.126912915 | 2.547795124 | 7.349211777 | 11.57998555 |
| 30600.00 | 0.932465243 | 2.166448114 | 6.524438254 | 10.37100586 |
| 32400.00 | 0.771569318 | 1.842180082 | 5.792225863 | 9.288246703 |
| 34200.00 | 0.63843582 | 1.566447603 | 5.142186827 | 8.318530328 |
| 36000.00 | 0.528274372 | 1.331986007 | 4.565099151 | 7.450054787 |
| 37800.00 | 0.437121169 | 1.132617982 | 4.052775785 | 6.672250282 |
| 39600.00 | 0.361696358 | 0.963090819 | 3.597948483 | 5.975650529 |
| 41400.00 | 0.299286021 | 0.818938017 | 3.194164685 | 5.351777547 |
| 43200.00 | 0.247644524 | 0.696361613 | 2.835695975 | 4.793038477 |
| 45000.00 | 0.204913714 | 0.592132111 | 2.517456818 | 4.292633175 |
| 46800.00 | 0.169556062 | 0.503503395 | 2.234932407 | 3.844471448 |
| 48600.00 | 0.140299337 | 0.428140383 | 1.984114614 | 3.443098935 |
| 50400.00 | 0.11609083 | 0.364057501 | 1.761445129 | 3.083630725 |
| 52200.00 | 0.096059475 | 0.309566369 | 1.563764977 | 2.761691902 |
| 54000.00 | 0.079484511 | 0.263231321 | 1.388269701 | 2.473364304 |
| 55800.00 | 0.06576954 | 0.223831576 | 1.232469578 | 2.215138834 |
| 57600.00 | 0.054421073 | 0.190329078 | 1.094154299 | 1.983872755 |
| 59400.00 | 0.045030772 | 0.161841142 | 0.971361608 | 1.776751437 |
| 61200.00 | 0.037260759 | 0.137617202 | 0.862349463 | 1.591254107 |
| 63000.00 | 0.030831453 | 0.117019035 | 0.765571329 | 1.425123166 |
| 64800.00 | 0.025511517 | 0.099503946 | 0.679654229 | 1.276336714 |
| 66600.00 | 0.021109531 | 0.084610467 | 0.603379272 | 1.143083943 |
| 68400.00 | 0.017467103 | 0.071946204 | 0.535664357 | 1.023743097 |
| 70200.00 | 0.014453172 | 0.061177493 | 0.475548825 | 0.916861737 |
| 72000.00 | 0.011959292 | 0.052020613 | 0.422179825 | 0.821139059 |
| 73800.00 | 0.009895728 | 0.04423431 | 0.374800221 | 0.735410071 |
| 75600.00 | 0.008188231 | 0.037613439 | 0.332737847 | 0.658631405 |
| 77400.00 | 0.00677536 | 0.031983562 | 0.295395969 | 0.589868626 |
| 79200.00 | 0.005606278 | 0.02719635 | 0.262244826 | 0.528284854 |
| 81000.00 | 0.004638921 | 0.023125675 | 0.232814106 | 0.473130583 |
| 82800.00 | 0.00383848 | 0.019664287 | 0.206686283 | 0.423734558 |
| 84600.00 | 0.003176154 | 0.01672099 | 0.183490683 | 0.379495601 |
| 86400.00 | 0.002628112 | 0.014218238 | 0.162898236 | 0.339875304 |

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DA RP4 205 DRAINAGE CALCULATIONS

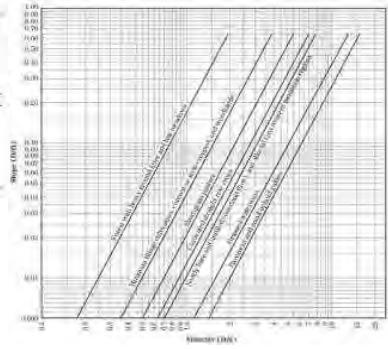
Time of Concentration:

$T_c = T_{cl} + T_1 + \dots + T_n$

Equation 8.8
 $T_{cl} = \frac{L}{V}$
 where:
 T_{cl} = travel time (min)
 L = Maximum length of travel (ft)
 V = Velocity (ft/min)
 V = 4.83 (1.48 P₂^{-0.76} S^{0.48})
 P₂ = Pipe diameter (in)
 S = Slope (ft/ft)

Table 2.3 Manning's Roughness Coefficients for Open Channel Flow

| Surface | n |
|----------------------------------------------|-------|
| Smooth finished concrete (12" dia. pipe and) | 0.012 |
| Cast iron pipe (12" dia. pipe and) | 0.013 |
| Galvanized steel (12" dia. pipe and) | 0.014 |
| Culverts (concrete, 12" dia. pipe and) | 0.015 |
| Concrete pipe (12" dia. pipe and) | 0.016 |
| Stucco pipe (12" dia. pipe and) | 0.017 |
| Asphalt pipe (12" dia. pipe and) | 0.018 |
| Unfinished concrete (12" dia. pipe and) | 0.019 |
| Brick pipe (12" dia. pipe and) | 0.020 |
| Stoneware pipe (12" dia. pipe and) | 0.021 |
| Cast iron pipe (12" dia. pipe and) | 0.022 |
| Galvanized steel (12" dia. pipe and) | 0.023 |
| Concrete pipe (12" dia. pipe and) | 0.024 |
| Stucco pipe (12" dia. pipe and) | 0.025 |
| Asphalt pipe (12" dia. pipe and) | 0.026 |
| Unfinished concrete (12" dia. pipe and) | 0.027 |
| Brick pipe (12" dia. pipe and) | 0.028 |
| Stoneware pipe (12" dia. pipe and) | 0.029 |
| Cast iron pipe (12" dia. pipe and) | 0.030 |
| Galvanized steel (12" dia. pipe and) | 0.031 |
| Concrete pipe (12" dia. pipe and) | 0.032 |
| Stucco pipe (12" dia. pipe and) | 0.033 |
| Asphalt pipe (12" dia. pipe and) | 0.034 |
| Unfinished concrete (12" dia. pipe and) | 0.035 |
| Brick pipe (12" dia. pipe and) | 0.036 |
| Stoneware pipe (12" dia. pipe and) | 0.037 |
| Cast iron pipe (12" dia. pipe and) | 0.038 |
| Galvanized steel (12" dia. pipe and) | 0.039 |
| Concrete pipe (12" dia. pipe and) | 0.040 |
| Stucco pipe (12" dia. pipe and) | 0.041 |
| Asphalt pipe (12" dia. pipe and) | 0.042 |
| Unfinished concrete (12" dia. pipe and) | 0.043 |
| Brick pipe (12" dia. pipe and) | 0.044 |
| Stoneware pipe (12" dia. pipe and) | 0.045 |
| Cast iron pipe (12" dia. pipe and) | 0.046 |
| Galvanized steel (12" dia. pipe and) | 0.047 |
| Concrete pipe (12" dia. pipe and) | 0.048 |
| Stucco pipe (12" dia. pipe and) | 0.049 |
| Asphalt pipe (12" dia. pipe and) | 0.050 |
| Unfinished concrete (12" dia. pipe and) | 0.051 |
| Brick pipe (12" dia. pipe and) | 0.052 |
| Stoneware pipe (12" dia. pipe and) | 0.053 |
| Cast iron pipe (12" dia. pipe and) | 0.054 |
| Galvanized steel (12" dia. pipe and) | 0.055 |
| Concrete pipe (12" dia. pipe and) | 0.056 |
| Stucco pipe (12" dia. pipe and) | 0.057 |
| Asphalt pipe (12" dia. pipe and) | 0.058 |
| Unfinished concrete (12" dia. pipe and) | 0.059 |
| Brick pipe (12" dia. pipe and) | 0.060 |
| Stoneware pipe (12" dia. pipe and) | 0.061 |
| Cast iron pipe (12" dia. pipe and) | 0.062 |
| Galvanized steel (12" dia. pipe and) | 0.063 |
| Concrete pipe (12" dia. pipe and) | 0.064 |
| Stucco pipe (12" dia. pipe and) | 0.065 |
| Asphalt pipe (12" dia. pipe and) | 0.066 |
| Unfinished concrete (12" dia. pipe and) | 0.067 |
| Brick pipe (12" dia. pipe and) | 0.068 |
| Stoneware pipe (12" dia. pipe and) | 0.069 |
| Cast iron pipe (12" dia. pipe and) | 0.070 |
| Galvanized steel (12" dia. pipe and) | 0.071 |
| Concrete pipe (12" dia. pipe and) | 0.072 |
| Stucco pipe (12" dia. pipe and) | 0.073 |
| Asphalt pipe (12" dia. pipe and) | 0.074 |
| Unfinished concrete (12" dia. pipe and) | 0.075 |
| Brick pipe (12" dia. pipe and) | 0.076 |
| Stoneware pipe (12" dia. pipe and) | 0.077 |
| Cast iron pipe (12" dia. pipe and) | 0.078 |
| Galvanized steel (12" dia. pipe and) | 0.079 |
| Concrete pipe (12" dia. pipe and) | 0.080 |
| Stucco pipe (12" dia. pipe and) | 0.081 |
| Asphalt pipe (12" dia. pipe and) | 0.082 |
| Unfinished concrete (12" dia. pipe and) | 0.083 |
| Brick pipe (12" dia. pipe and) | 0.084 |
| Stoneware pipe (12" dia. pipe and) | 0.085 |
| Cast iron pipe (12" dia. pipe and) | 0.086 |
| Galvanized steel (12" dia. pipe and) | 0.087 |
| Concrete pipe (12" dia. pipe and) | 0.088 |
| Stucco pipe (12" dia. pipe and) | 0.089 |
| Asphalt pipe (12" dia. pipe and) | 0.090 |
| Unfinished concrete (12" dia. pipe and) | 0.091 |
| Brick pipe (12" dia. pipe and) | 0.092 |
| Stoneware pipe (12" dia. pipe and) | 0.093 |
| Cast iron pipe (12" dia. pipe and) | 0.094 |
| Galvanized steel (12" dia. pipe and) | 0.095 |
| Concrete pipe (12" dia. pipe and) | 0.096 |
| Stucco pipe (12" dia. pipe and) | 0.097 |
| Asphalt pipe (12" dia. pipe and) | 0.098 |
| Unfinished concrete (12" dia. pipe and) | 0.099 |
| Brick pipe (12" dia. pipe and) | 0.100 |
| Stoneware pipe (12" dia. pipe and) | 0.101 |
| Cast iron pipe (12" dia. pipe and) | 0.102 |
| Galvanized steel (12" dia. pipe and) | 0.103 |
| Concrete pipe (12" dia. pipe and) | 0.104 |
| Stucco pipe (12" dia. pipe and) | 0.105 |
| Asphalt pipe (12" dia. pipe and) | 0.106 |
| Unfinished concrete (12" dia. pipe and) | 0.107 |
| Brick pipe (12" dia. pipe and) | 0.108 |
| Stoneware pipe (12" dia. pipe and) | 0.109 |
| Cast iron pipe (12" dia. pipe and) | 0.110 |
| Galvanized steel (12" dia. pipe and) | 0.111 |
| Concrete pipe (12" dia. pipe and) | 0.112 |
| Stucco pipe (12" dia. pipe and) | 0.113 |
| Asphalt pipe (12" dia. pipe and) | 0.114 |
| Unfinished concrete (12" dia. pipe and) | 0.115 |
| Brick pipe (12" dia. pipe and) | 0.116 |
| Stoneware pipe (12" dia. pipe and) | 0.117 |
| Cast iron pipe (12" dia. pipe and) | 0.118 |
| Galvanized steel (12" dia. pipe and) | 0.119 |
| Concrete pipe (12" dia. pipe and) | 0.120 |
| Stucco pipe (12" dia. pipe and) | 0.121 |
| Asphalt pipe (12" dia. pipe and) | 0.122 |
| Unfinished concrete (12" dia. pipe and) | 0.123 |
| Brick pipe (12" dia. pipe and) | 0.124 |
| Stoneware pipe (12" dia. pipe and) | 0.125 |
| Cast iron pipe (12" dia. pipe and) | 0.126 |
| Galvanized steel (12" dia. pipe and) | 0.127 |
| Concrete pipe (12" dia. pipe and) | 0.128 |
| Stucco pipe (12" dia. pipe and) | 0.129 |
| Asphalt pipe (12" dia. pipe and) | 0.130 |
| Unfinished concrete (12" dia. pipe and) | 0.131 |
| Brick pipe (12" dia. pipe and) | 0.132 |
| Stoneware pipe (12" dia. pipe and) | 0.133 |
| Cast iron pipe (12" dia. pipe and) | 0.134 |
| Galvanized steel (12" dia. pipe and) | 0.135 |
| Concrete pipe (12" dia. pipe and) | 0.136 |
| Stucco pipe (12" dia. pipe and) | 0.137 |
| Asphalt pipe (12" dia. pipe and) | 0.138 |
| Unfinished concrete (12" dia. pipe and) | 0.139 |
| Brick pipe (12" dia. pipe and) | 0.140 |
| Stoneware pipe (12" dia. pipe and) | 0.141 |
| Cast iron pipe (12" dia. pipe and) | 0.142 |
| Galvanized steel (12" dia. pipe and) | 0.143 |
| Concrete pipe (12" dia. pipe and) | 0.144 |
| Stucco pipe (12" dia. pipe and) | 0.145 |
| Asphalt pipe (12" dia. pipe and) | 0.146 |
| Unfinished concrete (12" dia. pipe and) | 0.147 |
| Brick pipe (12" dia. pipe and) | 0.148 |
| Stoneware pipe (12" dia. pipe and) | 0.149 |
| Cast iron pipe (12" dia. pipe and) | 0.150 |



| T_{cl} | T_1 | T_n |
|------------------------|----------------------|-------|
| $n = 0.15$ | $D = 79$ (ft) | |
| $L = 100$ (ft) | $S = 0.0051$ (ft/ft) | |
| $P_2 = 4.89$ (in) | $V = 0.5$ (ft/s) | |
| $S = 0.0051$ (ft/ft) | | |
| $T_{cl} = 13.69$ (min) | $T_1 = 2.63$ (min) | |

$T_c = 16.32$ (min)

Intensity:

SEE FIG. 2.1-2.1a

| | |
|-------------|---------------|
| I (500-YR)= | 11.98 (in/hr) |
| I (100-YR)= | 9.4 (in/hr) |
| I (10-YR)= | 6.3 (in/hr) |
| I (2-YR)= | 4.4 (in/hr) |

Peak Flow Rate:

Q=CIA

C= 0.4 Single family residential districts; lots 1/4-1/2 acre; basin slope <1%

| I (500-YR) | I (100-YR) | I (10-YR) | I (2-YR) |
|------------|------------|-----------|----------|
| 11.98 | 9.4 | 6.3 | 4.4 |

A= 1.08 (Ac)

| | |
|-------------|------------|
| Q (500-YR)= | 5.18 (cfs) |
| Q (100-YR)= | 4.06 (cfs) |
| Q (10-YR)= | 2.72 (cfs) |
| Q (2-YR)= | 1.90 (cfs) |

DA RP4 205 EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 95971.39 cft
 Volume (100-yr) = 1.38*area*43560 = 64921.82 cft
 Volume (10-yr) = 0.70*area*43560 = 32931.36 cft
 Volume (2-yr) = 0.41*area*43560 = 19288.368 cft
 A= 1.08 Ac

TP = time to Qp in seconds

$T_p = \frac{V}{1.39 Q_p}$

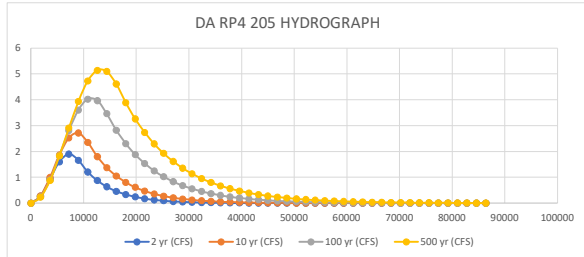
$Q_p = \frac{Q_p}{2} \left[2 - \cos \left(\frac{\pi t_i}{T_p} \right) \right]$
 $t_i = 1.25 T_p$

$Q_p = 4.34 Q_{ps} \left(\frac{t_i}{T_p} \right)^{-1.81}$
 $t_i = 1.25 T_p$

| DA RP4 205 Existing Conditions | | | | |
|--------------------------------|----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 1.90 | 2.72 | 4.06 | 5.18 |
| TP= | 7300.360 | 8705.036 | 11501.760 | 13338.574 |
| 1.25*TP= | 9125.450 | 10881.295 | 14377.200 | 16673.217 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.271149041 | 0.277166969 | 0.240492668 | 0.229123195 |
| 3600.00 | 0.929878566 | 0.995761455 | 0.904999904 | 0.87592507 |
| 5400.00 | 1.600317618 | 1.863057627 | 1.836105319 | 1.825885257 |
| 7200.00 | 1.899913785 | 2.525754704 | 2.813237573 | 2.910807294 |
| 9000.00 | 1.657717544 | 2.71389716 | 3.604921938 | 3.938598867 |
| 10800.00 | 1.205754593 | 2.350843498 | 4.023614792 | 4.727282972 |
| 12600.00 | 0.874961094 | 1.799348886 | 3.970131186 | 5.137218098 |
| 14400.00 | 0.635014143 | 1.375221696 | 3.461414745 | 5.095822635 |
| 16200.00 | 0.460869591 | 1.051066155 | 2.824214497 | 4.610425912 |
| 18000.00 | 0.334481968 | 0.803317796 | 2.304314309 | 3.88704854 |
| 19800.00 | 0.242754542 | 0.613966569 | 1.880120806 | 3.261603978 |
| 21600.00 | 0.176182197 | 0.4692476 | 1.534015663 | 2.736796415 |
| 23400.00 | 0.12786647 | 0.358640554 | 1.251623858 | 2.296432881 |
| 25200.00 | 0.092800717 | 0.274104858 | 1.021216613 | 1.926925929 |
| 27000.00 | 0.067351301 | 0.209495196 | 0.833224267 | 1.6168744 |
| 28800.00 | 0.048881063 | 0.160114773 | 0.679838803 | 1.356711634 |
| 30600.00 | 0.035476053 | 0.122373883 | 0.554689554 | 1.138410292 |
| 32400.00 | 0.025747197 | 0.093528954 | 0.452578612 | 0.955234672 |
| 34200.00 | 0.018686356 | 0.071483106 | 0.369264931 | 0.801532879 |
| 36000.00 | 0.01356186 | 0.054633717 | 0.301288187 | 0.672562434 |
| 37800.00 | 0.009842693 | 0.041755923 | 0.245825053 | 0.564343946 |
| 39600.00 | 0.007143459 | 0.031913572 | 0.200571943 | 0.473538326 |
| 41400.00 | 0.005184456 | 0.024391177 | 0.163649325 | 0.397343761 |
| 43200.00 | 0.003762685 | 0.018641897 | 0.133523669 | 0.33409264 |
| 45000.00 | 0.002730817 | 0.014247788 | 0.108943744 | 0.279762131 |
| 46800.00 | 0.001981925 | 0.01088942 | 0.088888655 | 0.234747076 |
| 48600.00 | 0.001438407 | 0.008322659 | 0.07252544 | 0.196975157 |
| 50400.00 | 0.001043942 | 0.006360913 | 0.059174475 | 0.165280919 |
| 52200.00 | 0.000757654 | 0.004861573 | 0.048281244 | 0.138686435 |
| 54000.00 | 0.000549877 | 0.003715644 | 0.039393312 | 0.116371129 |
| 55800.00 | 0.00039908 | 0.002839824 | 0.032141529 | 0.097646462 |
| 57600.00 | 0.000289638 | 0.002170445 | 0.026224702 | 0.081934683 |
| 59400.00 | 0.000210208 | 0.001658846 | 0.021397085 | 0.068751003 |
| 61200.00 | 0.000152561 | 0.001267837 | 0.017458167 | 0.057688641 |
| 63000.00 | 0.000110723 | 0.000968993 | 0.014244352 | 0.048406264 |
| 64800.00 | 8.03589E-05 | 0.00074059 | 0.011622157 | 0.040617467 |
| 66600.00 | 5.83215E-05 | 0.000566025 | 0.009482673 | 0.034081924 |
| 68400.00 | 4.23275E-05 | 0.000432606 | 0.007737039 | 0.02859798 |
| 70200.00 | 3.07198E-05 | 0.000330636 | 0.006312754 | 0.023996429 |
| 72000.00 | 2.22953E-05 | 0.000252701 | 0.00515066 | 0.02013529 |
| 73800.00 | 1.61811E-05 | 0.000193137 | 0.004202492 | 0.016895426 |
| 75600.00 | 1.17436E-05 | 0.000147612 | 0.003428869 | 0.014176872 |
| 77400.00 | 8.52308E-06 | 0.000112818 | 0.00279766 | 0.011895746 |
| 79200.00 | 6.18573E-06 | 8.62257E-05 | 0.002282648 | 0.009981664 |
| 81000.00 | 4.48937E-06 | 6.59013E-05 | 0.001862443 | 0.008375567 |
| 82800.00 | 3.25822E-06 | 5.03676E-05 | 0.001519592 | 0.007027898 |
| 84600.00 | 2.36469E-06 | 3.84954E-05 | 0.001239856 | 0.005897076 |
| 86400.00 | 1.71621E-06 | 2.94216E-05 | 0.001011615 | 0.004948209 |

ti (hrs)
 0
 0.5
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 3.5
 4
 4.5
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 5.5
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 6.5
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 8.5
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 22.5
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 23.5
 24



DA RP4 CVTR 9 DRAINAGE CALCULATIONS

Time of Concentration:

$T_c = T_{cl} + T_1 + \dots + T_n$

Equation 8.8

$T_{cl} = \frac{1.48 L^{0.77}}{48.3 Q^{0.385}}$

Equation 8.9

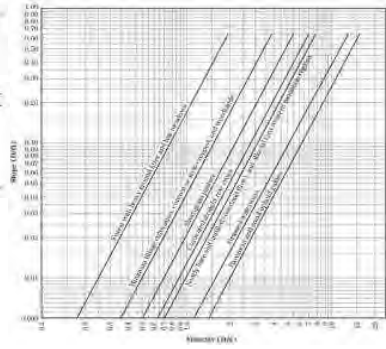
$T_1 = \frac{0.42 S^{0.0044} L^{1.47}}{Q^{0.0149}}$

Equation 8.10

$T_n = \frac{0.42 S^{0.0044} L^{1.47}}{Q^{0.0149}}$

Table 2.6. Manning's Roughness Coefficients for Open Channel Flow

| Surface | n |
|------------------------------------------------------|---------|
| Smooth finished concrete (as per ASTM, 4000 psi and) | 0.012 |
| Cast-in-place concrete | 0.013 |
| Galvanized steel (as per ASTM, 30 ksi) | 0.014 |
| Culverts (as per FHWA, 30 ksi) | 0.015 |
| Grass (as per FHWA, 10-20 ft) | 0.2-0.4 |
| Grass (as per FHWA, 20-40 ft) | 0.3-0.5 |
| Grass (as per FHWA, 40-60 ft) | 0.4-0.6 |
| Grass (as per FHWA, 60-80 ft) | 0.5-0.7 |
| Grass (as per FHWA, 80-100 ft) | 0.6-0.8 |
| Grass (as per FHWA, 100-120 ft) | 0.7-0.9 |
| Grass (as per FHWA, 120-140 ft) | 0.8-1.0 |
| Grass (as per FHWA, 140-160 ft) | 0.9-1.1 |
| Grass (as per FHWA, 160-180 ft) | 1.0-1.2 |
| Grass (as per FHWA, 180-200 ft) | 1.1-1.3 |
| Grass (as per FHWA, 200-220 ft) | 1.2-1.4 |
| Grass (as per FHWA, 220-240 ft) | 1.3-1.5 |
| Grass (as per FHWA, 240-260 ft) | 1.4-1.6 |
| Grass (as per FHWA, 260-280 ft) | 1.5-1.7 |
| Grass (as per FHWA, 280-300 ft) | 1.6-1.8 |



| T_{cl} | T_1 | T_n |
|------------------------|----------------------|-------|
| $n = 0.15$ | $D = 849$ (ft) | |
| $L = 100$ (ft) | $S = 0.0053$ (ft/ft) | |
| $P_2 = 4.89$ (in) | $V = 0.525$ (ft/s) | |
| $S = 0.0053$ (ft/ft) | | |
| $T_{cl} = 13.48$ (min) | $T_1 = 26.95$ (min) | |

$T_c = 40.43$ (min)

Intensity:

SEE FIG. 2.1-2.1a

| | |
|-------------|--------------|
| I (500-YR)= | 7.80 (in/hr) |
| I (100-YR)= | 5.8 (in/hr) |
| I (10-YR)= | 4.7 (in/hr) |
| I (2-YR)= | 2.7 (in/hr) |

Peak Flow Rate:

$Q = CIA$

$C = 0.28$ Mixed use area. Residential lots b/w 1/4 and 1/2 acres; sub-basin slope <1%; and MOSTLY golf course

| I (500-YR) | I (100-YR) | I (10-YR) | I (2-YR) |
|--------------------|--------------------|-----------|----------|
| 7.80 | 5.8 | 4.7 | 2.7 |
| A = 5.95 (Ac) | | | |
| Q (500-YR)= | 13.00 (cfs) | | |
| Q (100-YR)= | 9.66 (cfs) | | |
| Q (10-YR)= | 7.83 (cfs) | | |
| Q (2-YR)= | 4.50 (cfs) | | |

DA RP4 CVTR 9 EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 528731.28 cft
 Volume (100-yr) = 1.38*area*43560 = 357671.16 cft
 Volume (10-yr) = 0.70*area*43560 = 181427.4 cft
 Volume (2-yr) = 0.41*area*43560 = 106264.62 cft
 A= 5.95 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

$$Q_p = \frac{Q_p}{2} \left[2 - \cos \left(\frac{\pi t_i}{T_p} \right) \right] \quad t_i = 1.25 T_p$$

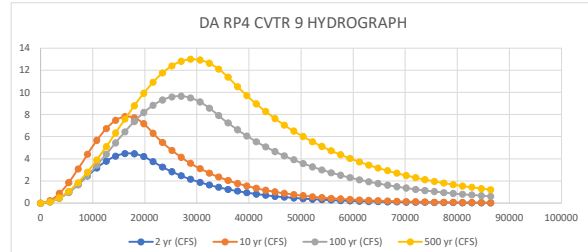
$$Q_p = 4.34 Q_{p^*} \left(\frac{1.25 t_i}{T_p} \right)^{0.5} \quad t_i = 1.25 T_p$$

| DA RP4 CVTR 9 Existing Conditions | | | | |
|-----------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 4.50 | 7.83 | 9.66 | 13.00 |
| TP= | 16995.546 | 16669.218 | 26629.691 | 29261.995 |
| 1.25*TP= | 21244.433 | 20836.522 | 33287.114 | 36577.494 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.123351077 | 0.223130096 | 0.108523276 | 0.120987688 |
| 3600.00 | 0.479874016 | 0.867087074 | 0.429217786 | 0.479446464 |
| 5400.00 | 1.030462074 | 1.85846981 | 0.947676603 | 1.062031158 |
| 7200.00 | 1.714721646 | 3.084276267 | 1.640608402 | 1.847052549 |
| 9000.00 | 2.457596792 | 4.404783642 | 2.47688381 | 2.805284838 |
| 10800.00 | 3.177602077 | 5.669474736 | 3.41893863 | 3.901053706 |
| 12600.00 | 3.79576064 | 6.734194539 | 4.424437761 | 5.093564442 |
| 14400.00 | 4.244267115 | 7.477581638 | 5.448224092 | 6.338420703 |
| 16200.00 | 4.473925152 | 7.814901526 | 6.444300123 | 7.58927736 |
| 18000.00 | 4.459543726 | 7.707705009 | 7.367917984 | 8.799565893 |
| 19800.00 | 4.202700327 | 7.168210815 | 8.177584922 | 9.924228103 |
| 21600.00 | 3.741004372 | 6.304856767 | 8.836927339 | 10.9213936 |
| 23400.00 | 3.259816794 | 5.479104852 | 9.316324834 | 11.75393861 |
| 25200.00 | 2.840522083 | 4.761502297 | 9.594240881 | 12.39086807 |
| 27000.00 | 2.475159254 | 4.137884697 | 9.658190337 | 12.80846952 |
| 28800.00 | 2.156791305 | 3.595942772 | 9.505300327 | 12.99119597 |
| 30600.00 | 1.87937351 | 3.124979396 | 9.142439305 | 12.93224464 |
| 32400.00 | 1.637638645 | 2.715698453 | 8.585908495 | 12.63381023 |
| 34200.00 | 1.426996984 | 2.360021349 | 7.897867857 | 12.10700327 |
| 36000.00 | 1.243449158 | 2.050927547 | 7.233485371 | 11.37143639 |
| 37800.00 | 1.083510214 | 1.782315997 | 6.624991903 | 10.52180755 |
| 39600.00 | 0.944143454 | 1.548884707 | 6.067685973 | 9.713171066 |
| 41400.00 | 0.822702778 | 1.346026091 | 5.557261594 | 8.96668103 |
| 43200.00 | 0.716882437 | 1.169736024 | 5.08975008 | 8.277561277 |
| 45000.00 | 0.624673263 | 1.016534802 | 4.661614214 | 7.641402707 |
| 46800.00 | 0.544324516 | 0.883398461 | 4.269471056 | 7.054135073 |
| 48600.00 | 0.474310645 | 0.767699089 | 3.910315667 | 6.512000943 |
| 50400.00 | 0.413302326 | 0.667152952 | 3.58137306 | 6.011531654 |
| 52200.00 | 0.360141216 | 0.579775419 | 3.280101681 | 5.549525122 |
| 54000.00 | 0.313817966 | 0.503841789 | 3.004173778 | 5.123025353 |
| 55800.00 | 0.273453055 | 0.437853244 | 2.751457415 | 4.729303534 |
| 57600.00 | 0.238280091 | 0.38050727 | 2.519999995 | 4.365840568 |
| 59400.00 | 0.207631258 | 0.330671941 | 2.308013178 | 4.03031096 |
| 61200.00 | 0.180924638 | 0.287363584 | 2.113859064 | 3.720567936 |
| 63000.00 | 0.157653163 | 0.249727356 | 1.936037535 | 3.434629711 |
| 64800.00 | 0.137374987 | 0.217020373 | 1.773174664 | 3.17066805 |
| 66600.00 | 0.119705097 | 0.188597049 | 1.624012104 | 2.926990341 |
| 68400.00 | 0.104308 | 0.163896349 | 1.487397359 | 2.702041238 |
| 70200.00 | 0.090891359 | 0.142430719 | 1.362274886 | 2.494380233 |
| 72000.00 | 0.079200436 | 0.123776458 | 1.247677935 | 2.302678679 |
| 73800.00 | 0.069013261 | 0.107565361 | 1.14272108 | 2.125710037 |
| 75600.00 | 0.060136414 | 0.093477443 | 1.04659338 | 1.962342034 |
| 77400.00 | 0.052401354 | 0.081234631 | 0.958552111 | 1.811529414 |
| 79200.00 | 0.045661217 | 0.070595269 | 0.877917027 | 1.672307254 |
| 81000.00 | 0.039788032 | 0.061349353 | 0.804065108 | 1.543784787 |
| 82800.00 | 0.034670287 | 0.053314381 | 0.736425742 | 1.425139707 |
| 84600.00 | 0.030210813 | 0.046331756 | 0.674476318 | 1.315612902 |
| 86400.00 | 0.02632494 | 0.040263655 | 0.617738188 | 1.214503602 |

ti (hrs)

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DA RP4 402 DRAINAGE CALCULATIONS

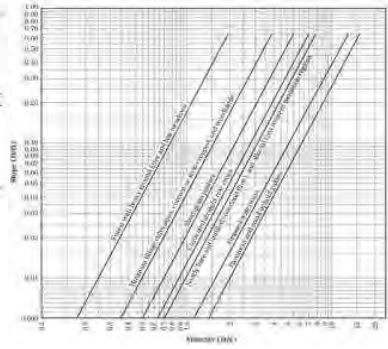
Time of Concentration:

$T_c = T_{cl} + T_1 + \dots + T_n$

$T_{cl} = \frac{1.48 L^{0.76}}{48.3 V^{1.48}}$
 where:
 L = length of pipe (ft)
 V = velocity of flow (ft/s)
 T_{cl} = time of concentration for pipe (min)

Table 2.3. Manning's Roughness Coefficients for Common Channel Flow
 Manning's Roughness Coefficient (n)

| | |
|-----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------|
| Smooth finished concrete (interior, exterior, pipe and) | 0.012 |
| Cast-in-place concrete | 0.013 |
| Galvanized steel (interior, exterior, pipe and) | 0.014 |
| Culverts (concrete, finished, exterior, pipe and) | 0.015 |
| Open channel (concrete) | 0.016 |
| Open channel (stone) | 0.017 |
| Open channel (brick) | 0.018 |
| Open channel (masonry) | 0.019 |
| Open channel (earth) | 0.020 |
| Open channel (grass) | 0.022 |
| Open channel (wood) | 0.024 |
| Open channel (cobble) | 0.026 |
| Open channel (sand) | 0.028 |
| Open channel (silt) | 0.030 |
| Open channel (clay) | 0.032 |
| Open channel (mud) | 0.034 |
| Open channel (ice) | 0.036 |
| Open channel (flood plain) | 0.038 |
| Open channel (flood plain with brush) | 0.040 |
| Open channel (flood plain with trees) | 0.042 |
| Open channel (flood plain with brush and trees) | 0.044 |
| Open channel (flood plain with trees and brush) | 0.046 |
| Open channel (flood plain with trees and brush and trees) | 0.048 |
| Open channel (flood plain with trees and brush and trees and brush) | 0.050 |
| Open channel (flood plain with trees and brush and trees and brush and trees) | 0.052 |
| Open channel (flood plain with trees and brush and trees and brush and trees and brush) | 0.054 |
| Open channel (flood plain with trees and brush and trees and brush and trees and brush and trees) | 0.056 |
| Open channel (flood plain with trees and brush and trees and brush and trees and brush and trees and brush) | 0.058 |
| Open channel (flood plain with trees and brush and trees and brush and trees and brush and trees and brush and trees) | 0.060 |
| Open channel (flood plain with trees and brush and trees and brush and trees and brush and trees and brush and trees and brush) | 0.062 |
| Open channel (flood plain with trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees) | 0.064 |
| Open channel (flood plain with trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush) | 0.066 |
| Open channel (flood plain with trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees) | 0.068 |
| Open channel (flood plain with trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush) | 0.070 |
| Open channel (flood plain with trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees) | 0.072 |
| Open channel (flood plain with trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush) | 0.074 |
| Open channel (flood plain with trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees) | 0.076 |
| Open channel (flood plain with trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush) | 0.078 |
| Open channel (flood plain with trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees) | 0.080 |
| Open channel (flood plain with trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush) | 0.082 |
| Open channel (flood plain with trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees) | 0.084 |
| Open channel (flood plain with trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush) | 0.086 |
| Open channel (flood plain with trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees) | 0.088 |
| Open channel (flood plain with trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush) | 0.090 |
| Open channel (flood plain with trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees) | 0.092 |
| Open channel (flood plain with trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush) | 0.094 |
| Open channel (flood plain with trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees) | 0.096 |
| Open channel (flood plain with trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush) | 0.098 |
| Open channel (flood plain with trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush and trees and brush) | 0.100 |



| | |
|------------------------|----------------------|
| $T_{cl} =$ | $T_1 =$ |
| $n = 0.15$ | $D = 335$ (ft) |
| $L = 100$ (ft) | $S = 0.0040$ (ft/ft) |
| $P_2 = 4.89$ (in) | $V = 0.5$ (ft/s) |
| $S = 0.0040$ (ft/ft) | |
| $T_{cl} = 15.09$ (min) | $T_1 = 11.17$ (min) |

Tc = 26.26 (min)

Intensity:

SEE FIG. 2.1-2.1a

| | |
|-------------|--------------|
| I (500-YR)= | 9.60 (in/hr) |
| I (100-YR)= | 7.3 (in/hr) |
| I (10-YR)= | 5 (in/hr) |
| I (2-YR)= | 3.5 (in/hr) |

Peak Flow Rate:

Q=CIA

C= 0.4 Single family residential districts; lots 1/4-1/2 acre; basin slope <1%

| | | | |
|--------------|------------|-----------|----------|
| I (500-YR) | I (100-YR) | I (10-YR) | I (2-YR) |
| 9.60 | 7.3 | 5 | 3.5 |
| A= 1.08 (Ac) | | | |
| Q (500-YR)= | 4.15 (cfs) | | |
| Q (100-YR)= | 3.15 (cfs) | | |
| Q (10-YR)= | 2.16 (cfs) | | |
| Q (2-YR)= | 1.51 (cfs) | | |

DA RP4 402 EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 95971.39 cft
 Volume (100-yr) = 1.38*area*43560 = 64921.82 cft
 Volume (10-yr) = 0.70*area*43560 = 32931.36 cft
 Volume (2-yr) = 0.41*area*43560 = 19288.368 cft
 A= 1.08 Ac

TP = time to Qp in seconds

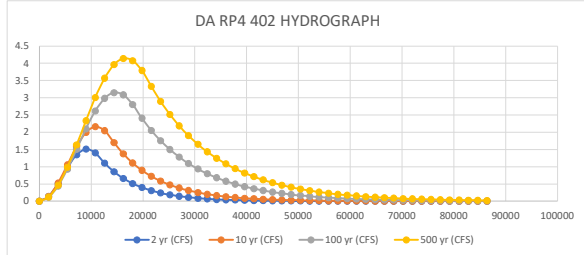
$T_p = \frac{V}{1.39 Q_p}$

$Q_p = \frac{Q_p}{2} \left[1 - \cos \left(\frac{\pi t_i}{T_p} \right) \right]$
 $t_i = 1.25 T_p$
 $Q_p = 4.34 Q_{ps} \left(\frac{t_i}{T_p} \right)^{-1.81}$
 $t_i = 1.25 T_p$

| DA RP4 402 Existing Conditions | | | | |
|--------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 1.51 | 2.16 | 3.15 | 4.15 |
| Tp= | 9177.595 | 10968.345 | 14810.486 | 16650.500 |
| 1.25*Tp= | 11471.994 | 13710.432 | 18513.107 | 20813.125 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.13902565 | 0.140383187 | 0.113545593 | 0.118427208 |
| 3600.00 | 0.504969976 | 0.525037489 | 0.437829502 | 0.460179907 |
| 5400.00 | 0.963241318 | 1.053964765 | 0.926148267 | 0.986216846 |
| 7200.00 | 1.345290812 | 1.589660391 | 1.50817408 | 1.636444454 |
| 9000.00 | 1.510603433 | 1.992860185 | 2.100083417 | 2.336581827 |
| 10800.00 | 1.398378402 | 2.158744753 | 2.616629328 | 3.006646455 |
| 12600.00 | 1.101338581 | 2.044189273 | 2.983418723 | 3.570091286 |
| 14400.00 | 0.853472101 | 1.701062296 | 3.147626488 | 3.962549334 |
| 16200.00 | 0.661390276 | 1.374254953 | 3.085603375 | 4.139186856 |
| 18000.00 | 0.51253825 | 1.110233693 | 2.80628197 | 4.079825079 |
| 19800.00 | 0.397186755 | 0.896936082 | 2.407192586 | 3.791245392 |
| 21600.00 | 0.307796186 | 0.724617115 | 2.055388742 | 3.332572968 |
| 23400.00 | 0.238523795 | 0.585403992 | 1.754999556 | 2.89564635 |
| 25200.00 | 0.184841799 | 0.472936433 | 1.498512073 | 2.516004261 |
| 27000.00 | 0.143241435 | 0.382076093 | 1.279509111 | 2.186136245 |
| 28800.00 | 0.111003619 | 0.308671801 | 1.092512763 | 1.89951653 |
| 30600.00 | 0.086021223 | 0.24936991 | 0.93284536 | 1.650474921 |
| 32400.00 | 0.066661348 | 0.201461072 | 0.79651286 | 1.430484633 |
| 34200.00 | 0.051658592 | 0.162756459 | 0.680104939 | 1.246064819 |
| 36000.00 | 0.040032346 | 0.13148776 | 0.580709679 | 1.082695887 |
| 37800.00 | 0.031022695 | 0.106226389 | 0.495840733 | 0.940745911 |
| 39600.00 | 0.024040749 | 0.085818221 | 0.423375125 | 0.817406698 |
| 41400.00 | 0.018630155 | 0.069330862 | 0.361500144 | 0.710238228 |
| 43200.00 | 0.014437266 | 0.056011047 | 0.308668002 | 0.617120391 |
| 45000.00 | 0.011188025 | 0.04525023 | 0.263557116 | 0.536211037 |
| 46800.00 | 0.008670056 | 0.036556775 | 0.225039049 | 0.465909538 |
| 48600.00 | 0.006718779 | 0.029533504 | 0.192150279 | 0.404825121 |
| 50400.00 | 0.005206656 | 0.02385954 | 0.164068103 | 0.351749353 |
| 52200.00 | 0.004034849 | 0.019275655 | 0.140090051 | 0.305632236 |
| 54000.00 | 0.003126769 | 0.015572425 | 0.119616318 | 0.265561438 |
| 55800.00 | 0.002423061 | 0.012580658 | 0.102134758 | 0.230744238 |
| 57600.00 | 0.001877728 | 0.010163667 | 0.087208075 | 0.200491847 |
| 59400.00 | 0.001455128 | 0.008211028 | 0.074462882 | 0.174205783 |
| 61200.00 | 0.001127638 | 0.006633529 | 0.063580359 | 0.15136603 |
| 63000.00 | 0.000873853 | 0.005359098 | 0.054288284 | 0.131520749 |
| 64800.00 | 0.000677184 | 0.004329511 | 0.046354217 | 0.114277341 |
| 66600.00 | 0.000524777 | 0.003497727 | 0.03957969 | 0.09929468 |
| 68400.00 | 0.000406671 | 0.002825745 | 0.033795239 | 0.086276363 |
| 70200.00 | 0.000315146 | 0.002282864 | 0.028856168 | 0.074964851 |
| 72000.00 | 0.00024422 | 0.001844281 | 0.024638927 | 0.065136368 |
| 73800.00 | 0.000189256 | 0.001489959 | 0.021038023 | 0.056596476 |
| 75600.00 | 0.000146662 | 0.001203709 | 0.01796338 | 0.049176231 |
| 77400.00 | 0.000113654 | 0.000972453 | 0.015338087 | 0.042728839 |
| 79200.00 | 8.80754E-05 | 0.000785625 | 0.013096473 | 0.037126751 |
| 81000.00 | 6.82532E-05 | 0.000634691 | 0.011182463 | 0.032259141 |
| 82800.00 | 5.28922E-05 | 0.000512755 | 0.00954818 | 0.028029713 |
| 84600.00 | 4.09883E-05 | 0.000414245 | 0.008152743 | 0.024354796 |
| 86400.00 | 3.17635E-05 | 0.00033466 | 0.006961244 | 0.02116169 |

ti (hrs)
 0
 0.5
 1
 1.5
 2
 2.5
 3
 3.5
 4
 4.5
 5
 5.5
 6
 6.5
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 7.5
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 17
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 24



DA FE 206E DRAINAGE CALCULATIONS

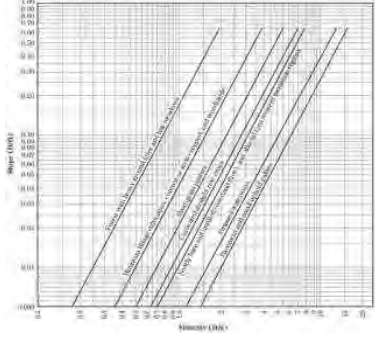
Time of Concentration:

$T_c = T_{c1} + T_1 + \dots + T_n$

Handwritten notes on the left side of the page describe various factors affecting runoff, such as surface material, slope, and vegetation. On the right, a table titled 'Table 2.3 Manning's Roughness Coefficients for Overland Flow' lists values for different materials like concrete, asphalt, grass, and gravel.

| | | |
|-----------------------------------------------------------------------------|----------------------|-------|
| $T_{c1} = T_t = T_o$; multiply by 60 to convert hrs. to min. (L= max 300') | | $T =$ |
| $n =$ 0.011 | $D =$ 475 (ft) | |
| $L =$ 100 (ft) | $S =$ 0.0073 (ft/ft) | |
| $P_2 =$ 4.89 (in) | $V =$ 0.6 (ft/s) | |
| $S =$ 0.0073 (ft/ft) | | |
| $T_{c1} =$ 1.47 (min) | $T_1 =$ 13.19 (min) | |

$T_c = 14.66$ (min)



Intensity:

SEE FIG. 2.1-2.1a

| | |
|----------------|---------------|
| I (500-YR) = | 12.30 (in/hr) |
| I (100-YR) = | 9.7 (in/hr) |
| I (10-YR) = | 6.6 (in/hr) |
| I (2-YR) = | 4.6 (in/hr) |

Peak Flow Rate:

$Q = CIA$

$C =$ 0.4 Single family residential districts; lots 1/4-1/2 acre; basin slope <1%

| | | | |
|--------------|--------------|-------------|------------|
| i (500-YR) | i (100-YR) | i (10-YR) | i (2-YR) |
| 12.30 | 9.7 | 6.6 | 4.6 |

$A =$ 3.92 (Ac)

| | |
|----------------|-------------|
| Q (500-YR) = | 19.29 (cfs) |
| Q (100-YR) = | 15.21 (cfs) |
| Q (10-YR) = | 10.35 (cfs) |
| Q (2-YR) = | 7.21 (cfs) |

DA FE 206E EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 348340.61 cft
 Volume (100-yr) = 1.38*area*43560 = 235642.18 cft
 Volume (10-yr) = 0.70*area*43560 = 119528.64 cft
 Volume (2-yr) = 0.41*area*43560 = 70009.632 cft
 A= 3.92 Ac

TP = time to Qp in seconds

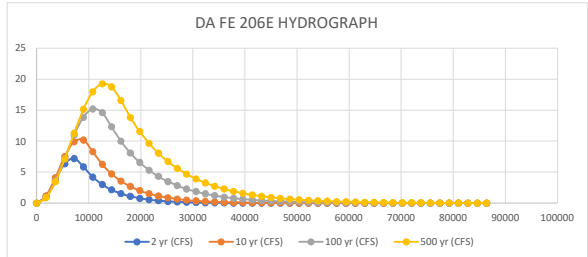
TP = $\frac{V}{1.39 Qp}$

$Q_t = \frac{Q_p}{2} \left[2 - \cos \left(\frac{\pi t_i}{T_p} \right) \right]$
 $t_i = 1.25 T_p$
 $Q_t = 4.34 Q_p \left(\frac{t_i - T_p}{T_p} \right)^2$
 $t_i = 1.25 T_p$

| DA FE 206E Existing Conditions | | | | |
|--------------------------------|----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 7.21 | 10.35 | 15.21 | 19.29 |
| TP= | 6982.953 | 8309.353 | 11146.036 | 12993.859 |
| 1.25*TP= | 8728.691 | 10386.691 | 13932.545 | 16242.323 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 1.119297275 | 1.152693111 | 0.957913101 | 0.898864811 |
| 3600.00 | 3.782409601 | 4.097205109 | 3.590331789 | 3.427888739 |
| 5400.00 | 6.336267787 | 7.521647198 | 7.234088499 | 7.115599531 |
| 7200.00 | 7.195619776 | 9.900304007 | 10.97123607 | 11.27451721 |
| 9000.00 | 5.860427796 | 10.17339612 | 13.8603 | 15.12931724 |
| 10800.00 | 4.191760487 | 8.29027036 | 15.17345782 | 17.96137011 |
| 12600.00 | 2.998220709 | 6.25556953 | 14.5798945 | 19.24271151 |
| 14400.00 | 2.144523153 | 4.720250179 | 12.30837906 | 18.7344679 |
| 16200.00 | 1.533902939 | 3.561747918 | 9.977575673 | 16.55203168 |
| 18000.00 | 1.097147504 | 2.687579631 | 8.088150017 | 13.82424285 |
| 19800.00 | 0.784751509 | 2.027960551 | 6.565519624 | 11.54599592 |
| 21600.00 | 0.561305502 | 1.530233356 | 5.314929804 | 9.64206022 |
| 23400.00 | 0.401482333 | 1.154664533 | 4.308456382 | 8.053997507 |
| 25200.00 | 0.287166371 | 0.871272462 | 3.492576023 | 6.726919 |
| 27000.00 | 0.205400133 | 0.657433984 | 2.83119665 | 5.618127381 |
| 28800.00 | 0.146915582 | 0.496078393 | 2.295060843 | 4.692255233 |
| 30600.00 | 0.105083614 | 0.37432469 | 1.860451577 | 3.918967599 |
| 32400.00 | 0.07516266 | 0.282453288 | 1.508143055 | 3.273118421 |
| 34200.00 | 0.05376124 | 0.213130104 | 1.222550214 | 2.733705735 |
| 36000.00 | 0.038453548 | 0.160821074 | 0.991039292 | 2.283188716 |
| 37800.00 | 0.027504488 | 0.121350374 | 0.803368948 | 1.906917283 |
| 39600.00 | 0.019673005 | 0.091567062 | 0.651237213 | 1.5926557 |
| 41400.00 | 0.014071417 | 0.06909354 | 0.527914239 | 1.330184693 |
| 43200.00 | 0.010064796 | 0.052135748 | 0.427944593 | 1.110969129 |
| 45000.00 | 0.007198999 | 0.039339947 | 0.34690592 | 0.927880476 |
| 46800.00 | 0.005149194 | 0.02968465 | 0.281213314 | 0.774964989 |
| 48600.00 | 0.00368304 | 0.022399075 | 0.227960734 | 0.647250102 |
| 50400.00 | 0.00263435 | 0.016901617 | 0.184792446 | 0.540582738 |
| 52200.00 | 0.001884259 | 0.012753413 | 0.149798816 | 0.451494245 |
| 54000.00 | 0.001347745 | 0.009623312 | 0.121431833 | 0.377087611 |
| 55800.00 | 0.000963995 | 0.00726144 | 0.098436625 | 0.314943254 |
| 57600.00 | 0.000689512 | 0.005479247 | 0.079795956 | 0.263040339 |
| 59400.00 | 0.000493184 | 0.004134463 | 0.064685219 | 0.219691068 |
| 61200.00 | 0.000352758 | 0.003119732 | 0.05243596 | 0.183485794 |
| 63000.00 | 0.000252315 | 0.002354048 | 0.042506308 | 0.15324718 |
| 64800.00 | 0.000180472 | 0.001776289 | 0.034457007 | 0.127991915 |
| 66600.00 | 0.000129086 | 0.00134033 | 0.02793198 | 0.106898739 |
| 68400.00 | 9.23304E-05 | 0.00101137 | 0.022642579 | 0.089281736 |
| 70200.00 | 6.60408E-05 | 0.000763147 | 0.018354817 | 0.074568031 |
| 72000.00 | 4.72367E-05 | 0.000575846 | 0.014879016 | 0.062279156 |
| 73800.00 | 3.37867E-05 | 0.000434515 | 0.012061419 | 0.052015498 |
| 75600.00 | 2.41665E-05 | 0.000327871 | 0.009777381 | 0.0434433 |
| 77400.00 | 1.72854E-05 | 0.000247401 | 0.007925866 | 0.036283808 |
| 79200.00 | 1.23637E-05 | 0.00018668 | 0.006424967 | 0.030304205 |
| 81000.00 | 8.84331E-06 | 0.000140863 | 0.005208289 | 0.025310047 |
| 82800.00 | 6.32531E-06 | 0.000106291 | 0.00422201 | 0.02113893 |
| 84600.00 | 4.52428E-06 | 8.02035E-05 | 0.0034225 | 0.017655216 |
| 86400.00 | 3.23606E-06 | 6.0519E-05 | 0.00277439 | 0.014745622 |

ti (hrs)
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DA RP5 001 DRAINAGE CALCULATIONS

Time of Concentration:

$T_c = T_{c1} + T_1 + \dots + T_n$

Handwritten notes on the left side of the page provide definitions for various terms related to time of concentration, such as T_{c1} , T_1 , and T_n . On the right side, there is a table titled "Table 2.3 Manning's Roughness Coefficients for Open Channel Flow".

| Surface | n |
|------------------------------------------------------------------------------------------------------------------------------------|-------|
| Smooth finished concrete (open, grade, pipe and) | 0.012 |
| Cast-in-place concrete | 0.013 |
| Galvanized steel (open, pipe) | 0.014 |
| Unfinished steel (open, pipe) | 0.015 |
| Cast-in-place concrete (interior) | 0.013 |
| Cast-in-place concrete (exterior) | 0.014 |
| Cast-in-place concrete (interior) with formwork | 0.014 |
| Cast-in-place concrete (exterior) with formwork | 0.015 |
| Cast-in-place concrete (interior) with formwork and rough finish | 0.016 |
| Cast-in-place concrete (exterior) with formwork and rough finish | 0.017 |
| Cast-in-place concrete (interior) with formwork and rough finish and exposed aggregate | 0.018 |
| Cast-in-place concrete (exterior) with formwork and rough finish and exposed aggregate | 0.019 |
| Cast-in-place concrete (interior) with formwork and rough finish and exposed aggregate and aggregate exposed | 0.020 |
| Cast-in-place concrete (exterior) with formwork and rough finish and exposed aggregate and aggregate exposed | 0.021 |
| Cast-in-place concrete (interior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.022 |
| Cast-in-place concrete (exterior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.023 |
| Cast-in-place concrete (interior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.024 |
| Cast-in-place concrete (exterior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.025 |
| Cast-in-place concrete (interior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.026 |
| Cast-in-place concrete (exterior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.027 |
| Cast-in-place concrete (interior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.028 |
| Cast-in-place concrete (exterior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.029 |
| Cast-in-place concrete (interior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.030 |
| Cast-in-place concrete (exterior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.031 |
| Cast-in-place concrete (interior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.032 |
| Cast-in-place concrete (exterior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.033 |
| Cast-in-place concrete (interior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.034 |
| Cast-in-place concrete (exterior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.035 |
| Cast-in-place concrete (interior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.036 |
| Cast-in-place concrete (exterior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.037 |
| Cast-in-place concrete (interior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.038 |
| Cast-in-place concrete (exterior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.039 |
| Cast-in-place concrete (interior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.040 |
| Cast-in-place concrete (exterior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.041 |
| Cast-in-place concrete (interior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.042 |
| Cast-in-place concrete (exterior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.043 |
| Cast-in-place concrete (interior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.044 |
| Cast-in-place concrete (exterior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.045 |
| Cast-in-place concrete (interior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.046 |
| Cast-in-place concrete (exterior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.047 |
| Cast-in-place concrete (interior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.048 |
| Cast-in-place concrete (exterior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.049 |
| Cast-in-place concrete (interior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.050 |
| Cast-in-place concrete (exterior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.051 |
| Cast-in-place concrete (interior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.052 |
| Cast-in-place concrete (exterior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.053 |
| Cast-in-place concrete (interior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.054 |
| Cast-in-place concrete (exterior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.055 |
| Cast-in-place concrete (interior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.056 |
| Cast-in-place concrete (exterior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.057 |
| Cast-in-place concrete (interior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.058 |
| Cast-in-place concrete (exterior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.059 |
| Cast-in-place concrete (interior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.060 |
| Cast-in-place concrete (exterior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.061 |
| Cast-in-place concrete (interior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.062 |
| Cast-in-place concrete (exterior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.063 |
| Cast-in-place concrete (interior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.064 |
| Cast-in-place concrete (exterior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.065 |
| Cast-in-place concrete (interior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.066 |
| Cast-in-place concrete (exterior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.067 |
| Cast-in-place concrete (interior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.068 |
| Cast-in-place concrete (exterior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.069 |
| Cast-in-place concrete (interior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.070 |
| Cast-in-place concrete (exterior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.071 |
| Cast-in-place concrete (interior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.072 |
| Cast-in-place concrete (exterior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.073 |
| Cast-in-place concrete (interior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.074 |
| Cast-in-place concrete (exterior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.075 |
| Cast-in-place concrete (interior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.076 |
| Cast-in-place concrete (exterior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.077 |
| Cast-in-place concrete (interior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.078 |
| Cast-in-place concrete (exterior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.079 |
| Cast-in-place concrete (interior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.080 |
| Cast-in-place concrete (exterior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.081 |
| Cast-in-place concrete (interior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.082 |
| Cast-in-place concrete (exterior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.083 |
| Cast-in-place concrete (interior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.084 |
| Cast-in-place concrete (exterior) with formwork and rough finish and exposed aggregate and aggregate exposed and aggregate exposed | 0.085 |

| | | |
|-----------------------|--------------------------------------------------------------------|-------|
| $T_{c1} =$ | $T_t = T_o$; multiply by 60 to convert hrs. to min. (L= max 300') | $T =$ |
| $n = 0.011$ | $D = 3090$ (ft) | |
| $L = 100$ (ft) | $S = 0.0073$ (ft/ft) | |
| $P_2 = 4.89$ (in) | $V = 0.6$ (ft/s) | |
| $S = 0.0073$ (ft/ft) | | |
| $T_{c1} = 1.47$ (min) | $T_1 = 85.83$ (min) | |

$T_c = 87.30$ (min)

Intensity:

SEE FIG. 2.1-2.1a

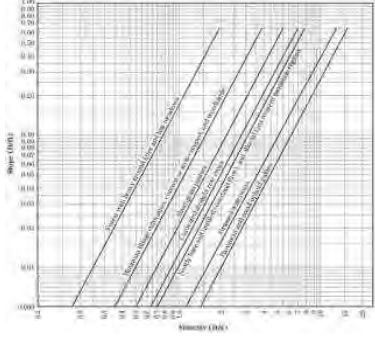
| | |
|----------------|--------------|
| i (500-YR) = | 5.48 (in/hr) |
| i (100-YR) = | 3.9 (in/hr) |
| i (10-YR) = | 2.5 (in/hr) |
| i (2-YR) = | 1.6 (in/hr) |

Peak Flow Rate:

$Q = CIA$

$C = 0.4$ Single family residential districts; lots 1/4-1/2 acre; basin slope <1%

| | | | |
|------------------|--------------|-------------|------------|
| i (500-YR) | i (100-YR) | i (10-YR) | i (2-YR) |
| 5.48 | 3.9 | 2.5 | 1.6 |
| $A = 41.38$ (Ac) | | | |
| Q (500-YR) = | 90.75 (cfs) | | |
| Q (100-YR) = | 64.55 (cfs) | | |
| Q (10-YR) = | 41.38 (cfs) | | |
| Q (2-YR) = | 26.48 (cfs) | | |



DA RPS 001 EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 3677126.11 cft
 Volume (100-yr) = 1.38*area*43560 = 2487467.66 cft
 Volume (10-yr) = 0.70*area*43560 = 1261758.96 cft
 Volume (2-yr) = 0.41*area*43560 = 739030.248 cft
 A= 41.38 Ac

TP = time to Qp in seconds

$$T_p = \frac{V}{1.39 Q_p}$$

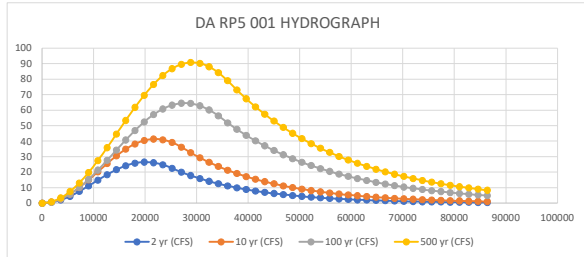
$$Q_p = \frac{Q_p}{2} \left[2 - \cos \left(\frac{\pi t_i}{T_p} \right) \right] \quad t_i = 1.25 T_p$$

$$Q_p = 4.34 Q_{ps} \left(\frac{t_i}{T_p} \right)^{-1.81} \quad t_i = 1.25 T_p$$

| DA RPS 001 Existing Conditions | | | | |
|--------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 26.48 | 41.38 | 64.55 | 90.75 |
| Tp= | 20075.989 | 21936.691 | 27722.191 | 29149.110 |
| 1.25*Tp= | 25094.987 | 27420.863 | 34652.739 | 36436.388 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.521828765 | 0.683638871 | 0.669172863 | 0.851216607 |
| 3600.00 | 2.046186305 | 2.6893779 | 2.648944099 | 3.372931074 |
| 5400.00 | 4.452927983 | 5.88466985 | 5.8572222 | 7.470535464 |
| 7200.00 | 7.552362668 | 10.05835708 | 10.16097544 | 12.9902987 |
| 9000.00 | 11.10020354 | 14.93462569 | 15.38174804 | 19.72513412 |
| 10800.00 | 14.81682194 | 20.1912324 | 21.3030599 | 27.42236884 |
| 12600.00 | 18.40928675 | 25.48079965 | 27.67938294 | 35.79322334 |
| 14400.00 | 21.5944522 | 30.45377176 | 34.24632198 | 44.5236457 |
| 16200.00 | 24.12127447 | 34.78151487 | 40.73157791 | 53.28609399 |
| 18000.00 | 25.79059808 | 38.17803447 | 46.86623863 | 61.75182474 |
| 19800.00 | 26.47085267 | 40.41887498 | 52.39592952 | 69.60322653 |
| 21600.00 | 26.10842291 | 41.35595272 | 57.09136112 | 76.545723592 |
| 23400.00 | 24.73187426 | 40.92734186 | 60.75783668 | 82.31888663 |
| 25200.00 | 22.47907502 | 39.16136672 | 63.24332523 | 86.70609153 |
| 27000.00 | 20.00591004 | 36.17472997 | 64.44476561 | 89.54274859 |
| 28800.00 | 17.80484455 | 32.58794343 | 64.31233994 | 90.72243606 |
| 30600.00 | 15.84594197 | 29.29075052 | 62.85153925 | 90.20089525 |
| 32400.00 | 14.10255934 | 26.32716201 | 60.12293586 | 87.99769297 |
| 34200.00 | 12.550985 | 23.66342436 | 56.3503543 | 84.19548743 |
| 36000.00 | 11.17011606 | 21.26919917 | 51.78909556 | 78.93692714 |
| 37800.00 | 9.941171365 | 19.11721763 | 47.59704624 | 72.98239453 |
| 39600.00 | 8.847436107 | 17.18296994 | 43.74432081 | 67.35258936 |
| 41400.00 | 7.874034436 | 15.44442615 | 40.20345282 | 62.15706299 |
| 43200.00 | 7.007727159 | 13.88178528 | 36.94919909 | 57.36231548 |
| 45000.00 | 6.23673167 | 12.47724977 | 33.95835974 | 52.93743107 |
| 46800.00 | 5.550561693 | 11.21482277 | 31.20961278 | 48.8538788 |
| 48600.00 | 4.939884661 | 10.080126 | 28.68336213 | 45.08532857 |
| 50400.00 | 4.396394781 | 9.060235933 | 26.36159792 | 41.60748138 |
| 52200.00 | 3.912700073 | 8.143536611 | 24.22776805 | 38.39791262 |
| 54000.00 | 3.482221826 | 7.319587374 | 22.26666026 | 35.4359275 |
| 55800.00 | 3.099105123 | 6.579003924 | 20.46429362 | 32.70242761 |
| 57600.00 | 2.758139213 | 5.913351453 | 18.80781889 | 30.17978777 |
| 59400.00 | 2.454686632 | 5.315048571 | 17.2854269 | 27.85174241 |
| 61200.00 | 2.184620136 | 4.777280962 | 15.88626436 | 25.70328065 |
| 63000.00 | 1.944266562 | 4.293923768 | 14.60035653 | 23.72054957 |
| 64800.00 | 1.730356871 | 3.859471835 | 13.41853603 | 21.89076482 |
| 66600.00 | 1.539981688 | 3.468977014 | 12.33237756 | 20.20212824 |
| 68400.00 | 1.370551728 | 3.117991797 | 11.33413778 | 18.64375178 |
| 70200.00 | 1.219762581 | 2.802518669 | 10.41670016 | 17.2058726 |
| 72000.00 | 1.085563371 | 2.518964578 | 9.573524192 | 15.87836164 |
| 73800.00 | 0.966128861 | 2.26410001 | 8.798598792 | 14.65351717 |
| 75600.00 | 0.859834626 | 2.035022207 | 8.086399443 | 13.52315625 |
| 77400.00 | 0.765234965 | 1.829122107 | 7.431848809 | 12.47999049 |
| 79200.00 | 0.68104323 | 1.644054632 | 6.830280536 | 11.51729373 |
| 81000.00 | 0.606114334 | 1.477711969 | 6.277405986 | 10.62885865 |
| 82800.00 | 0.539429173 | 1.328199576 | 5.769283663 | 9.808956754 |
| 84600.00 | 0.480080764 | 1.193814593 | 5.302291115 | 9.052301457 |
| 86400.00 | 0.427261912 | 1.073026455 | 4.873099108 | 8.354013961 |

ti (hrs)
 0
 0.5
 1
 1.5
 2
 2.5
 3
 3.5
 4
 4.5
 5
 5.5
 6
 6.5
 7
 7.5
 8
 8.5
 9
 9.5
 10
 10.5
 11
 11.5
 12
 12.5
 13
 13.5
 14
 14.5
 15
 15.5
 16
 16.5
 17
 17.5
 18
 18.5
 19
 19.5
 20
 20.5
 21
 21.5
 22
 22.5
 23
 23.5
 24



DA RP5 203 DRAINAGE CALCULATIONS

Time of Concentration:

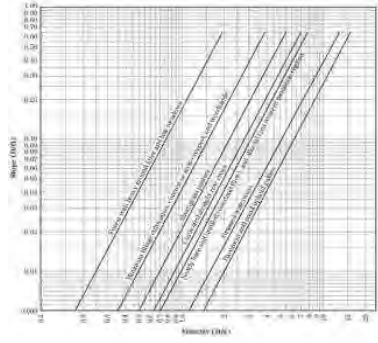
$T_c = T_{c1} + T_1 + \dots + T_n$

Handwritten notes detailing the calculation of time of concentration components. A table lists Manning's roughness coefficients (n) for various materials:

| Material | n |
|-------------------------------------------------------|-------|
| Smooth finished concrete (open, green, clean and dry) | 0.012 |
| Cast-in-place concrete | 0.013 |
| Galvanized steel (open) | 0.014 |
| Unfinished steel (open) | 0.015 |
| Cast-in-place concrete (interior) | 0.012 |
| Smooth finished concrete (interior) | 0.013 |
| Cast-in-place concrete (interior) | 0.014 |
| Cast-in-place concrete (interior) | 0.015 |
| Cast-in-place concrete (interior) | 0.016 |
| Cast-in-place concrete (interior) | 0.017 |
| Cast-in-place concrete (interior) | 0.018 |
| Cast-in-place concrete (interior) | 0.019 |
| Cast-in-place concrete (interior) | 0.020 |
| Cast-in-place concrete (interior) | 0.021 |
| Cast-in-place concrete (interior) | 0.022 |
| Cast-in-place concrete (interior) | 0.023 |
| Cast-in-place concrete (interior) | 0.024 |
| Cast-in-place concrete (interior) | 0.025 |
| Cast-in-place concrete (interior) | 0.026 |
| Cast-in-place concrete (interior) | 0.027 |
| Cast-in-place concrete (interior) | 0.028 |
| Cast-in-place concrete (interior) | 0.029 |
| Cast-in-place concrete (interior) | 0.030 |
| Cast-in-place concrete (interior) | 0.031 |
| Cast-in-place concrete (interior) | 0.032 |
| Cast-in-place concrete (interior) | 0.033 |
| Cast-in-place concrete (interior) | 0.034 |
| Cast-in-place concrete (interior) | 0.035 |
| Cast-in-place concrete (interior) | 0.036 |
| Cast-in-place concrete (interior) | 0.037 |
| Cast-in-place concrete (interior) | 0.038 |
| Cast-in-place concrete (interior) | 0.039 |
| Cast-in-place concrete (interior) | 0.040 |
| Cast-in-place concrete (interior) | 0.041 |
| Cast-in-place concrete (interior) | 0.042 |
| Cast-in-place concrete (interior) | 0.043 |
| Cast-in-place concrete (interior) | 0.044 |
| Cast-in-place concrete (interior) | 0.045 |
| Cast-in-place concrete (interior) | 0.046 |
| Cast-in-place concrete (interior) | 0.047 |
| Cast-in-place concrete (interior) | 0.048 |
| Cast-in-place concrete (interior) | 0.049 |
| Cast-in-place concrete (interior) | 0.050 |
| Cast-in-place concrete (interior) | 0.051 |
| Cast-in-place concrete (interior) | 0.052 |
| Cast-in-place concrete (interior) | 0.053 |
| Cast-in-place concrete (interior) | 0.054 |
| Cast-in-place concrete (interior) | 0.055 |
| Cast-in-place concrete (interior) | 0.056 |
| Cast-in-place concrete (interior) | 0.057 |
| Cast-in-place concrete (interior) | 0.058 |
| Cast-in-place concrete (interior) | 0.059 |
| Cast-in-place concrete (interior) | 0.060 |
| Cast-in-place concrete (interior) | 0.061 |
| Cast-in-place concrete (interior) | 0.062 |
| Cast-in-place concrete (interior) | 0.063 |
| Cast-in-place concrete (interior) | 0.064 |
| Cast-in-place concrete (interior) | 0.065 |
| Cast-in-place concrete (interior) | 0.066 |
| Cast-in-place concrete (interior) | 0.067 |
| Cast-in-place concrete (interior) | 0.068 |
| Cast-in-place concrete (interior) | 0.069 |
| Cast-in-place concrete (interior) | 0.070 |
| Cast-in-place concrete (interior) | 0.071 |
| Cast-in-place concrete (interior) | 0.072 |
| Cast-in-place concrete (interior) | 0.073 |
| Cast-in-place concrete (interior) | 0.074 |
| Cast-in-place concrete (interior) | 0.075 |
| Cast-in-place concrete (interior) | 0.076 |
| Cast-in-place concrete (interior) | 0.077 |
| Cast-in-place concrete (interior) | 0.078 |
| Cast-in-place concrete (interior) | 0.079 |
| Cast-in-place concrete (interior) | 0.080 |
| Cast-in-place concrete (interior) | 0.081 |
| Cast-in-place concrete (interior) | 0.082 |
| Cast-in-place concrete (interior) | 0.083 |
| Cast-in-place concrete (interior) | 0.084 |
| Cast-in-place concrete (interior) | 0.085 |
| Cast-in-place concrete (interior) | 0.086 |
| Cast-in-place concrete (interior) | 0.087 |
| Cast-in-place concrete (interior) | 0.088 |
| Cast-in-place concrete (interior) | 0.089 |
| Cast-in-place concrete (interior) | 0.090 |
| Cast-in-place concrete (interior) | 0.091 |
| Cast-in-place concrete (interior) | 0.092 |
| Cast-in-place concrete (interior) | 0.093 |
| Cast-in-place concrete (interior) | 0.094 |
| Cast-in-place concrete (interior) | 0.095 |
| Cast-in-place concrete (interior) | 0.096 |
| Cast-in-place concrete (interior) | 0.097 |
| Cast-in-place concrete (interior) | 0.098 |
| Cast-in-place concrete (interior) | 0.099 |
| Cast-in-place concrete (interior) | 0.100 |

| $T_{c1} =$ | $T_t = T_o$; multiply by 60 to convert hrs. to min. (L=max 300') | $T =$ |
|------------------------|-------------------------------------------------------------------|----------------------|
| $n = 0.15$ | | $D = 522$ (ft) |
| $L = 100$ (ft) | | $S = 0.0051$ (ft/ft) |
| $P_2 = 4.89$ (in) | | $V = 0.525$ (ft/s) |
| $S = 0.0051$ (ft/ft) | | |
| $T_{c1} = 13.69$ (min) | | $T_1 = 16.57$ (min) |

$T_c = 30.26$ (min)



Intensity:

SEE FIG. 2.1-2.1a

| | |
|----------------|--------------|
| i (500-YR) = | 8.70 (in/hr) |
| i (100-YR) = | 6.8 (in/hr) |
| i (10-YR) = | 4.6 (in/hr) |
| i (2-YR) = | 3.2 (in/hr) |

Peak Flow Rate:

$Q = CIA$

$C = 0.35$ Mixed use area. Residential lots b/w 1/4 and 1/2 acres; sub-basin slope <1%; and golf course

| i (500-YR) | i (100-YR) | i (10-YR) | i (2-YR) |
|----------------------------------|-------------------|-------------|------------|
| 8.70 | 6.8 | 4.6 | 3.2 |
| $A = 1.82$ (Ac) | | | |
| Q (500-YR) = | 5.54 (cfs) | | |
| Q (100-YR) = | 4.33 (cfs) | | |
| Q (10-YR) = | 2.93 (cfs) | | |
| Q (2-YR) = | 2.04 (cfs) | | |

DA RPS 203 EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 161729.57 cft
 Volume (100-yr) = 1.38*area*43560 = 109405.30 cft
 Volume (10-yr) = 0.70*area*43560 = 55495.44 cft
 Volume (2-yr) = 0.41*area*43560 = 32504.472 cft
 A= 1.82 Ac

TP = time to Qp in seconds

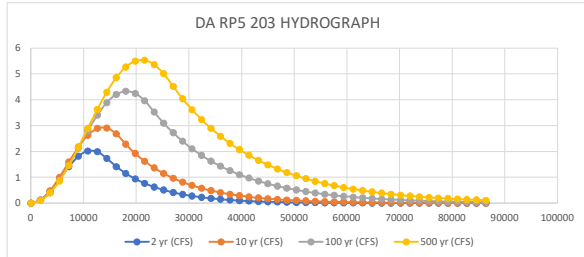
$T_p = \frac{V}{1.39 Q_p}$

$Q_t = \frac{Q_p}{2} \left[2 - \cos \left(\frac{\pi t_i}{T_p} \right) \right]$
 $t_i = 1.25 T_p$
 $Q_t = 4.34 Q_p e^{-1.8 t_i / T_p}$
 $t_i = 1.25 T_p$

| DA RPS 203 Existing Conditions | | | | |
|--------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 2.04 | 2.93 | 4.33 | 5.54 |
| Tp= | 11471.994 | 13625.274 | 18170.848 | 20995.003 |
| 1.25*Tp= | 14339.992 | 17031.592 | 22713.560 | 26243.754 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.121334645 | 0.124379476 | 0.104033881 | 0.099904363 |
| 3600.00 | 0.456449066 | 0.476399544 | 0.40614102 | 0.392413509 |
| 5400.00 | 0.925553254 | 0.996290807 | 0.877298073 | 0.856435077 |
| 7200.00 | 1.416954527 | 1.595781062 | 1.472241124 | 1.458509221 |
| 9000.00 | 1.813651317 | 2.173083014 | 2.133814169 | 2.15521348 |
| 10800.00 | 2.021190987 | 2.630176712 | 2.798460084 | 2.896332673 |
| 12600.00 | 1.990158795 | 2.889452336 | 3.402326533 | 3.628402856 |
| 14400.00 | 1.7302043 | 2.906887543 | 3.887400245 | 4.2986435 |
| 16200.00 | 1.410951768 | 2.679522016 | 4.207080334 | 4.858724635 |
| 18000.00 | 1.150606833 | 2.283132341 | 4.330655228 | 5.268259716 |
| 19800.00 | 0.938300029 | 1.922850392 | 4.246253125 | 5.49771783 |
| 21600.00 | 0.765167492 | 1.619421514 | 3.961982508 | 5.53053123 |
| 23400.00 | 0.623980893 | 1.363874199 | 3.524368474 | 5.364397895 |
| 25200.00 | 0.508845657 | 1.148652661 | 3.098516864 | 5.011233333 |
| 27000.00 | 0.414954858 | 0.967393427 | 2.724112165 | 4.519427673 |
| 28800.00 | 0.33838853 | 0.814737191 | 2.39496393 | 4.042770695 |
| 30600.00 | 0.27595001 | 0.686170354 | 2.105578965 | 3.616385984 |
| 32400.00 | 0.225032474 | 0.577891571 | 1.851160564 | 3.234971402 |
| 34200.00 | 0.183510102 | 0.486699353 | 1.627483694 | 2.893784021 |
| 36000.00 | 0.149649323 | 0.409897414 | 1.430833839 | 2.588581139 |
| 37800.00 | 0.122036442 | 0.345214944 | 1.257945306 | 2.31556753 |
| 39600.00 | 0.099518614 | 0.290739472 | 1.105947001 | 2.071348239 |
| 41400.00 | 0.081155713 | 0.244860316 | 0.972314745 | 1.852886375 |
| 43200.00 | 0.066181085 | 0.206220965 | 0.854829356 | 1.657465343 |
| 45000.00 | 0.053969533 | 0.173678966 | 0.751539799 | 1.482655062 |
| 46800.00 | 0.044011224 | 0.146272146 | 0.660730783 | 1.326281748 |
| 48600.00 | 0.035890394 | 0.123190167 | 0.580894276 | 1.186400883 |
| 50400.00 | 0.029267997 | 0.103750561 | 0.510704464 | 1.061273035 |
| 52200.00 | 0.023867547 | 0.087378556 | 0.448995729 | 0.949342226 |
| 54000.00 | 0.019463573 | 0.073590079 | 0.394743299 | 0.849216584 |
| 55800.00 | 0.015872208 | 0.061977447 | 0.347046224 | 0.759651037 |
| 57600.00 | 0.012943512 | 0.052197306 | 0.305112415 | 0.679531829 |
| 59400.00 | 0.010555211 | 0.043960487 | 0.268245494 | 0.607862668 |
| 61200.00 | 0.008607592 | 0.037023452 | 0.235833226 | 0.543752342 |
| 63000.00 | 0.007019343 | 0.031181092 | 0.207337352 | 0.486403631 |
| 64800.00 | 0.005724153 | 0.026260665 | 0.182284653 | 0.4351034 |
| 66600.00 | 0.004667948 | 0.02211669 | 0.160259086 | 0.389213724 |
| 68400.00 | 0.003806631 | 0.018626641 | 0.140894882 | 0.34816396 |
| 70200.00 | 0.003104242 | 0.015687327 | 0.123870467 | 0.311443651 |
| 72000.00 | 0.002531456 | 0.013211842 | 0.108903122 | 0.278596176 |
| 73800.00 | 0.002064359 | 0.011126992 | 0.095744291 | 0.249213072 |
| 75600.00 | 0.001683449 | 0.009371135 | 0.084175449 | 0.222928959 |
| 77400.00 | 0.001372824 | 0.007892355 | 0.074004478 | 0.19941699 |
| 79200.00 | 0.001119514 | 0.006646928 | 0.065062471 | 0.178384791 |
| 81000.00 | 0.000912944 | 0.005598032 | 0.057200933 | 0.159570826 |
| 82800.00 | 0.00074449 | 0.004714654 | 0.050289309 | 0.14274114 |
| 84600.00 | 0.000607119 | 0.003970674 | 0.044212821 | 0.127686455 |
| 86400.00 | 0.000495095 | 0.003344095 | 0.038870559 | 0.114219564 |

ti (hrs)
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DA FE 20B DRAINAGE CALCULATIONS

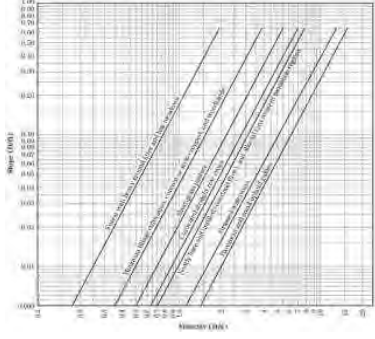
Time of Concentration:

$T_c = T_{c1} + T_1 + \dots + T_n$

The screenshot shows a software interface with various input fields and a table of Manning's roughness coefficients (n) for different materials. The table includes values for concrete, asphalt, grass, etc.

| | | |
|------------------------|-------------------------------------------------------------------|-------|
| $T_{c1} =$ | $T_t = T_o$; multiply by 60 to convert hrs. to min. (L=max 300') | $T =$ |
| $n = 0.15$ | $D = 1004$ (ft) | |
| $L = 100$ (ft) | $S = 0.0051$ (ft/ft) | |
| $P_2 = 4.89$ (in) | $V = 0.525$ (ft/s) | |
| $S = 0.0051$ (ft/ft) | $T_1 = 31.87$ (min) | |
| $T_{c1} = 13.69$ (min) | | |

$T_c = 45.56$ (min)



Intensity:

SEE FIG. 2.1-2.1a

| | |
|---------------|--------------|
| I (500-YR)= | 7.36 (in/hr) |
| I (100-YR)= | 5.4 (in/hr) |
| I (10-YR)= | 3.7 (in/hr) |
| I (2-YR)= | 2.5 (in/hr) |

Peak Flow Rate:

$Q = CIA$

$C = 0.35$ Mixed use area. Residential lots b/w 1/4 and 1/2 acres; sub-basin slope <1%; and golf course

| | | | |
|--------------|--------------|-------------|------------|
| i (500-YR) | i (100-YR) | i (10-YR) | i (2-YR) |
| 7.36 | 5.4 | 3.7 | 2.5 |

$A = 13.63$ (Ac)

| | |
|---------------|-------------|
| Q (500-YR)= | 35.12 (cfs) |
| Q (100-YR)= | 25.76 (cfs) |
| Q (10-YR)= | 17.65 (cfs) |
| Q (2-YR)= | 11.93 (cfs) |

DA FE 206B EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 1211194.51 cft
 Volume (100-yr) = 1.38*area*43560 = 819337.46 cft
 Volume (10-yr) = 0.70*area*43560 = 415605.96 cft
 Volume (2-yr) = 0.41*area*43560 = 243426.348 cft
 A= 13.63 Ac

TP = time to Qp in seconds

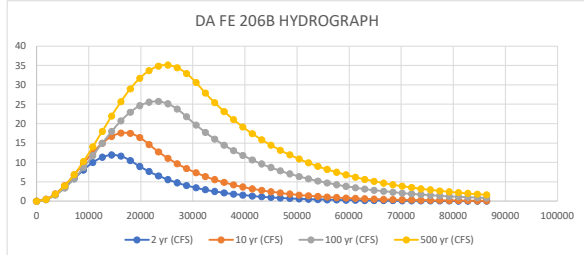
$T_p = \frac{V}{1.39 Q_p}$

$Q_p = \frac{Q_p}{2} \left[1 - \cos \left(\frac{\pi t_i}{T_p} \right) \right]$
 $t_i = 1.25 T_p$
 $Q_p = 4.34 Q_{ps} \left(\frac{t_i}{T_p} \right)^{-1.81}$
 $t_i = 1.25 T_p$

| DA FE 206B Existing Conditions | | | | |
|--------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 11.93 | 17.65 | 25.76 | 35.12 |
| TP= | 14684.152 | 16939.529 | 22881.809 | 24812.466 |
| 1.25*TP= | 18355.190 | 21174.412 | 28602.261 | 31015.583 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.436734044 | 0.487203943 | 0.391336369 | 0.454039313 |
| 3600.00 | 1.682964139 | 1.895023987 | 1.541565974 | 1.792676189 |
| 5400.00 | 3.556144688 | 4.068023884 | 3.380795268 | 3.946681785 |
| 7200.00 | 5.78189549 | 6.766284509 | 5.79726373 | 6.804659711 |
| 9000.00 | 8.034192472 | 9.691893136 | 8.644134978 | 10.218807 |
| 10800.00 | 9.983123125 | 12.52183573 | 11.74841926 | 14.01255786 |
| 12600.00 | 11.34321151 | 14.94366067 | 14.92148517 | 17.98971498 |
| 14400.00 | 11.91523425 | 16.68997626 | 17.97052177 | 21.94459598 |
| 16200.00 | 11.61540248 | 17.56797324 | 20.71025476 | 25.67267056 |
| 18000.00 | 10.48763502 | 17.48071269 | 22.97420465 | 28.98113787 |
| 19800.00 | 8.968388465 | 16.43782897 | 24.62480281 | 31.69889749 |
| 21600.00 | 7.647283823 | 15.5964381 | 25.56175087 | 33.68539796 |
| 23400.00 | 6.520786883 | 12.71597023 | 25.72811532 | 34.83790557 |
| 25200.00 | 5.560230608 | 11.07533177 | 25.11378702 | 35.09681732 |
| 27000.00 | 4.741170807 | 9.646371581 | 23.75609558 | 34.44874337 |
| 28800.00 | 4.042764088 | 8.401778528 | 21.76906975 | 32.92719944 |
| 30600.00 | 3.447237431 | 7.317765217 | 19.65291161 | 30.61087359 |
| 32400.00 | 2.939435902 | 6.373613349 | 17.74246393 | 27.91189551 |
| 34200.00 | 2.506436993 | 5.551277734 | 16.01772971 | 25.39990738 |
| 36000.00 | 2.13722177 | 4.835041412 | 14.46065587 | 23.11399075 |
| 37800.00 | 1.822394462 | 4.211215251 | 13.05494424 | 21.03379987 |
| 39600.00 | 1.553943358 | 3.667876317 | 11.78588099 | 19.14082003 |
| 41400.00 | 1.325036928 | 3.194639998 | 10.64018261 | 17.41820277 |
| 43200.00 | 1.129849973 | 2.78246152 | 9.605856875 | 15.85061598 |
| 45000.00 | 0.963415384 | 2.423463088 | 8.672077323 | 14.42410737 |
| 46800.00 | 0.821497743 | 2.11078331 | 7.829699919 | 13.12598032 |
| 48600.00 | 0.700485536 | 1.838446066 | 7.068010755 | 11.94468087 |
| 50400.00 | 0.597299251 | 1.601246288 | 6.380933694 | 10.86969489 |
| 52200.00 | 0.509313007 | 1.394650472 | 5.760646979 | 9.891454459 |
| 54000.00 | 0.434287736 | 1.214710038 | 5.200657962 | 9.00125278 |
| 55800.00 | 0.370314197 | 1.057985858 | 4.695105139 | 8.191166623 |
| 57600.00 | 0.315764396 | 0.921482527 | 4.238696801 | 7.453985827 |
| 59400.00 | 0.269250152 | 0.802591114 | 3.826655642 | 6.783149124 |
| 61200.00 | 0.229587773 | 0.699039295 | 3.454668756 | 6.172685743 |
| 63000.00 | 0.195767932 | 0.608847927 | 3.118842491 | 5.617162263 |
| 64800.00 | 0.166929983 | 0.530293219 | 2.815661694 | 5.111634254 |
| 66600.00 | 0.142340061 | 0.461873788 | 2.541952919 | 4.651602273 |
| 68400.00 | 0.121372402 | 0.402281961 | 2.29485121 | 4.232971811 |
| 70200.00 | 0.103493421 | 0.350378783 | 2.071770108 | 3.852016854 |
| 72000.00 | 0.088248136 | 0.305172252 | 1.870374586 | 3.505346717 |
| 73800.00 | 0.075248585 | 0.265798353 | 1.688556601 | 3.189875869 |
| 75600.00 | 0.064163956 | 0.231504548 | 1.524413032 | 2.902796465 |
| 77400.00 | 0.054712169 | 0.201635394 | 1.376225761 | 2.641553359 |
| 79200.00 | 0.046652694 | 0.175620016 | 1.242443685 | 2.403821361 |
| 81000.00 | 0.039780435 | 0.15296119 | 1.121666484 | 2.18748454 |
| 82800.00 | 0.033920506 | 0.133225849 | 1.012629962 | 1.990617394 |
| 84600.00 | 0.028923785 | 0.116036799 | 0.914192814 | 1.81146771 |
| 86400.00 | 0.024663115 | 0.101065512 | 0.825324682 | 1.648440968 |

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DA FE 203 W/ WEIR DRAINAGE CALCULATIONS

Time of Concentration:

$$T_c = T_{OL} + T_1 + \dots + T_n$$

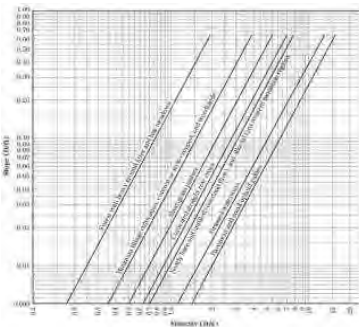
Handwritten calculations for time of concentration components:

- $T_{OL} = 1.49 \cdot L^{0.76} \cdot S^{-0.48}$
- $T_1 = 0.0118 \cdot L^{0.0167} \cdot S^{-0.0141}$
- $T_n = 0.0118 \cdot L^{0.0167} \cdot S^{-0.0141}$
- $T_c = 13.69 + 0.15 + 0.15 = 14.0$ (Note: handwritten result is 13.69)

| Material | n |
|------------------------------------------------------------------|-------------|
| Smooth finished, new metal (cast iron, galvanized, brass, steel) | 0.012 |
| Galvanized iron (old) | 0.014 |
| Cast iron (old) | 0.015 |
| Concrete (new) | 0.012-0.014 |
| Concrete (old) | 0.014-0.016 |
| Brick (new) | 0.015 |
| Brick (old) | 0.016-0.018 |
| Stoneware (new) | 0.014 |
| Stoneware (old) | 0.016 |
| Wood stave (new) | 0.012-0.014 |
| Wood stave (old) | 0.014-0.016 |
| Asbestos-cement | 0.014 |
| Plastic (PVC) | 0.012 |
| Plastic (HDPE) | 0.012 |
| Plastic (LDPE) | 0.012 |
| Plastic (PP) | 0.012 |
| Plastic (PE) | 0.012 |
| Plastic (PS) | 0.012 |
| Plastic (PC) | 0.012 |
| Plastic (PMMA) | 0.012 |
| Plastic (ABS) | 0.012 |
| Plastic (SAN) | 0.012 |
| Plastic (PSU) | 0.012 |
| Plastic (PEI) | 0.012 |
| Plastic (PPS) | 0.012 |
| Plastic (PI) | 0.012 |
| Plastic (PII) | 0.012 |
| Plastic (PIR) | 0.012 |
| Plastic (PIE) | 0.012 |
| Plastic (PIS) | 0.012 |
| Plastic (PIK) | 0.012 |
| Plastic (PIL) | 0.012 |
| Plastic (PIM) | 0.012 |
| Plastic (PIN) | 0.012 |
| Plastic (PIO) | 0.012 |
| Plastic (PIU) | 0.012 |
| Plastic (PIV) | 0.012 |
| Plastic (PIW) | 0.012 |
| Plastic (PIX) | 0.012 |
| Plastic (PIY) | 0.012 |
| Plastic (PIZ) | 0.012 |
| Plastic (PIAA) | 0.012 |
| Plastic (PIAB) | 0.012 |
| Plastic (PIAC) | 0.012 |
| Plastic (PIAD) | 0.012 |
| Plastic (PIAE) | 0.012 |
| Plastic (PIAF) | 0.012 |
| Plastic (PIAG) | 0.012 |
| Plastic (PIAH) | 0.012 |
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| Plastic (PIAL) | 0.012 |
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| Plastic (PIOJ) | 0.012 |
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| Plastic (PIOX) | 0.012 |
| Plastic (PIOY) | 0.012 |
| Plastic (PIOZ) | 0.012 |
| Plastic (PIOA) | 0.012 |
| Plastic (PIOB) | 0.012 |
| Plastic (PIOC) | 0.012 |
| Plastic (PIOD) | 0.012 |
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| Plastic (PIOQ) | 0.012 |
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| Plastic (PIOU) | 0.012 |
| Plastic (PIOV) | 0.012 |
| Plastic (PIOW) | 0.012 |
| Plastic (PIOX) | 0.012 |
| Plastic (PIOY) | 0.012 |
| Plastic (PIOZ) | 0.012 |

| T_{OL} = | T_1 = | T_n = | T_c = |
|-------------|---------|---------|------------|
| 13.69 (min) | 0.15 | 0.15 | 14.0 (min) |

$T_c = 47.88$ (min)



Intensity:

SEE FIG. 2.1-2.1a

| | |
|-------------|--------------|
| I (500-YR)= | 7.16 (in/hr) |
| I (100-YR)= | 5.2 (in/hr) |
| I (10-YR)= | 3.6 (in/hr) |
| I (2-YR)= | 2.4 (in/hr) |

Peak Flow Rate:

Q=CIA

C= 0.35 Mixed use area. Residential lots b/w 1/4 and 1/2 acres; sub-basin slope <1%; and golf course

| i (500-YR) | i (100-YR) | i (10-YR) | i (2-YR) |
|------------|------------|-----------|----------|
| 7.16 | 5.2 | 3.6 | 2.4 |

A= 8.05 (Ac)

| | |
|-------------|-------------|
| Q (500-YR)= | 20.18 (cfs) |
| Q (100-YR)= | 14.65 (cfs) |
| Q (10-YR)= | 10.14 (cfs) |
| Q (2-YR)= | 6.76 (cfs) |

DA FE 203 W/ WEIR EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 715342.32 cft
 Volume (100-yr) = 1.38*area*43560 = 483908.04 cft
 Volume (10-yr) = 0.70*area*43560 = 245460.6 cft
 Volume (2-yr) = 0.41*area*43560 = 143769.78 cft
 A= 8.05 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

$$Q_p = \frac{Q_p}{2} \left[2 - \cos \left(\frac{\pi t_i}{T_p} \right) \right] \quad t_i = 1.25 T_p$$

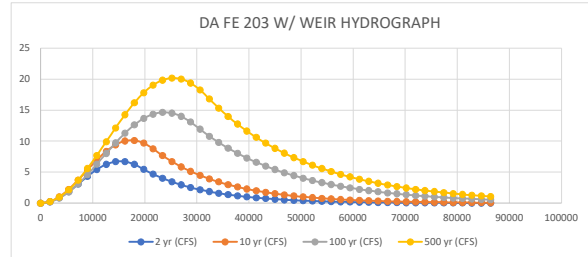
$$Q_p = 4.34 Q_p \left(\frac{t_i - 1.25 T_p}{T_p} \right)^2 \quad t_i = 1.25 T_p$$

| DA FE 203 W/ WEIR Existing Conditions | | | | |
|---------------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 6.76 | 10.14 | 14.65 | 20.18 |
| TP= | 15295.992 | 17410.072 | 23761.878 | 25502.921 |
| 1.25*TP= | 19119.990 | 21762.590 | 29702.348 | 31878.652 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.228429697 | 0.265127572 | 0.206461864 | 0.24702106 |
| 3600.00 | 0.882852106 | 1.032960231 | 0.814209617 | 0.97598888 |
| 5400.00 | 1.874838057 | 2.223072638 | 1.788985737 | 2.151209631 |
| 7200.00 | 3.070344928 | 3.711055423 | 3.075844051 | 3.715138759 |
| 9000.00 | 4.307829229 | 5.341304829 | 4.602246939 | 5.591198644 |
| 10800.00 | 5.420075245 | 6.94339767 | 6.282154136 | 7.687528222 |
| 12600.00 | 6.256790151 | 8.349629633 | 8.020872645 | 9.901480943 |
| 14400.00 | 6.704912408 | 9.413113596 | 9.720394393 | 12.12465086 |
| 16200.00 | 6.703889262 | 10.02257928 | 11.28492075 | 14.24818069 |
| 18000.00 | 6.253858965 | 10.11429266 | 12.62626251 | 16.16809204 |
| 19800.00 | 5.454272578 | 9.678662917 | 13.66881093 | 17.79037666 |
| 21600.00 | 4.680561152 | 8.761245445 | 14.35379965 | 19.03559956 |
| 23400.00 | 4.016603935 | 7.670591244 | 14.64261722 | 19.84278853 |
| 25200.00 | 3.446831832 | 6.705906727 | 14.51898359 | 20.17241966 |
| 27000.00 | 2.957884289 | 5.862544828 | 13.98986772 | 20.0083526 |
| 28800.00 | 2.538296006 | 5.125247526 | 13.08509483 | 19.35862087 |
| 30600.00 | 2.178228078 | 4.480675709 | 11.92065807 | 18.25053851 |
| 32400.00 | 1.869237296 | 3.917167846 | 10.80269678 | 16.79301949 |
| 34200.00 | 1.604078151 | 3.424529006 | 9.789581827 | 15.32076503 |
| 36000.00 | 1.376532942 | 2.993846415 | 8.871480366 | 13.97758402 |
| 37800.00 | 1.181265974 | 2.617328205 | 8.039481693 | 12.75216054 |
| 39600.00 | 1.013698445 | 2.288162445 | 7.285510786 | 11.63417069 |
| 41400.00 | 0.869901072 | 2.0003939 | 6.602249926 | 10.61419571 |
| 43200.00 | 0.746501959 | 1.748816288 | 5.983067676 | 9.683642565 |
| 45000.00 | 0.640607527 | 1.528878093 | 5.421954518 | 8.834671596 |
| 46800.00 | 0.549734664 | 1.336600212 | 4.913464528 | 8.060130441 |
| 48600.00 | 0.471752498 | 1.168503974 | 4.45266252 | 7.35349379 |
| 50400.00 | 0.404832429 | 1.021548198 | 4.035076147 | 6.708808415 |
| 52200.00 | 0.347405252 | 0.893074173 | 3.656652495 | 6.120643007 |
| 54000.00 | 0.298124361 | 0.78075756 | 3.313718746 | 5.584042427 |
| 55800.00 | 0.255834171 | 0.682566338 | 3.002946532 | 5.094485953 |
| 57600.00 | 0.219543021 | 0.59672404 | 2.72131963 | 4.6478492 |
| 59400.00 | 0.188399924 | 0.521677616 | 2.466104691 | 4.240369369 |
| 61200.00 | 0.161674605 | 0.456069333 | 2.234824708 | 3.868613548 |
| 63000.00 | 0.138740384 | 0.398712213 | 2.025234976 | 3.529449792 |
| 64800.00 | 0.119059479 | 0.348568556 | 1.835301307 | 3.20020732 |
| 66600.00 | 0.102170393 | 0.304731167 | 1.663180287 | 2.937719511 |
| 68400.00 | 0.087677095 | 0.266406945 | 1.507201382 | 2.680167814 |
| 70200.00 | 0.075239731 | 0.232902533 | 1.365850729 | 2.445195834 |
| 72000.00 | 0.06456666 | 0.20361177 | 1.237756437 | 2.230823994 |
| 73800.00 | 0.055407609 | 0.178004732 | 1.121675279 | 2.035246267 |
| 75600.00 | 0.047547807 | 0.155618138 | 1.016480621 | 1.85681496 |
| 77400.00 | 0.040802951 | 0.136046973 | 0.921151489 | 1.694026838 |
| 79200.00 | 0.035014882 | 0.118937157 | 0.834762658 | 1.545510451 |
| 81000.00 | 0.030047874 | 0.10397914 | 0.756475676 | 1.410014588 |
| 82800.00 | 0.025785457 | 0.090902303 | 0.685530723 | 1.286397732 |
| 84600.00 | 0.022127682 | 0.079470063 | 0.621239237 | 1.173618442 |
| 86400.00 | 0.018988778 | 0.069475587 | 0.562977234 | 1.070726583 |

ti (hrs)

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DA FE 211 DRAINAGE CALCULATIONS

Time of Concentration:

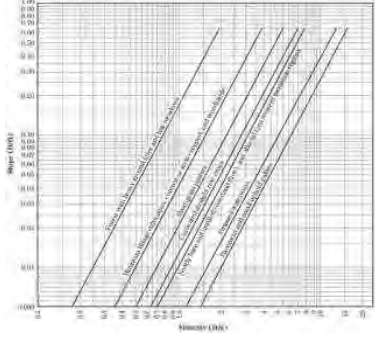
$T_c = T_{c1} + T_1 + \dots + T_n$

Handwritten notes on the left side of the page include:

- Table 2.3 Manning's Roughness Coefficients for Open Channel Flow
- Materials: 0
- Smooth finished concrete (open, pipes and): 0.012
- Cast-in-place concrete: 0.013
- Galvanized steel (open): 0.014
- Unfinished steel: 0.015
- Cast iron pipe: 0.013
- Asphalt: 0.016
- Gravel: 0.020
- Concrete: 0.012
- Earth: 0.022
- Grass: 0.030
- Wood: 0.012
- Ice: 0.010
- Ice: 0.015
- Ice: 0.020
- Ice: 0.025
- Ice: 0.030
- Ice: 0.035
- Ice: 0.040
- Ice: 0.045
- Ice: 0.050
- Ice: 0.055
- Ice: 0.060
- Ice: 0.065
- Ice: 0.070
- Ice: 0.075
- Ice: 0.080
- Ice: 0.085
- Ice: 0.090
- Ice: 0.095
- Ice: 0.100
- Ice: 0.105
- Ice: 0.110
- Ice: 0.115
- Ice: 0.120
- Ice: 0.125
- Ice: 0.130
- Ice: 0.135
- Ice: 0.140
- Ice: 0.145
- Ice: 0.150
- Ice: 0.155
- Ice: 0.160
- Ice: 0.165
- Ice: 0.170
- Ice: 0.175
- Ice: 0.180
- Ice: 0.185
- Ice: 0.190
- Ice: 0.195
- Ice: 0.200
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- Ice: 0.220
- Ice: 0.225
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- Ice: 0.245
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- Ice: 0.255
- Ice: 0.260
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- Ice: 0.270
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- Ice: 0.280
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- Ice: 0.295
- Ice: 0.300
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- Ice: 0.310
- Ice: 0.315
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- Ice: 0.345
- Ice: 0.350
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- Ice: 0.360
- Ice: 0.365
- Ice: 0.370
- Ice: 0.375
- Ice: 0.380
- Ice: 0.385
- Ice: 0.390
- Ice: 0.395
- Ice: 0.400
- Ice: 0.405
- Ice: 0.410
- Ice: 0.415
- Ice: 0.420
- Ice: 0.425
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- Ice: 0.730
- Ice: 0.735
- Ice: 0.740
- Ice: 0.745
- Ice: 0.750
- Ice: 0.755
- Ice: 0.760
- Ice: 0.765
- Ice: 0.770
- Ice: 0.775
- Ice: 0.780
- Ice: 0.785
- Ice: 0.790
- Ice: 0.795
- Ice: 0.800
- Ice: 0.805
- Ice: 0.810
- Ice: 0.815
- Ice: 0.820
- Ice: 0.825
- Ice: 0.830
- Ice: 0.835
- Ice: 0.840
- Ice: 0.845
- Ice: 0.850
- Ice: 0.855
- Ice: 0.860
- Ice: 0.865
- Ice: 0.870
- Ice: 0.875
- Ice: 0.880
- Ice: 0.885
- Ice: 0.890
- Ice: 0.895
- Ice: 0.900
- Ice: 0.905
- Ice: 0.910
- Ice: 0.915
- Ice: 0.920
- Ice: 0.925
- Ice: 0.930
- Ice: 0.935
- Ice: 0.940
- Ice: 0.945
- Ice: 0.950
- Ice: 0.955
- Ice: 0.960
- Ice: 0.965
- Ice: 0.970
- Ice: 0.975
- Ice: 0.980
- Ice: 0.985
- Ice: 0.990
- Ice: 0.995
- Ice: 1.000

| | | |
|------------------------|-------------------------------------------------------------------|-------|
| $T_{c1} =$ | $T_t = T_o$; multiply by 60 to convert hrs. to min. (L=max 300') | $T =$ |
| $n = 0.15$ | $D = 442$ (ft) | |
| $L = 100$ (ft) | $S = 0.0051$ (ft/ft) | |
| $P_2 = 4.89$ (in) | $V = 0.525$ (ft/s) | |
| $S = 0.0051$ (ft/ft) | | |
| $T_{c1} = 13.69$ (min) | $T_1 = 14.03$ (min) | |

$T_c = 27.72$ (min)



Intensity:

SEE FIG. 2.1-2.1a

| | |
|-------------|--------------|
| i (500-YR)= | 9.25 (in/hr) |
| i (100-YR)= | 7.2 (in/hr) |
| i (10-YR)= | 4.9 (in/hr) |
| i (2-YR)= | 3.4 (in/hr) |

Peak Flow Rate:

Q=CIA

C= 0.35 Mixed use area. Residential lots b/w 1/4 and 1/2 acres; sub-basin slope <1%; and golf course

| | | | |
|--------------------|--------------|--------------|-----------|
| i (500-YR) | i (100-YR) | i (10-YR) | i (2-YR) |
| 9.25 | 7.2 | 4.9 | 3.4 |
| A= | | | 4.36 (Ac) |
| Q (500-YR)= | 14.11 | (cfs) | |
| Q (100-YR)= | 10.99 | (cfs) | |
| Q (10-YR)= | 7.48 | (cfs) | |
| Q (2-YR)= | 5.19 | (cfs) | |

DA FE 211 EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 387440.06 cft
 Volume (100-yr) = 1.38*area*43560 = 262091.81 cft
 Volume (10-yr) = 0.70*area*43560 = 132945.12 cft
 Volume (2-yr) = 0.41*area*43560 = 77867.856 cft
 A= 4.36 Ac

TP = time to Qp in seconds

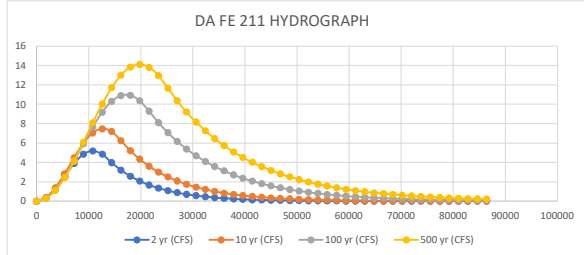
TP = $\frac{V}{1.39 Q_p}$

$Q_t = \frac{Q_p}{2} \left[1 - \cos \left(\frac{\pi t_i}{T_p} \right) \right]$ $t_i = 1.25 T_p$
 $Q_t = 4.34 Q_p e^{-1.8 t_i / T_p}$ $t_i = 1.25 T_p$

| DA FE 211 Existing Conditions | | | | |
|-------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 5.19 | 7.48 | 10.99 | 14.11 |
| Tp= | 10797.171 | 12791.073 | 17161.357 | 19754.113 |
| 1.25*Tp= | 13496.463 | 15988.842 | 21451.696 | 24692.642 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.347734888 | 0.359448236 | 0.295553042 | 0.287100603 |
| 3600.00 | 1.297716554 | 1.368676388 | 1.150410945 | 1.125035784 |
| 5400.00 | 2.595267819 | 2.833624873 | 2.472591818 | 2.445607435 |
| 7200.00 | 3.892532815 | 4.472605861 | 4.119830271 | 4.141336491 |
| 9000.00 | 4.841732423 | 5.970467654 | 5.914885028 | 6.074210468 |
| 10800.00 | 5.188399121 | 7.03919368 | 7.664609919 | 8.086916065 |
| 12600.00 | 4.839596278 | 7.473283799 | 9.180736229 | 10.01564262 |
| 14400.00 | 3.976937973 | 7.189268931 | 10.30013022 | 11.70341438 |
| 16200.00 | 3.202041986 | 6.241760916 | 10.90234618 | 13.0128665 |
| 18000.00 | 2.57813246 | 5.208847696 | 10.92258624 | 13.83742491 |
| 19800.00 | 2.075790077 | 4.338022404 | 10.3586726 | 14.10998021 |
| 21600.00 | 1.671327797 | 3.612783379 | 9.284729185 | 13.8083496 |
| 23400.00 | 1.345673936 | 3.008791225 | 8.10124838 | 12.95708227 |
| 25200.00 | 1.083472881 | 2.505775654 | 7.068620313 | 11.66253118 |
| 27000.00 | 0.872361017 | 2.086855205 | 6.167616494 | 10.35971677 |
| 28800.00 | 0.702383749 | 1.737970692 | 5.381459398 | 9.202438984 |
| 30600.00 | 0.565526108 | 1.447413371 | 4.695510053 | 8.174440009 |
| 32400.00 | 0.455334822 | 1.205431987 | 4.096995449 | 7.261278187 |
| 34200.00 | 0.36661402 | 1.003905523 | 3.574770689 | 6.450125128 |
| 36000.00 | 0.295180235 | 0.836070644 | 3.119111465 | 5.729585494 |
| 37800.00 | 0.237665136 | 0.696294727 | 2.721532982 | 5.089536913 |
| 39600.00 | 0.191356704 | 0.57988682 | 2.37463196 | 4.520987778 |
| 41400.00 | 0.15407135 | 0.482940213 | 2.071948781 | 4.015950927 |
| 43200.00 | 0.124050949 | 0.402201329 | 1.807847205 | 3.567331443 |
| 45000.00 | 0.099879946 | 0.334960528 | 1.577409416 | 3.168826973 |
| 46800.00 | 0.080418599 | 0.278961176 | 1.376344449 | 2.8148392 |
| 48600.00 | 0.064749245 | 0.232323903 | 1.200908289 | 2.500395191 |
| 50400.00 | 0.052133023 | 0.193483541 | 1.047834152 | 2.221077534 |
| 52200.00 | 0.04197504 | 0.161136586 | 0.914271656 | 1.972962286 |
| 54000.00 | 0.033796313 | 0.134197458 | 0.797733744 | 1.752563845 |
| 55800.00 | 0.027211189 | 0.111762066 | 0.696050371 | 1.556785982 |
| 57600.00 | 0.02190916 | 0.093077467 | 0.607328101 | 1.382878348 |
| 59400.00 | 0.017640217 | 0.077516595 | 0.529914841 | 1.228397832 |
| 61200.00 | 0.014203067 | 0.06455722 | 0.462369086 | 1.091174242 |
| 63000.00 | 0.011435637 | 0.053764418 | 0.403433071 | 0.969279818 |
| 64800.00 | 0.009207433 | 0.044775978 | 0.352009353 | 0.861002147 |
| 66600.00 | 0.007413388 | 0.037290243 | 0.307140375 | 0.76482011 |
| 68400.00 | 0.005968909 | 0.031055988 | 0.267990635 | 0.679382512 |
| 70200.00 | 0.004805883 | 0.025863987 | 0.233831127 | 0.603489096 |
| 72000.00 | 0.003869469 | 0.021539995 | 0.204025772 | 0.536073689 |
| 73800.00 | 0.003115513 | 0.017938897 | 0.178019566 | 0.476189217 |
| 75600.00 | 0.002508463 | 0.014939837 | 0.155328248 | 0.422994403 |
| 77400.00 | 0.002019696 | 0.012442166 | 0.135529286 | 0.37574195 |
| 79200.00 | 0.001626163 | 0.010362061 | 0.118254005 | 0.333768041 |
| 81000.00 | 0.00130931 | 0.008629711 | 0.103180722 | 0.296483012 |
| 82800.00 | 0.001054194 | 0.007186979 | 0.090028761 | 0.263363071 |
| 84600.00 | 0.000848787 | 0.005985446 | 0.078553217 | 0.23394294 |
| 86400.00 | 0.000683403 | 0.004984788 | 0.068540408 | 0.207809313 |

ti (hrs)
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DA FE 202Y EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 354560.98 cft
 Volume (100-yr) = 1.38*area*43560 = 239850.07 cft
 Volume (10-yr) = 0.70*area*43560 = 121663.08 cft
 Volume (2-yr) = 0.41*area*43560 = 71259.804 cft
 A= 3.99 Ac

TP = time to Qp in seconds

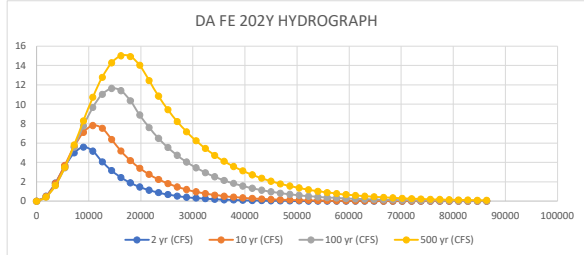
TP = $\frac{V}{1.39 Qp}$

$Qp = \frac{Qp}{2} \left[2 - \cos \left(\frac{\pi t_i}{TP} \right) \right]$ $t_i = 1.25 TP$
 $Qp = 4.34 Qp \left(\frac{-1.8 t_i}{TP} \right)^{0.75}$ $t_i = 1.25 TP$

| DA FE 202Y Existing Conditions | | | | |
|--------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 5.59 | 7.82 | 11.65 | 15.08 |
| TP= | 9177.595 | 11192.189 | 14810.486 | 16918.247 |
| 1.25*TP= | 11471.994 | 13990.236 | 18513.107 | 21147.809 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.513622538 | 0.48856806 | 0.419487884 | 0.417203268 |
| 3600.00 | 1.865583521 | 1.832181939 | 1.617536771 | 1.622635123 |
| 5400.00 | 3.58641537 | 3.695080384 | 3.421603319 | 3.482872905 |
| 7200.00 | 4.970102166 | 5.611735962 | 5.571865351 | 5.792017067 |
| 9000.00 | 5.580840461 | 7.103187651 | 7.758641514 | 8.29448107 |
| 10800.00 | 5.166231319 | 7.796730393 | 9.666991684 | 10.71328086 |
| 12600.00 | 4.068834202 | 7.51905191 | 11.02207473 | 12.78069271 |
| 14400.00 | 3.153105264 | 6.372647548 | 11.62873119 | 14.26788612 |
| 16200.00 | 2.44346963 | 5.170351273 | 11.39959025 | 15.01025177 |
| 18000.00 | 1.893544089 | 4.194886362 | 10.36765283 | 14.92562127 |
| 19800.00 | 1.4673844 | 3.403457649 | 8.893239275 | 14.02336192 |
| 21600.00 | 1.137135908 | 2.761343924 | 7.59351952 | 12.4491099 |
| 23400.00 | 0.881212908 | 2.240374658 | 6.483749837 | 10.83736175 |
| 25200.00 | 0.682887756 | 1.817694118 | 5.536169604 | 9.437464814 |
| 27000.00 | 0.529197522 | 1.474758651 | 4.727075327 | 8.218397078 |
| 28800.00 | 0.410096703 | 1.196523142 | 4.036227708 | 7.15680025 |
| 30600.00 | 0.31780063 | 0.970780967 | 3.446345357 | 6.232333304 |
| 32400.00 | 0.246276646 | 0.787628466 | 2.94267251 | 5.427282732 |
| 34200.00 | 0.190849799 | 0.639030451 | 2.512609912 | 4.726223136 |
| 36000.00 | 0.147897279 | 0.518467699 | 2.145399648 | 4.115721666 |
| 37800.00 | 0.114611622 | 0.420650931 | 1.831856043 | 3.584080639 |
| 39600.00 | 0.088817212 | 0.341288775 | 1.564135878 | 3.121113395 |
| 41400.00 | 0.068828073 | 0.27689949 | 1.335542197 | 2.717949123 |
| 43200.00 | 0.053337676 | 0.224658216 | 1.140356785 | 2.366862878 |
| 45000.00 | 0.041333536 | 0.182273048 | 0.973697124 | 2.061127574 |
| 46800.00 | 0.03203104 | 0.147884483 | 0.831394263 | 1.794885085 |
| 48600.00 | 0.024822157 | 0.11998384 | 0.709888531 | 1.563033996 |
| 50400.00 | 0.0192357 | 0.097347075 | 0.606140491 | 1.361131859 |
| 52200.00 | 0.014906527 | 0.078981078 | 0.51755491 | 1.185310071 |
| 54000.00 | 0.011551675 | 0.064080104 | 0.441915841 | 1.032199751 |
| 55800.00 | 0.008951863 | 0.051990424 | 0.37733119 | 0.898867183 |
| 57600.00 | 0.006937163 | 0.042181645 | 0.32218539 | 0.782757613 |
| 59400.00 | 0.00537589 | 0.03422344 | 0.275098979 | 0.68164629 |
| 61200.00 | 0.004165996 | 0.027766671 | 0.234894104 | 0.593595843 |
| 63000.00 | 0.0032284 | 0.022528069 | 0.200565048 | 0.516919156 |
| 64800.00 | 0.002501819 | 0.018277808 | 0.171253079 | 0.450147043 |
| 66600.00 | 0.001938761 | 0.014829423 | 0.146224964 | 0.392000099 |
| 68400.00 | 0.001502425 | 0.012031628 | 0.124854632 | 0.341364183 |
| 70200.00 | 0.00116429 | 0.00976168 | 0.106607509 | 0.297269072 |
| 72000.00 | 0.000902256 | 0.007919991 | 0.091027147 | 0.258869868 |
| 73800.00 | 0.000699195 | 0.006425765 | 0.077723808 | 0.225430813 |
| 75600.00 | 0.000541835 | 0.005213448 | 0.066364711 | 0.196311189 |
| 77400.00 | 0.00041989 | 0.004229852 | 0.056665711 | 0.17095304 |
| 79200.00 | 0.00032539 | 0.003431826 | 0.04838419 | 0.148870485 |
| 81000.00 | 0.000252158 | 0.00278436 | 0.041312989 | 0.129640405 |
| 82800.00 | 0.000195407 | 0.002259049 | 0.035275222 | 0.112894336 |
| 84600.00 | 0.000151429 | 0.001832845 | 0.030119856 | 0.098311411 |
| 86400.00 | 0.000117348 | 0.001487051 | 0.025717931 | 0.085612209 |

ti (hrs)
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DA FE 201X DRAINAGE CALCULATIONS

Time of Concentration:

$T_c = T_{OL} + T_1 + \dots + T_n$

Equation 5.1

$T_1 = \frac{0.47L^{0.76}}{V}$

$T_2 = \frac{0.0119L^{0.0148}S^{-0.0148}}{V}$

$T_3 = \frac{0.000062L^{0.0148}S^{-0.0148}}{V}$

$T_4 = \frac{0.00000001L^{0.0148}S^{-0.0148}}{V}$

$T_5 = \frac{0.0000000001L^{0.0148}S^{-0.0148}}{V}$

$T_6 = \frac{0.000000000001L^{0.0148}S^{-0.0148}}{V}$

$T_7 = \frac{0.00000000000001L^{0.0148}S^{-0.0148}}{V}$

$T_8 = \frac{0.0000000000000001L^{0.0148}S^{-0.0148}}{V}$

$T_9 = \frac{0.000000000000000001L^{0.0148}S^{-0.0148}}{V}$

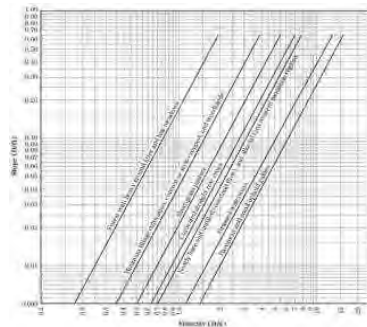
$T_{OL} = \frac{L}{V}$

Table 5.3 Manning's Roughness Coefficients for Overland Flow

| Surface | n |
|----------------------------------------------------------|-------|
| Gravelly Barren, Unimproved (asphalt, gravel, open soil) | 0.015 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.016 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.017 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.018 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.019 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.020 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.021 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.022 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.023 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.024 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.025 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.026 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.027 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.028 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.029 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.030 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.031 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.032 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.033 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.034 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.035 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.036 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.037 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.038 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.039 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.040 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.041 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.042 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.043 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.044 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.045 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.046 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.047 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.048 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.049 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.050 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.051 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.052 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.053 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.054 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.055 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.056 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.057 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.058 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.059 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.060 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.061 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.062 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.063 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.064 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.065 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.066 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.067 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.068 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.069 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.070 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.071 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.072 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.073 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.074 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.075 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.076 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.077 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.078 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.079 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.080 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.081 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.082 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.083 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.084 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.085 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.086 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.087 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.088 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.089 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.090 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.091 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.092 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.093 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.094 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.095 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.096 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.097 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.098 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.099 |
| Gravelly Barren, Improved (asphalt, gravel, open soil) | 0.100 |

| T_{OL} = | T_1 = |
|------------|------------|
| 9.96 (min) | 8.05 (min) |

$T_c = 18.01$ (min)



Intensity:

SEE FIG. 2.1-2.1a

| | |
|-------------|---------------|
| i (500-YR)= | 11.58 (in/hr) |
| i (100-YR)= | 8.8 (in/hr) |
| i (10-YR)= | 6 (in/hr) |
| i (2-YR)= | 4.1 (in/hr) |

Peak Flow Rate:

Q=CIA C= 0.4 Mixed use area. Residential lots b/w 1/4 and 1/2 acres; sub-basin slope 1-3.5%; and golf course

| i (500-YR) | i (100-YR) | i (10-YR) | i (2-YR) |
|--------------------|-------------------|-----------|----------|
| 11.58 | 8.8 | 6 | 4.1 |
| A= 1.27 (Ac) | | | |
| Q (500-YR)= | 5.88 (cfs) | | |
| Q (100-YR)= | 4.47 (cfs) | | |
| Q (10-YR)= | 3.05 (cfs) | | |
| Q (2-YR)= | 2.08 (cfs) | | |

DA FE 201X EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 112855.25 cft
 Volume (100-yr) = 1.38*area*43560 = 76343.26 cft
 Volume (10-yr) = 0.70*area*43560 = 38724.84 cft
 Volume (2-yr) = 0.41*area*43560 = 22681.692 cft
 A= 1.27 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Qp}$

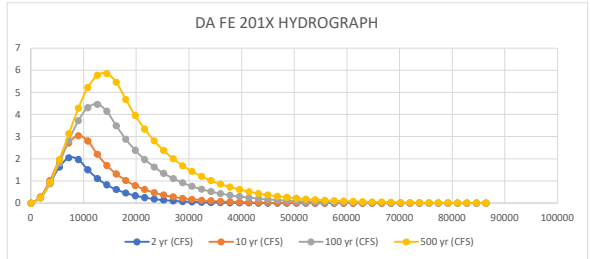
$Qp = \frac{Qp}{2} \left[2 - \cos\left(\frac{\pi t_i}{TP}\right) \right]$ $t_i = 1.25 TP$

$Qp = 4.34 Qp^{0.8} \left(\frac{t_i}{TP} \right)^{0.5}$ $t_i = 1.25 TP$

| DA FE 201X Existing Conditions | | | | |
|--------------------------------|----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 2.08 | 3.05 | 4.47 | 5.88 |
| TP= | 7834.532 | 9140.288 | 12285.971 | 13803.797 |
| 1.25*TP= | 9793.165 | 11425.360 | 15357.464 | 17254.746 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|--------------|--------------|--------------|
| 0 | 0 | 0.000000000 | 0 | 0 |
| 1800.00 | 0.259698143 | 0.2824769634 | 0.232611681 | 0.243340211 |
| 3600.00 | 0.909268614 | 1.0251923224 | 0.882032092 | 0.933091055 |
| 5400.00 | 1.624739364 | 1.9528180201 | 1.813094112 | 1.955107318 |
| 7200.00 | 2.049270706 | 2.7214788724 | 2.832011143 | 3.140257979 |
| 9000.00 | 1.971128434 | 3.0462287068 | 3.726710884 | 4.292415294 |
| 10800.00 | 1.506096757 | 2.8066812409 | 4.310974999 | 5.220911511 |
| 12600.00 | 1.117220259 | 2.2040440340 | 4.463197676 | 5.772092016 |
| 14400.00 | 0.828752271 | 1.7062268722 | 4.151696045 | 5.854743268 |
| 16200.00 | 0.614767161 | 1.3208493545 | 3.494541014 | 5.455187511 |
| 18000.00 | 0.456033335 | 1.0225152619 | 2.888510316 | 4.685849117 |
| 19800.00 | 0.338284827 | 0.7915645016 | 2.387578744 | 3.955189689 |
| 21600.00 | 0.250939165 | 0.6127775139 | 1.973519785 | 3.338461203 |
| 23400.00 | 0.186146287 | 0.4743723105 | 1.631267807 | 2.817898528 |
| 25200.00 | 0.138083029 | 0.3672280459 | 1.348369892 | 2.378506632 |
| 27000.00 | 0.102429779 | 0.2842839573 | 1.114532731 | 2.007628644 |
| 28800.00 | 0.075982253 | 0.2200740638 | 0.921248106 | 1.694581262 |
| 30600.00 | 0.056363518 | 0.1703669599 | 0.76148331 | 1.430347024 |
| 32400.00 | 0.041810371 | 0.1318869681 | 0.629425263 | 1.207314546 |
| 34200.00 | 0.031014869 | 0.1020982728 | 0.520269002 | 1.019059284 |
| 36000.00 | 0.023006782 | 0.0790378114 | 0.43004285 | 0.860158462 |
| 37800.00 | 0.017066396 | 0.0611859090 | 0.355463909 | 0.726034876 |
| 39600.00 | 0.012659826 | 0.0473661327 | 0.293818606 | 0.612825036 |
| 41400.00 | 0.00939104 | 0.0366677649 | 0.242863961 | 0.517267886 |
| 43200.00 | 0.006966259 | 0.0283857876 | 0.200745979 | 0.436610859 |
| 45000.00 | 0.00516756 | 0.0219744219 | 0.165932187 | 0.368530596 |
| 46800.00 | 0.003833288 | 0.0170111616 | 0.137155876 | 0.311066015 |
| 48600.00 | 0.002843527 | 0.0131689297 | 0.113370013 | 0.262561825 |
| 50400.00 | 0.002109324 | 0.0101945249 | 0.093709146 | 0.221620841 |
| 52200.00 | 0.001564693 | 0.0078919350 | 0.077457907 | 0.187063741 |
| 54000.00 | 0.001160687 | 0.0061094204 | 0.064024993 | 0.157895093 |
| 55800.00 | 0.000860996 | 0.0047295141 | 0.052921643 | 0.13327468 |
| 57600.00 | 0.000638685 | 0.0036612808 | 0.04374386 | 0.112493302 |
| 59400.00 | 0.000473776 | 0.0028343243 | 0.036157707 | 0.094952342 |
| 61200.00 | 0.000351446 | 0.0021941487 | 0.029887161 | 0.080146525 |
| 63000.00 | 0.000260702 | 0.0016985665 | 0.024704066 | 0.067649364 |
| 64800.00 | 0.000193389 | 0.0013149192 | 0.020419835 | 0.057100871 |
| 66600.00 | 0.000143455 | 0.0010179245 | 0.016878584 | 0.048197193 |
| 68400.00 | 0.000106415 | 0.0007880107 | 0.013951464 | 0.040681857 |
| 70200.00 | 7.89384E-05 | 0.0006100264 | 0.011531972 | 0.034338378 |
| 72000.00 | 5.85564E-05 | 0.0004722426 | 0.009532073 | 0.028984032 |
| 73800.00 | 4.34371E-05 | 0.0003655793 | 0.007879001 | 0.024464583 |
| 75600.00 | 3.22215E-05 | 0.0002830076 | 0.006512608 | 0.020649847 |
| 77400.00 | 2.39019E-05 | 0.0002190860 | 0.005383177 | 0.017429938 |
| 79200.00 | 1.77304E-05 | 0.0001696021 | 0.004449615 | 0.014712107 |
| 81000.00 | 1.31524E-05 | 0.0001312948 | 0.003677954 | 0.012418064 |
| 82800.00 | 9.75641E-06 | 0.0001016399 | 0.003040115 | 0.010481728 |
| 84600.00 | 7.23729E-06 | 0.0000786830 | 0.002512892 | 0.008847324 |
| 86400.00 | 5.36861E-06 | 0.0000609112 | 0.002077101 | 0.00746777 |

ti (hrs)
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DA FV 311A EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 120852.86 cft
 Volume (100-yr) = 1.38*area*43560 = 81753.41 cft
 Volume (10-yr) = 0.70*area*43560 = 41469.12 cft
 Volume (2-yr) = 0.41*area*43560 = 24289.056 cft
 A= 1.36 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

$Q_t = \frac{Q_p}{2} \left[1 - \cos \left(\frac{\pi t}{T_p} \right) \right]$ $t_1 = 1.25 T_p$

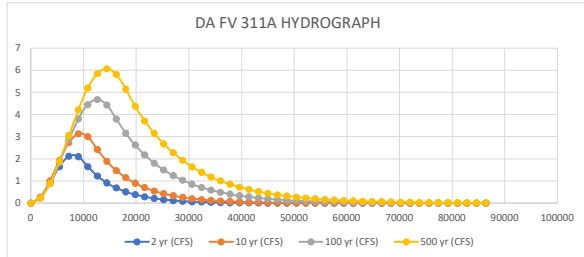
$Q_t = 4.34 Q_p e^{-1.8 t / T_p}$ $t_1 = 1.25 T_p$

| DA FV 311A Existing Conditions | | | | |
|--------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 2.18 | 3.16 | 4.68 | 6.07 |
| TP= | 8030.396 | 9455.470 | 12571.691 | 14334.385 |
| 1.25*TP= | 10037.995 | 11819.338 | 15714.614 | 17917.981 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0.000000000 | 0 | 0 |
| 1800.00 | 0.258790755 | 0.273818139 | 0.23268039 | 0.232943208 |
| 3600.00 | 0.912051523 | 1.000221372 | 0.88443209 | 0.895988163 |
| 5400.00 | 1.649014202 | 1.927051509 | 1.825595524 | 1.887278087 |
| 7200.00 | 2.119092157 | 2.732575660 | 2.868935505 | 3.054531303 |
| 9000.00 | 2.098660704 | 3.137170189 | 3.80688983 | 4.218434703 |
| 10800.00 | 1.643791545 | 3.000387174 | 4.452861732 | 5.200189777 |
| 12600.00 | 1.22827731 | 2.422004868 | 4.67834147 | 5.848979589 |
| 14400.00 | 0.917795906 | 1.891026604 | 4.438472071 | 6.065137232 |
| 16200.00 | 0.685797351 | 1.476455173 | 3.802422185 | 5.815456663 |
| 18000.00 | 0.512442912 | 1.152770602 | 3.156632547 | 5.345100186 |
| 19800.00 | 0.38290865 | 0.900047686 | 2.620521487 | 4.370166041 |
| 21600.00 | 0.286117791 | 0.702729438 | 2.175461591 | 3.711949337 |
| 23400.00 | 0.213793526 | 0.548669443 | 1.805989059 | 3.152870566 |
| 25200.00 | 0.15975124 | 0.428384157 | 1.499266406 | 2.677997975 |
| 27000.00 | 0.119369651 | 0.334469120 | 1.24463642 | 2.27464877 |
| 28800.00 | 0.089195637 | 0.261143160 | 1.03325187 | 1.932050388 |
| 30600.00 | 0.066648948 | 0.203892514 | 0.857768108 | 1.641052786 |
| 32400.00 | 0.049801564 | 0.159192979 | 0.712087873 | 1.393884064 |
| 34200.00 | 0.037212828 | 0.124292961 | 0.591149443 | 1.183942893 |
| 36000.00 | 0.027806246 | 0.097044106 | 0.490750759 | 1.005622211 |
| 37800.00 | 0.02077744 | 0.075769041 | 0.407403424 | 0.854159468 |
| 39600.00 | 0.015525362 | 0.059158127 | 0.338211499 | 0.725509429 |
| 41400.00 | 0.011600893 | 0.046188839 | 0.280770881 | 0.616236139 |
| 43200.00 | 0.008668443 | 0.036062819 | 0.23308577 | 0.523421148 |
| 45000.00 | 0.006477252 | 0.028156735 | 0.193499325 | 0.444585575 |
| 46800.00 | 0.004839946 | 0.021983909 | 0.160636099 | 0.377623897 |
| 48600.00 | 0.003616514 | 0.017164358 | 0.133354245 | 0.320747716 |
| 50400.00 | 0.002702339 | 0.013401400 | 0.110705842 | 0.272437994 |
| 52200.00 | 0.002019247 | 0.010463399 | 0.091903962 | 0.231404487 |
| 54000.00 | 0.001508826 | 0.008169499 | 0.076295325 | 0.196551281 |
| 55800.00 | 0.001127428 | 0.006378493 | 0.063337603 | 0.166947523 |
| 57600.00 | 0.000842439 | 0.004980130 | 0.052580574 | 0.141802564 |
| 59400.00 | 0.000629489 | 0.003888332 | 0.043650479 | 0.120444836 |
| 61200.00 | 0.000470368 | 0.003035889 | 0.036237039 | 0.102303923 |
| 63000.00 | 0.00035147 | 0.002370329 | 0.030082672 | 0.08689532 |
| 64800.00 | 0.000262626 | 0.001850679 | 0.024973539 | 0.073807499 |
| 66600.00 | 0.00019624 | 0.001444953 | 0.020732124 | 0.062690913 |
| 68400.00 | 0.000146635 | 0.001128175 | 0.017211055 | 0.053248661 |
| 70200.00 | 0.000109569 | 0.000880844 | 0.014287992 | 0.045228564 |
| 72000.00 | 8.18721E-05 | 0.000687736 | 0.011861371 | 0.038416421 |
| 73800.00 | 6.11767E-05 | 0.000536963 | 0.009846878 | 0.032630295 |
| 75600.00 | 4.57126E-05 | 0.000419244 | 0.00817452 | 0.027715652 |
| 77400.00 | 3.41574E-05 | 0.000327333 | 0.006786189 | 0.023541233 |
| 79200.00 | 2.55232E-05 | 0.000255571 | 0.005633647 | 0.019995548 |
| 81000.00 | 1.90715E-05 | 0.000199542 | 0.004676849 | 0.016983899 |
| 82800.00 | 1.42506E-05 | 0.000155796 | 0.00388255 | 0.014425853 |
| 84600.00 | 1.06484E-05 | 0.000121641 | 0.003223152 | 0.01225309 |
| 86400.00 | 7.95671E-06 | 0.000094974 | 0.002675743 | 0.010407579 |

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24



DA FV 310 EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 55094.69 cft
 Volume (100-yr) = 1.38*area*43560 = 37269.94 cft
 Volume (10-yr) = 0.70*area*43560 = 18905.04 cft
 Volume (2-yr) = 0.41*area*43560 = 11072.952 cft
 A= 0.62 Ac

TP = time to Qp in seconds

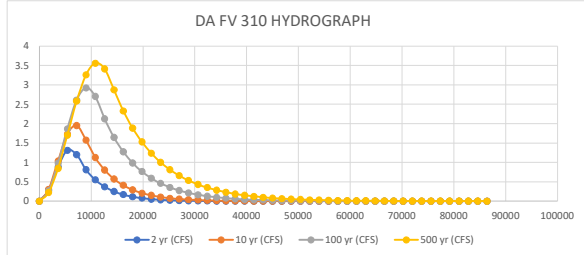
TP = $\frac{V}{1.39 Q_p}$

$Q_p = \frac{Q_p}{2} \left[2 - \cos \left(\frac{\pi t_i}{T_p} \right) \right]$
 $t_i = 1.25 T_p$
 $Q_p = 4.34 Q_{ps} \left(\frac{-1.8 t_i}{T_p} \right)^{0.75}$
 $t_i = 1.25 T_p$

| DA FV 310 Existing Conditions | | | | |
|-------------------------------|----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 1.34 | 1.96 | 2.93 | 3.57 |
| TP= | 5948.441 | 6941.991 | 9162.419 | 11116.990 |
| 1.25*TP= | 7435.552 | 8677.488 | 11453.024 | 13896.238 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|---------------|--------------|--------------|
| 0 | 0 | 0.0000000000 | 0.0000000000 | 0 |
| 1800.00 | 0.280457386 | 0.30743012873 | 0.2699407507 | 0.225700997 |
| 3600.00 | 0.886894222 | 1.03675750134 | 0.9801621158 | 0.84565359 |
| 5400.00 | 1.311306658 | 1.73020913285 | 1.8686114867 | 1.702877808 |
| 7200.00 | 1.198170194 | 1.95252997150 | 2.6074749076 | 2.580313449 |
| 9000.00 | 0.813056183 | 1.57619712226 | 2.9241316205 | 3.255782522 |
| 10800.00 | 0.548627578 | 1.12517205133 | 2.7017438032 | 3.558247566 |
| 12600.00 | 0.370198549 | 0.80320673551 | 2.1252934632 | 3.411120541 |
| 14400.00 | 0.249799629 | 0.57337103175 | 1.6462810392 | 2.872665411 |
| 16200.00 | 0.168557805 | 0.40930226991 | 1.2752315419 | 2.327399824 |
| 18000.00 | 0.113738093 | 0.29218139542 | 0.9878115866 | 1.885632041 |
| 19800.00 | 0.076747285 | 0.20857438160 | 0.7651722049 | 1.527716964 |
| 21600.00 | 0.051786922 | 0.14889131662 | 0.5927127310 | 1.237738366 |
| 23400.00 | 0.034944367 | 0.10628641925 | 0.4591232917 | 1.002801108 |
| 25200.00 | 0.023579482 | 0.07587281228 | 0.3556431066 | 0.812457696 |
| 27000.00 | 0.015910775 | 0.05416198686 | 0.2754859568 | 0.658243697 |
| 28800.00 | 0.010736146 | 0.03866366269 | 0.2133951452 | 0.533301323 |
| 30600.00 | 0.007244451 | 0.02760014724 | 0.1652987635 | 0.432074477 |
| 32400.00 | 0.004888353 | 0.01970243052 | 0.1280426561 | 0.350061674 |
| 34200.00 | 0.003298524 | 0.01406462672 | 0.0991835719 | 0.283615862 |
| 36000.00 | 0.002225752 | 0.01004006712 | 0.0768289352 | 0.229782245 |
| 37800.00 | 0.001501875 | 0.00716712571 | 0.0595127315 | 0.18616688 |
| 39600.00 | 0.001013423 | 0.00511626967 | 0.0460993661 | 0.150830223 |
| 41400.00 | 0.00068383 | 0.00365226123 | 0.0357091920 | 0.122200878 |
| 43200.00 | 0.000461429 | 0.00260717534 | 0.0276608227 | 0.099005718 |
| 45000.00 | 0.000311359 | 0.00186113829 | 0.0214264471 | 0.080213271 |
| 46800.00 | 0.000210097 | 0.00132857798 | 0.0165972155 | 0.064987852 |
| 48600.00 | 0.000141767 | 0.00094840854 | 0.0128564274 | 0.052652395 |
| 50400.00 | 9.56607E-05 | 0.00067702368 | 0.0099587624 | 0.042658353 |
| 52200.00 | 6.45491E-05 | 0.00048329496 | 0.0077141920 | 0.034561297 |
| 54000.00 | 4.3556E-05 | 0.00034500125 | 0.0059755174 | 0.028001158 |
| 55800.00 | 2.93903E-05 | 0.00024627996 | 0.0046287165 | 0.02268621 |
| 57600.00 | 1.98318E-05 | 0.00017580754 | 0.0035854664 | 0.018380101 |
| 59400.00 | 1.33819E-05 | 0.00012550063 | 0.0027773507 | 0.014891342 |
| 61200.00 | 9.02975E-06 | 0.00008958892 | 0.0021513734 | 0.012064791 |
| 63000.00 | 6.09302E-06 | 0.00006395326 | 0.0016664829 | 0.009774752 |
| 64800.00 | 4.1114E-06 | 0.00004565319 | 0.0012908802 | 0.007919389 |
| 66600.00 | 2.77426E-06 | 0.00003258964 | 0.0009999332 | 0.006416196 |
| 68400.00 | 1.87199E-06 | 0.00002326419 | 0.0007745618 | 0.005198327 |
| 70200.00 | 1.26317E-06 | 0.00001660720 | 0.0005999860 | 0.004211624 |
| 72000.00 | 8.52351E-07 | 0.00001185509 | 0.0004647573 | 0.003412208 |
| 73800.00 | 5.75142E-07 | 0.00000846278 | 0.0003600073 | 0.002764531 |
| 75600.00 | 3.8809E-07 | 0.00000604118 | 0.0002788665 | 0.002239791 |
| 77400.00 | 2.61872E-07 | 0.00000431251 | 0.0002160138 | 0.001814652 |
| 79200.00 | 1.76704E-07 | 0.00000307849 | 0.0001673272 | 0.00147021 |
| 81000.00 | 1.19235E-07 | 0.00000219759 | 0.0001296139 | 0.001191147 |
| 82800.00 | 8.04564E-08 | 0.00000156876 | 0.0001004007 | 0.000965053 |
| 84600.00 | 5.42897E-08 | 0.00000111986 | 0.0000777717 | 0.000781875 |
| 86400.00 | 3.66332E-08 | 0.00000079941 | 0.0000602430 | 0.000633466 |

ti (hrs)
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DA FV 309 EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 183945.17 cft
 Volume (100-yr) = 1.38*area*43560 = 124433.50 cft
 Volume (10-yr) = 0.70*area*43560 = 63118.44 cft
 Volume (2-yr) = 0.41*area*43560 = 36969.372 cft
 A= 2.07 Ac

TP = time to Qp in seconds

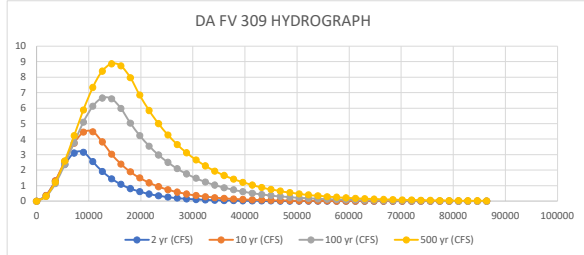
TP = $\frac{V}{1.39 Q_p}$

$Q_p = \frac{Q_p}{2} \left[1 - \cos \left(\frac{\pi t_i}{T_p} \right) \right]$
 $t_i = 1.25 T_p$
 $Q_p = 4.34 Q_{ps} \left(\frac{t_i}{T_p} \right)^{-1.81}$
 $t_i = 1.25 T_p$

| DA FV 309 Existing Conditions | | | | |
|-------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 3.23 | 4.55 | 6.71 | 8.89 |
| TP= | 8236.303 | 9971.223 | 13347.722 | 14883.594 |
| 1.25*TP= | 10295.379 | 12464.029 | 16684.652 | 18604.493 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.365836779 | 0.356459035 | 0.296469669 | 0.317032814 |
| 3600.00 | 1.297564199 | 1.31423048 | 1.133457693 | 1.222914161 |
| 5400.00 | 2.372959842 | 2.573440568 | 2.362970057 | 2.588441882 |
| 7200.00 | 3.104696471 | 3.739836497 | 3.76760763 | 4.218856333 |
| 9000.00 | 3.161179671 | 4.448225148 | 5.099006103 | 5.881618156 |
| 10800.00 | 2.548386771 | 4.476813342 | 6.121751111 | 7.339574422 |
| 12600.00 | 1.918133308 | 3.823449567 | 6.655003581 | 8.384782779 |
| 14400.00 | 1.443750779 | 3.02368933 | 6.604475219 | 8.668169427 |
| 16200.00 | 1.086690014 | 2.391216886 | 5.979100315 | 8.720790901 |
| 18000.00 | 0.817935619 | 1.89104024 | 5.0424301 | 7.963667199 |
| 19800.00 | 0.615648132 | 1.495486758 | 4.231587901 | 6.845063979 |
| 21600.00 | 0.46338931 | 1.182672159 | 3.551132253 | 5.849216493 |
| 23400.00 | 0.34878633 | 0.93528975 | 2.980096497 | 4.998248912 |
| 25200.00 | 0.26252635 | 0.73965292 | 2.500885492 | 4.271083524 |
| 27000.00 | 0.197599729 | 0.584937922 | 2.098733464 | 3.649709085 |
| 28800.00 | 0.148730415 | 0.462585035 | 1.761249032 | 3.118734703 |
| 30600.00 | 0.1119472 | 0.365824999 | 1.478033398 | 2.665008614 |
| 32400.00 | 0.084261014 | 0.289304495 | 1.240359929 | 2.277292424 |
| 34200.00 | 0.063422028 | 0.228789971 | 1.040905271 | 1.945982747 |
| 36000.00 | 0.047736829 | 0.180933417 | 0.873523691 | 1.662873337 |
| 37800.00 | 0.03593081 | 0.143087134 | 0.733057714 | 1.420951825 |
| 39600.00 | 0.027044594 | 0.113157251 | 0.615179207 | 1.214226028 |
| 41400.00 | 0.020356068 | 0.089487874 | 0.516256019 | 1.037575534 |
| 43200.00 | 0.015321714 | 0.070769478 | 0.433240061 | 0.886624865 |
| 45000.00 | 0.011532429 | 0.055966454 | 0.363573389 | 0.757635108 |
| 46800.00 | 0.00868029 | 0.044259815 | 0.305109387 | 0.6474113 |
| 48600.00 | 0.006533527 | 0.035001882 | 0.256046621 | 0.553223296 |
| 50400.00 | 0.00491769 | 0.027680453 | 0.214873337 | 0.472738142 |
| 52200.00 | 0.003701473 | 0.021890466 | 0.180320876 | 0.403962292 |
| 54000.00 | 0.002786044 | 0.017311584 | 0.151324584 | 0.34519223 |
| 55800.00 | 0.002097015 | 0.013690478 | 0.126991008 | 0.294972274 |
| 57600.00 | 0.001578392 | 0.010826807 | 0.106570364 | 0.252058519 |
| 59400.00 | 0.001188033 | 0.008562138 | 0.089433439 | 0.21538803 |
| 61200.00 | 0.000894215 | 0.006771174 | 0.075052197 | 0.184052512 |
| 63000.00 | 0.000673062 | 0.005354831 | 0.062983514 | 0.157275811 |
| 64800.00 | 0.000506604 | 0.004234748 | 0.052855522 | 0.134394692 |
| 66600.00 | 0.000381313 | 0.003348956 | 0.044356151 | 0.114842411 |
| 68400.00 | 0.000287009 | 0.002648447 | 0.03723511 | 0.098134674 |
| 70200.00 | 0.000216027 | 0.002094465 | 0.031237827 | 0.083857647 |
| 72000.00 | 0.000162601 | 0.00165636 | 0.026214664 | 0.071657698 |
| 73800.00 | 0.000122387 | 0.001309895 | 0.021999245 | 0.061232648 |
| 75600.00 | 9.2119E-05 | 0.001035901 | 0.018461681 | 0.052324275 |
| 77400.00 | 6.93366E-05 | 0.000819219 | 0.015492972 | 0.044711929 |
| 79200.00 | 5.21887E-05 | 0.000647861 | 0.013001642 | 0.038207057 |
| 81000.00 | 3.92816E-05 | 0.000512347 | 0.010910928 | 0.032648541 |
| 82800.00 | 2.95667E-05 | 0.000405178 | 0.009156409 | 0.0278987 |
| 84600.00 | 2.22544E-05 | 0.000320426 | 0.007684023 | 0.023839884 |
| 86400.00 | 1.67506E-05 | 0.000253402 | 0.006448402 | 0.020371562 |

ti (hrs)
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DA FV 304 DRAINAGE CALCULATIONS

Time of Concentration:

$T_c = T_{OL} + T_1 + \dots + T_n$

Equation 5.1

$T_1 = \frac{L}{V}$

$T_2 = \frac{L}{V}$

$T_3 = \frac{L}{V}$

$T_4 = \frac{L}{V}$

$T_5 = \frac{L}{V}$

$T_6 = \frac{L}{V}$

$T_7 = \frac{L}{V}$

$T_8 = \frac{L}{V}$

$T_9 = \frac{L}{V}$

$T_{10} = \frac{L}{V}$

$T_{11} = \frac{L}{V}$

$T_{12} = \frac{L}{V}$

$T_{13} = \frac{L}{V}$

$T_{14} = \frac{L}{V}$

$T_{15} = \frac{L}{V}$

$T_{16} = \frac{L}{V}$

$T_{17} = \frac{L}{V}$

$T_{18} = \frac{L}{V}$

$T_{19} = \frac{L}{V}$

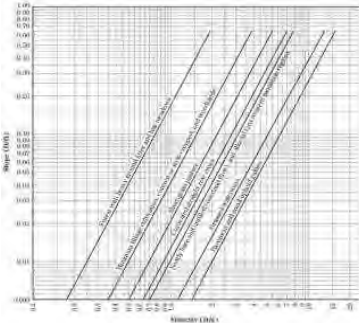
$T_{20} = \frac{L}{V}$

Table 5.1: Manning's Roughness Coefficients for Overland Flow

| Surface | n |
|------------------------------------------------------------|------|
| Gravelly Substrata, loose (e.g. sand, gravel, open soil) | 0.15 |
| Gravelly Substrata, compact (e.g. sand, gravel, open soil) | 0.18 |
| Gravelly Substrata, packed (e.g. sand, gravel, open soil) | 0.20 |
| Gravelly Substrata, packed (e.g. sand, gravel, open soil) | 0.22 |
| Gravelly Substrata, packed (e.g. sand, gravel, open soil) | 0.24 |
| Gravelly Substrata, packed (e.g. sand, gravel, open soil) | 0.26 |
| Gravelly Substrata, packed (e.g. sand, gravel, open soil) | 0.28 |
| Gravelly Substrata, packed (e.g. sand, gravel, open soil) | 0.30 |
| Gravelly Substrata, packed (e.g. sand, gravel, open soil) | 0.32 |
| Gravelly Substrata, packed (e.g. sand, gravel, open soil) | 0.34 |
| Gravelly Substrata, packed (e.g. sand, gravel, open soil) | 0.36 |
| Gravelly Substrata, packed (e.g. sand, gravel, open soil) | 0.38 |
| Gravelly Substrata, packed (e.g. sand, gravel, open soil) | 0.40 |
| Gravelly Substrata, packed (e.g. sand, gravel, open soil) | 0.42 |
| Gravelly Substrata, packed (e.g. sand, gravel, open soil) | 0.44 |
| Gravelly Substrata, packed (e.g. sand, gravel, open soil) | 0.46 |
| Gravelly Substrata, packed (e.g. sand, gravel, open soil) | 0.48 |
| Gravelly Substrata, packed (e.g. sand, gravel, open soil) | 0.50 |
| Gravelly Substrata, packed (e.g. sand, gravel, open soil) | 0.52 |
| Gravelly Substrata, packed (e.g. sand, gravel, open soil) | 0.54 |
| Gravelly Substrata, packed (e.g. sand, gravel, open soil) | 0.56 |
| Gravelly Substrata, packed (e.g. sand, gravel, open soil) | 0.58 |
| Gravelly Substrata, packed (e.g. sand, gravel, open soil) | 0.60 |
| Gravelly Substrata, packed (e.g. sand, gravel, open soil) | 0.62 |
| Gravelly Substrata, packed (e.g. sand, gravel, open soil) | 0.64 |
| Gravelly Substrata, packed (e.g. sand, gravel, open soil) | 0.66 |
| Gravelly Substrata, packed (e.g. sand, gravel, open soil) | 0.68 |
| Gravelly Substrata, packed (e.g. sand, gravel, open soil) | 0.70 |
| Gravelly Substrata, packed (e.g. sand, gravel, open soil) | 0.72 |
| Gravelly Substrata, packed (e.g. sand, gravel, open soil) | 0.74 |
| Gravelly Substrata, packed (e.g. sand, gravel, open soil) | 0.76 |
| Gravelly Substrata, packed (e.g. sand, gravel, open soil) | 0.78 |
| Gravelly Substrata, packed (e.g. sand, gravel, open soil) | 0.80 |
| Gravelly Substrata, packed (e.g. sand, gravel, open soil) | 0.82 |
| Gravelly Substrata, packed (e.g. sand, gravel, open soil) | 0.84 |
| Gravelly Substrata, packed (e.g. sand, gravel, open soil) | 0.86 |
| Gravelly Substrata, packed (e.g. sand, gravel, open soil) | 0.88 |
| Gravelly Substrata, packed (e.g. sand, gravel, open soil) | 0.90 |
| Gravelly Substrata, packed (e.g. sand, gravel, open soil) | 0.92 |
| Gravelly Substrata, packed (e.g. sand, gravel, open soil) | 0.94 |
| Gravelly Substrata, packed (e.g. sand, gravel, open soil) | 0.96 |
| Gravelly Substrata, packed (e.g. sand, gravel, open soil) | 0.98 |
| Gravelly Substrata, packed (e.g. sand, gravel, open soil) | 1.00 |

| T_{OL} | T_1 | T_2 | T_3 | T_4 | T_5 | T_6 | T_7 | T_8 | T_9 | T_{10} | T_{11} | T_{12} | T_{13} | T_{14} | T_{15} | T_{16} | T_{17} | T_{18} | T_{19} | T_{20} | |
|----------|-------|-------|--------|-------|--------|-------|-------|-------|-------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|--|
| 0.15 | 100 | 4.89 | 0.0113 | 297 | 0.0113 | 0.7 | 9.96 | 7.07 | | | | | | | | | | | | | |

$T_c = 17.03$ (min)



Intensity:

SEE FIG. 2.1-2.1a

| | | |
|-------------|-------|---------|
| I (500-YR)= | 11.81 | (in/hr) |
| I (100-YR)= | 9.1 | (in/hr) |
| I (10-YR)= | 6.2 | (in/hr) |
| I (2-YR)= | 4.3 | (in/hr) |

Peak Flow Rate:

$Q = CIA$
 $C = 0.4$ Mixed use area. Residential lots b/w 1/4 and 1/2 acres; sub-basin slope 1-3.5%; and golf course

| i (500-YR) | i (100-YR) | i (10-YR) | i (2-YR) |
|---------------------|-------------|--------------|----------|
| 11.81 | 9.1 | 6.2 | 4.3 |
| A = 1.23 (Ac) | | | |
| Q (500-YR) = | 5.81 | (cfs) | |
| Q (100-YR) = | 4.48 | (cfs) | |
| Q (10-YR) = | 3.05 | (cfs) | |
| Q (2-YR) = | 2.12 | (cfs) | |

DA FV 304 EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 109300.75 cft
 Volume (100-yr) = 1.38*area*43560 = 73938.74 cft
 Volume (10-yr) = 0.70*area*43560 = 37505.16 cft
 Volume (2-yr) = 0.41*area*43560 = 21967.308 cft
 A= 1.23 Ac

TP = time to Qp in seconds

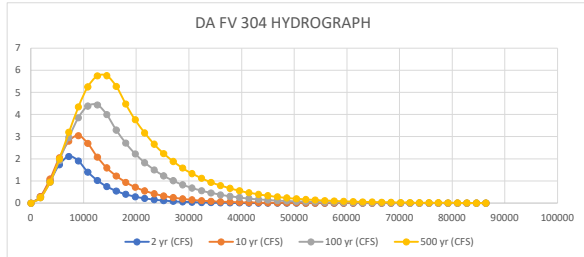
TP = $\frac{V}{1.39 Qp}$

$Q_t = \frac{Q_p}{2} \left[2 - \cos \left(\frac{\pi t_i}{T_p} \right) \right]$
 $t_i = 1.25 T_p$
 $Q_t = 4.34 Q_p e^{-1.8 t_i / T_p}$
 $t_i = 1.25 T_p$

| DA FV 304 Existing Conditions | | | | |
|-------------------------------|----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 2.12 | 3.05 | 4.48 | 5.81 |
| TP= | 7470.136 | 8845.440 | 11880.939 | 13530.018 |
| 1.25*TP= | 9337.669 | 11056.800 | 14851.174 | 16912.523 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|-------------|--------------|--------------|
| 0 | 0 | 0.000000000 | 0 | 0 |
| 1800.00 | 0.288883188 | 0.301203907 | 0.248814367 | 0.250130587 |
| 3600.00 | 0.997745843 | 1.085849206 | 0.939947375 | 0.957461396 |
| 5400.00 | 1.739409852 | 2.044024764 | 1.919763873 | 2.000222683 |
| 7200.00 | 2.108781127 | 2.797280251 | 2.970455926 | 3.198899043 |
| 9000.00 | 1.904110469 | 3.048102560 | 3.858460345 | 4.347133687 |
| 10800.00 | 1.401760341 | 2.697424475 | 4.386378526 | 5.247253563 |
| 12600.00 | 1.024783637 | 2.077874352 | 4.436857096 | 5.744299539 |
| 14400.00 | 0.749187626 | 1.594886114 | 3.998674942 | 5.752703221 |
| 16200.00 | 0.547707905 | 1.224165317 | 3.301196779 | 5.271017883 |
| 18000.00 | 0.400412312 | 0.939616134 | 2.711036236 | 4.473966557 |
| 19800.00 | 0.292729059 | 0.721208539 | 2.226379694 | 3.76341435 |
| 21600.00 | 0.214005162 | 0.553568353 | 1.828366023 | 3.165711543 |
| 23400.00 | 0.156452556 | 0.424895027 | 1.50150593 | 2.662935473 |
| 25200.00 | 0.114377626 | 0.326130971 | 1.23307917 | 2.240009943 |
| 27000.00 | 0.083617945 | 0.250323970 | 1.012639517 | 1.884253147 |
| 28800.00 | 0.061130494 | 0.192137808 | 0.831608235 | 1.584997394 |
| 30600.00 | 0.044690614 | 0.147476637 | 0.682940221 | 1.333269228 |
| 32400.00 | 0.032671926 | 0.113196662 | 0.560849841 | 1.121520352 |
| 34200.00 | 0.023885434 | 0.086884842 | 0.460585764 | 0.943401282 |
| 36000.00 | 0.017461902 | 0.066689031 | 0.378246066 | 0.793570957 |
| 37800.00 | 0.012765857 | 0.051187604 | 0.310626376 | 0.667536579 |
| 39600.00 | 0.009332723 | 0.039289382 | 0.255095172 | 0.561518891 |
| 41400.00 | 0.006822865 | 0.030156823 | 0.209491376 | 0.472338858 |
| 43200.00 | 0.004987986 | 0.023147068 | 0.172040248 | 0.397322334 |
| 45000.00 | 0.003646562 | 0.017766684 | 0.141284321 | 0.334219882 |
| 46800.00 | 0.002665889 | 0.013636935 | 0.116026684 | 0.281139316 |
| 48600.00 | 0.001948949 | 0.010467119 | 0.095284397 | 0.236488969 |
| 50400.00 | 0.001424816 | 0.008034106 | 0.078250244 | 0.198929958 |
| 52200.00 | 0.001041639 | 0.006166631 | 0.064261315 | 0.167336043 |
| 54000.00 | 0.00076151 | 0.004733238 | 0.052773211 | 0.140759851 |
| 55800.00 | 0.000556717 | 0.003633028 | 0.043338854 | 0.118404471 |
| 57600.00 | 0.000406998 | 0.002788555 | 0.035591094 | 0.099599556 |
| 59400.00 | 0.000297544 | 0.002140373 | 0.029228414 | 0.083781225 |
| 61200.00 | 0.000217525 | 0.001642858 | 0.024003201 | 0.07047515 |
| 63000.00 | 0.000159026 | 0.001260986 | 0.019712108 | 0.059282337 |
| 64800.00 | 0.000116259 | 0.000967878 | 0.016188141 | 0.049867158 |
| 66600.00 | 8.49933E-05 | 0.000742901 | 0.01329416 | 0.041947291 |
| 68400.00 | 6.2136E-05 | 0.000570219 | 0.01091754 | 0.035285252 |
| 70200.00 | 4.54257E-05 | 0.000437675 | 0.008965793 | 0.029681273 |
| 72000.00 | 3.32093E-05 | 0.000335940 | 0.007362963 | 0.024967314 |
| 73800.00 | 2.42783E-05 | 0.000257853 | 0.006046674 | 0.021002023 |
| 75600.00 | 1.77491E-05 | 0.000197917 | 0.0049657 | 0.017666497 |
| 77400.00 | 1.29758E-05 | 0.000151912 | 0.004077973 | 0.0148660716 |
| 79200.00 | 9.48623E-06 | 0.000116601 | 0.003348947 | 0.012500548 |
| 81000.00 | 6.93509E-06 | 0.000089498 | 0.00275025 | 0.01051522 |
| 82800.00 | 5.07003E-06 | 0.000068695 | 0.002258583 | 0.0088452 |
| 84600.00 | 3.70654E-06 | 0.000052727 | 0.001854812 | 0.007440411 |
| 86400.00 | 2.70974E-06 | 0.000040471 | 0.001523224 | 0.006258731 |

ti (hrs)
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DA FV 302 DRAINAGE CALCULATIONS

Time of Concentration:

$T_c = T_{OL} + T_1 + \dots + T_n$

Equation 2.1

$T_{OL} = \frac{L}{V}$

$T_1 = 0.0119 L^{0.77} S^{-0.385}$

$T_n = 0.0119 L_n^{0.77} S_n^{-0.385}$

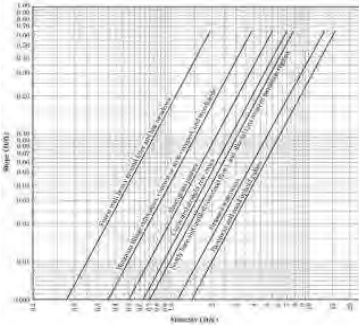
$T_c = T_{OL} + T_1 + \dots + T_n$

Table 2.3 Manning's Roughness Coefficients for Overland Flow

| Surface | n |
|-------------------------------------------------------|-------|
| Smooth finished concrete (interior, gutter, open end) | 0.012 |
| Galvanized metal (interior, gutter, open end) | 0.014 |
| Asphalt concrete (interior, gutter, open end) | 0.016 |
| Gravel (interior, gutter, open end) | 0.018 |
| Grass (interior, gutter, open end) | 0.020 |
| Gravel (interior, gutter, open end) | 0.022 |
| Gravel (interior, gutter, open end) | 0.024 |
| Gravel (interior, gutter, open end) | 0.026 |
| Gravel (interior, gutter, open end) | 0.028 |
| Gravel (interior, gutter, open end) | 0.030 |
| Gravel (interior, gutter, open end) | 0.032 |
| Gravel (interior, gutter, open end) | 0.034 |
| Gravel (interior, gutter, open end) | 0.036 |
| Gravel (interior, gutter, open end) | 0.038 |
| Gravel (interior, gutter, open end) | 0.040 |
| Gravel (interior, gutter, open end) | 0.042 |
| Gravel (interior, gutter, open end) | 0.044 |
| Gravel (interior, gutter, open end) | 0.046 |
| Gravel (interior, gutter, open end) | 0.048 |
| Gravel (interior, gutter, open end) | 0.050 |
| Gravel (interior, gutter, open end) | 0.052 |
| Gravel (interior, gutter, open end) | 0.054 |
| Gravel (interior, gutter, open end) | 0.056 |
| Gravel (interior, gutter, open end) | 0.058 |
| Gravel (interior, gutter, open end) | 0.060 |
| Gravel (interior, gutter, open end) | 0.062 |
| Gravel (interior, gutter, open end) | 0.064 |
| Gravel (interior, gutter, open end) | 0.066 |
| Gravel (interior, gutter, open end) | 0.068 |
| Gravel (interior, gutter, open end) | 0.070 |
| Gravel (interior, gutter, open end) | 0.072 |
| Gravel (interior, gutter, open end) | 0.074 |
| Gravel (interior, gutter, open end) | 0.076 |
| Gravel (interior, gutter, open end) | 0.078 |
| Gravel (interior, gutter, open end) | 0.080 |
| Gravel (interior, gutter, open end) | 0.082 |
| Gravel (interior, gutter, open end) | 0.084 |
| Gravel (interior, gutter, open end) | 0.086 |
| Gravel (interior, gutter, open end) | 0.088 |
| Gravel (interior, gutter, open end) | 0.090 |
| Gravel (interior, gutter, open end) | 0.092 |
| Gravel (interior, gutter, open end) | 0.094 |
| Gravel (interior, gutter, open end) | 0.096 |
| Gravel (interior, gutter, open end) | 0.098 |
| Gravel (interior, gutter, open end) | 0.100 |

| T_{OL} = | T_1 = |
|------------|------------|
| 9.96 (min) | 3.95 (min) |

$T_c = 13.91$ (min)



Intensity:

SEE FIG. 2.1-2.1a

| | |
|-------------|---------------|
| I (500-YR)= | 12.82 (in/hr) |
| I (100-YR)= | 10 (in/hr) |
| I (10-YR)= | 6.8 (in/hr) |
| I (2-YR)= | 4.7 (in/hr) |

Peak Flow Rate:

Q=CIA
C= 0.4 Mixed use area. Residential lots b/w 1/4 and 1/2 acres; sub-basin slope 1-3.5%; and golf course

| i (500-YR) | i (100-YR) | i (10-YR) | i (2-YR) |
|--------------------|--------------------|-----------|----------|
| 12.82 | 10 | 6.8 | 4.7 |
| A= 2.88 (Ac) | | | |
| Q (500-YR)= | 14.77 (cfs) | | |
| Q (100-YR)= | 11.52 (cfs) | | |
| Q (10-YR)= | 7.83 (cfs) | | |
| Q (2-YR)= | 5.41 (cfs) | | |

DA FV 302 EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 255923.71 cft
 Volume (100-yr) = 1.38*area*43560 = 173124.86 cft
 Volume (10-yr) = 0.70*area*43560 = 87816.96 cft
 Volume (2-yr) = 0.41*area*43560 = 51435.648 cft
 A= 2.88 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

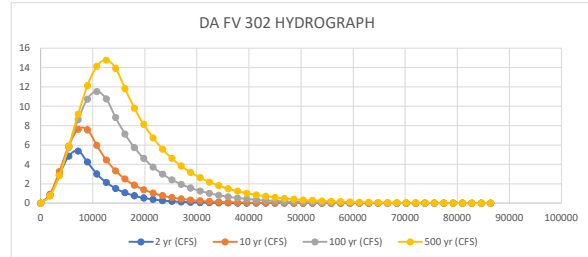
$Q_t = \frac{Q_p}{2} \left[2 - \cos \left(\frac{\pi t_i}{T_p} \right) \right]$ $t_i = 1.25 T_p$
 $Q_t = 4.34 Q_p e^{-1.25 t_i / T_p}$ $t_i = 1.25 T_p$

| DA FV 302 Existing Conditions | | | | |
|-------------------------------|----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 5.41 | 7.83 | 11.52 | 14.77 |
| TP= | 6834.379 | 8064.960 | 10811.655 | 12464.562 |
| 1.25*TP= | 8542.974 | 10081.200 | 13514.568 | 15580.702 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|--------------|--------------|--------------|
| 0 | 0 | 0 | 0 | 0 |
| 1800.00 | 0.875017983 | 0.9240075269 | 0.770068923 | 0.747115391 |
| 3600.00 | 2.934427376 | 3.2600671225 | 2.874370781 | 2.837308606 |
| 5400.00 | 4.846948442 | 5.9059848278 | 5.750246731 | 5.847701342 |
| 7200.00 | 5.376255585 | 7.6133701836 | 8.628730559 | 9.169244751 |
| 9000.00 | 4.241866315 | 7.5766487823 | 10.74015874 | 12.12993941 |
| 10800.00 | 3.012037396 | 5.9621568064 | 11.51996697 | 14.13079115 |
| 12600.00 | 2.138768316 | 4.4606221780 | 10.75964618 | 14.76699684 |
| 14400.00 | 1.518682973 | 3.3372403412 | 8.850678806 | 13.90984225 |
| 16200.00 | 1.078376726 | 2.4967757077 | 7.128216419 | 11.8339245 |
| 18000.00 | 0.765726872 | 1.8679772198 | 5.740968623 | 9.808389937 |
| 19800.00 | 0.543722457 | 1.3975379859 | 4.623698103 | 8.129552721 |
| 21600.00 | 0.386082976 | 1.0455761458 | 3.72386361 | 6.738070965 |
| 23400.00 | 0.274147339 | 0.7822538548 | 2.99914914 | 5.584759936 |
| 25200.00 | 0.194664795 | 0.5852477563 | 2.415473956 | 4.628853525 |
| 27000.00 | 0.138226337 | 0.4378565016 | 1.945389895 | 3.83656329 |
| 28800.00 | 0.098150876 | 0.3275848800 | 1.566790581 | 3.179884134 |
| 30600.00 | 0.069694349 | 0.2450845270 | 1.261871839 | 2.635604404 |
| 32400.00 | 0.049488119 | 0.1833614097 | 1.016294429 | 2.184485435 |
| 34200.00 | 0.035140208 | 0.1371829016 | 0.818509721 | 1.810581515 |
| 36000.00 | 0.024952135 | 0.1026341831 | 0.659216604 | 1.500676255 |
| 37800.00 | 0.017717853 | 0.0767863591 | 0.530924094 | 1.243815429 |
| 39600.00 | 0.01258098 | 0.0574481597 | 0.427599049 | 1.030919771 |
| 41400.00 | 0.008933422 | 0.0429801737 | 0.344382463 | 0.854464054 |
| 43200.00 | 0.006343387 | 0.0321558661 | 0.277360955 | 0.708211095 |
| 45000.00 | 0.004504272 | 0.0240575976 | 0.223382743 | 0.586991287 |
| 46800.00 | 0.003198365 | 0.0179988311 | 0.179909425 | 0.486519872 |
| 48600.00 | 0.002271075 | 0.0134659299 | 0.144896606 | 0.403245484 |
| 50400.00 | 0.00161263 | 0.0100746135 | 0.116697757 | 0.334224622 |
| 52200.00 | 0.001145086 | 0.0075373805 | 0.093986788 | 0.277017605 |
| 54000.00 | 0.000813095 | 0.0056391349 | 0.075695681 | 0.229602334 |
| 55800.00 | 0.000577358 | 0.0042189515 | 0.060964273 | 0.190302822 |
| 57600.00 | 0.000409966 | 0.0031564330 | 0.049099797 | 0.157729947 |
| 59400.00 | 0.000291106 | 0.0023615036 | 0.039544309 | 0.130732355 |
| 61200.00 | 0.000206707 | 0.0017667726 | 0.031848449 | 0.108355763 |
| 63000.00 | 0.000146777 | 0.0013218212 | 0.025650308 | 0.089809224 |
| 64800.00 | 0.000104223 | 0.0009889282 | 0.020658409 | 0.074437173 |
| 66600.00 | 7.40057E-05 | 0.0007398724 | 0.016638002 | 0.061696255 |
| 68400.00 | 5.25495E-05 | 0.0005535398 | 0.013400021 | 0.051136115 |
| 70200.00 | 3.7314E-05 | 0.0004141340 | 0.010792195 | 0.042383484 |
| 72000.00 | 2.64957E-05 | 0.0003098368 | 0.008691887 | 0.035128984 |
| 73800.00 | 1.88139E-05 | 0.0002318062 | 0.007000328 | 0.029116188 |
| 75600.00 | 1.33593E-05 | 0.0001734271 | 0.005637969 | 0.024132563 |
| 77400.00 | 9.48605E-06 | 0.0001297505 | 0.004540743 | 0.020001952 |
| 79200.00 | 6.7358E-06 | 0.0000970736 | 0.003657053 | 0.01657835 |
| 81000.00 | 4.78291E-06 | 0.0000726262 | 0.002945341 | 0.013740743 |
| 82800.00 | 3.39622E-06 | 0.0000543357 | 0.002372137 | 0.011388831 |
| 84600.00 | 2.41157E-06 | 0.0000406516 | 0.001910487 | 0.00943948 |
| 86400.00 | 1.71239E-06 | 0.0000304137 | 0.00153868 | 0.007823787 |

ti (hrs)

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DA FV 201 DRAINAGE CALCULATIONS

Time of Concentration:

$T_c = T_{OL} + T_1 + \dots + T_n$

Equation 2.1

$T_1 = \frac{L}{V}$

$T_2 = \frac{L}{V}$

$T_3 = \frac{L}{V}$

$T_4 = \frac{L}{V}$

$T_5 = \frac{L}{V}$

$T_6 = \frac{L}{V}$

$T_7 = \frac{L}{V}$

$T_8 = \frac{L}{V}$

$T_9 = \frac{L}{V}$

$T_{10} = \frac{L}{V}$

$T_{11} = \frac{L}{V}$

$T_{12} = \frac{L}{V}$

$T_{13} = \frac{L}{V}$

$T_{14} = \frac{L}{V}$

$T_{15} = \frac{L}{V}$

$T_{16} = \frac{L}{V}$

$T_{17} = \frac{L}{V}$

$T_{18} = \frac{L}{V}$

$T_{19} = \frac{L}{V}$

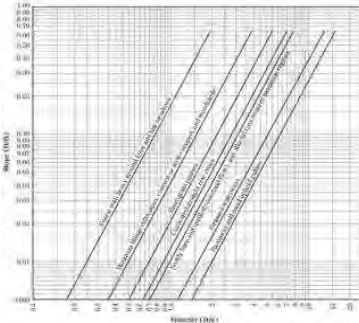
$T_{20} = \frac{L}{V}$

Table 2.1: Manning's Roughness Coefficients for Overland Flow

| Surface | n |
|------------------------------------------------------|-------|
| Smooth finished concrete (dry side, gutter open end) | 0.012 |
| Galvanized steel (dry side) | 0.016 |
| Cast-in-place concrete (finished) | 0.012 |
| Asphalt concrete (finished) | 0.016 |
| Gravel (finished) | 0.024 |
| Grass (finished) | 0.040 |
| Grass (rough) | 0.050 |
| Wooden logs (rough) | 0.080 |
| Wooden timbers (rough) | 0.080 |

| T_{OL} = | T_1 = |
|------------|------------|
| 9.96 (min) | 6.07 (min) |

$T_c = 16.03$ (min)



Intensity:

SEE FIG. 2.1-2.1a

| | |
|--------------|---------------|
| i (500-YR) = | 15.65 (in/hr) |
| i (100-YR) = | 9.4 (in/hr) |
| i (10-YR) = | 6.4 (in/hr) |
| i (2-YR) = | 4.6 (in/hr) |

Peak Flow Rate:

$Q = CIA$

C = 0.4 Mixed use area. Residential lots b/w 1/4 and 1/2 acres; sub-basin slope 1-3.5%; and golf course

| i (500-YR) | i (100-YR) | i (10-YR) | i (2-YR) |
|---------------------|-------------------|-----------|----------|
| 15.65 | 9.4 | 6.4 | 4.6 |
| A = 1.09 (Ac) | | | |
| Q (500-YR) = | 6.82 (cfs) | | |
| Q (100-YR) = | 4.10 (cfs) | | |
| Q (10-YR) = | 2.79 (cfs) | | |
| Q (2-YR) = | 2.01 (cfs) | | |

DA FV 201 EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 96860.02 cft
 Volume (100-yr) = 1.38*area*43560 = 65522.95 cft
 Volume (10-yr) = 0.70*area*43560 = 33236.28 cft
 Volume (2-yr) = 0.41*area*43560 = 19466.964 cft
 A= 1.09 Ac

TP = time to Qp in seconds

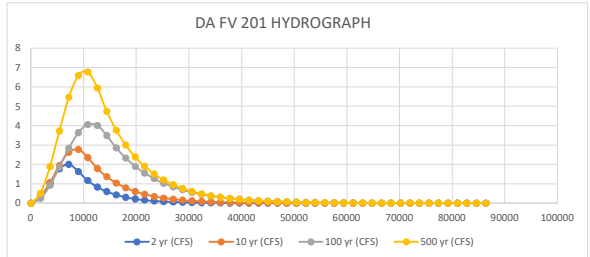
TP = $\frac{V}{1.39 Q_p}$

$Q_p = \frac{Q_p}{2} \left[1 - \cos \left(\frac{\pi t_i}{T_p} \right) \right]$ $t_i = 1.25 T_p$
 $Q_p = 4.34 Q_{p^*} \left(\frac{-1.8 t_i}{T_p} \right)^{0.7}$ $t_i = 1.25 T_p$

| DA FV 201 Existing Conditions | | | | |
|-------------------------------|----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 2.01 | 2.79 | 4.10 | 6.82 |
| TP= | 6982.953 | 8569.020 | 11501.760 | 10210.740 |
| 1.25*TP= | 8728.691 | 10711.275 | 14377.200 | 12763.425 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|--------------|--------------|--------------|
| 0 | 0 | 0.000000000 | 0 | 0 |
| 1800.00 | 0.311233171 | 0.2929343327 | 0.242719452 | 0.510051491 |
| 3600.00 | 1.051741445 | 1.0487291265 | 0.913379533 | 1.887725034 |
| 5400.00 | 1.76187038 | 1.9500130461 | 1.853106295 | 3.721162323 |
| 7200.00 | 2.000822846 | 2.6183213501 | 2.839286069 | 5.462253552 |
| 9000.00 | 1.629557729 | 2.7730197968 | 3.638300845 | 6.59049596 |
| 10800.00 | 1.165566054 | 2.3527829327 | 4.060870485 | 6.768599184 |
| 12600.00 | 0.833688922 | 1.7905487064 | 4.00689166 | 5.943318904 |
| 14400.00 | 0.596308734 | 1.3626691291 | 3.493464881 | 4.735245789 |
| 16200.00 | 0.426518929 | 1.0370380593 | 2.850364632 | 3.765434205 |
| 18000.00 | 0.305074178 | 0.7892216191 | 2.325650553 | 2.994246843 |
| 19800.00 | 0.218208966 | 0.6006247875 | 1.897529332 | 2.381004067 |
| 21600.00 | 0.156077295 | 0.4570961143 | 1.548219512 | 1.893357717 |
| 23400.00 | 0.111636669 | 0.3478658591 | 1.263212967 | 1.505584763 |
| 25200.00 | 0.079849833 | 0.2647378793 | 1.030672323 | 1.197230433 |
| 27000.00 | 0.057113812 | 0.2014746285 | 0.840939307 | 0.952029235 |
| 28800.00 | 0.040851527 | 0.1533291195 | 0.686133606 | 0.757046963 |
| 30600.00 | 0.029219678 | 0.1166887318 | 0.559825569 | 0.60199843 |
| 32400.00 | 0.020899821 | 0.0888041369 | 0.456769155 | 0.478704925 |
| 34200.00 | 0.014948916 | 0.0675830015 | 0.372684051 | 0.380662795 |
| 36000.00 | 0.010692441 | 0.0514329878 | 0.304077892 | 0.302700382 |
| 37800.00 | 0.007647932 | 0.0391422721 | 0.248101211 | 0.240705219 |
| 39600.00 | 0.0054703 | 0.0297886149 | 0.20242909 | 0.1914071 |
| 41400.00 | 0.003912715 | 0.0226701601 | 0.165164597 | 0.152205582 |
| 43200.00 | 0.00279863 | 0.0172527713 | 0.134759999 | 0.12103281 |
| 45000.00 | 0.002001763 | 0.0131299522 | 0.109952483 | 0.096244441 |
| 46800.00 | 0.001431791 | 0.0099923450 | 0.089711698 | 0.076532904 |
| 48600.00 | 0.001024111 | 0.0076045181 | 0.073196972 | 0.060858428 |
| 50400.00 | 0.000732511 | 0.0057872998 | 0.059722387 | 0.048394194 |
| 52200.00 | 0.000523939 | 0.0044043341 | 0.048728293 | 0.038482724 |
| 54000.00 | 0.000374756 | 0.0033518497 | 0.039758064 | 0.030601192 |
| 55800.00 | 0.00026805 | 0.0025508729 | 0.032439135 | 0.024333853 |
| 57600.00 | 0.000191727 | 0.0019413019 | 0.026467524 | 0.019350109 |
| 59400.00 | 0.000137135 | 0.0014773975 | 0.021595206 | 0.015387071 |
| 61200.00 | 9.80882E-05 | 0.0011243503 | 0.017619817 | 0.012235691 |
| 63000.00 | 7.01591E-05 | 0.0008556692 | 0.014376244 | 0.009729735 |
| 64800.00 | 5.01824E-05 | 0.0006511937 | 0.011729769 | 0.007737017 |
| 66600.00 | 3.58937E-05 | 0.0004955808 | 0.009570475 | 0.006152422 |
| 68400.00 | 2.56735E-05 | 0.0003771540 | 0.007808678 | 0.004892363 |
| 70200.00 | 1.83634E-05 | 0.0002870272 | 0.006371205 | 0.003890372 |
| 72000.00 | 1.31347E-05 | 0.0002184376 | 0.005198351 | 0.003093597 |
| 73800.00 | 9.39478E-06 | 0.0001662385 | 0.004241404 | 0.002460006 |
| 75600.00 | 6.71976E-06 | 0.0001265132 | 0.003460618 | 0.00195618 |
| 77400.00 | 4.80641E-06 | 0.0000962809 | 0.002823565 | 0.00155554 |
| 79200.00 | 3.43786E-06 | 0.0000732731 | 0.002303784 | 0.001236955 |
| 81000.00 | 2.45898E-06 | 0.0000557633 | 0.001879688 | 0.000983618 |
| 82800.00 | 1.75882E-06 | 0.0000424378 | 0.001533663 | 0.000782166 |
| 84600.00 | 1.25803E-06 | 0.0000322966 | 0.001251336 | 0.000621973 |
| 86400.00 | 8.99822E-07 | 0.0000245788 | 0.001020982 | 0.000494588 |

ti (hrs)
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DA FV 203 DRAINAGE CALCULATIONS

Time of Concentration:

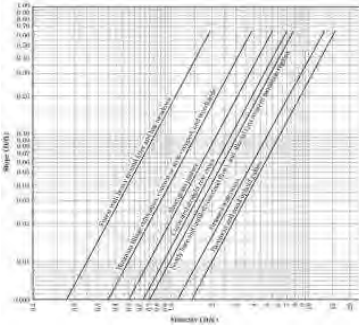
$T_c = T_{c1} + T_{c2} + \dots + T_{cn}$

Handwritten notes on the left side of the page define variables for the time of concentration calculation, including n , L , P , and S .

| Material | n |
|-----------------------------------------------|-------|
| Smooth Barbed Wire (smooth), galvanized steel | 0.013 |
| Galvanized Steel (Standard) | 0.014 |
| Cast Iron (Standard) | 0.013 |
| Concrete (Standard) | 0.012 |
| Asphalt (Standard) | 0.013 |
| Brick (Standard) | 0.015 |
| Stoneware (Standard) | 0.014 |
| Wood (Standard) | 0.013 |
| Plastic (Standard) | 0.010 |

| T_{c1} = | T_{c2} = |
|-----------------------|------------------------|
| $n = 0.15$ | $D = 520$ (ft) |
| $L = 100$ (ft) | $S = 0.0113$ (ft/ft) |
| $P = 4.89$ (in) | $V = 0.7$ (ft/s) |
| $S = 0.0113$ (ft/ft) | |
| $T_{c1} = 9.96$ (min) | $T_{c2} = 12.38$ (min) |

$T_c = 22.34$ (min)



Intensity:

SEE FIG. 2.1-2.1a

| | |
|----------------|---------------|
| i (500-YR) = | 14.14 (in/hr) |
| i (100-YR) = | 7.9 (in/hr) |
| i (10-YR) = | 5.3 (in/hr) |
| i (2-YR) = | 3.4 (in/hr) |

Peak Flow Rate:

$Q = CIA$
 $C = 0.4$ Mixed use area. Residential lots b/w 1/4 and 1/2 acres; sub-basin slope 1-3.5%; and golf course

| i (500-YR) | i (100-YR) | i (10-YR) | i (2-YR) |
|-----------------|--------------|-------------|------------|
| 14.14 | 7.9 | 5.3 | 3.4 |
| $A = 2.73$ (Ac) | | | |
| Q (500-YR) = | 15.44 (cfs) | | |
| Q (100-YR) = | 8.63 (cfs) | | |
| Q (10-YR) = | 5.79 (cfs) | | |
| Q (2-YR) = | 3.71 (cfs) | | |

DA FV 203 EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 242594.35 cft
 Volume (100-yr) = 1.38*area*43560 = 164107.94 cft
 Volume (10-yr) = 0.70*area*43560 = 83243.16 cft
 Volume (2-yr) = 0.41*area*43560 = 48756.708 cft
 A= 2.73 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Qp}$

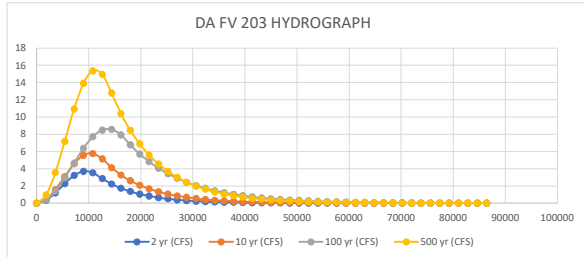
$Qp = \frac{Qp}{2} \left[2 - \cos\left(\frac{\pi t_i}{TP}\right) \right]$ $t_i = 1.25 TP$

$Qp = 4.34 Qp \left(\frac{t_i - TP}{TP} \right)^2$ $t_i = 1.25 TP$

| DA FV 203 Existing Conditions | | | | |
|-------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 3.71 | 5.79 | 8.63 | 15.44 |
| TP= | 9447.524 | 10347.496 | 13685.639 | 11304.364 |
| 1.25*TP= | 11809.405 | 12934.369 | 17107.049 | 14130.455 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|--------------|--------------|--------------|
| 0 | 0 | 0.000000000 | 0 | 0 |
| 1800.00 | 0.322734338 | 0.4214799764 | 0.363008285 | 0.945881796 |
| 3600.00 | 1.178722903 | 1.5631433691 | 1.390932841 | 3.551726892 |
| 5400.00 | 2.270339209 | 3.0924252049 | 2.910756961 | 7.178939999 |
| 7200.00 | 3.218029209 | 4.5638477922 | 4.666669106 | 10.93862668 |
| 9000.00 | 3.69228191 | 5.5487877588 | 6.363120218 | 13.90942819 |
| 10800.00 | 3.528200055 | 5.7603334494 | 7.714569511 | 15.36331204 |
| 12600.00 | 2.845882219 | 5.1368618959 | 8.493545716 | 14.94398562 |
| 14400.00 | 2.22151452 | 4.1142585431 | 8.568934251 | 12.79142278 |
| 16200.00 | 1.734128956 | 3.2815532628 | 7.928045979 | 10.39968119 |
| 18000.00 | 1.353672555 | 2.6173838305 | 6.772880316 | 8.455147693 |
| 19800.00 | 1.056685767 | 2.0876386703 | 5.70843152 | 6.874203279 |
| 21600.00 | 0.824855913 | 1.665112332 | 4.811275099 | 5.588864019 |
| 23400.00 | 0.643887992 | 1.3281011979 | 4.055118818 | 4.54385763 |
| 25200.00 | 0.502623233 | 1.0593002779 | 3.417802618 | 3.694246647 |
| 27000.00 | 0.392351027 | 0.8449032953 | 2.880649189 | 3.003496016 |
| 28800.00 | 0.306271812 | 0.6738991704 | 2.427916612 | 2.441902012 |
| 30600.00 | 0.239077806 | 0.5375054096 | 2.046337018 | 1.985314914 |
| 32400.00 | 0.18662572 | 0.4287170516 | 1.724727766 | 1.61410052 |
| 34200.00 | 0.145681273 | 0.3419469033 | 1.453663712 | 1.312295833 |
| 36000.00 | 0.113719767 | 0.2727385911 | 1.225201002 | 1.066922619 |
| 37800.00 | 0.088770404 | 0.2175376890 | 1.032644265 | 0.867429314 |
| 39600.00 | 0.069294766 | 0.1735091684 | 0.870350397 | 0.705237289 |
| 41400.00 | 0.054091953 | 0.1383917962 | 0.733563182 | 0.573371946 |
| 43200.00 | 0.042224537 | 0.1103820013 | 0.61827391 | 0.466162798 |
| 45000.00 | 0.032960754 | 0.0880412463 | 0.521103889 | 0.378999629 |
| 46800.00 | 0.025729383 | 0.0702221463 | 0.439205438 | 0.308134238 |
| 48600.00 | 0.020084527 | 0.0560095415 | 0.370178425 | 0.250519265 |
| 50400.00 | 0.015678115 | 0.0446734955 | 0.31199993 | 0.203677146 |
| 52200.00 | 0.01223844 | 0.0356318074 | 0.262964965 | 0.165593572 |
| 54000.00 | 0.009553407 | 0.0284201110 | 0.221636501 | 0.134630868 |
| 55800.00 | 0.007457453 | 0.0226680253 | 0.186803358 | 0.109457574 |
| 57600.00 | 0.005821337 | 0.0180801324 | 0.15744471 | 0.088991185 |
| 59400.00 | 0.004544175 | 0.0144208056 | 0.132700167 | 0.072351604 |
| 61200.00 | 0.003547213 | 0.0115021080 | 0.111844559 | 0.058823293 |
| 63000.00 | 0.002768978 | 0.0091741399 | 0.09426669 | 0.047824508 |
| 64800.00 | 0.002161482 | 0.0073173407 | 0.079451418 | 0.038882276 |
| 66600.00 | 0.001687267 | 0.0058363482 | 0.066964564 | 0.031612064 |
| 68400.00 | 0.001317092 | 0.0046551010 | 0.056440186 | 0.025701237 |
| 70200.00 | 0.001028131 | 0.0037129323 | 0.047569856 | 0.020895617 |
| 72000.00 | 0.000802566 | 0.0029614537 | 0.040093616 | 0.016988552 |
| 73800.00 | 0.000626488 | 0.0023620706 | 0.033792368 | 0.013812031 |
| 75600.00 | 0.000489041 | 0.0018839995 | 0.028481445 | 0.011229456 |
| 77400.00 | 0.000381749 | 0.0015026876 | 0.024005205 | 0.009129771 |
| 79200.00 | 0.000297995 | 0.0011985513 | 0.020232465 | 0.007422686 |
| 81000.00 | 0.000232617 | 0.0009559706 | 0.017052663 | 0.006034791 |
| 82800.00 | 0.000181583 | 0.0007624870 | 0.014372608 | 0.004906405 |
| 84600.00 | 0.000141745 | 0.0006081635 | 0.012113761 | 0.003989005 |
| 86400.00 | 0.000110647 | 0.0004850743 | 0.010209921 | 0.00324314 |

ti (hrs)
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DA FE 101 DRAINAGE CALCULATIONS

Time of Concentration:

$T_c = T_{OL} + T_1 + \dots + T_n$

Equation 2.1

$T_1 = \frac{L}{V}$

$T_2 = \frac{L}{V}$

$T_3 = \frac{L}{V}$

$T_4 = \frac{L}{V}$

$T_5 = \frac{L}{V}$

$T_6 = \frac{L}{V}$

$T_7 = \frac{L}{V}$

$T_8 = \frac{L}{V}$

$T_9 = \frac{L}{V}$

$T_{10} = \frac{L}{V}$

$T_{11} = \frac{L}{V}$

$T_{12} = \frac{L}{V}$

$T_{13} = \frac{L}{V}$

$T_{14} = \frac{L}{V}$

$T_{15} = \frac{L}{V}$

$T_{16} = \frac{L}{V}$

$T_{17} = \frac{L}{V}$

$T_{18} = \frac{L}{V}$

$T_{19} = \frac{L}{V}$

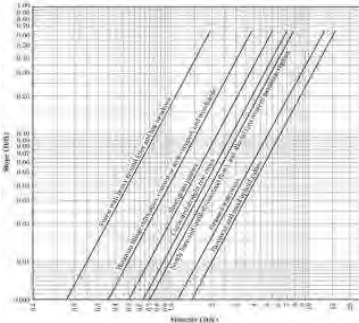
$T_{20} = \frac{L}{V}$

Table 2.1: Manning's Roughness Coefficients for Overland Flow

| Surface | n |
|-------------------------------------------------|-------|
| Smooth finished concrete (dry side, gutter and) | 0.012 |
| Galvanized steel (dry side) | 0.014 |
| Cast-in-place concrete (dry side) | 0.015 |
| Asphalt concrete (dry side) | 0.016 |
| Gravel (dry side) | 0.017 |
| Grass (dry side) | 0.018 |
| Grass (wet side) | 0.019 |
| Gravel (wet side) | 0.020 |
| Grass (wet side) | 0.021 |
| Gravel (wet side) | 0.022 |
| Grass (wet side) | 0.023 |
| Gravel (wet side) | 0.024 |
| Grass (wet side) | 0.025 |
| Gravel (wet side) | 0.026 |
| Grass (wet side) | 0.027 |
| Gravel (wet side) | 0.028 |
| Grass (wet side) | 0.029 |
| Gravel (wet side) | 0.030 |
| Grass (wet side) | 0.031 |
| Gravel (wet side) | 0.032 |
| Grass (wet side) | 0.033 |
| Gravel (wet side) | 0.034 |
| Grass (wet side) | 0.035 |
| Gravel (wet side) | 0.036 |
| Grass (wet side) | 0.037 |
| Gravel (wet side) | 0.038 |
| Grass (wet side) | 0.039 |
| Gravel (wet side) | 0.040 |
| Grass (wet side) | 0.041 |
| Gravel (wet side) | 0.042 |
| Grass (wet side) | 0.043 |
| Gravel (wet side) | 0.044 |
| Grass (wet side) | 0.045 |
| Gravel (wet side) | 0.046 |
| Grass (wet side) | 0.047 |
| Gravel (wet side) | 0.048 |
| Grass (wet side) | 0.049 |
| Gravel (wet side) | 0.050 |
| Grass (wet side) | 0.051 |
| Gravel (wet side) | 0.052 |
| Grass (wet side) | 0.053 |
| Gravel (wet side) | 0.054 |
| Grass (wet side) | 0.055 |
| Gravel (wet side) | 0.056 |
| Grass (wet side) | 0.057 |
| Gravel (wet side) | 0.058 |
| Grass (wet side) | 0.059 |
| Gravel (wet side) | 0.060 |
| Grass (wet side) | 0.061 |
| Gravel (wet side) | 0.062 |
| Grass (wet side) | 0.063 |
| Gravel (wet side) | 0.064 |
| Grass (wet side) | 0.065 |
| Gravel (wet side) | 0.066 |
| Grass (wet side) | 0.067 |
| Gravel (wet side) | 0.068 |
| Grass (wet side) | 0.069 |
| Gravel (wet side) | 0.070 |
| Grass (wet side) | 0.071 |
| Gravel (wet side) | 0.072 |
| Grass (wet side) | 0.073 |
| Gravel (wet side) | 0.074 |
| Grass (wet side) | 0.075 |
| Gravel (wet side) | 0.076 |
| Grass (wet side) | 0.077 |
| Gravel (wet side) | 0.078 |
| Grass (wet side) | 0.079 |
| Gravel (wet side) | 0.080 |
| Grass (wet side) | 0.081 |
| Gravel (wet side) | 0.082 |
| Grass (wet side) | 0.083 |
| Gravel (wet side) | 0.084 |
| Grass (wet side) | 0.085 |
| Gravel (wet side) | 0.086 |
| Grass (wet side) | 0.087 |
| Gravel (wet side) | 0.088 |
| Grass (wet side) | 0.089 |
| Gravel (wet side) | 0.090 |
| Grass (wet side) | 0.091 |
| Gravel (wet side) | 0.092 |
| Grass (wet side) | 0.093 |
| Gravel (wet side) | 0.094 |
| Grass (wet side) | 0.095 |
| Gravel (wet side) | 0.096 |
| Grass (wet side) | 0.097 |
| Gravel (wet side) | 0.098 |
| Grass (wet side) | 0.099 |
| Gravel (wet side) | 0.100 |

| T_{OL} = | T_1 = |
|-----------------------|----------------------|
| $n = 0.15$ | $D = 328$ (ft) |
| $L = 100$ (ft) | $S = 0.0113$ (ft/ft) |
| $P_2 = 4.89$ (in) | $V = 0.7$ (ft/s) |
| $S = 0.0113$ (ft/ft) | |
| $T_{OL} = 9.96$ (min) | $T_1 = 7.81$ (min) |

$T_c = 17.77$ (min)



Intensity:

SEE FIG. 2.1-2.1a

| | |
|--------------|---------------|
| i (500-YR) = | 15.24 (in/hr) |
| i (100-YR) = | 8.8 (in/hr) |
| i (10-YR) = | 6 (in/hr) |
| i (2-YR) = | 4.1 (in/hr) |

Peak Flow Rate:

$Q = CIA$
 $C = 0.4$ Mixed use area. Residential lots b/w 1/4 and 1/2 acres; sub-basin slope 1-3.5%; and golf course

| i (500-YR) | i (100-YR) | i (10-YR) | i (2-YR) |
|---------------------|--------------------|-----------|----------|
| 15.24 | 8.8 | 6 | 4.1 |
| $A = 2.99$ (Ac) | | | |
| Q (500-YR) = | 18.22 (cfs) | | |
| Q (100-YR) = | 10.52 (cfs) | | |
| Q (10-YR) = | 7.18 (cfs) | | |
| Q (2-YR) = | 4.90 (cfs) | | |

DA FE 101 EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 265698.58 cft
 Volume (100-yr) = 1.38*area*43560 = 179737.27 cft
 Volume (10-yr) = 0.70*area*43560 = 91171.08 cft
 Volume (2-yr) = 0.41*area*43560 = 53400.204 cft
 A= 2.99 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Qp}$

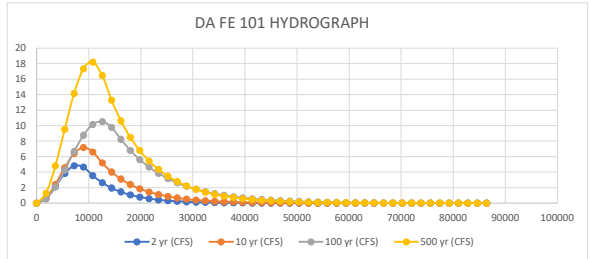
$Q_i = \frac{Q_p}{2} \left[2 - \cos \left(\frac{\pi t_i}{T_p} \right) \right]$ $t_i = 1.25 T_p$

$Q_i = 4.34 Q_p \exp \left(-1.8 t_i / T_p \right)$ $t_i = 1.25 T_p$

| DA FE 101 Existing Conditions | | | | |
|-------------------------------|----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 4.90 | 7.18 | 10.52 | 18.22 |
| TP= | 7834.532 | 9140.288 | 12285.971 | 10490.308 |
| 1.25*TP= | 9793.165 | 11425.360 | 15357.464 | 13112.885 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|--------------|--------------|--------------|
| 0 | 0 | 0.000000000 | 0 | 0 |
| 1800.00 | 0.611415314 | 0.6650441895 | 0.547644825 | 1.291969825 |
| 3600.00 | 2.14071902 | 2.4136417670 | 2.076595241 | 4.801459822 |
| 5400.00 | 3.825173779 | 4.5975794332 | 4.268623145 | 9.5331329 |
| 7200.00 | 4.824660954 | 6.4072612824 | 6.667490801 | 14.14502492 |
| 9000.00 | 4.640688203 | 7.1718297900 | 8.773909875 | 17.32914321 |
| 10800.00 | 3.545849844 | 6.6078558350 | 10.14946083 | 18.18243034 |
| 12600.00 | 2.630305964 | 5.1890485526 | 10.50784335 | 16.46288295 |
| 14400.00 | 1.951156922 | 4.0170223213 | 9.774465492 | 13.27625359 |
| 16200.00 | 1.447365205 | 3.1097161968 | 8.227305222 | 10.62185804 |
| 18000.00 | 1.073653285 | 2.407339813 | 6.800508538 | 8.498170619 |
| 19800.00 | 0.796434356 | 1.8636046139 | 5.621149955 | 6.79908389 |
| 21600.00 | 0.590793781 | 1.4426809185 | 4.646318234 | 5.439705063 |
| 23400.00 | 0.438249919 | 1.1168292980 | 3.840543892 | 4.35211444 |
| 25200.00 | 0.325093116 | 0.8645762655 | 3.174508643 | 3.481971886 |
| 27000.00 | 0.241153574 | 0.6692984507 | 2.623978635 | 2.785801794 |
| 28800.00 | 0.178887351 | 0.5181271266 | 2.168922707 | 2.228820877 |
| 30600.00 | 0.132698362 | 0.4011001654 | 1.792783541 | 1.783200267 |
| 32400.00 | 0.098435441 | 0.3105055390 | 1.481875225 | 1.426675076 |
| 34200.00 | 0.073019259 | 0.2403730989 | 1.224885288 | 1.141431957 |
| 36000.00 | 0.054165574 | 0.1860811465 | 1.012463089 | 0.913219089 |
| 37800.00 | 0.040179939 | 0.1440518645 | 0.836879597 | 0.730634095 |
| 39600.00 | 0.029805417 | 0.1115155407 | 0.691746166 | 0.584554338 |
| 41400.00 | 0.022109613 | 0.0863280448 | 0.571782082 | 0.467681124 |
| 43200.00 | 0.016400877 | 0.0668295314 | 0.472622423 | 0.374175024 |
| 45000.00 | 0.012166145 | 0.0517350564 | 0.390659242 | 0.299364121 |
| 46800.00 | 0.009024828 | 0.0400499001 | 0.32291029 | 0.23951058 |
| 48600.00 | 0.006694603 | 0.0310040157 | 0.266910504 | 0.191623891 |
| 50400.00 | 0.004966046 | 0.0240012830 | 0.22062232 | 0.153311456 |
| 52200.00 | 0.003683806 | 0.0185802250 | 0.18236153 | 0.12265904 |
| 54000.00 | 0.002732641 | 0.0143835961 | 0.150736007 | 0.098135133 |
| 55800.00 | 0.002027069 | 0.0111348402 | 0.12459505 | 0.078514428 |
| 57600.00 | 0.001503677 | 0.0086198657 | 0.102987513 | 0.0628166 |
| 59400.00 | 0.001115425 | 0.0066729368 | 0.0851272 | 0.050257326 |
| 61200.00 | 0.000827421 | 0.0051657516 | 0.070364261 | 0.040209098 |
| 63000.00 | 0.000613779 | 0.0039989874 | 0.058161542 | 0.032169868 |
| 64800.00 | 0.000455301 | 0.0030957547 | 0.048075044 | 0.025737967 |
| 66600.00 | 0.000337741 | 0.0023965310 | 0.039737768 | 0.020592031 |
| 68400.00 | 0.000250536 | 0.0018552377 | 0.032846361 | 0.016474951 |
| 70200.00 | 0.000185847 | 0.0014362038 | 0.027150075 | 0.013181022 |
| 72000.00 | 0.000137861 | 0.001118151 | 0.022441652 | 0.010545667 |
| 73800.00 | 0.000102265 | 0.0008606946 | 0.018549773 | 0.008437213 |
| 75600.00 | 7.58602E-05 | 0.0006662935 | 0.015332832 | 0.006750314 |
| 77400.00 | 5.6273E-05 | 0.0005158009 | 0.01267378 | 0.005400686 |
| 79200.00 | 4.17432E-05 | 0.0003992994 | 0.010475866 | 0.004320897 |
| 81000.00 | 3.0965E-05 | 0.0003091115 | 0.008659119 | 0.003456996 |
| 82800.00 | 2.29698E-05 | 0.0002392939 | 0.007157436 | 0.002765819 |
| 84600.00 | 1.7039E-05 | 0.0001852457 | 0.005916179 | 0.002212833 |
| 86400.00 | 1.26395E-05 | 0.0001434051 | 0.004890182 | 0.001770409 |

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DA FE 102 DRAINAGE CALCULATIONS

Time of Concentration:

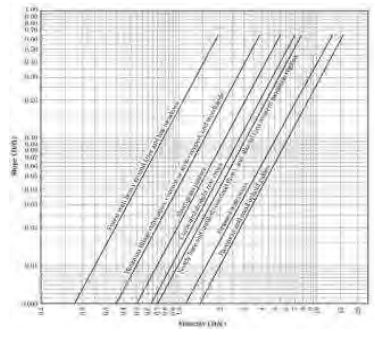
$T_c = T_{OL} + T_1 + \dots + T_n$

Handwritten notes detailing the calculation of time of concentration components. A table lists Manning's roughness coefficients for various materials:

| Material | n |
|-------------------------------------|-------|
| Smooth finished concrete (open and) | 0.012 |
| Galvanized iron (open) | 0.014 |
| Cast-iron pipe (open) | 0.013 |
| Concrete pipe (open) | 0.012 |
| Steel pipe (open) | 0.014 |
| Asphalt (open) | 0.016 |
| Gravel (open) | 0.024 |
| Stone (open) | 0.030 |
| Wood (open) | 0.040 |
| Earth (open) | 0.040 |

| T_{OL} = T_t ; multiply by 60 to convert hrs. to min. (L=max 300') | $T =$ |
|------------------------------------------------------------------------|----------------------|
| $n = 0.15$ | $D = 421$ (ft) |
| $L = 100$ (ft) | $S = 0.0113$ (ft/ft) |
| $P_s = 4.89$ (in) | $V = 0.7$ (ft/s) |
| $S = 0.0113$ (ft/ft) | |
| $T_{OL} = 9.96$ (min) | $T_1 = 10.02$ (min) |

$T_c = 19.98$ (min)



Intensity:

SEE FIG. 2.1-2.1a

| | | |
|----------------|-------|---------|
| I (500-YR) = | 14.70 | (in/hr) |
| I (100-YR) = | 8.3 | (in/hr) |
| I (10-YR) = | 5.7 | (in/hr) |
| I (2-YR) = | 4 | (in/hr) |

Peak Flow Rate:

$Q = CIA$

C = 0.4 Mixed use area. Residential lots b/w 1/4 and 1/2 acres; sub-basin slope 1-3.5%; and golf course

| | i (500-YR) | i (100-YR) | i (10-YR) | i (2-YR) |
|---------------------|--------------------|--------------|-------------|------------|
| | 14.70 | 8.3 | 5.7 | 4 |
| A = | 2.48 (Ac) | | | |
| Q (500-YR) = | 14.59 (cfs) | | | |
| Q (100-YR) = | 8.23 (cfs) | | | |
| Q (10-YR) = | 5.65 (cfs) | | | |
| Q (2-YR) = | 3.97 (cfs) | | | |

DA FE 102 EXISTING CALCULATIONS

Volume (500-yr) = 2.04*area*43560 = 220378.75 cft
 Volume (100-yr) = 1.38*area*43560 = 149079.74 cft
 Volume (10-yr) = 0.70*area*43560 = 75620.16 cft
 Volume (2-yr) = 0.41*area*43560 = 44291.808 cft
 A= 2.48 Ac

TP = time to Qp in seconds

TP = $\frac{V}{1.39 Q_p}$

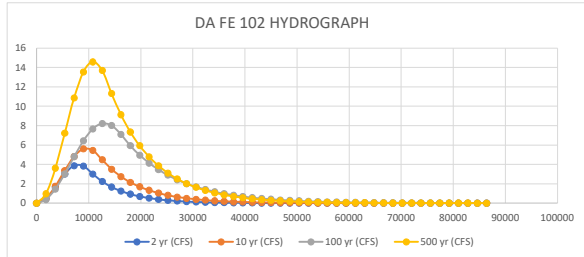
$Q_p = \frac{Q_p}{2} \left[2 - \cos \left(\frac{\pi t_i}{T_p} \right) \right]$
 $t_i = 1.25 T_p$

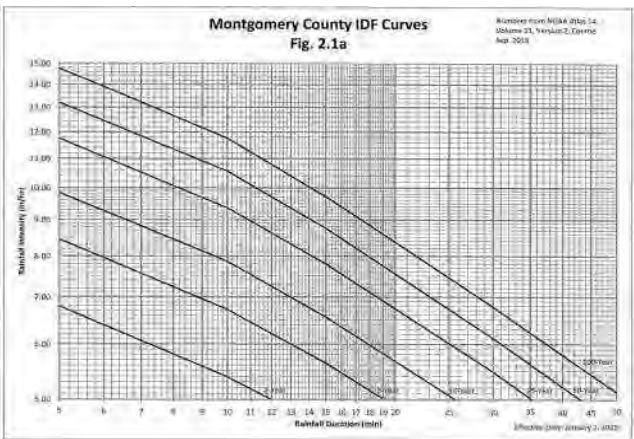
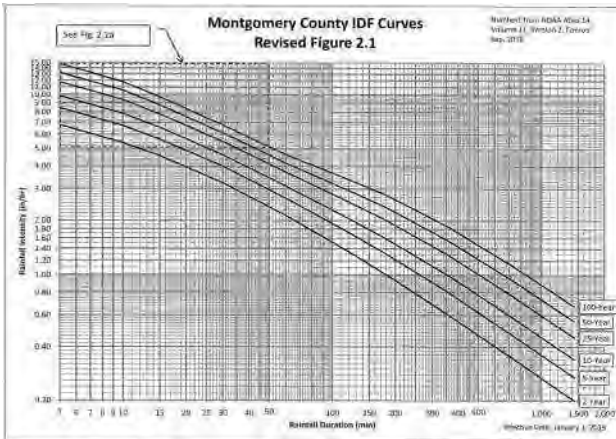
$Q_p = 4.34 Q_{ps} \left(\frac{t_i}{T_p} \right)^{-0.8}$
 $t_i = 1.25 T_p$

| DA FE 102 Existing Conditions | | | | |
|-------------------------------|-----------|-----------|------------|------------|
| | 2 - Year | 10 - Year | 100 - Year | 500 - Year |
| Qp= | 3.97 | 5.65 | 8.23 | 14.59 |
| TP= | 8030.396 | 9621.356 | 13026.090 | 10869.446 |
| 1.25*TP= | 10037.995 | 12026.694 | 16282.612 | 13586.808 |

| ti (sec) | 2 yr (CFS) | 10 yr (CFS) | 100 yr (CFS) | 500 yr (CFS) |
|----------|-------------|--------------|--------------|--------------|
| 0 | 0 | 0.000000000 | 0 | 0 |
| 1800.00 | 0.471912554 | 0.4744174972 | 0.381869598 | 0.964938439 |
| 3600.00 | 1.663152778 | 1.7384510005 | 1.456634828 | 3.60441796 |
| 5400.00 | 3.007025897 | 3.3678789403 | 3.024907736 | 7.219996496 |
| 7200.00 | 3.864226875 | 4.8158499265 | 4.795745966 | 10.85494294 |
| 9000.00 | 3.82696952 | 5.5964112347 | 6.440627714 | 13.54740119 |
| 10800.00 | 2.997502229 | 5.4475991253 | 7.65439833 | 14.58491027 |
| 12600.00 | 2.239799801 | 4.4720438503 | 8.211881903 | 13.69293122 |
| 14400.00 | 1.673627829 | 3.5065637470 | 8.009655371 | 11.31018505 |
| 16200.00 | 1.25057164 | 2.7495234222 | 7.09466002 | 9.119557588 |
| 18000.00 | 0.934454721 | 2.1559232302 | 5.928094999 | 7.35322457 |
| 19800.00 | 0.698245185 | 1.6904751613 | 4.953346633 | 5.929005991 |
| 21600.00 | 0.521744208 | 1.3255144883 | 4.138874777 | 4.780638985 |
| 23400.00 | 0.389858784 | 1.0393460365 | 3.458325388 | 3.854694891 |
| 25200.00 | 0.291311085 | 0.8149591672 | 2.889677783 | 3.108093448 |
| 27000.00 | 0.21767407 | 0.6390157088 | 2.414532109 | 2.506098447 |
| 28800.00 | 0.162650868 | 0.5010570990 | 2.017513972 | 2.020701607 |
| 30600.00 | 0.121536317 | 0.3928826991 | 1.685776973 | 1.629319467 |
| 32400.00 | 0.090814618 | 0.3080623258 | 1.408587024 | 1.31374267 |
| 34200.00 | 0.067858686 | 0.2415540231 | 1.17697503 | 1.059288763 |
| 36000.00 | 0.050705507 | 0.1894043548 | 0.983446673 | 0.854119083 |
| 37800.00 | 0.037888274 | 0.1485134016 | 0.821739912 | 0.688687951 |
| 39600.00 | 0.028310954 | 0.1164504927 | 0.686622368 | 0.555298556 |
| 41400.00 | 0.02115457 | 0.0913097210 | 0.573722013 | 0.447744854 |
| 43200.00 | 0.015807161 | 0.0715966498 | 0.479385705 | 0.361022827 |
| 45000.00 | 0.01181146 | 0.0561394800 | 0.400560984 | 0.291097666 |
| 46800.00 | 0.008825783 | 0.0440193952 | 0.334697302 | 0.234716047 |
| 48600.00 | 0.00659482 | 0.0345159440 | 0.279663493 | 0.189254773 |
| 50400.00 | 0.004927795 | 0.0270642154 | 0.233678816 | 0.152598724 |
| 52200.00 | 0.003682157 | 0.0212212581 | 0.195255335 | 0.123042447 |
| 54000.00 | 0.002751389 | 0.0166397506 | 0.163149774 | 0.099210816 |
| 55800.00 | 0.002055899 | 0.0130473555 | 0.136323285 | 0.079995044 |
| 57600.00 | 0.001536213 | 0.0102305311 | 0.113907838 | 0.064501103 |
| 59400.00 | 0.001147892 | 0.0080218376 | 0.095178131 | 0.052008125 |
| 61200.00 | 0.00085773 | 0.0062899842 | 0.079528124 | 0.041934866 |
| 63000.00 | 0.000640915 | 0.0049320246 | 0.066451426 | 0.033812658 |
| 64800.00 | 0.000478906 | 0.0038672382 | 0.055524911 | 0.027263611 |
| 66600.00 | 0.000357849 | 0.0030323310 | 0.046395028 | 0.021983024 |
| 68400.00 | 0.000267393 | 0.0023776739 | 0.038766358 | 0.017725214 |
| 70200.00 | 0.000199802 | 0.0018643523 | 0.03239206 | 0.014292084 |
| 72000.00 | 0.000149296 | 0.0014618529 | 0.027065879 | 0.011523904 |
| 73800.00 | 0.000111557 | 0.0011462500 | 0.022615474 | 0.009291882 |
| 75600.00 | 8.33582E-05 | 0.0008987834 | 0.018896844 | 0.007492172 |
| 77400.00 | 6.22871E-05 | 0.0007047429 | 0.015789662 | 0.006041041 |
| 79200.00 | 4.65423E-05 | 0.0005525943 | 0.01319339 | 0.004870974 |
| 81000.00 | 3.47774E-05 | 0.0004332934 | 0.011024019 | 0.003927534 |
| 82800.00 | 2.59865E-05 | 0.0003397487 | 0.009211355 | 0.003166824 |
| 84600.00 | 1.94177E-05 | 0.0002663995 | 0.007696745 | 0.002553454 |
| 86400.00 | 1.45093E-05 | 0.0002088859 | 0.00643118 | 0.002058885 |

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POINT PRECIPITATION FREQUENCY (PF) ESTIMATES WITH 95% CONFIDENCE INTERVALS AND SUPPLEMENTARY INFORMATION (Table 2.2, Volume 1)

PF Station: **PF Station** | **Supplementary information** | **Thumbnail**

PDS-based precipitation frequency estimates with 95% confidence intervals (in inches)

| Return Period | 1 | 5 | 10 | 25 | 50 | 100 | 250 | 500 | 1000 |
|---------------|------|------|------|------|------|------|------|------|------|
| 100-Year | 1.92 | 2.10 | 2.27 | 2.54 | 2.73 | 3.01 | 3.27 | 3.57 | 3.84 |
| 50-Year | 1.80 | 1.97 | 2.13 | 2.39 | 2.57 | 2.84 | 3.09 | 3.37 | 3.63 |
| 25-Year | 1.68 | 1.84 | 1.99 | 2.24 | 2.41 | 2.67 | 2.90 | 3.15 | 3.40 |
| 10-Year | 1.56 | 1.71 | 1.85 | 2.09 | 2.25 | 2.50 | 2.71 | 2.94 | 3.16 |
| 5-Year | 1.44 | 1.58 | 1.71 | 1.94 | 2.09 | 2.32 | 2.51 | 2.72 | 2.92 |
| 2-Year | 1.32 | 1.45 | 1.57 | 1.79 | 1.93 | 2.14 | 2.31 | 2.50 | 2.68 |

Supplementary information: **Supplementary information** | **Thumbnail**

POINT PRECIPITATION FREQUENCY (PF) ESTIMATES WITH 95% CONFIDENCE INTERVALS AND SUPPLEMENTARY INFORMATION (Table 2.2, Volume 1)

PF Station: **PF Station** | **Supplementary information** | **Thumbnail**

PDS-based precipitation frequency estimates with 95% confidence intervals (in inches/hour)

| Return Period | 1 | 5 | 10 | 25 | 50 | 100 | 250 | 500 | 1000 |
|---------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 100-Year | 0.032 | 0.035 | 0.037 | 0.042 | 0.045 | 0.050 | 0.054 | 0.059 | 0.063 |
| 50-Year | 0.030 | 0.032 | 0.034 | 0.039 | 0.042 | 0.046 | 0.050 | 0.054 | 0.058 |
| 25-Year | 0.028 | 0.030 | 0.031 | 0.036 | 0.038 | 0.042 | 0.045 | 0.049 | 0.052 |
| 10-Year | 0.026 | 0.028 | 0.029 | 0.034 | 0.036 | 0.040 | 0.043 | 0.046 | 0.049 |
| 5-Year | 0.024 | 0.026 | 0.027 | 0.032 | 0.034 | 0.037 | 0.040 | 0.043 | 0.046 |
| 2-Year | 0.022 | 0.024 | 0.025 | 0.030 | 0.032 | 0.035 | 0.038 | 0.041 | 0.044 |

Supplementary information: **Supplementary information** | **Thumbnail**

POINT PRECIPITATION FREQUENCY (PF) ESTIMATES WITH 95% CONFIDENCE INTERVALS AND SUPPLEMENTARY INFORMATION (Table 2.2, Volume 1)

TABLE 2.2 Rational Method Runoff Coefficients (for 5-10 Year Frequency Storms)

| Description of Area | Basin Slope < 1% | Basin Slope 1%-3.4% | Basin Slope 3.5%-5.5% |
|--------------------------------------------|------------------|---------------------|-----------------------|
| Single-Family Residential Districts | | | |
| Lots greater than 1/2 acre | 0.30 | 0.35 | 0.40 |
| Lots 1/4 - 1/2 acre | 0.40 | 0.45 | 0.50 |
| Lots less than 1/4 acre | 0.50 | 0.55 | 0.60 |
| Multi-Family Residential Districts | 0.60 | 0.65 | 0.70 |
| Apartment Dwelling Areas | 0.75 | 0.80 | 0.85 |
| Business Districts | | | |
| Downtown | 0.85 | 0.87 | 0.90 |
| Neighborhood | 0.75 | 0.80 | 0.85 |
| Industrial Districts | | | |
| Light | 0.50 | 0.55 | 0.60 |
| Heavy | 0.60 | 0.75 | 0.90 |
| Railroad Yard Areas | 0.20 | 0.30 | 0.40 |
| Cemeteries (%) | 0.10 | 0.15 | 0.25 |
| Playgrounds | 0.20 | 0.25 | 0.35 |
| Streets | | | |
| Asphalt | 0.80 | 0.80 | 0.80 |
| Concrete | 0.85 | 0.85 | 0.85 |
| Concrete Driveways and Walks | 0.85 | 0.85 | 0.85 |
| Roofs | 0.85 | 0.95 | 0.95 |
| Lawn Areas | | | |
| Sandy Soil | 0.05 | 0.08 | 0.12 |
| Clay Soil | 0.15 | 0.18 | 0.22 |
| Woodlands | | | |
| Sandy Soil | 0.15 | 0.18 | 0.25 |
| Clay Soil | 0.18 | 0.20 | 0.30 |
| Pasture | | | |
| Sandy Soil | 0.25 | 0.33 | 0.40 |
| Clay Soil | 0.30 | 0.40 | 0.50 |
| Cultivated | | | |
| Sandy Soil | 0.30 | 0.55 | 0.70 |
| Clay Soil | 0.35 | 0.60 | 0.80 |