



IAGT 2015 SYMPOSIUM

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LOW EMISSIONS COMBUSTION SYSTEM RETROFITS FOR MATURE FRAME GAS TURBINE POWER PLANTS

By

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Agenda

NOx, CO & Combustion Fundamentals

LEC-III® System

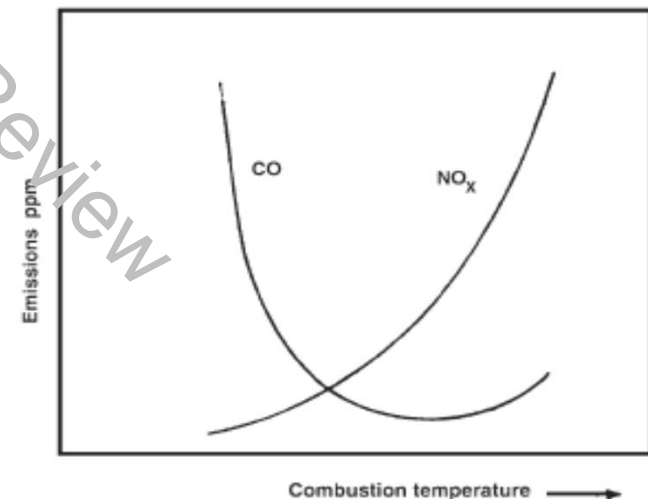
Fr7B Low Emissions Conversion Case Study

Analytical Approach

Results and Summary

Gas Turbine Combustion Emissions

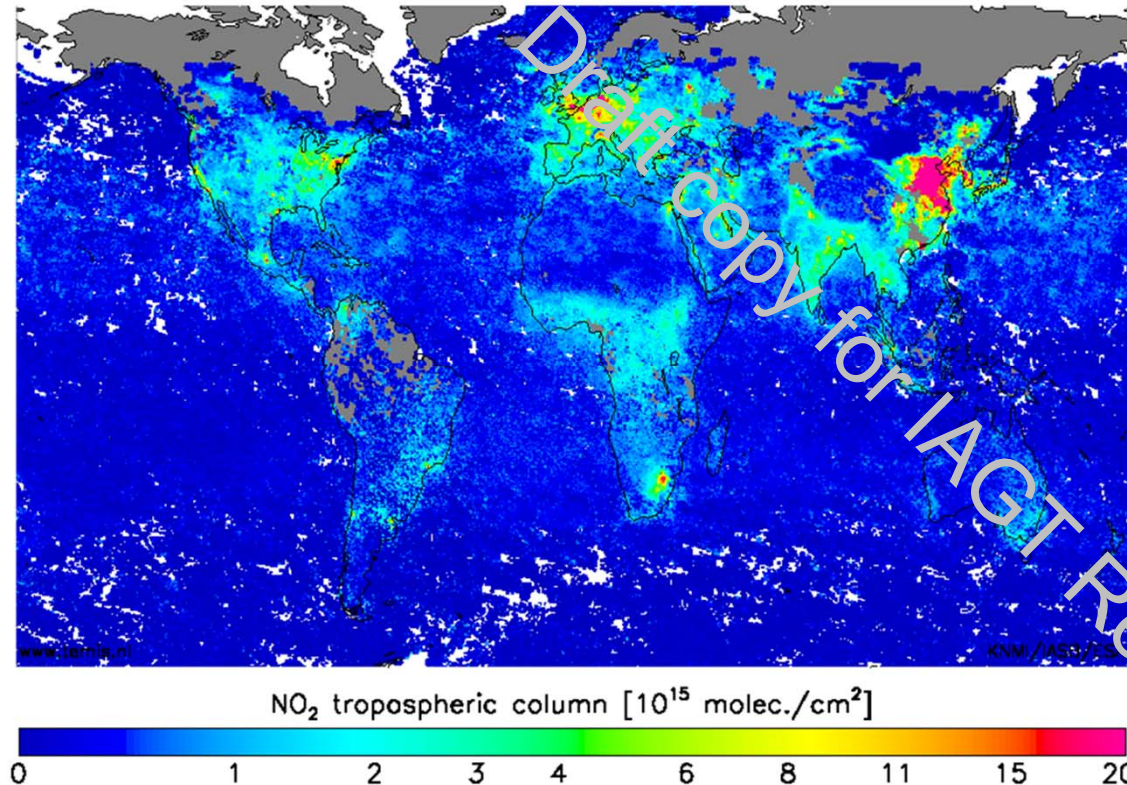
- NO_x & CO: combustion bi-products
 - Limited by regulations
 - US: EPA, EU: EEA,
 - CA: AQMS, BLIERS,etc
- NO_x generation:
 - High firing temperature
- CO generation:
 - Typical at low load.



NOx & CO Pollution

SCIAMACHY tropospheric NO₂ March 2012

KNMI/IASB/ESA



GT Pollution Control

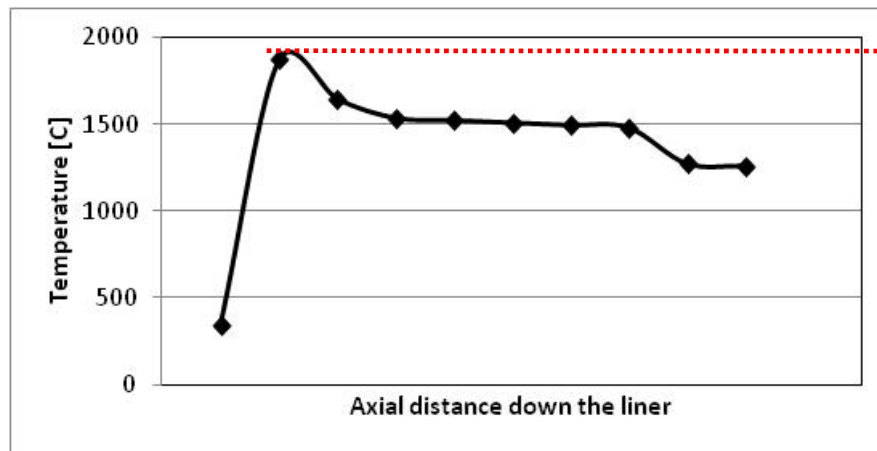
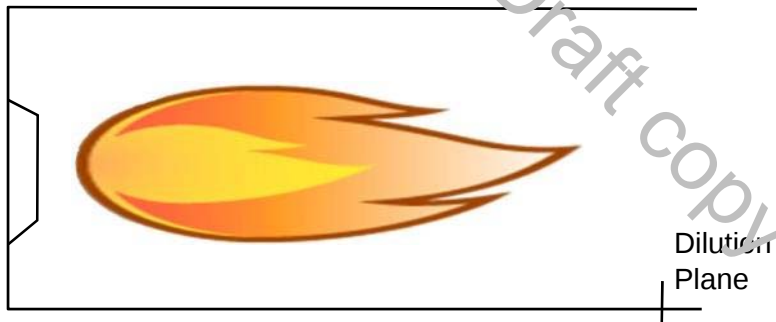
- Post Treatment:
Exhaust SCR can be impractical and/or costly
- or
- Pre-Treatment: Water / Steam injection can be costly
- or
- Combustion Pre-Mix

<http://www.esa.int> Photo: KNMI/IASB/ESA .

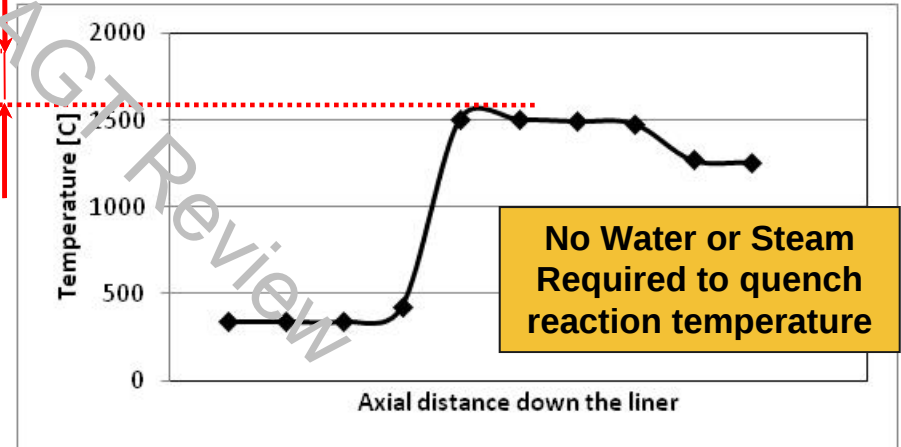
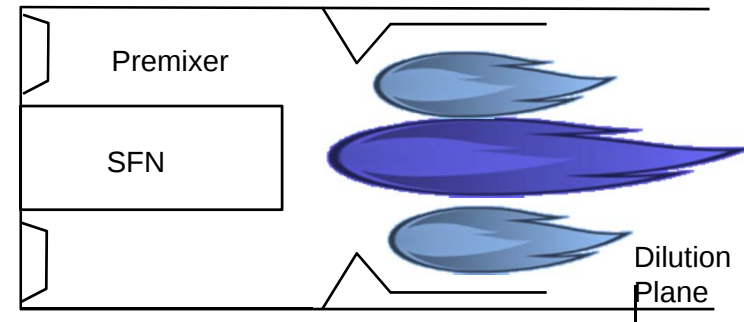
NOx emissions – A global issue

Combustion Concept

Diffusion Burning (Single Body Nozzle)



Premix Burning (LEC-III[®] or DLN-1)



Premix Combustion : Lower reaction temperatures : Lower NOx & Saves water!

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LEC-III® System

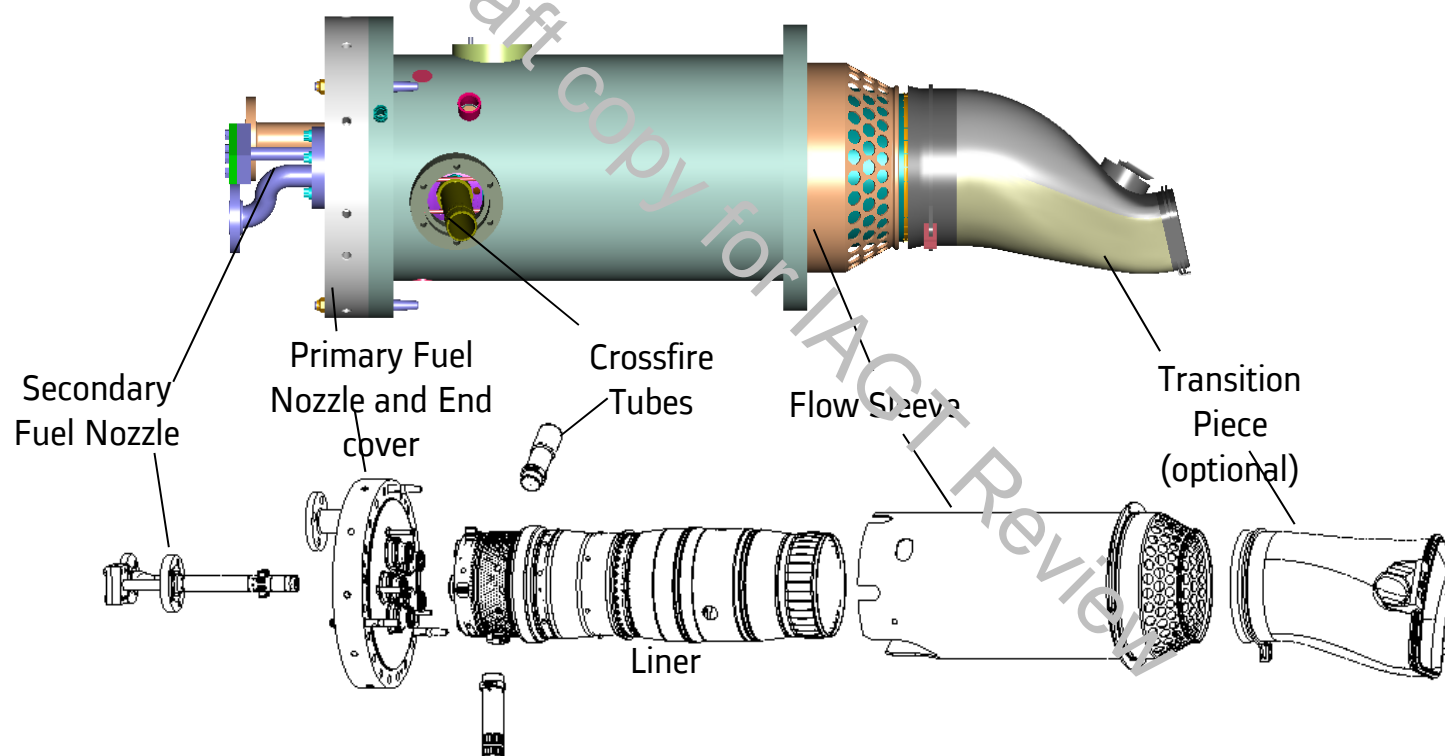
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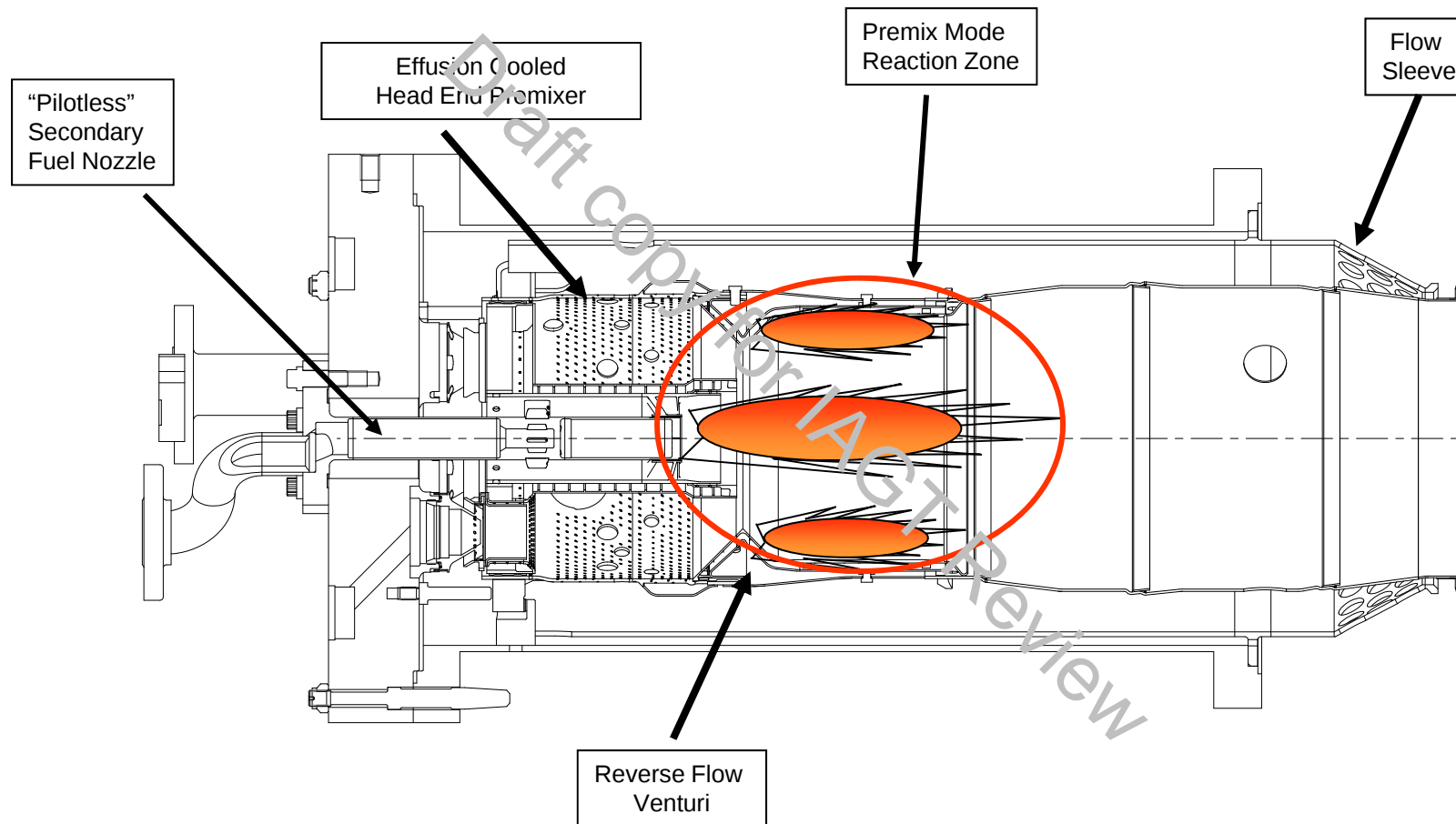
LEC-III® Combustion System

- Fleet Leader ~50K Hrs
- +1.2M fleet fired hours
- +9000 starts in fleet
- 24,000 FFH / 900 FFS



Sub-5 PPM NOX Consistently Achieved

LEC-III[®] Technology Features



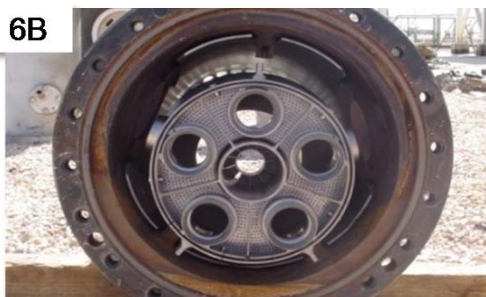
Improved Mixing Allows Stable Ultra-low Emissions

LEC-III® – Over 3.6 GW Installed



LEC-III® Experience

6B



9E & 7E



501B6 & D5



Company	Location	GT Frame	# of Installations	Dates of Install(s)	Type
BTEC	Mississippi, USA	7B/E	3	1999	Conversion
BTEC	Georgia, USA	7E	6	2000	Conversion
TransAlta	Alberta, CAN	7EA	1	2001	Drop In
GWF Power	California, USA	7EA	1	2003	Drop In
DOW	Texas, USA	7EA	3	2003-04	Drop In
DOW	Texas, USA	6B	1	2004	Drop In
Roquette	France	6B	1	2004	Drop In
ENEL	Italy	9E	1	2004	Drop In
PDO	Oman	6B	3	2004-06	Drop In
Calpine	Texas, USA	W 501D5	2	2005-07	Conversion
NRG	Texas, USA	7B-E	8	2005-09	Drop In
Amquide	Netherlands	6B	1	2006	Drop In
Optim	Texas, USA	7E	5	2006-07	Conversion
NRG	Texas, USA	7EA	2	2007	Drop In
PDO	Oman	6B	2	2007	Drop In
Dalkia	France	6B	1	2007	Drop In
Tate & Lyle	France	6B	2	2007-09	Drop In
Air Products	Texas, USA	7EA	1	2008	Drop In
NV Energy	Nevada, USA	W 501B6	4	2008-09	Conversion
Vattenfall SP	Germany	6B	1	2009	Drop In
AES Elsta	Netherlands	9E	3	2009-10	Drop In
BlueSky, CPU	China	9E	2	2011-12	Conversion
Tampeeren	Finland	6B	1	2011	Drop In
NRG Petronova	Texas, USA	7E	1	2012	Conversion
WFEC	Oklahoma, USA	7E	1	2012	Conversion
Helsingor	Denmark	6B	1	2012	Conversion
GasCo	Abu Dhabi UAE	6B	1	2013	Conversion
Hunstman Chem	Port Neches, TX	6B	1	2014	Conversion
MPC- Henneng	China	9E	1	2014	Conversion
NRG - Gilbert	NJ, USA	7B	4	2014-15*	Conversion
AEP-Comanche	Oklahoma, USA	W501B6	1	2015*	Conversion
25			68		

Technology Platform – 1.2 Million+ fired hours and 9000 Starts

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LEC-III® System

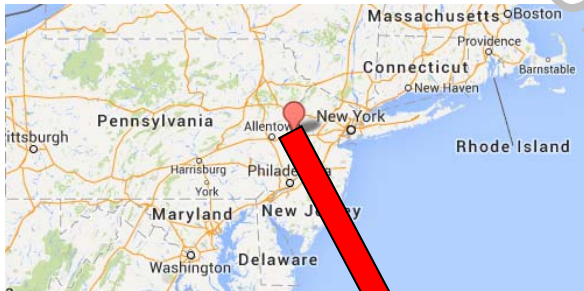
Fr7B Low Emissions Conversion Case Study

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Fr 7B Conversion Case Study

Frame 7B LEC-III® Combustion Conversion



Overview

- Combined Cycle Facility
- 4 x Frame 7B's GT's - CC or SC
- Began operation in 1974
- Units measured at (with water injection):
 - ~35 ppm NOx
 - 20-100 ppm CO
- HEDD Ruling : (High Energy Demand Day)
Likely to close older peaking units due to tighter emissions cap

Scope

Frame 7B Conversion to ultra low Nox

- Replace combustion system
- Remove liquid fuel system
- Remove water injection system
- Controls (Ovation) upgrade

Fr 7B Conversion Case Study

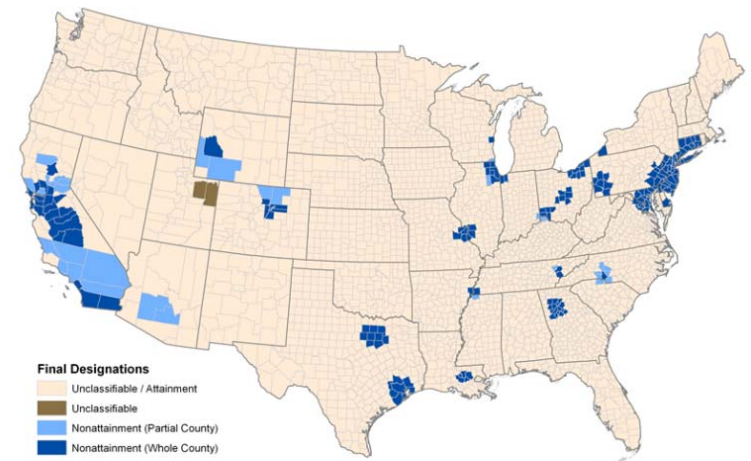
High Electric Demand Day (HEDD)

Peaking plants typically cause elevated ozone concentrations in the following conditions:

- Elevated Temperatures
- Elevated Electricity Demand

HEDD restrict NO_x Emissions on hot days

- Older units only profitable on hot days
- Older units would be limited to cold day operations



Nonattainment Areas for 2008
Ozone Standards

Source: EPA
<http://www.epa.gov/ozonedesignations/2008standards/final/finalmap.htm>

Peaking Plants Must Reduce Emissions

Source: https://www1.eere.energy.gov/wip/solutioncenter/pdfs/tap_webinar_20080717_mcnevin.pdf

Conversion Project Scope

Combustion System

- Remove Diffusion Flame – Dual Fuel
- Install LEC-III® Combustion System – Gas Only



Old



New



Conversion Project Scope

Fuel Delivery System

- Removal of Water Injection & Fuel Oil Systems
- New gas skids
- New Fuel Manifolds



Old



New



Conversion Project Scope

Control System

- Upgrade of Control System to Ovation™ platform
- New HMI in Control Room



Old

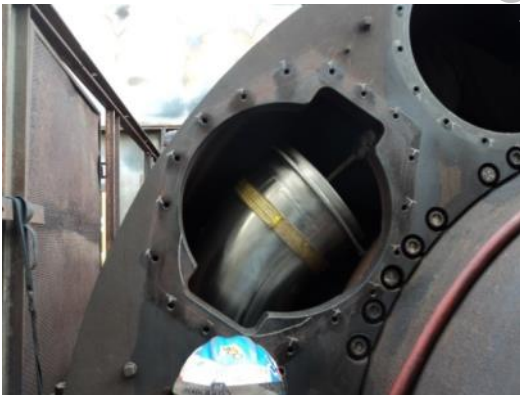


New



Conversion Project Scope

Conversion Complete



New

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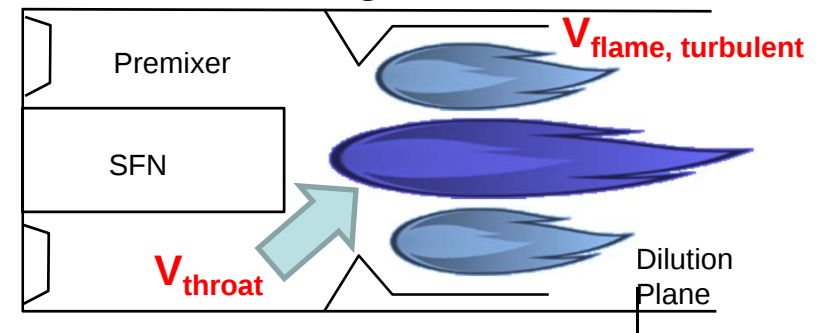
Challenges – Flashback avoidance

- **Flashback avoidance:**

- Flame flashback into the premixer prevented by maintaining:

$$V_{\text{throat}} \gg V_{\text{flame, turbulent}}$$

Premix Burning (LEC-III[®] or DLN-1)



- LEC-III[®] hardware previously used for 7B/E and 7E/EA units
- 7B running conditions decreases V_{throat} due to lower:
 - compressor air flow
 - compressor discharge temperature
- Flashback was identified as a risk item early on in the project
- 7B compressor pressure ratio was found to be lower than the 7E/EA
 - Net effect is 7B V_{throat} to $V_{\text{flame, turbulent}}$ ratio similar to 7EA

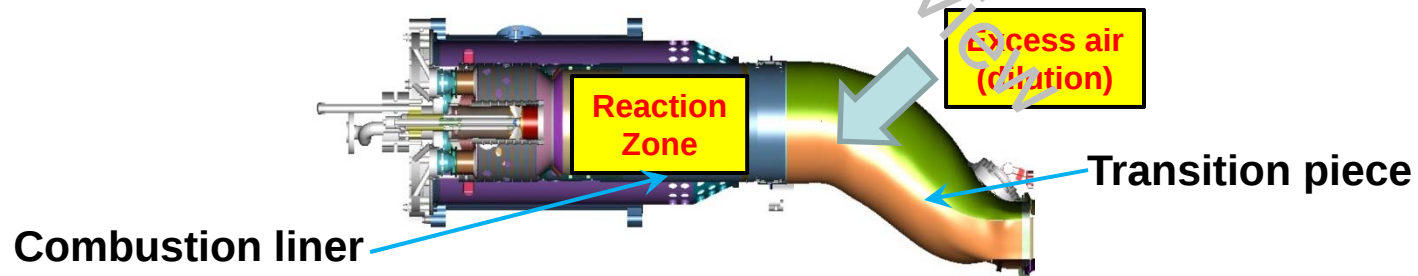
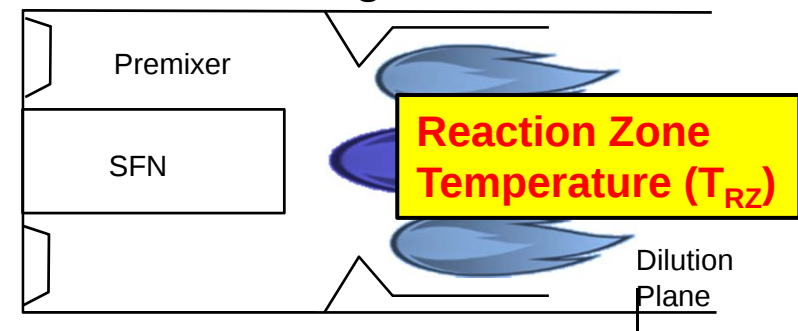
Flashback was a risk item, mitigations were ready but not needed

Challenges – Dilution air injection

- **Dilution air injection:**

- LEC-III[®] Reaction Zone Temperature (T_{RZ}) precisely set by:
 - Dilution air hole sizing
- Allows exact tuning to NO_x and CO emission targets
- 7B T_{RZ} target similar to previous 7B/E and 7E/EA applications
- 7B lower firing temperature increased the amount of dilution air
- Needed to identify injection location between the reaction zone region and the exit of the transition piece

Premix Burning (LEC-III[®] or DLN-1)

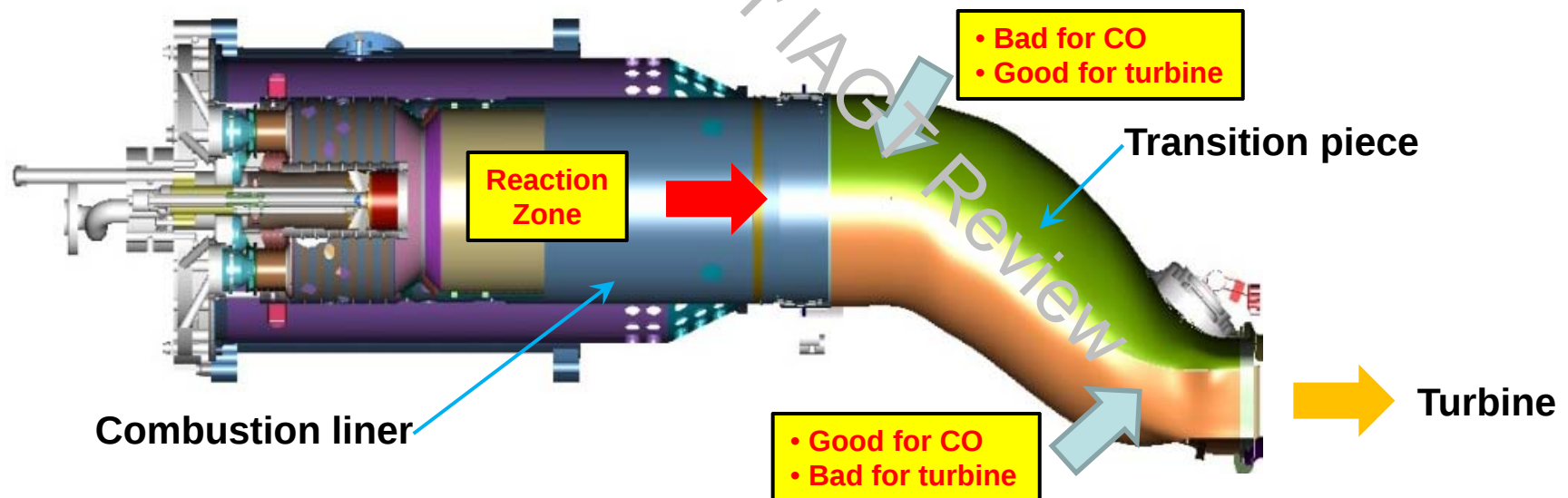


We have a lot of excess air, where/how are we going to use it?

Challenges – Dilution air injection (cont.)

- **Dilution air injection conundrum:**

- “Early” dilution air introduction
 - After the reaction zone
 - Poor CO characteristic
 - Good turbine inlet profile
- “Late” dilution air introduction
 - Before the transition piece exit
 - Good CO characteristic
 - Poor inlet temperature profile



How do we balance CO requirement and turbine life?

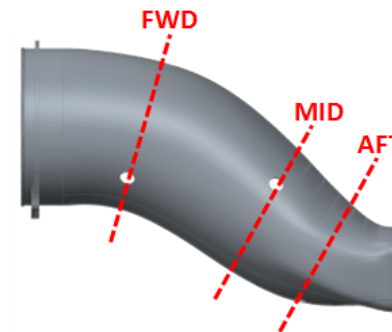
Solving the conundrum

- **Engineering approach:**

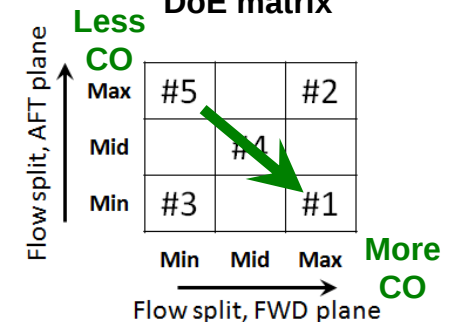
1. Design of Experiments Used

- Three injection planes defined on transition piece flowpath
- Hole locations selected in known low stress regions

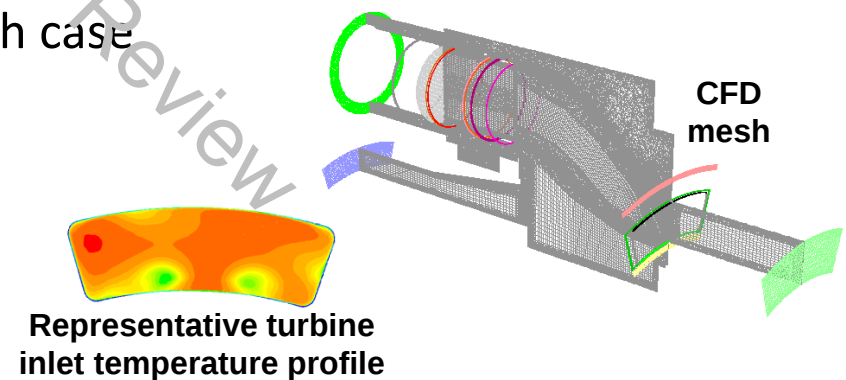
Three injection planes



Half factorial DoE matrix



2. Available air flow split according to a $\frac{1}{2}$ factorial matrix (five cases)
3. Five CFD runs performed to derive turbine inlet temperature
4. Impact on turbine assessed for each case
5. CO impact estimated for each case
6. Final decision on dilution scheme



Sturdy DoE approach, turbine life and CO requirement balanced

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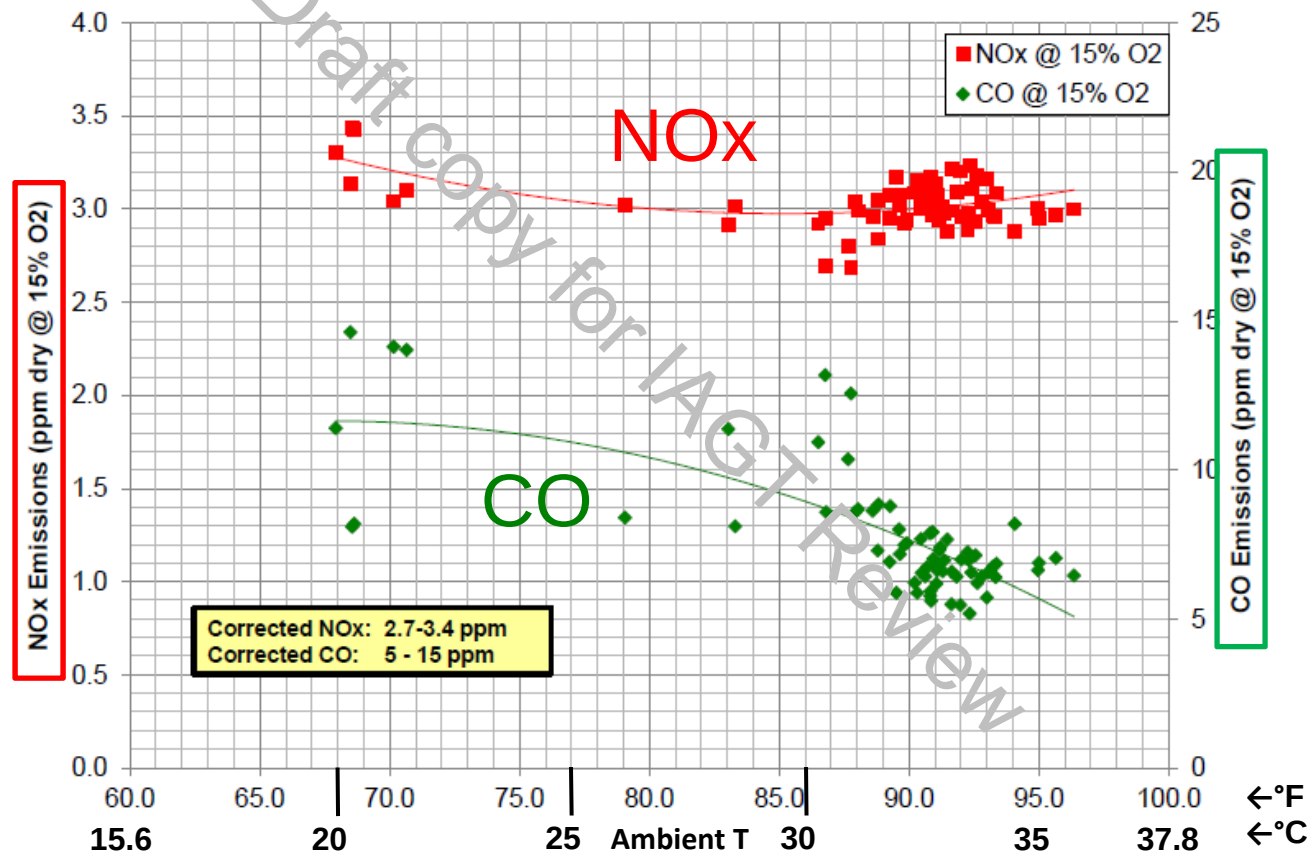
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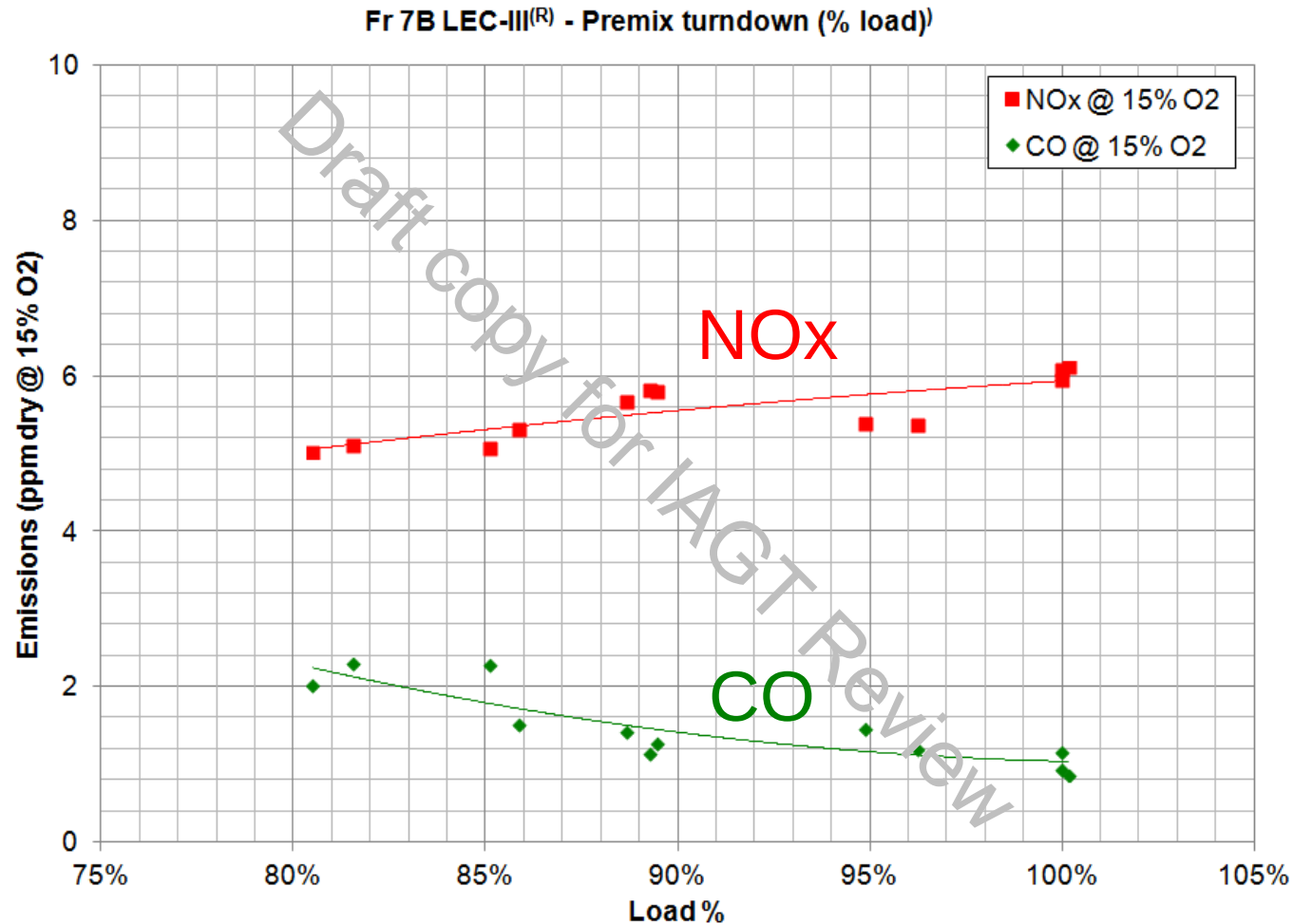
Fr 7B – Conversion 1st Results

First installation @ Baseload, across ambient temperature
Firing temperature remains at 1005°C (1840°F)



NOx: 35 ppm to <4 ppm | CO: 20-100 ppm to <15 ppm

Fr 7B – Conversion Final/Typical Results



NOx: 35 ppm to 6 ppm | CO: 20-100 ppm to <3ppm

Summary

- Proven: Frame 7B Ultra Low Emissions Combustion System
 - Performance: Sub 3-6 ppm NOx & Sub 15 ppm CO
- No need to upgrade turbine firing temperature or turbine components
- LEC-III ® technology running since 2001
 - Sub 5ppm NOx & Sub 15ppm CO
 - Improved CI's: 24k OH or 900 Starts
 - Platform Technology: Across multiple OEM's
 - Control System Independent: (Mark, Ovation, Triconix, WDPF)