10-PV Array Operation

Off-Grid Electrical Systems in Developing Countries
Chapter 7.6—7.15



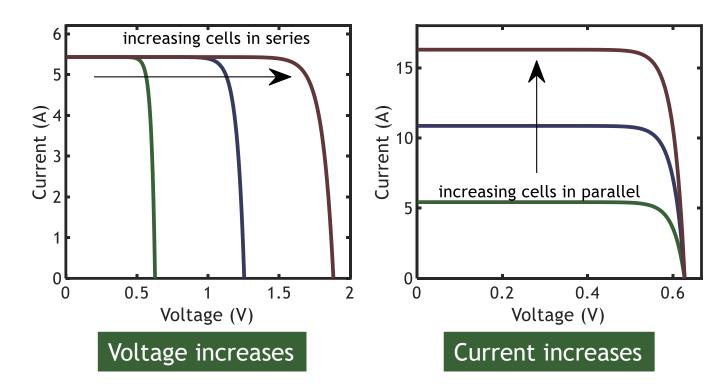
Learning Outcomes

At the end of this lecture, you will be able to:

- ✓understand how to mathematically model a PV module
- ✓interpret a PV specification sheet (data sheet)
- ✓ model the effects of irradiance and temperature on PV module voltage, current, and maximum power
- ✓ compute the voltage, current, and maximum power from a PV array

PV Modules

- PV modules are made by connecting several PV cells
- Increasing number of series or parallelconnected cells affects the I-V curve of the module



PV Modules

- Most modules are made from connected PV cells in series
- Module voltage is simply the cell voltage multiplied by the number of seriesconnected cells:

$$V_{\text{module}} = N_{\text{ser}} \times V_{\text{cell}}$$

$$I_{\text{cell}} = I_{\text{G}} - I_{0} \left(e^{V_{\text{cell}}/V_{\text{T}}} - 1 \right)$$

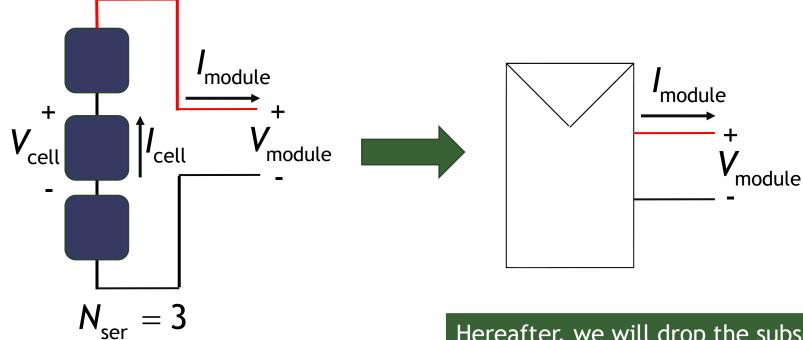
$$I_{\text{module}} = I_{\text{G}} - I_{0} \left(e^{V_{\text{module}}/(V_{\text{T}}N_{\text{ser}})} - 1 \right)$$

 V_{module} : PV module voltage (V)

 I_{module} : PV module current (A)

 N_{ser} : number of series-connected cells

PV Modules



Hereafter, we will drop the subscript "module" since we are usually not interested in the characteristics of an individual cell

PV Spec Sheets

See handout (also on Canvas)

Itek SE 72-Cell Module

Design & Engineering Data

Collina	72 high-efficiency monocrystalline p-type cells		
CellType	6 x 12 cell matrix		
Solar Glass	Ultra-clear anti-reflective treatment Tempered, with low iron content Anti-glare prismatic subsurface texture		
Backsheet	Multi-layered Engineered adhesion for maximum weather protection		
Frame	High-strength corrosion-resistant anodized aluminum		
	 Compatible with standard racking, accommodating both top-dox clamps and bottom-flange mounting 	W/F	
Cable			
Cable Junction Box	clamps and bottom-flange mounting		
	clamps and bottom-flange mounting • 90°C 12AWG PV wire		
Junction Box	clamps and bottom-flange mounting • 90°C 12AWG PV wire • 3 bypass diodes • 1000 VDC MC4 connectors • Tigo T\$4 • Certified for Wiley Bectronics WEE®™ grounding clips • Bight standard grounding locations per module for reduced ground wire length		
Junction Box Grounding	clamps and bottom-flange mounting • 90°C 12AWG PV wire • 3 bypass diodes • 1000 VDC MC4 connectors • Tigo T\$4 • Certified for Wiley Bectronics WEE®™ grounding clips • Bight standard grounding locations per module for reduced ground wire length		

ELECTRICAL DATA*	350 SE	355 SE	360 SE	365 SE	370 SE
Maximum Power - P _{MX} (Wp)	350	355	360	365	370
Madmum Power Voltage - Vur (V)	38.55	38.74	38.94	39.12	39.32
Maximum Power Current - Lier (A)	9.08	9.16	9.25	9.33	9.41
Madmum Current - Iwx(A) (OJ.)	12	12	12	12	12
Madmum Voltage (TS4-L only) - Vwx(V)	43.57	43.77	43.99	44.19	44.40
Open Circuit Voltage - Voc(V) (D.M.S.O)	47.43	47.64	47.87	48.08	48.31
Short Circuit Current - ixc(A) (D,M,S)	9.49	9.55	9.62	9.69	9.76
Module Efficiency	17.54%	17.79%	18.05%	18.30%	18.55%

MECHANICAL DAT	ſΑ
Dimensions	1001 mm x 1993 mm x 40 m
Weight	49 lbs/22.2kg

MAXIMUM RATINGS	
Operational Temperature	-40+90°C
Maximum System Voltage	1000 VDC
Maximum Design Load (UL 1703)	113 psf/{5400pa}
Max Series Puse Railing	15A
Max Reverse Current	15A

TEMPERATURE RATINGS	
Nominal Operating Cell Temperature (NOCT)	45.01°C
Temperature Coefficient of Per-	-0.39%/°C
Temperature Coefficient of Voc (D,M,S,O)	-0.29%/°C
Temperature Coefficient of Voc (TS4 - L only)	0.0%/°C
Temperature Coefficient of Isc	+0.04%/°C
Temperature Coefficient of Var-	-0.38%/°C

"Electrical characteristics may vary within ±2% of the indicated values at Standard Test Conditions (STC): Irradiance of 1,000W/m², AM 1.5 spectrum, cell temperature at 25°C.

Note: specifications subject to change without notice.





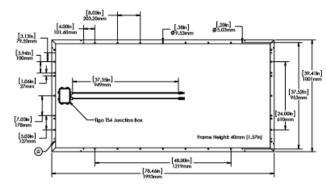






:hoose from Safety | Safety + Optimization | Safety + Optimization + Long Strings All of these options include Monitoring

n	TS4-L	LONG STRINGS
	TS4-0	OPTIMIZATION
	TS4-S	SAFETY (
	TS4-M	MONTORING TO
		Tigo
	TS4-D	DIODES

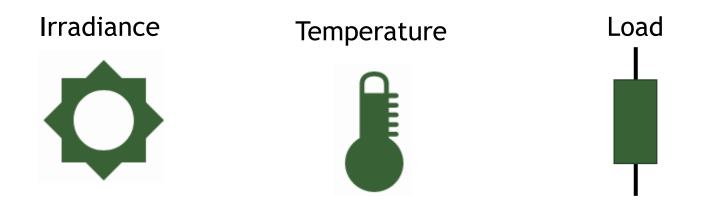


What PV Capacity (Power rating) Means

Itek SE 350 module has a maximum power rating of 350 W

- How should that be interpreted?
- Will it produce 350 W on a winter day in Seattle?
- Will it produce 350 W on a summer day in Las Vegas?
- Will it ever produce more than 350 W?
- Do the characteristics of the load or battery that it is connected to matter?

Main Factors Affecting PV Power Production



Spectral distribution of irradiance also affects production

PV Module Spec Sheets

- Modules rated at Standard Test Conditions (STC)
 - Irradiance: 1000 W/m²
 - Cell temperature: 25°C
 - Spectral distribution: AM 1.5
- PV modules rarely operate under STC

Itek SE 72-Cell Module

Design & Engineering Data

CellType	 72 high-efficiency n 	nonocnata	lline n-tvn	e cels		
- The	6 x 12 cell matrix	v.rysiu	р ур			
Solar Glass	Ultra-clear anti-refle					
	 Tempered, with low Anti-glare prismatic 					
Baclaheet	Multi-layered					
	Engineered adhesic	on for maxii	mum wed	ther prote	ection	
Frame	High-strength corros					
		 Compatible with standard racking, accommodating both top-down clamps and bottom-flange mounting 				
Cable	• 90°C 12AWG PV wir	e				
Junction Box	- 3 bypass diodes	- 1000 VD	C MC4 co	nnectors	• Tigo	TS4
QUALIFIC	 Certified for Wiley E Eight standard ground wireduced ground ground	nding loca				
Fire Rating	Type 1					
PID free	500+ hours					
ARRA, BAA, an	d TAA Compliant					
	CAL DATA*	350 SE	355 SE	360 SE	365 SE	370 SE
ELECTRIC	CAL DATA*	350 SE	355 SE 355	360 SE	365 SE 365	370 S ≡
ELECTRIC Maximum Power	CAL DATA*					
ELECTRIC Maximum Power	CAL DATA* r-P _{Max} (Wp) r-Voltage - Varr(V)	350	355	360	365	370
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ELECTRIC Maximum Power Maximum Power Maximum Power Maximum Currer	CAL DATA* r - Paux (Wp) r Voltage - Vurr(V) r Current - Lurr(A)	350 38.55 9.08	355 38.74 9.16	360 38.94 9.25	365 39.12 9.33	370 39.32 9.41
ELECTRIC Madmum Power Madmum Power Madmum Currer Madmum Currer Madmum Volta	CAL DATA* r - Puux (Wp) r Voltage - Vurr(V) r Current - Lurr(A) nt - Lux(A) (O.L)	350 38.55 9.08 12	355 38.74 9.16 12	360 38.94 9.25 12	365 39.12 9.33 12	370 39.32 9.41 12

MECHANICAL DA	TA
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Weight	49 lbs/22.2kg

MAXIMUM RATINGS	
Operational Temperature	-40+90°C
Maximum System Voltage	1000 VDC
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Max Series Puse Railing	15A
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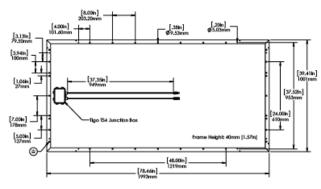






17.54% 17.79% 18.05% 18.30% 18.55%





Standard Test Conditions

- We use subscript "STC" to denote a variable referenced to Standard Test Conditions
- Examples:

```
G_{STC}: irradiance at STC (G_{STC} \triangleq 1000 \text{ W/m}^2)
```

 P_{STC}^* : maximum power output under STC

 V_{STC}^* : voltage at the maximum power point under STC

 $I_{SC,STC}$: short-circuit current under STC

Spec Sheet Interpretation

For the 350 SE module, determine:

$$P_{\text{STC}}^*$$

$$V_{\mathsf{STC}}^*$$

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Frame	High-strength corrosion-resistant anodized aluminum Compatible with standard racking, accommodating both top-down clamps and bottom-flange mounting
Cable	• 90°C 12AWG PV wire
Junction Box	- 3 bypass diodes - 1000 VDC MC4 connectors - Tigo TS4
Grounding	Cerified for Wiley Bectronics WEE8™ grounding clips Eight standard grounding locations per module for reduced ground wire length

QUALIFICA	TIONS
tre Rating	Type 1
ID Free	500+ hours

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Platform	TS4-L	LONG STRINGS

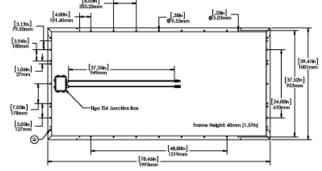












Rated Power Interpretation

The 350 SE module will produce 350 W when the <u>irradiance</u> incident to it is 1000 W/m², the <u>cell temperature</u> is 25° C, the <u>spectral distribution</u> of the irradiance is AM 1.5, and it is connected to a <u>load</u> that maximizes the power production under these conditions

We will generally assume that that the load maximizes power production (i.e. the module operates at the MMP for a given set of conditions)

Correcting for Irradiance

- Irradiance varies throughout the day
- Whenever the irradiance differs from G_{STC} (1000 W/m²), the maximum power output is affected
 - Maximum power is a function of irradiance $P^*(G)$
- Maximum power is approximately proportional to the irradiance
 - Doubling irradiance doubles maximum power

Correcting for Irradiance

Maximum power accounting for actual irradiance

$$P^*(G) = P_{STC}^* \times \frac{G}{G_{STC}}$$

Estimate the power produced by the Itek SE 370 if the irradiance is 750 W/m²

Estimate the power produced by the Itek SE 370 if the irradiance is 750 W/m²

$$P^*(G) = P_{STC}^* \times \frac{G}{G_{STC}}$$

$$P^*(G) = 370 \times \frac{750}{1000} = 277.5 \text{ W}$$

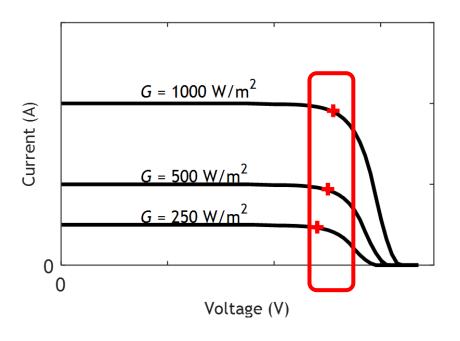
Correcting for Irradiance

The model assumes (approximates)

$$V^*(G) = V_{\mathsf{STC}}^*$$

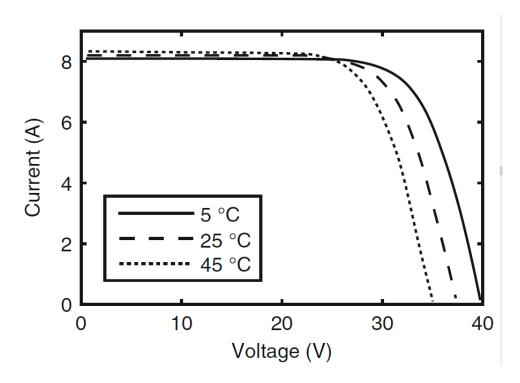
Voltage at MPP is not affected by irradiance

$$I^*(G) = I_{STC}^* \times \frac{G}{G_{STC}}$$
 Current at MPP changes in proportion to irradiance



Correcting for Temperature

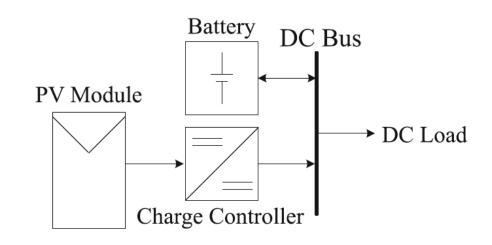
- I-V characteristic of PV module is influenced by the temperature
- Increasing temperature:
 - Decreases voltage
 - Increases current
- Change in voltage dominates the change in current, so power (voltage x current) decreases



How does temperature affect the design and operation of off-grid PV systems?

 Charge controllers have a maximum input voltage rating; cold temperatures can increase the PV module voltage, possibly exceeding (and damaging) the charge controller

 Overall energy reduction will be reduced (perhaps significantly) due to temperature-related losses



Correcting for Temperature

- Sensitivity of voltage, current, and power to temperature is empirically determined and reported by the manufacturer as "temperature coefficients"
- Coefficients are used to determine how open-circuit voltage, short-circuit current, and maximum change as the <u>cell</u> temperature deviates from 25° C
- Power can be reduced by 10 to 15% because cell temperature is often >20° C higher than that of STC

Temperature Coefficients

```
\alpha_{\rm v}: open-circuit voltage temperature coefficient (%/K or %/C)
```

```
\alpha_i: short-circuit current temperature coefficient (%/K or %/C)
```

 $\alpha_{\rm p}$: maximum power temperature coefficient (%/K or %/C)

Temperature coefficients are provided in module spec sheet

Correcting for Temperature

$$I_{SC}(T_C) = I_{SC}(25^{\circ} \text{ C}) \left(1 + \frac{\alpha_i}{100} \times (T_C - 25)\right)$$

$$V_{\rm OC}(T_{\rm C}) = V_{\rm OC}(25^{\circ}\,{\rm C}) \left(1 + \frac{\alpha_{\rm v}}{100} \times \left(T_{\rm C} - 25\right)\right)$$

$$P^*(T_c) = P^*(25^{\circ} \text{ C}) \left(1 + \frac{\alpha_p}{100} \times (T_c - 25) \right)$$

 V_{oc} : open-circuit voltage at 25° C (V) I_{oc} : short-circuit current at 25° C (A) T_c : temperature of the PV cell, (C)

Note that if the cell temperature is 25° C, then no correction is applied. This makes sense since because 25° C corresponds to STC

Example

The cell temperature of the Itek 370 SE module is 47° C. What is the short-circuit current at this temperature? Assume that other than temperature, the module is operating under STC.

Example

Referring to the spec sheet, we see that α_i = +0.04%/C and $I_{SC,STC}$ is 9.76A.

$$I_{SC}(T_{C}) = I_{SC}(25^{\circ} \text{ C}) \left(1 + \frac{\alpha_{i}}{100} \times (T_{C} - 25) \right)$$

$$I_{SC}(47^{\circ} \text{ C}) = 9.76 \left(1 + \frac{0.04}{100} \times (47 - 25) \right)$$

$$I_{SC}(47^{\circ} \text{ C}) = 9.846 A$$

We shouldn't be concerned about the units being in Celsius, since the temperature is also expressed in these units (moreover, the difference in one degree Celsius is the same as the difference in one degree Kelvin)

How do we determine the temperature of the cell?

- Manufacturers report the cell temperature when the PV module is exposed to "Standard Operating Conditions" (SOC)
- The reported temperature is known as "Nominal Operating Cell Temperature" (NOCT)
 - typically between 45° C and 50° C
- When module is not exposed to SOC (often the case), then the cell temperature will likely not be NOCT and the cell temperature must be estimated

Standard Operating Conditions

Standard Operating Conditions

- Irradiance: 800 W/m² (0.8 G_{STC})
- Ambient temperature: 20°C
- Wind speed: 1 m/s
- Spectral distribution: AM 1.5
- Power output: 0 W (no load)
- see IEC 61215 for test procedure

Do not confuse SOC with STC!

Nominal Operating Cell Temperature

What happens when the module does not operate under SOC? Approximate the cell temperature from:

$$T_{\rm C} = T_{\rm a} + \left(NOCT - 20\right) \frac{G}{800}$$
 $T_{\rm a}$: ambient temperature (C)

Other formulations exist for correcting for non-SOC wind speed, but it is not commonly employed

Example

What is the cell temperature of the Itek 370 SE when the irradiance is 400 W/m², and the ambient temperature is 15° C? (Assume SOC otherwise)

Example

From the spec sheet the NOCT is 45.01° C

$$T_{\rm c} = T_{\rm a} + (NOCT - 20) \frac{G}{800}$$

$$T_{\rm c} = 15 + (45.01 - 20) \frac{400}{800}$$

This is a cold day (about 59° F)

$$T_{\rm c} = 15 + (45.01 - 20) \frac{400}{800}$$

$$T_{\rm C} = 27.5^{\circ}{\rm C}$$

We see that the PV module is hotter than the ambient temperature

What is the maximum power produced by the Itek SE 370 when the ambient temperature is 30° C and the irradiance on the module is 1000 W/m²?

What is the maximum power produced by the Itek SE 370 when the ambient temperature is 30° C and the irradiance on the module is 1000 W/m²?

The temperature coefficient for power is -0.39%/°C

The NOCT is 45.01° C

The irradiance corresponds to G_{STC} , so use P_{STC}^* from the spec sheet (370 W)

First compute cell temperature

$$T_{\rm C} = T_{\rm a} + \left(NOCT - 20\right) \frac{G}{800}$$

$$T_{\rm C} = 30 + (45.01 - 20) \frac{1000}{800}$$

$$T_{\rm c} = 61.27^{\circ}{\rm C}$$

Now compute maximum power

$$P^*(T_c) = P^*(25^{\circ} \text{ C}) \left(1 + \frac{\alpha_p}{100} \times (T_c - 25) \right)$$

$$P^*(30^{\circ} \text{ C}) = 370 \left(1 + \frac{-0.39}{100} \times (T_C - 25)\right)$$

$$P^*(30^{\circ} C) = 317.7 W$$

Power has been reduced by 14% due to temperature

Correcting for Temperature & Irradiance

- Last example conveniently had an irradiance of 1000 W/m² (STC)
- What about when the cell temperature AND irradiance deviate from STC?
 - Mostly concerned about maximum power, not open-circuit voltage or short-circuit current

PV Power Production

- Several different methods possible
- Osterwald's method:

$$P = P_{\text{STC}}^* \times \frac{G}{1000} \times \left(1 + \frac{\alpha_P}{100} \times (T_C - 25)\right)$$

P: power produced by PV module (W)

: rated power under Standard Test Conditions (W)

G: irradiance (W/m²)

 $\alpha_{\rm P}$: power coefficient (% /K)

 $T_{\rm C}$: PV cell temperature (C)

Osterwald's Method

$$P = P_{\text{STC}}^* \times \boxed{\frac{G}{1000}} \times \left(1 + \frac{\alpha_P}{100} \times (T_{\text{c}} - 25)\right)$$
 Corrects for temperature

Corrects for irradiance

What is the maximum power produced by the Itek SE 370 when the ambient temperature is 30° C and the irradiance on the module is 900 W/m²?

What is the maximum power produced by the Itek SE 370 when the ambient temperature is 30° C and the irradiance on the module is 900 W/m²?

The temperature coefficient is -0.39%/°C The NOCT is 45.01° C

First compute cell temperature

$$T_{c} = T_{a} + (NOCT - 20) \frac{G}{800}$$

$$T_{c} = 30 + (45.01 - 20) \frac{900}{800}$$

$$T_{\rm c} = 58.14^{\circ}{\rm C}$$

Now compute maximum power

$$P = P_{STC}^* \times \frac{G}{1000} \times \left(1 + \frac{\alpha_p}{100} \times (T_c - 25)\right)$$

$$P = 370 \times \frac{900}{1000} \times \left(1 + \frac{-0.39}{100} \times (58.14 - 25)\right)$$

$$P = 289.96 \text{ W}$$

Compare this to the result of the previous exercise

Short-Circuit Current

 We generally only correct the short-circuit current based on irradiance (not temperature) using:

$$I_{STC}(G) = I_{SC,STC} \times \frac{G}{G_{STC}}$$

 Important when determining fuse ratings and charge controller compatibility

Open-Circuit Voltage

 We generally only correct the open-circuit current based on temperature (not irradiance) using:

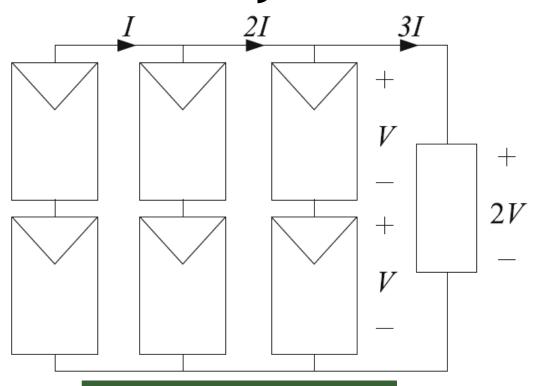
$$V_{\text{OC}}(T_{\text{C}}) = V_{\text{OC}}(25^{\circ} \,\text{C}) \left(1 + \frac{\alpha_{\text{v}}}{100} \times (T_{\text{C}} - 25)\right)$$

 Important when determining insulation ratings and charge controller compatibility

PV Arrays

- PV modules connected together are known as a PV Array
- Series-connected modules are known as "strings"
- Strings with the <u>same</u> number of series-connected modules can be connected in parallel
- Assume that all modules in the array are operating under the same conditions

PV Arrays



$$V_{\text{array}} = N_{\text{ser,str}} \times V$$
 $I_{\text{array}} = N_{\text{par,str}} \times I$

 $N_{\text{ser,str}}$: number of modules connected in series per string $N_{\text{par,str}}$: number of strings connected in parallel

This array has three strings of two modules

PV Array Power

Power produced by the array:

$$P_{\text{array}} = V_{\text{array}} \times I_{\text{array}} = N_{\text{ser,str}} \times V \times N_{\text{par,str}} \times I$$

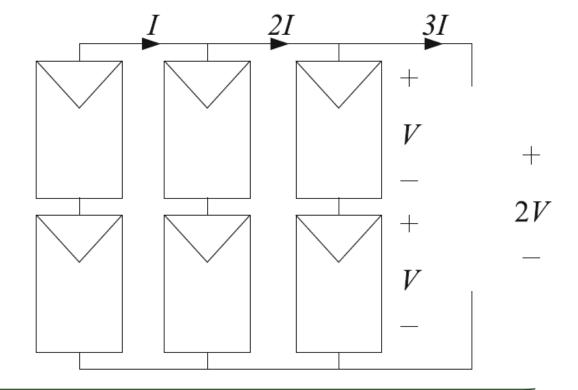
$$= N_{\text{ser,str}} \times N_{\text{par,str}} \times P$$

$$= \text{Number of modules} \times P$$

 In other words, the power produced is independent of how the modules are connected (as long as each string has the same number of modules connected in series)

Example

Compute the open-circuit voltage, short-circuit current and maximum power of this array assuming operation under STC (let the modules be Itek 370 SE)



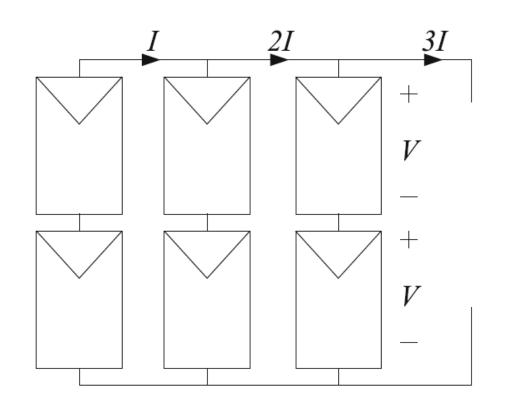
Example

From the spec sheet:

$$I_{SC,STC} = 9.76 A$$

$$V_{\text{OC,STC}} = 48.31 \text{ V}$$

$$P_{\text{STC}}^* = 370 \text{ W}$$



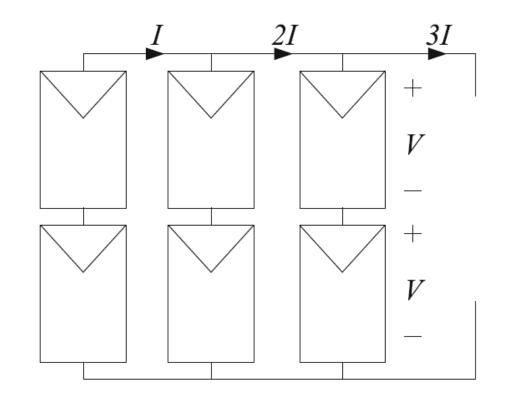
Example

There are three strings in parallel, and two modules in each string so:

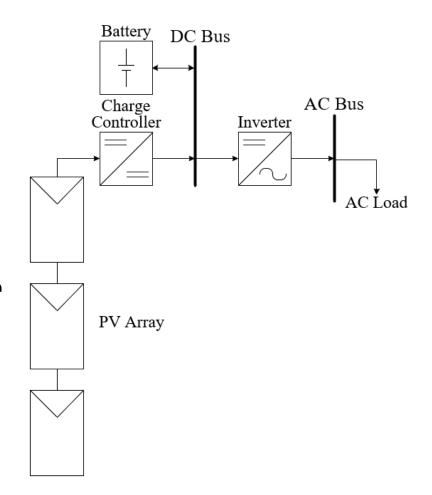
$$I_{\text{array},SC,STC} = 3 \times 9.76 = 29.28 \text{ A}$$

$$V_{\text{array,OC,STC}} = 2 \times 48.31 = 96.62 \text{ V}$$

$$P_{\text{array,STC}}^* = (3 \times 2)370 = 2220 \text{ W}$$



A design calls for three Itek 370 SE modules to be arranged in a single string and connected to a charge controller. The maximum voltage input rating of the charge controller is 150 VDC. Verify the charge controller can be used if the array operates under STC.



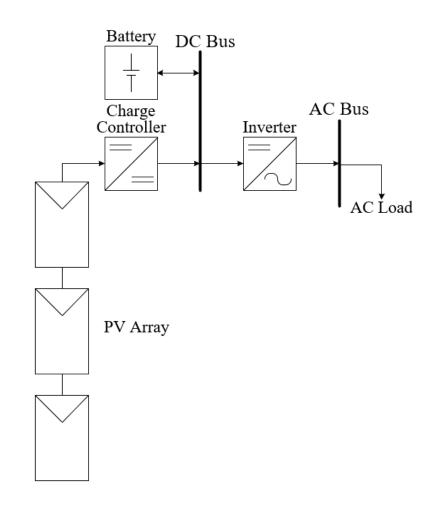
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The PV modules are arranged in a string, so that:

$$V_{\text{OC,array}} = N_{\text{ser,str}} \times V_{\text{OC,STC}}$$

$$V_{\text{OC,array}} = 3 \times 48.31$$
 (from the spec sheet)

$$V_{\text{OC,array}} = 144.93 \text{ V}$$



We know that STC operation almost never happens. The array open-circuit voltage was very close to the charge controller rating. We should check to see if the controller can be used if the temperature is low (why?). Assume the lowest cell temperature will be 5° C. Can the controller be used?



We know that STC operation almost never happens. The array open-circuit voltage was very close to the charge controller rating. We should check to see $V_{OC,array}(5^{\circ}C) = 3 \times 48.31 \left(1 + \frac{-0.29}{100} \times (5-25)\right)$ if the controller can be used if the if the controller can be used if the temperature is low (why?). Assume the lowest cell temperature will be 5° C. Can the controller be used?

$$V_{\text{OC,array}}(T_{\text{C}}) = 3 \times V_{\text{OC}}(25^{\circ} \, \text{C}) \left(1 + \frac{\alpha_{\text{V}}}{100} \times (T_{\text{C}} - 25)\right)$$

$$V_{\text{OC,array}}(5^{\circ} \, \text{C}) = 3 \times 48.31 \left(1 + \frac{-0.29}{100} \times (5 - 25)\right)$$

$$V_{\text{OC,array}}(5^{\circ} \, \text{C}) = 153.3 \, \text{V}$$

This exceeds the charge controller rating.

Shading

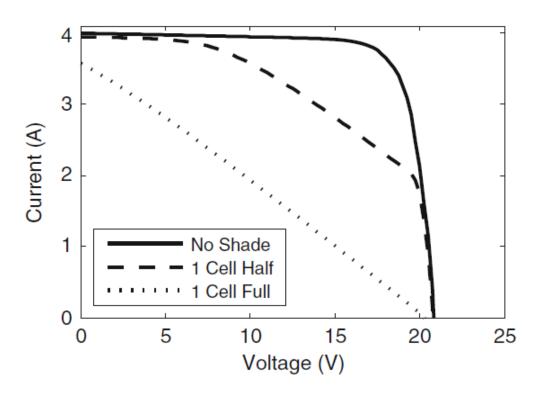
- Complete or <u>partial</u> shading of PV module or array can severely reduce power production
- Avoid locations where shading occurs



Shading

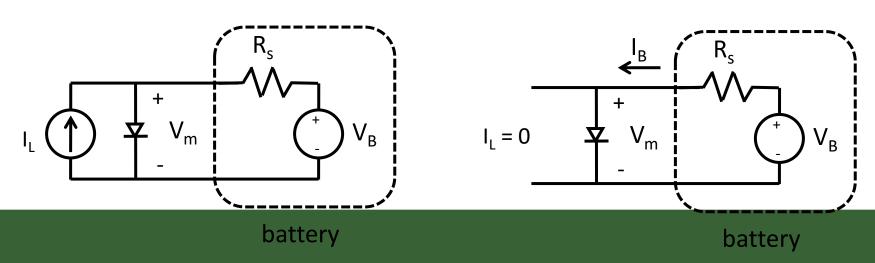
Read Chapter 7.12 of text for details, including how to mitigate the effects of shading by using diodes

"The current supplied by a PV module is limited to the current produced by its least productive cell."---not exactly correct, but easy to remember



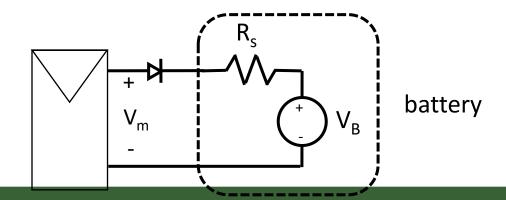
Discharge Protection

- Consider a PV panel connected to a battery
- What happens at night?
 - $I_1 = 0$
 - Diode can be forward biased
 - depends on number of cells in series in the module
 - Battery discharges through PV
 - How can we prevent this?



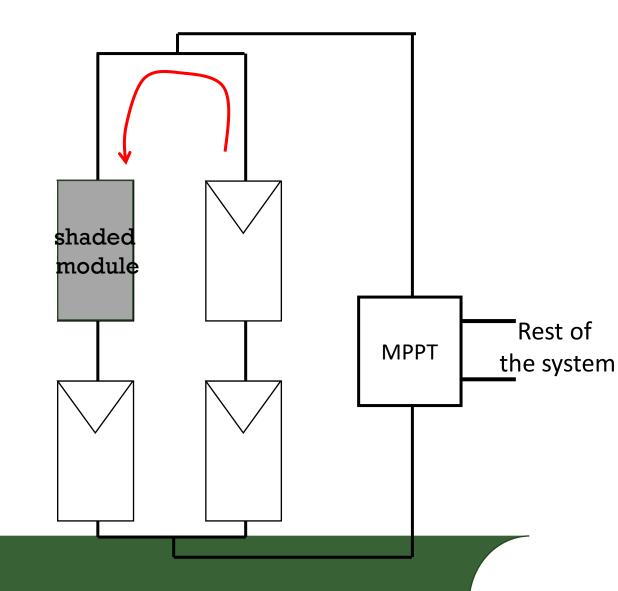
Battery Charging

- Add a blocking diode
- Less efficient operation during charging
 - Power loss due to diode voltage drop
- Prevents discharging when V_m < V_B



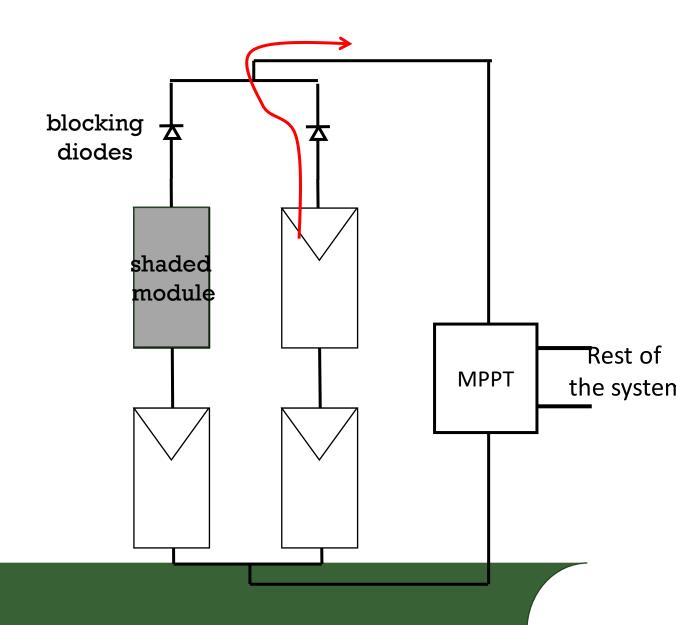
Blocking Diodes

- The same problem can occur when a portion of a PV module (or a PV module in string) is shaded
- Voltage in shaded string is reduced
- Any strings in parallel may have current flow through the shaded string



Blocking Diodes

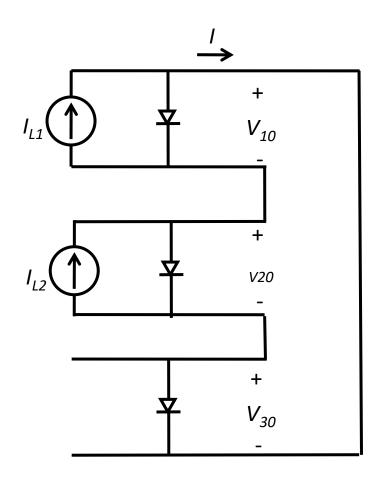
- Blocking diodes installed when strings are in parallel to prevent on string from sending current through the other
- Under unshaded operation, there is loss associated with the blocking diodes



Shading V_{10} V_{10} R_{Load} V20 V20 $\mathsf{R}_{\mathsf{Load}}$ shaded V_{30} V_{30} cell $I_{L3} = 0$

Shading

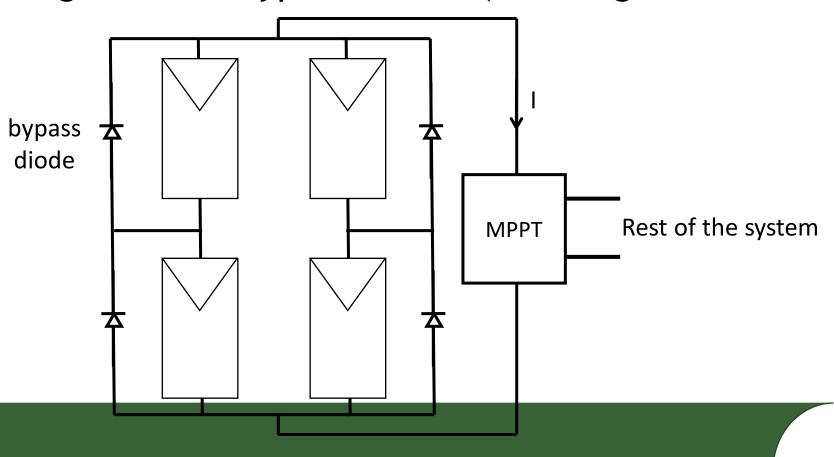
- Voltage across shaded cell
 - $V_{30} = -V_{10} V_{20}$
- Shaded cell is a reversed biased diode
- Power is <u>dissipated</u>
 - Overheating and damage can occur
- Output current is severely reduced



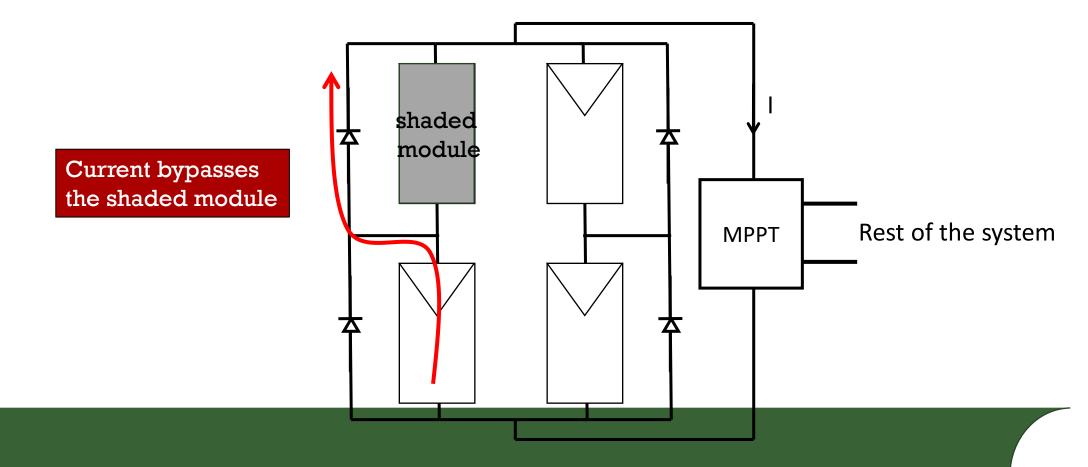
Shading

• Solution to shading is to use bypass diodes (blocking diodes not

shown)

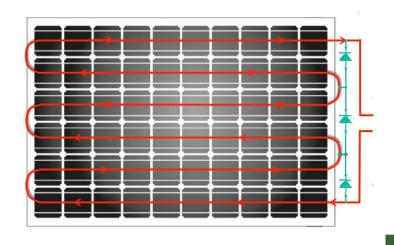


Bypass-Diodes



Bypass diodes

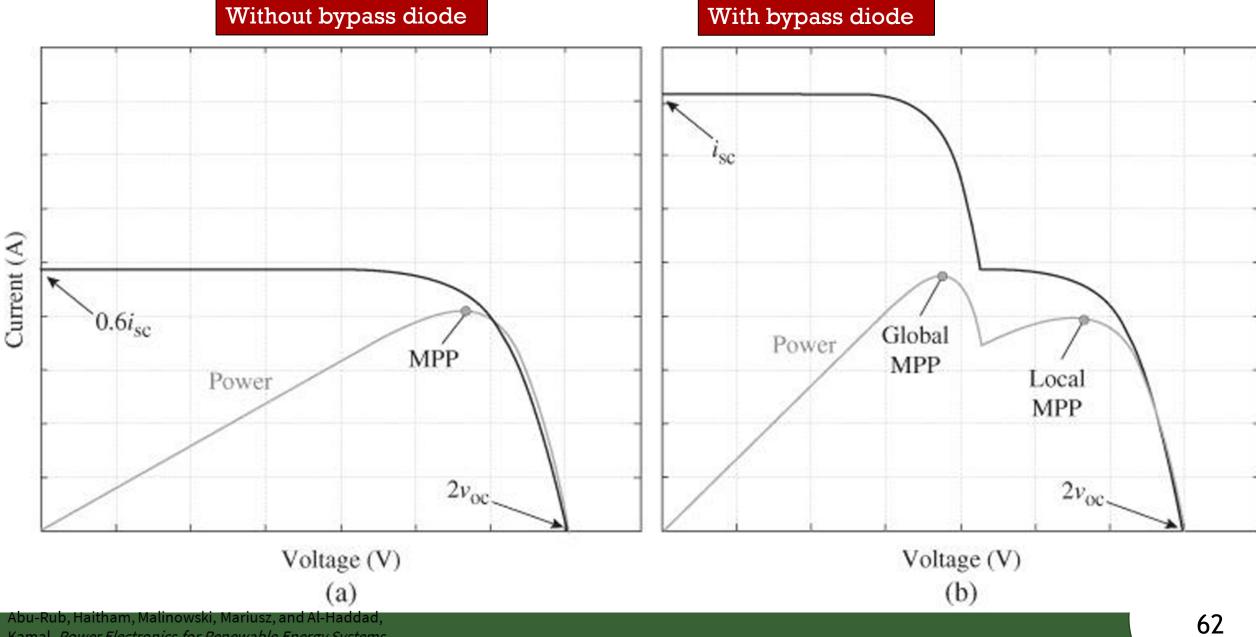
 Most larger PV modules contain bypass diodes



Itek SE 72-Cell Module

Design & Engineering Data

GENERAL DATA	
Cell Type	 72 high-efficiency monocrystalline p-type cells 6 x 12 cell matrix
Solar Glass	Ultra-clear anti-reflective treatment Tempered, with low iron content Anti-glare prismatic subsurface texture
Backsheet	Multi-layered Engineered adhesion for maximum weather protection
Frame	High-strength corrosion-resistant anodized aluminum Compatible with standard racking, accommodating both top-down clamps and bottom-flange mounting
Cable	• 90°C 12AWG PV wire
Junction Box	• 3 bypass diodes • 1000 VDC MC4 connectors • Tigo TS4
Grounding	 Certified for Wiley Electronics WEEB™ grounding clips Eight standard grounding locations per module for reduced ground wire length



Kamal. *Power Electronics for Renewable Energy Systems, Transportation and Industrial Applications*. 1st ed. New

York: Wiley, 2014. Wiley

PV Energy Production

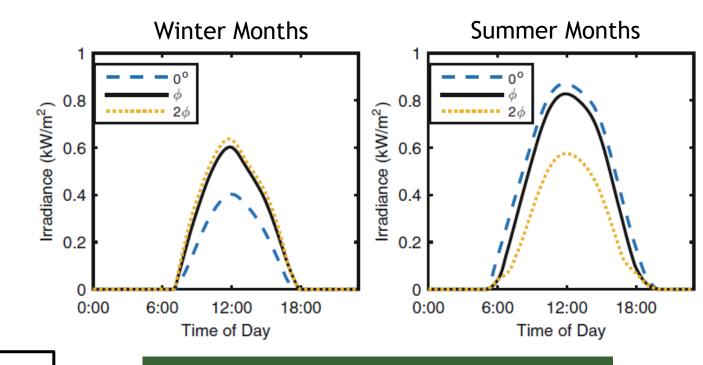
Average daily PV array energy production can be estimated from array's average daily insolation (kWh/m²/day)

- Insolation: integral of irradiance
- Typical insolation for SSA 4 to 7 kWh/m²/day

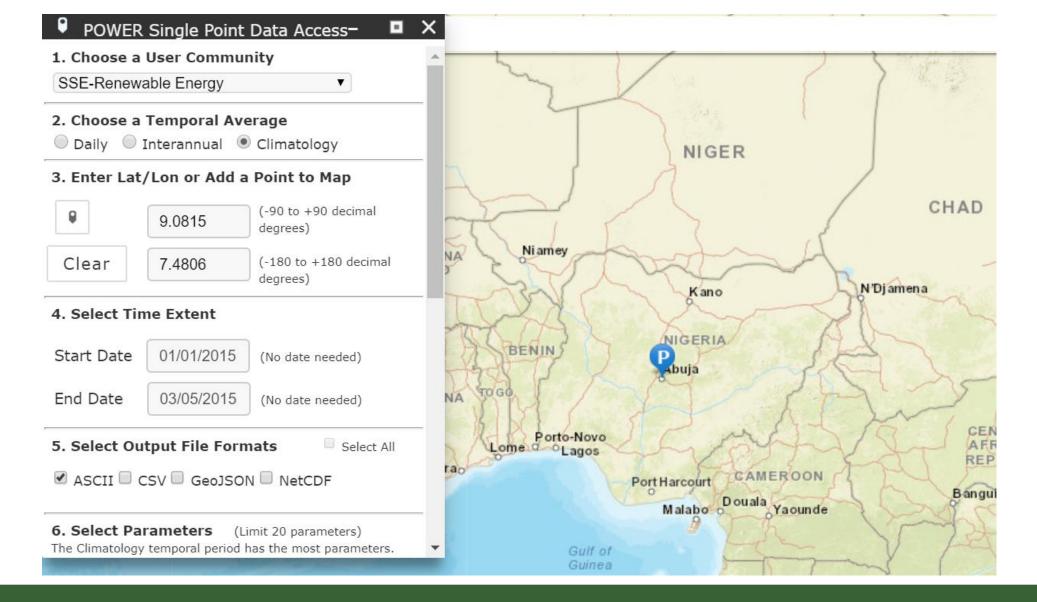
$$\overline{\overline{\mathbf{E}}}_{ ext{PV}} = \overline{\mathbf{P}}_{ ext{STC}}^* imes \overline{\mathbf{I}}$$

 \overline{E}_{PV} : average PV array energy production, kWh/day

 \bar{I} : average insolation, kWh/m²/day



Insolation depends on: array location, tilt, azimuth, season



Parameter Charts

All Sky Insolation Incident on a Horizontal Surface ▼

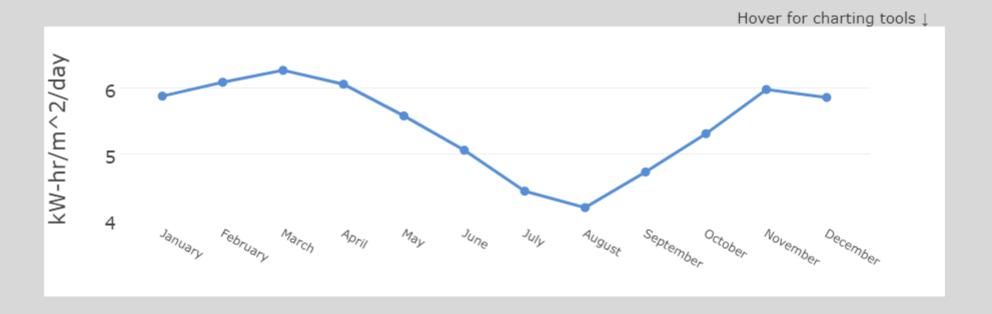
Latitude: 9.0815 Longitude: 7.4806

Time Extent:

22 Year Solar Climatological Averages (Jul 1983 - Jun 2005)

30 Year Meteorology Climatological Averages (Jan 1984 - Dec 2013)

Elevation: 404.65 meters



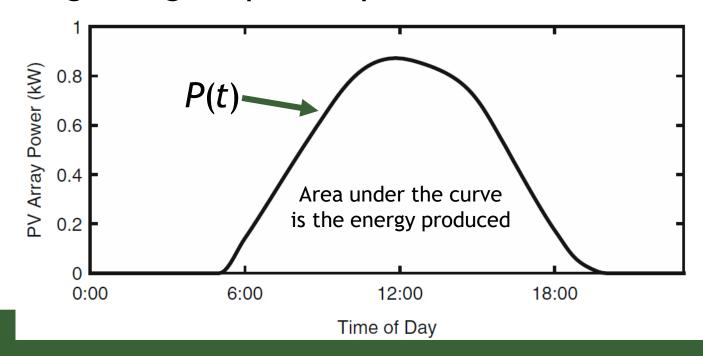
The average insolation on the a 350 W module for the month of September is 4.7 kWh/m²/day. What is the average daily energy produced by the module?

The average insolation on the a 350 W module for the month of September is 4.7 kWh/m²/day. What is the average daily energy produced by the module?

$$\overline{E}_{pv} = 350 \times 4.7 = 1645 \text{ Wh}$$

Energy Production from PV Arrays

The energy produced by a PV array over the course of a day is found by integrating its power production



Energy Production from PV Arrays

Integrate power between sunrise and sunset times (be careful of the units)

$$P(t) = P_{\text{STC}}^* \times \frac{G(t)}{1000} \times \left(1 + \alpha_{\text{p}} \times \left(T_{\text{c}}(t) - 25\right)\right)$$

We expect both the irradiance and cell temperature to vary with time (t)

$$E = \int_{t_{\text{rise}}}^{t_{\text{set}}} P(t) dt$$

 $E = \int_{t_{\text{rise}}}^{t_{\text{set}}} P(t)dt$ $t_{\text{set}}: \text{ time the sun sets}$ $t_{\text{rise}}: \text{ time the sun rises}$

Practical Considerations: Advantages



- No fuel costs
- Wide resource data availability
- Modularity
- Low maintenance (periodic washing of panels)
- No noise or air pollution
- Widely available, mature supply chains

Practical Considerations: Disadvantages 🔀



- Variable and uncertain power production
- Requires charge controllers and batteries, and requires an inverter to serve AC load
- Higher capital costs than gen sets
- Relatively low power density so large amount of space needed
- Often requires custom racking to optimize incident irradiance



(courtesy GVE Projects)

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