



### Pro-Science/KIT experimental work on cryogenic H<sub>2</sub> releases as part of the PRESLHY project

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ELVHYS-Workshop "Experimental research and case studies of cryogenic hydrogen incidents"

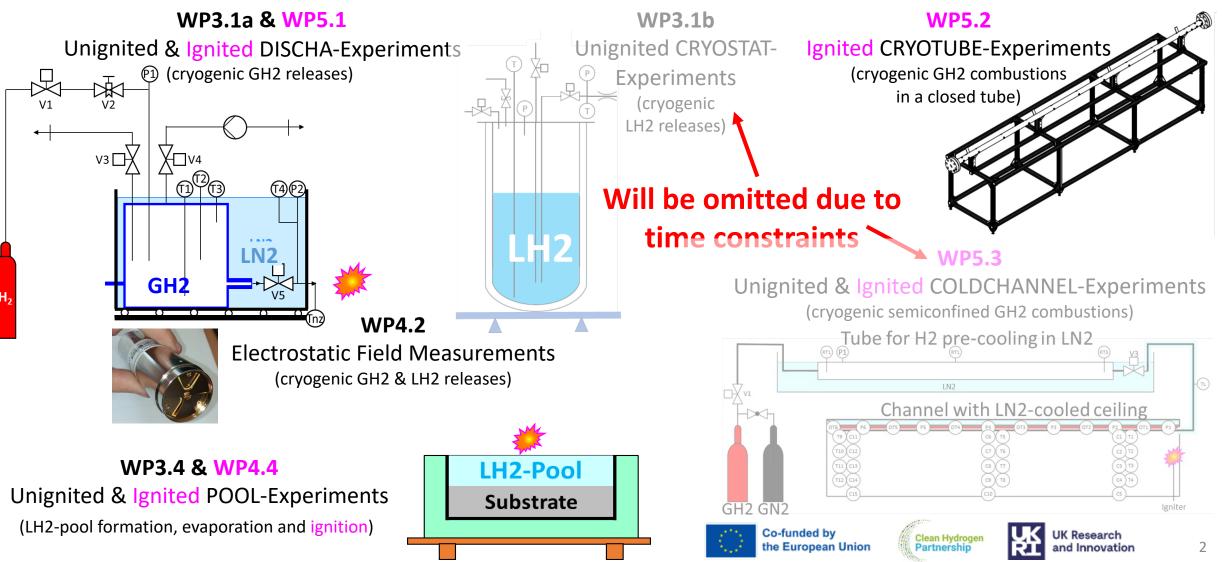
28.-30.11.2023, Buxton (UK)



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### **Overview**

#### **PS/KIT-Experiments for the PRESLHY-Project**





#### Main features of the DISCHA pressure vessel



- Designed for investigation of blow-down behavior of cryogenic hydrogen stored at elevated pressure and its dispersion in surrounding air,
- stainless steel vessel (Di = 160 mm, Hi = 140 mm, V = 2.81 dm<sup>3</sup>)
- designed for gaseous releases (p up to 200 bar, T down to 80 K).
- Circumference equipped with:
  - 2 nozzle ports (di = 12 mm, only lower port used),
  - 1 rod opposite to nozzle ports for connection with force sensor.
- Nozzle Properties (release line: di = 10 mm):
  - 4 Nozzles with circular apertures d<sub>i</sub> = 0.5, 1, 2 and 4 mm.











#### **DISCHA-Facility Instrumentation (UNignited experiments)**



- 1 static pressure sensor in vessel and 1 dynamic pressure sensor close to nozzle
- 3 thermocouples in vessel, 1 close to nozzle and 5 downstream the nozzle,
- 5 sampling positions for H2-concentration measurements downstream the nozzle,
- 1 scale and 1 force sensor

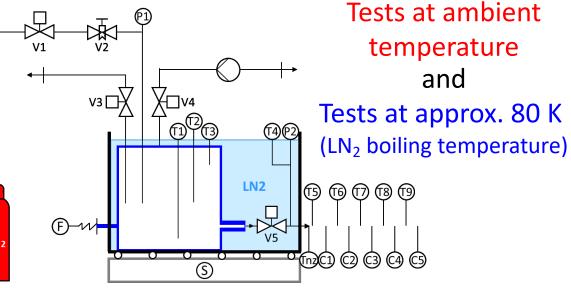






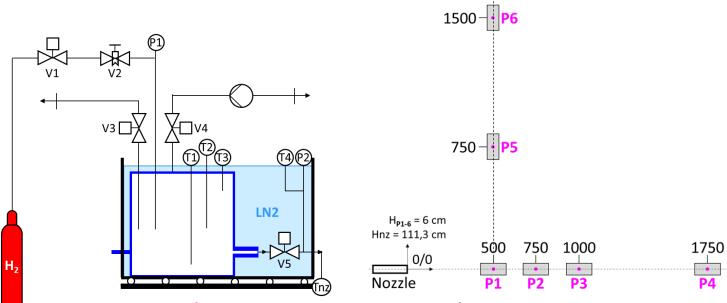






# Pro-Science

#### **DISCHA-Facility Instrumentation (ignited experiments)**



Tests at ambient temperature and approx. 80 K

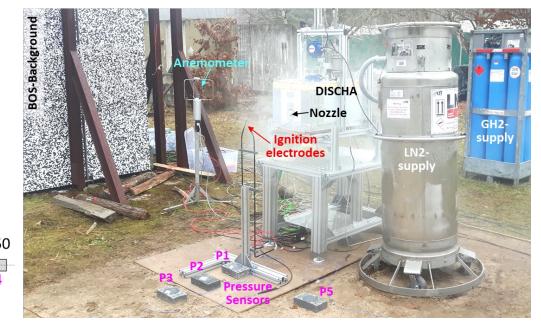
DISCHA-facility (on free field test site) equipped with:

- 1 static pressure sensor in vessel and 1 dynamic pressure sensor close to nozzle
- 3 thermocouples in vessel, 1 close to nozzle,
- Neither temperature nor H2-concentration measurements downstream the nozzle,
- Ignition electrodes and 6 fast dynamic pressure sensors on ground,
- Neither scale nor force sensor.





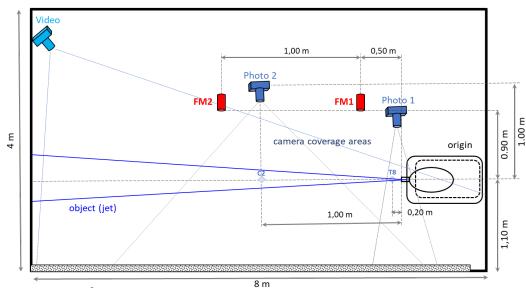






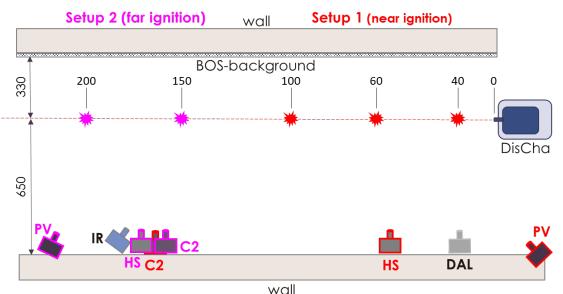
#### **DISCHA-Facility Optical and additional equipment**

Photos/Videos processed using different BOS-procedures optimized for different jet-regions.



#### Unignited experiments.

- 2 Photo-cameras (Canon EOS5D Mark I & II)
- 1 Panasonic video camera
- 2 Field mills (FM, electrostatic field),



#### Ignited experiments:

- **HS**: PHOTRON FastCAM SA 1.1 (≤ 5.000 fps)
- **DAL**: DALSA video camera (70 fps)
- PV: Panasonic video camera (24 fps)
- C2: CANON EOS5D Mark II
  - IR: Thermocamera FLIR T450 (IR)



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#### **Test matrix Unignited Experiments**

- Test matrix for unignited DISCHA-experiments:
   7 initial pressure stages x 4 nozzle diameters
   x 2 initial temperatures = 56 cases,
   all cases tested at least once,
- Up to 7 repetitions to check reproducibility (facility improved several times),
- In total > 200 experiments performed.

#### **Theoretical Utilization of Experimental Data**

- Data of unignited DISCHA-experiments used by PRESLHY-Partners for validation of models on blowdown behavior of cryogenic GH2.
- (1) S. Giannissi, A. Venetsanos et al.: Cold hydrogen blowdown release: an inter-comparison study; International Conference on Hydrogen Safety - Online, Edinburgh, United Kingdom, Sept. 21-24 2021
- (2) Cirrone, D., Molkov, V. et al.: Modelling the non-adiabatic blowdown of pressurised cryogenic hydrogen storage tank; International Conference on Hydrogen Safety 2023 (ICHS2023), Quebec, Kanada, 19.–21.09.2023



	Nozzle diameter [mm]			
	0.5	1	2	4
5	A/C	A/C	A/C	A/C
10	A/C	A/C	A/C	A/C
20	A/C	A/C	A/C	A/C
50	A/C	A/C	A/C	A/C
100	A/C	A/C	A/C	A/C
150	A/C	A/C	A/C	A/C
200	A/C	A/C	A/C	A/C
	10 20 50 100 150	0.5         5       A/C         10       A/C         20       A/C         50       A/C         100       A/C         100       A/C         100       A/C	0.5       1         5       A/C       A/C         10       A/C       A/C         20       A/C       A/C         50       A/C       A/C         100       A/C       A/C         100       A/C       A/C         100       A/C       A/C         150       A/C       A/C	0.5         1         2           5         A/C         A/C         A/C           10         A/C         A/C         A/C           20         A/C         A/C         A/C           50         A/C         A/C         A/C           100         A/C         A/C         A/C           100         A/C         A/C         A/C           100         A/C         A/C         A/C           150         A/C         A/C         A/C

A: ambient temperature (290 K) C: cryogenic temperature (80 K)

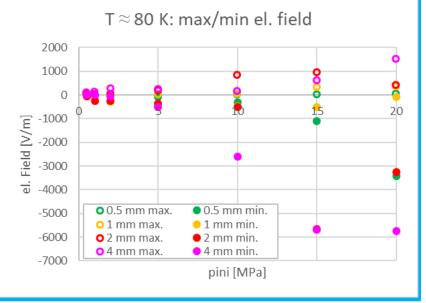




#### Unignited Experiments: Electrostatic field measurements (WP4.2)



- No ignition due to electrostatic discharge observed in complete experimental program,
- Highest positive and lowest negative electric field values measured for T ≈ 80 K:

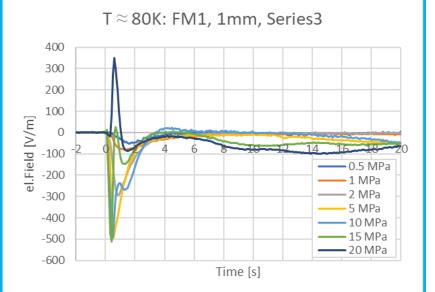


- Max. field values >> 1000 V/m measured,
- Most extremal values measured for largest d<sub>noz</sub> (4 mm) and highest p<sub>ini</sub> (20 MPa),

Assumption: Electrostatic field built-up during release mainly connected with ice crystals due to frozen humidity at cold nozzle prior to release.

#### **Reproducibility**

- Extremal field values within a series mostly consistent,
- Extremal field values always at t < 1 s,
- Within few hours positive and negative values measured.







#### **Test Matrix Ignited Experiments**

- Test matrix of main ignited DISCHA-experiments: 4 initial pressures x 3 nozzle diameters x 5 ignition distances x 2 initial temperatures = 120 cases, Experiments on almost complete test matrix performed for both initial temperatures,
- Variation of ignition delay time in initial test series:
   → Main series with ignition delay time of 120 ms.

#### **Theoretical Utilization of Experimental Data**

• Ignited DISCHA-experimental data used by PRESLHY-Partners for model validation ignited cryogenic H2.

Z. Ren, J. Wen et al.: The evolution and structure of ignited high-pressure cryogenic hydrogen jets; Int J Hydrogen Energy (2022) Volume 47, Issue 50, pp. 21596-21611



<b>p</b> <sub>ini</sub>	<b>d</b> <sub>ign</sub>	Nozzle diam. [mm]		
[bar]	[cm]	1	2	4
5	39.5	A/C	A/C	A/C
	62.5	A/C	A/C	A/C
	106.5	A/C	A/C	A/C
	150	-/-	-/C	A/C
	200	-/-	-/C	A/C
50	39.5	A/C	A/C	A/C
	62.5	A/C	A/C	A/C
	106.5	A/C	A/C	A/C
	150	A/C	A/C	A/C
	200	-/C	A/C	A/C
100	39.5	A/C	A/C	A/C
	62.5	A/C	A/C	A/C
	106.5	A/C	A/C	A/C
	150	A/C	A/C	A/C
	200	A/C	A/C	A/C
200	39.5	A/C*	A/C	A/C
	62.5	A/C*	A/C	A/C
	106.5	A/C*	A/C	A/C
	150	A/C	A/C	A/C
	200	A/C	A/-*	A/C

A: ambient temperature (290 K)

C: cryogenic temperature (80 K)

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\* Omitted or pressure slightly below 200 bar due to lack of pressure in H<sub>2</sub>-bundle





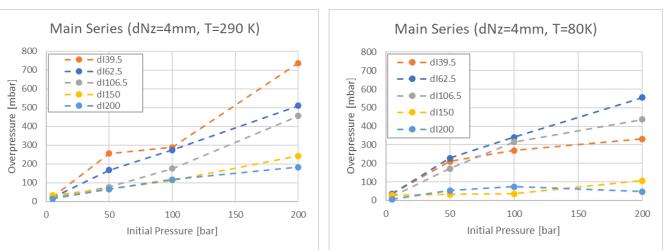
#### **Test Matrix Ignited Experiments**

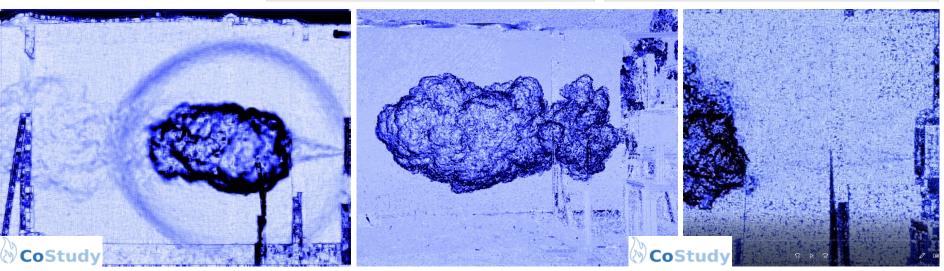
- Warm/cold experiments differ concerning influence of ignition distance on maximum combustion overpressures.
- After ignition flame can either burn back to nozzle or not, determining whether the flame continues to burn

when ignition is turned off.

 Pressure waves generated by the ignition could be visualized using the BOS method.





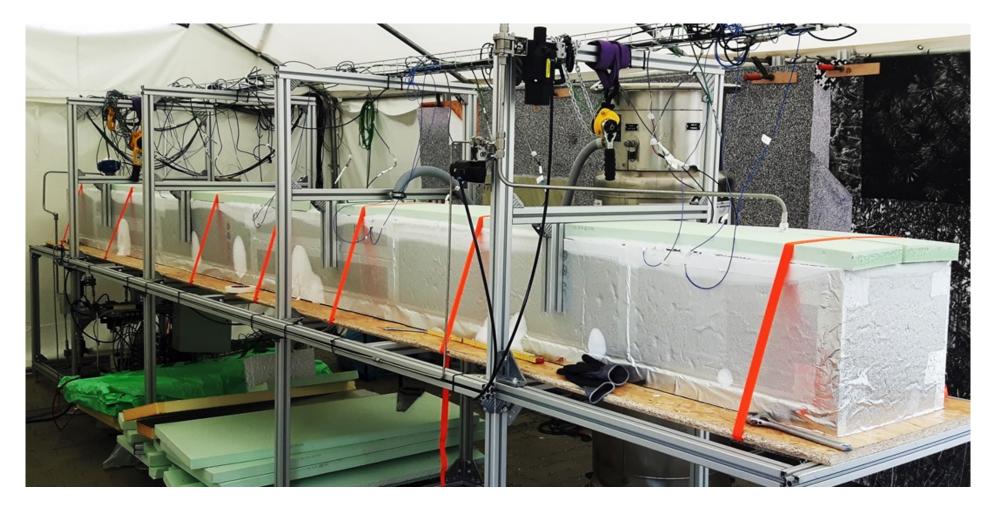




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#### **Combustion-Tube**



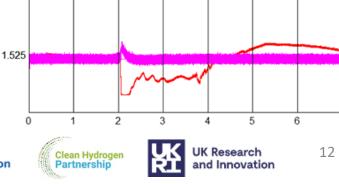
• Combustion of H2-air-mixtures in an obstructed tube at cryogenic temperatures



- Tube placed in basin filled with LN2 (77K) to cool it down for cryogenic experiments, uniformity of temperature checked with an array of 6 calibrated thermocouples,
- In experiments flame position detected by:
  - 13 Pressure Sensors (with/without thermal compensation),
  - 15 Phototransistors (InGaAs)



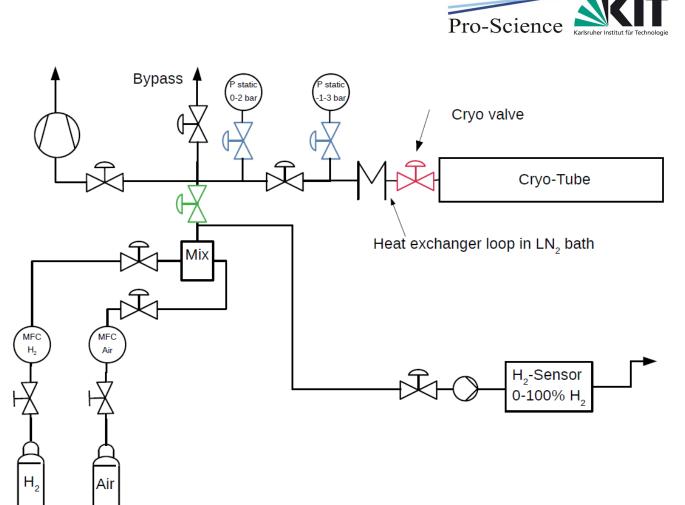
X.m



11.3%H<sub>2</sub>

#### **Combustion-Tube: Test Matrix**

- Temperatures: ambient (293 K), above LN2-temperature (90-130 K)
- Blockage ratios: 0%, 30% and 60%
- H2-concentrations: 8 to 60 Vol% H2
- Higher hydrogen concentration in mixture leads to lower condensation temperature, mainly for air components
- To cover flammable range, lowest initial temperature should be higher than 80 K to avoid condensation.



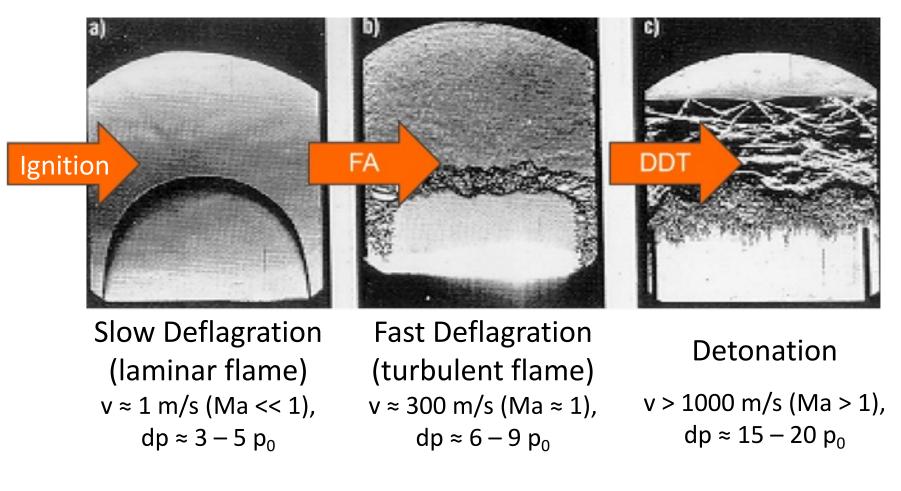


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#### Hydrogen Combustion regimes



• For gaseous hydrogen combustions three main combustion regimes are distinguished:

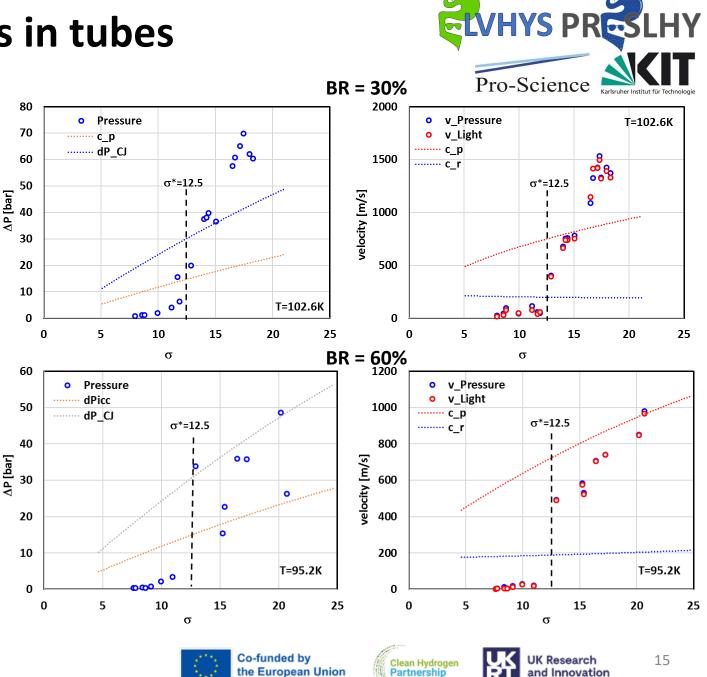






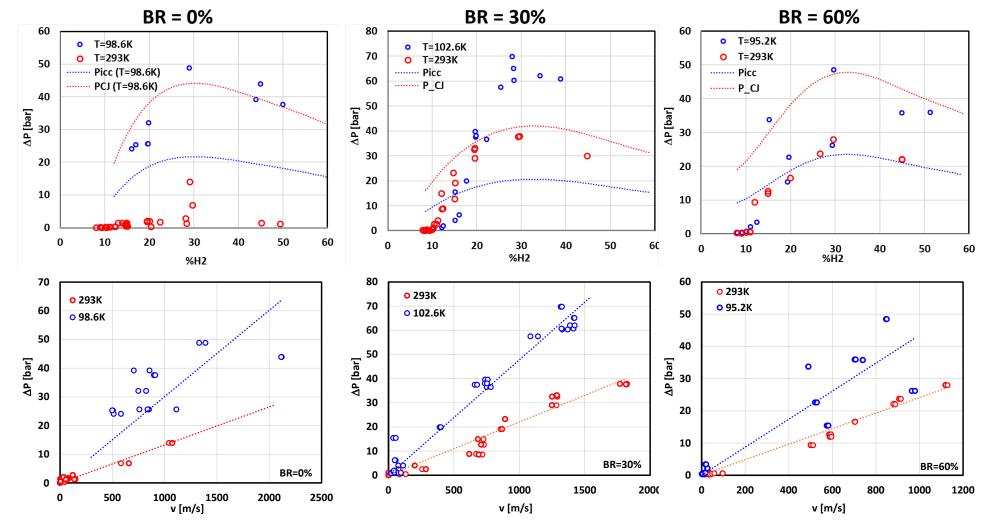
#### Critical expansion ratio for effective flame acceleration in cold experiments (T = 90 – 130 K)

- For cryogenic temperature
   T ≈ 100 K critical expansion ratio is
   σ\* = 12.5 (corresponds to 16% H2)
- Detonation achieved when flame speed becomes larger than speed of sound in products (c<sub>p</sub>) and approaches theoretical detonation velocity (D<sub>CJ</sub>).











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#### Conclusions



- Three typical flame propagation regimes were experimentally observed:
   (1) slow subsonic deflagration, (2) fast sonic deflagration, and (3) detonation.
- Critical conditions for FA evaluated as a function of  $T_{ini}$  within range ( $T_{ini} = >90 650$  K).
- Detonation cell sizes at cryogenic temperature T = 100 K were evaluated on the basis of existing criteria for detonation onset in smooth and obstructed tubes,
- Maximum combustion pressure at cryogenic temperatures found to be 2-3 times higher than for ambient conditions, resulting in much higher hazard potential of cryogenic combustions, compared to combustions at ambient conditions.
- Run-up distance to detonation at cryogenic temperatures found to be 2 times shorter than at ambient temperature,
- Further information see:

M. Kuznetsov, T. Jordan et al.: Shock tube experiments on flame propagation regimes and critical conditions for flame acceleration and detonation transition for hydrogen-air mixtures at cryogenic temperatures; International Conference on Hydrogen Safety - Online, Edinburgh, United Kingdom, Sept. 21-24 2021





### **POOL-Experiments**











### **POOL-Experiments**

#### Motivation



- Leakages or failures during LH2 transport and refueling lead to LH2-releases that will produce large clouds of GH2 and might even form LH2-pools.
- Pool evaporation and mixing of GH2 with air leads to generation of flammable H2/air clouds that can produce huge temperature and pressure loads in case of ignition.
- Evaporation rates of LH2 from pools above different substrates are of fundamental interest for safety assessments of LH2 applications, but only limited data are available.
- Most data concentrate on free spills above flat grounds and water surfaces, where mostly
  expansion and shrinking of puddle is investigated and computational models are
  proposed.
- Only few data is available for confining basins, in which LH2-pools of considerable depth might form and where evaporation is governed by heat transfer from ground material.







#### **Pool properties**

- Box-material: stainless steel
- Inner dimensions: 50 x 50 x 20 cm (L x W x H),
- Insulated with styrofoam plates on bottom and sides,
- In-substrate instrumentation positioned with holders,
- 3 Pools filled up to half the height (10 cm) with different substrates







**Concrete** (prepared > 1 month prior to 1<sup>st</sup> experiment) **Sand** (equipped with baffle plate)

#### Gravel

(gravel removed for tests with water) (water removed for tests with gravel)







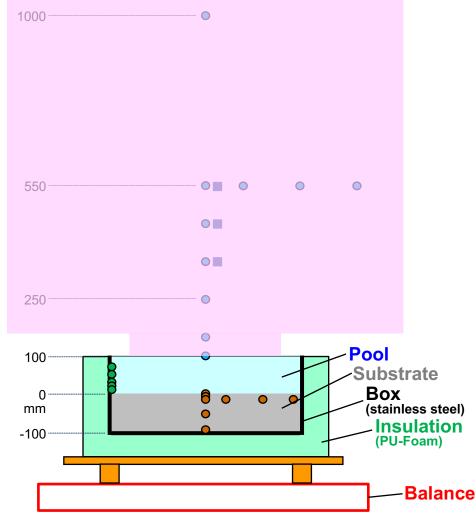
Water

#### Instrumentation

Every pool is equipped with:

- Balance for weight measurement of LH<sub>2</sub>-pool,
- 8 Thermocouples in substrate,
- 6 Thermocouples in pool,
- 10 Thermocouples above pool,
- 3 H<sub>2</sub>-concentration measurement positions above pool,
- Experiments observed with up to 5 cameras,
- Wind conditions recorded with anemometer
- In ignited tests no sensors (T, cH<sub>2</sub>) above pool, but additional fast pressure sensors on ground around facility.









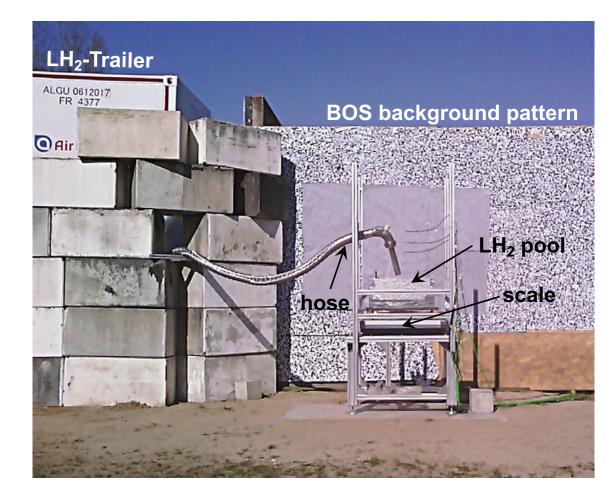
#### Test procedure

- Hose positioned and fixed above pool,
- Data acquisition started manually and then controlled remotely from shelter,
- Cameras started manually,
- LH2-release started manually at trailer (same valve opening) & stopped remotely,
- After pool evaporation following release again started manually (after safety check with H2-sensor) and stopped remotely,
- Unignited experiments:

Pool usually filled 3x in one experiment,

Ignited experiments:

Ignition during evaporation after 2nd filling





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#### Test matrix unignited experiments

- In total 10 unignited experiments performed with pool-facility,
- Experiments performed with all 4 substrates (concrete, sand, gravel, water),
- 4 Experiments performed with "artificial side wind" of known velocity and direction.

Date	Substrate	Procedure	Conditions	Comments
20.03.2020	Concrete01	2 Fillings	Natural	No scales data (Not used)
24.03.2020	Concrete02	4 Fillings	Natural	
08.04.2020	Gravel01	3 Fillings	Natural	
09.04.2020	Sand01	3 Fillings	Natural	
15.04.2020	Sand02	3 Fillings	Wind	No natural wind data
16.04.2020	Sand03	3 Fillings	Wind	
17.04.2020	Concrete03	3 Fillings	Wind	
22.04.2020	Gravel02	3 Fillings	Natural	Gas-Samples
23.04.2020	Gravel03	3 Fillings	Wind	Gas-Samples
23.04.2020	Water01	3 Fillings	Natural	









#### Test matrix ignited experiments

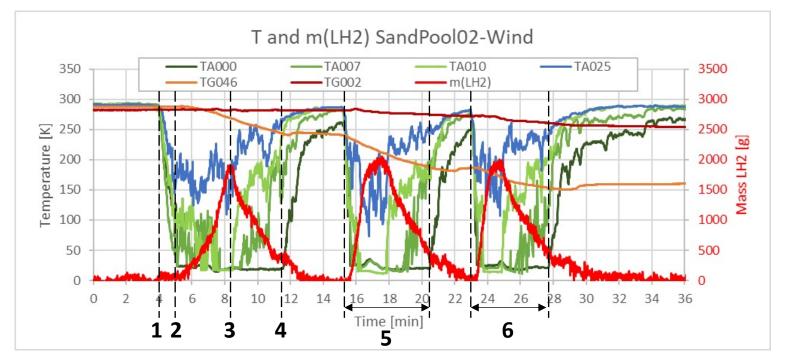
- In total 14 ignited experiments were performed with the pool-facility,
- Experiments performed with all 4 substrates (concrete, sand, gravel, water),
- Main variable apart from substrate was ignition height.

			Ignition	
Date	Substrate	Procedure	Height [cm]	Comments
24.04.2020	Sand04	2 Fillings	25	
24.04.2020	Sand05	2 Fillings	25	T100 moved near ignition
24.04.2020	Sand06	2 Fillings	15	
27.04.2020	Sand07	2 Fillings	45	No ignition
27.04.2020	Sand08	2 Fillings	40	
27.04.2020	Sand09	2 Fillings	35	
27.04.2020	Sand10	2 Fillings	8	
27.04.2020	Sand11	2 Fillings	45	Repetition of Sand 07
27.04.2020	Concrete04	2 Fillings	45	
27.04.2020	Concrete04	2 Fillings	25	
27.04.2020	Concrete04	2 Fillings	15	
27.04.2020	Concrete04	2 Fillings	8	Ignition in 3 <sup>rd</sup> attempt
27.04.2020	Water02	2 Fillings	25	
04.05.2020	Gravel04	2 Fillings	25	





LH2-Evaporation above sand and concrete (Example SandPool02)



- 1. Beginning LH2-release
- 2. Beginning (1st) pool-formation
- 3. End (1st) release, beginning (1st) evaporation

4. End (1st) evaporation

**Balance** 

5. 2nd release and evaporation

•TA025

TA010

TA000

TG002

6. 3rd release and evaporation



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**TA007** 

100 -----

-100 -----





Pool

Substrate

(stainless steel)

(PU-Foam) Palette

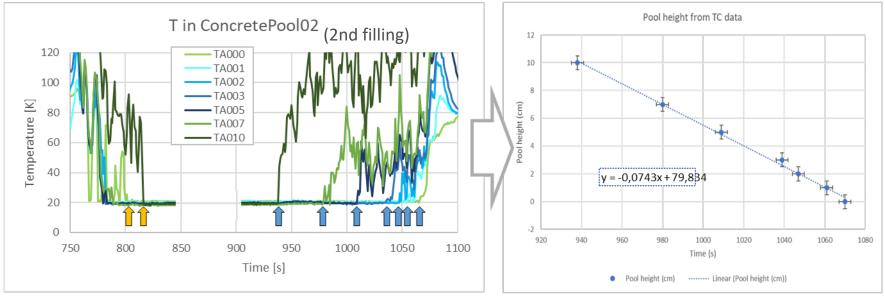
Insulation

(for transport)

Box



#### LH2-Evaporation above sand and concrete (Example ConcretePool02)



- For filling periods (yellow arrows in left graph) no clear order of TCs reaching T<sub>b</sub>(LH2) in positions above substrate can be determined → no detailed analysis of pool formation.
- For evaporating pool, passing-times of LH2 level for pool-TCs can be clearly identified and when plotted over time, vaporization velocity of boiling LH2 pool in form of a height reduction velocity can be determined from slope,
- Further evaluation yields mass reduction velocity and heat transfer from substrate to LH2.







#### LH2-Evaporation above sand and concrete (Example ConcretePool02)

- In similar manner, analysis of evaporation behavior in all other experiments with concrete and sand as substrate was performed.
- Evaporation of cryogenic fluids is governed by heat conduction from ground into liquid.
- Phenomena might be described by one-dimensional heat conduction equation, whose solution gives LH2 evaporation rate in kg/s:

 $dm_{LH2}/dt = L^2 k \Delta T / [\Delta h_{fg} (\pi \alpha t)^{1/2}],$ 

where L – side length of square pool ground face, m; k – thermal conductivity of substrate, W/mK;  $\Delta T$  – temperature difference between boiling temperature of liquid and environment, K;  $\Delta h_{fg}$  – heat of LH2 vaporization, J/g;  $\alpha$  –thermal diffusivity of substrate, m<sup>2</sup>/s; t – time after coverage of ground with liquid pool.

• Derivation and further results presented in:

Friedrich, A., Breitung, W. et al.: Liquid hydrogen pool evaporation above four different substrates; International Conference on Hydrogen Safety 2023 (ICHS2023), Quebec, Kanada, 19.–21.09.2023

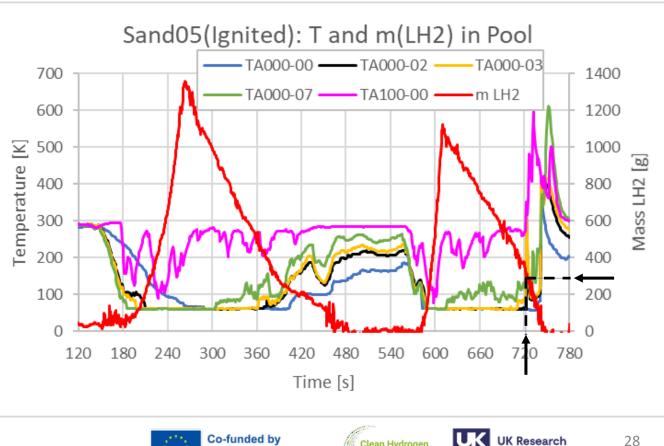




(8)

#### Test procedure - Ignited Pool Experiment Sand05

- After second filling LH2-level in pool was closely monitored,
- Increase in temperatures indicates that respective thermocouple is no longer covered by LH2,
- At filling level 3 cm (increase in T03) ignition was prepared,
- Ignition was activated at filling level of 2 cm (increase in TO2),
- Thermocouple TA100 positioned close to electrodes to record moment of ignition,
- According to graph: in experiment Sand05 approx. 300 g LH2 was in pool in moment of ignition.



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#### Degree of damage in Ignited Pool Experiment

- Almost undamaged: minor burns (e.g.: Water02),
- More severe damage: torn off insulation (e.g.: Sand11, Concrete05),









Complete destruction of facility with substrate gravel.



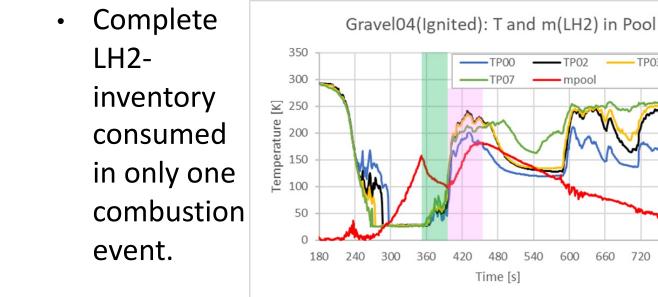


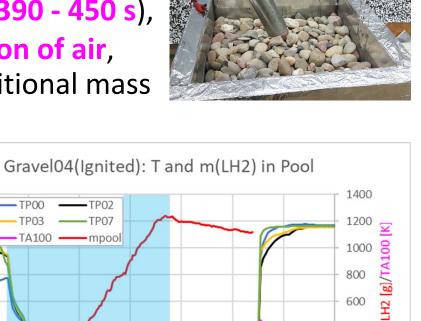


#### **Ignited** Pool Experiment Gravel04

Possible explanation for different behavior of experiment Gravel04:

- Main difference to other ignited experiments is phase of mass • increase after  $1^{st}$  evaporation of pool above substrate ( $t \approx 390 - 450 s$ ),
- Mass increase most likely due to condensation/solidification of air, •
- When ignition was activated after  $2^{nd}$  filling (t  $\approx 859$  s) additional mass in pool was about 1100 g,









870

800

600

400

200

0

890

Mass



300

Temperature [K] 200 150 100

50

750

1400

1200

1000

800 600

400

200

780

Mass LH2 [g]

**TP03** 

720

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770

TPOO

TP03

TA100



790



830

Time [s]

810

850

#### **Ignited** Pool Experiment Gravel04

Video observation (PHOTRON High-Speed Camera, 2000 fps)









#### Experimental Data available from: https://publikationen.bibliothek.kit.edu/1000145885

## **PRESLHY EVHYS** Thank you for your attention



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UK Research and Innovation

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